Ingvild Emilie Solnes

# Machine Learning Modelling of the Oxidative and Thermal Degradation of Monoethanolamine (MEA)

Master's thesis in Chemical Engineering and Biotechnology Supervisor: Hanna Knuutila & Andrés Carranza-Abaid Co-supervisor: Lucas Braakhuis & Vanja Buvik June 2021

NDU Norwegian University of Science and Technology Faculty of Natural Sciences Department of Chemical Engineering

Master's thesis



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### Abstract

The human population is growing, leading to increased consumption of resources and emission of greenhouse gases. As a result, the concentration of greenhouse gases in the atmosphere is rising to dangerous levels, and the need for measures to reduce emissions is growing.<sup>[1]</sup> One measure is  $CO_2$ -capture and storage, which opens up the possibility of removing  $CO_2$  from flue gas, compressing and storing it instead of emitting it to the atmosphere.

One example of a  $CO_2$ -capture technology is chemical absorption with an aminebased solvent. With this technology, there are also difficulties, mainly degradation of the solvent. Therefore, further understanding of degradation is important for reducing operational costs, solvent management and emission control.

In this thesis, the main focus has been on oxidative and thermal degradation of monoethanolamine (MEA), one of the most researched solvents for chemical absorption. Mathematical machine learning modelling has been used to make a predictive model that can describe the degradation and trends in experimental data. The objective of the work has been to see if machine learning modelling has the potential to give good model predictions, describe the degradation of MEA and the formation of selected degradation compounds.

For the oxidative degradation models, two models were developed. The first model had 3 inputs (MEA-concentration, oxygen concentration, temperature), and the second model had 10 or 11 inputs that included experimental data from the other measured degradation products. This was done to see if the modelled results would improve with more inputs to the model. The output was the calculated experimental reaction rate. For the thermal degradation models, two models were also developed. Here, there was one model with 3 inputs (MEA-concentration,  $\rm CO_2$ -loading, temperature) and one with 6 inputs that included the other measured degradation products.

From the results, the models seem to be able to capture the trend of the experimental data. The models are data-driven, hence requiring a lot of experimental data. However, the model seems to be sensitive to outliers in the datasets so that the models can identify outliers in experimental data. The results are promising for further modelling, and with more research and more experimental data, the model predictions should quickly improve.

### Sammendrag

Folketallet i verden vokser, noe som fører til en økning i forbruket av ressurser og utslipp av klimagasser. Som et resultat av dette øker konsentrasjonene av klimagasser i atmosfæren til farlige nivåer, og behovet for tiltak for å redusere utslippene øker.<sup>[1]</sup> Ett tiltak som kan redusere utslipp er CO<sub>2</sub>-fangst og lagring, som åpner mulighetene for å fjerne CO<sub>2</sub> fra røykgass, komprimere og lagre det i stedet for å slippe den ut i atmosfæren.

Et eksempel på en  $\rm CO_2$ -fangst<br/>teknologi er kjemisk absorbsjon med aminbasert solvent. Med denne teknologi<br/>en er det også utfordringer, hovedsakelig degradering av solventen. Ytter<br/>ligere forståelse av degradering er viktig for å redusere driftskostnader, kontroll av solventen og utslippskontroll.

I denne oppgaven har hovedfokuset vært på oksidativ og termisk degradering av monoetanolamin (MEA), som er et det absorbsjonskjemikaliet som er forsket mest på innen kjemisk absorbsjon. Matematisk maskinlæringsmodellering har blitt brukt til å lage en prediktiv modell som kan beskrive degradering og trender i eksperimentelle data. Målet med arbeidet har vært å se om maskinlæringsmodellering har potensial til å gi gode modellforutsigelser, beskrive degradering av MEA og dannelsen av utvalgte degraderingsforbindelser.

For de oksidative degraderingsmodellene ble det utviklet to modeller. Den første modellen hadde 3 inputs (MEA-konsentrasjon, oksygenkonsentrasjon, temperatur) og den andre modellen hadde 10 eller 11 inputs, og inkluderte eksperimentelle data fra de andre målte degraderingsproduktene. Dette ble gjort for å se om de modellerte resultatene ville forbedres med flere inputs til modellen. Output fra modellene var den beregnede eksperimentelle reaksjonshastigheten. For modellene for termisk degradering ble det også utviklet to modeller. Her var det en modell med 3 inputs (MEA-konsentrasjon, CO<sub>2</sub>-loading, temperatur) og en med 6 inputs, som inkluderte de andre målte degraderingsproduktene.

Fra resultatene ser modellene ut til å være i stand til å fange trenden til den eksperimentelle dataen. Modellene er datadrevne, og krever derfor eksperimentell data. Modellen ser ut til å være følsom for avvikende verdier i datasettene, og kan anvendes til å identifisere avvikere i eksperimentelle data. Resultatene er lovende for videre modellering, og med mer forskning og eksperimentelle data, bør modellprediksjonene lett forbedres.

## Preface

This master thesis has been carried out at the Department of Chemical Engineering at the Norwegian University of Science and Technology (NTNU) during the spring of 2021. The thesis has been written for TKP4900 - Chemical Process Technology, Master's Thesis in the Environmental- and Reactor Technology group.

I want to thank Hanna Knuutila, Andrés Carranza-Abaid, Lucas Braakhuis and Vanja Buvik for their guidance and help throughout the fall and spring semester, for teaching me a lot and for the opportunity to work with them on the interesting subject of amine degradation.

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Symbol	Dimension	Description
<u>a</u>	-	Vector of linear transformed variables
$\alpha$	$[\mathrm{mol}~\mathrm{CO}_2/\mathrm{mol}~\mathrm{MEA}]$	$\rm CO_2$ -loading
$\underline{b_1}$	-	Biases of the hidden layer
$b_2$	-	Biases of the output layer
C	-	Chemical component
$c^e$	$[\rm kmol/m^3]$	Experimental concentration
$c^{mod}$	$[\rm kmol/m^3]$	Modelled concentration
$C_{MEA,0}$	$[\rm kmol/m^3]$	Initial concentration of MEA in experimental dataset
<u>I</u>	-	Hidden layer weight matrix
N	-	Number of datapoints in the dataset
n	-	Measurement number
$\underline{n}$	-	Simplified variable
<u>O</u>	-	Output layer weight matrix
$O_2$	[%]	Concentration of oxygen
Ω	-	Vector of nonlinear functions
$r^e$	$[\rm kmol/m^{3}*t]$	Experimental reaction rate
$r^{mod}$	$[\rm kmol/m^{3}*t]$	Modelled reaction rate
T	$[K/^{\circ}C]$	Temperature in Kelvin or Celsius
t	[days]	Time in days
$\underline{\omega}$	-	Weight parameter
$\underline{X}$	-	Vector of input variables
$\underline{x_A}$	-	Constant of the hidden layer
$\underline{x_B}$	-	Constant of the hidden layer
$\underline{x_C}$	-	Constant of the hidden layer
	-	Normalized input vector
$\frac{\underline{x_n}}{\underline{\hat{Y}}}$	$[\text{kmol}/\text{m}^{3}\text{*t}]$	Vector of predicted output variables
$\underline{Y^e}$	$[\rm kmol/m^{3}*t]$	Vector of experimental values
$\underline{y_A}$	-	Constant of the output layer
$\overline{y_B}$	-	Constant of the output layer
$\overline{y_C}$	-	Constant of the output layer
$\overline{Z}$	-	Vector of the sigmoid transformed normalized input variables

### 1 Introduction

The Holocene is the name of the current geological epoch and has been one of the most stable periods in the history of our planet, with relatively small-scale climate shifts. During this period, the average temperature has not wavered more than  $\pm 1$  °C.<sup>[8]</sup> This period has also been called Anthropocene, meaning "The Age of Man", because of the impact humans have had on the planet.<sup>[9;10]</sup> No other species has changed its habitat more and faster than humans, with agriculture and urbanization of the wilderness. The human species have grown exponentially with the help of improved sanitation and medical care, which has led to increased pressure on the biodiversity of the planet. With an increasing human population, there is also an increase in resource consumption, and the need to meet demands has pushed technological progress forward.<sup>[8;9;10]</sup>

With increased production, there is also an increase of waste and emissions of greenhouse gases, such as  $CO_2$ , methane and nitrous oxide. As a result, greenhouse gas concentrations in the atmosphere are growing, affecting human health and global temperatures. In light of these effects, measures are needed to stop the anthropogenic, human-made emissions and possibly slow down global warming. Today, most anthropogenic emissions are from combustion. One measure that is very relevant and widely researched lately is  $CO_2$ -capture and storage technology, and one of the most promising  $CO_2$ -capture technologies is chemical absorption with amine-based solvents. Instead of emitting  $CO_2$  from flue gas to the atmosphere, it can be removed for compression and storage.

#### 1.1 Chemical absorption with amine-based solvents

Amines are well suited for separating  $\text{CO}_2$  from flue gas because of their temperature dependant reversible reactions with  $\text{CO}_2$ .<sup>[11]</sup> A schematic of a typical amine-based  $\text{CO}_2$ -capture unit is shown in Figure 1.1. Flue gas is passed through the absorber, where an aqueous amine-based solvent absorbs the  $\text{CO}_2$ .<sup>[2]</sup> The rich amine is then sent to the top of the desorber to be separated from the solvent. The aqueous solution is heated with steam from a steam cycle, which will trigger the reversible reaction and thus separating the  $\text{CO}_2$  from the amine. The lean amine is sent through a reboiler and back to the absorber again, and the cycle is repeated. The separated stream of  $\text{CO}_2$  is taken out at the top of the desorber, compressed and transported through a pipeline for storage.<sup>[2]</sup>

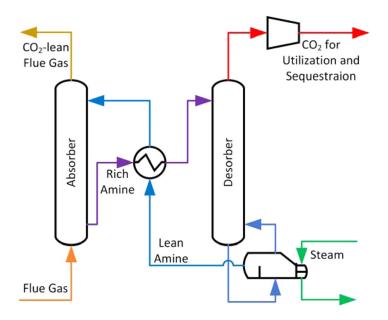


Figure 1.1: Schematic of an absorption based CO<sub>2</sub>-capture unit.<sup>[2]</sup>

The ideal amine for amine-based  $\text{CO}_2$  capture combines a high absorption rate and cyclic capacity with a low energy requirement for stripping, in addition to low degradation and corrosion.<sup>[5]</sup> One of the most researched amines for  $\text{CO}_2$ absorption is monoethanolamine (MEA). MEA has a high affinity for  $\text{CO}_2$  at low temperatures and a low affinity at high temperatures. It is also a cheap solvent that is not volatile, and it is therefore well suited for application in chemical absorption of  $\text{CO}_2$ .<sup>[12]</sup>

There are, however, challenges with chemical absorption, such as corrosion in the system and degradation of the solvent. These problems often have a significant impact on the costs and efficiency of the plant. Degradation can occur oxidatively or thermally and is when a chemical compound is broken down into smaller compounds. Oxidative degradation happens mainly in the absorber, where there is oxygen present in the gas stream. 80-90 % of degradation of amine solvents used in an amine-based  $CO_2$ -capture plant comes from oxidative degradation. Thermal degradation occurs mainly in the stripper and reboiler and is impacted by, for example, temperature and  $CO_2$ -loading. Other factors can have an impact on the degradation rate, such as the presence of  $NO_X$ ,  $SO_X$ , iron and particles in the system.<sup>[5;11;12]</sup> Understanding the degradation process is vital for emission control and solvent management.

It is estimated that 10 % of the operational cost of a chemical absorption  $\rm CO_2$ capture unit can be related to degradation of the solvent.<sup>[6;13]</sup> It has therefore been essential to review issues related to degradation at an earlier stage of the process before installing a unit.

Oxidative degradation is not well understood today compared to thermal degradation. How fast oxidative degradation occurs, what products are formed, and in how large quantities are questions that are raised. One method that can help to understand further the degradation of solvents in absorption-based  $\rm CO_2$ -capture plants is mathematical modelling and machine learning. By making a predictive model that can anticipate how fast and in what quantities the most known degradation products are formed, the plant may save money on operational costs. In addition, it is important to research at which conditions, such as temperature, oxygen levels and  $\rm CO_2$ -loading, the degradation process is affected the most.

### 1.2 Mathematical modelling and machine learning

Mathematical modelling is a helpful tool to increase the understanding of complex problems that are not easily solved by hand and helps us describe the world around us according to our understanding. With a mathematical model, it is easier to see the effects of changes in the system and to get a deeper scientific understanding of a problem.<sup>[14]</sup>

One category of modelling is a mechanistic model. A mechanistic model uses mechanisms and theoretical information, such as equations of state or reaction equations, together with empirically fitted parameters to describe changes in a system. A mechanistic model often gives accurate predictions, but they are also computationally complex.<sup>[4]</sup> Therefore, empirical models have also been developed. There is no consideration of mechanisms in empirical models. Instead, the models try to account for changes in a system with different conditions quantitatively. One drawback of an empirical model is that its validity range is often limited.<sup>[4;14]</sup>

Machine learning (ML) has become increasingly popular because of its simplicity and computational speed. Machine learning technology is used to classify, find patterns and develop data predictions from a dataset.<sup>[4]</sup> There are three paradigms of machine learning; supervised learning, unsupervised learning and reinforcement learning.<sup>[15]</sup>

## 1.3 Scope of work and objective

In this thesis, the focus is on oxidative and thermal degradation of MEA. Based on experimental data from degradation experiments, a predictive model will be developed using mathematical machine learning.

This thesis aims to see if the developed machine learning models have good prediction abilities, capture trends in the datasets, and describe the degradation of MEA. The ultimate goal is to develop an ML model that can be applied in different chemical absorption plants to indicate how the solvent will degrade over time and how fast the degradation happens at the given conditions used in that specific plant. However, before this is possible, there is a need to see if machine learning has potential and can be used as a start in the research and development of predictive models for oxidative and thermal degradation.

Furthermore, the impact of the number of inputs have on the results is investigated. For oxidative degradation, two models are developed, one with three inputs and one with ten or eleven inputs. Two models are also developed for thermal degradation, one with three inputs and one with six inputs. The second models use all the available experimental data as inputs to see if there is a possible correlation between MEA and the measured degradation products. Developing these models can help in the further understanding of degradation. Compared to thermal degradation, oxidative degradation is not well understood today. A better understanding of what affects the degradation rate in a capture plant can help reduce operational costs, increase the understanding of the system and the efficiency of the plant.

First, the theoretical background of oxidative and thermal degradation and machine learning is presented in Chapter 2. Then, the methodology of the thesis is given in chapter 3 before the results are presented and discussed in Chapter 4. Finally, the conclusion and recommendations for future work are given in Chapter 5 and 6.

## 2 Theoretical background

In this chapter, the main principles for oxidative and thermal degradation are presented. In this thesis, two publications were used as the primary sources, one publication from Vevelstad et al. (2016) and one publication from Davis (2009). The experimental data that has been used in the machine learning models were retrieved from these two papers. In this chapter, the experimental setup, the methodology, and the main findings from these publications are presented. Furthermore, the suggested reaction mechanisms for the formation of the degradation compounds from MEA are shown. Also, the main principles of machine learning and the theory behind artificial neural networks is explained.

 Table 2.1: Table of abbreviations, compound names and CAS-numbers for the compounds used for further modelling of oxidative and thermal degradation.

 [5:6;7]

Abbreviation	Compound	CAS
BHEOX	N,N-bis(2-hydroxyethyl)oxalamide	1871-89-2
	Formate	N/A
HEA	N-(2-hydroxyethyl)-acetamide	142-26-7
HEEDA	N-(2-hydroxyethyl)ethylenediamine	111-41-1
HEF	N-(2-hydroxyethyl)formamide	693-06-1
HEGly	N-(2-hydroxyethyl)glycine	5835-28-9
HEI	N-(2-hydroxyethyl)imidazole	1615-14-1
HEIA	N-(2-hydroxyethyl)imidazolidin-2-one	3699-54-5
HEPO	4-(2-hydroxyethyl)-2-piperazinone	23936-04-1
MEA	2-Monoethanolamine	141-43-5
	Oxalic acid	144-62-7
TriHEIA	1-(2-((2-hydroxyethyl)amino)ethyl)-2-imidazolidone	N/A

#### 2.1 Oxidative degradation

Oxidative degradation occurs when oxygen is present in the gas stream. Several factors can affect the degradation rate, such as temperature and oxygen concentration. There are still some gaps in the understanding of oxidative degradation. The experimental data for oxidative degradation is from a systematic study of the degradation of MEA under simulated absorber conditions in lab-scale experiments. The study was conducted by Vevelstad et al. (2016).<sup>[5]</sup>

Many degradation products have been identified in oxidative degradation studies, and these products are divided into primary and secondary degradation compounds. Primary degradation compounds are those that are first formed through oxidation reactions or radical reactions.<sup>[5]</sup> Many compounds are considered as primary degradation compounds, but in this study, the focus will be on two of them, formate and oxalic acid, because of available experimental data. Ammonia is also considered a primary degradation compound. However, due to high ammonia volatility, there were uncertainties in the analyses, and the data was not included in the modelling. The primary degradation compounds are reactive, chemical species and may react further with MEA or other degradation compounds to become secondary degradation compounds.<sup>[5]</sup> There are also many secondary degradation compounds, but in this study, the compounds that will be focused on are HEF, HEI, BHEOX, HEPO, HEA and HEGly. The compound names, abbreviations and CAS-numbers are given in Table 2.1.

When comparing lab-scale experiments to pilot-scale, it is seen that similar degradation products are formed. However, there is a larger variety of degradation products formed in a pilot plant. This is expected, though, because the conditions are more varied in a pilot plant than in the lab-scale experiments, where the conditions are often constant. When comparing lab-scale and pilot-scale experiments, the degraded solvent from the pilot was more similar to the solvent from the oxidative degradation experiments than the solvent from the thermal degradation experiments, suggesting that oxidative degradation dominates in pilot plants.<sup>[16]</sup>

As mentioned, oxidative degradation is still not well understood. This applies to, for example, under given conditions, what products are formed, their reaction paths, how fast they are formed, and in what quantities. A further understanding of these problems could help optimize the efficiency and possibly decrease the operational costs of a capture plant.

#### 2.1.1 Reaction equations describing the degradation of MEA

Suggested reaction equations for the formation of the degradation compounds are presented in this subsection. They are simplified reaction equations collected from previous research where oxidatively degraded solutions from lab-scale experiments and pilot plants have been analyzed. Many components have been found in solvent analyses, and likely reaction paths have been suggested based on these findings. There are still many uncertainties in the formation reactions, there are several different reaction paths presented in different papers, and they are often very complicated. When the reactions that occur are not entirely understood, this has made it challenging to develop a model that accurately describes oxidative degradation. Complex reaction mechanisms are often simplified in degradation modelling. This is also the case in this thesis. Only the most relevant reaction equations have been included in this thesis.

$$2MEA + CO_2 \leftrightarrows MEACOO^- + MEAH^{+[2]}$$
(2.1)

$$MEA + 3H_2O \rightarrow 2CH_2O + NH_3 + 2H_3O^{+[17]}$$
(2.2)

$$CH_2O + \frac{1}{2}O_2 \rightarrow HCOOH^{[18]}$$

$$(2.3)$$

$$MEAH^{+} + HCOO^{-} \leftrightarrows HEF + H_2O^{[18]}$$
(2.4)

$$MEA + O_2 \to C_2 H_2 O_2 + H_2 O + NH_3^{[17]}$$
(2.5)

$$\mathrm{MEA} + \mathrm{CH}_{2}\mathrm{O} + \mathrm{C}_{2}\mathrm{H}_{2}\mathrm{O}_{2} + \mathrm{NH}_{3} \leftrightarrows \mathrm{HEI} + 3\mathrm{H}_{2}\mathrm{O}^{[19]}$$
(2.6)

$$C_2H_2O_2 + O_2 \to C_2H_2O_4^{[17]}$$
 (2.7)

$$2\mathrm{MEA} + \mathrm{C}_{2}\mathrm{H}_{2}\mathrm{O}_{4} \leftrightarrows \mathrm{BHEOX} + 2\mathrm{H}_{2}\mathrm{O}^{[18]}$$

$$(2.8)$$

$$\mathrm{MEA} + \mathrm{C}_{2}\mathrm{H}_{2}\mathrm{O}_{4} \to \mathrm{HEGly} + \mathrm{H}_{2}\mathrm{O} + \mathrm{CO}_{2}^{[18]}$$
(2.9)

$$MEAH^{+} + CH_{3}COOH \leftrightarrows HEA + H_{2}O^{[18]}$$
(2.10)

$$MEA + HEGly \rightarrow HEPO + 2 H_2 O^{[18]}$$
(2.11)

#### 2.1.2 Extensive dataset for oxidative degradation of MEA

The experiments were conducted in an open batch reactor. The experimental setup is shown in Figure 2.1. First, a feed gas, a mixture of  $CO_2$  (7.5 mL/min) and air (0.35 L/min), was bubbled through a water vapour saturation tank. Then, the feed gas and a recycle gas stream (50 L/min) were pumped to the glass reactor filled with a preloaded solution of MEA (30 wt% MEA and 0.4 mol  $CO_2$  per mol of MEA).<sup>[3;5]</sup>

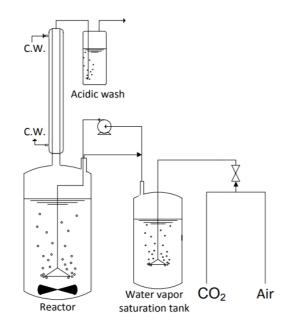


Figure 2.1: Overview of the experimental setup for the oxidative degradation experiments.<sup>[3]</sup>

After the gas was bubbled through the glass reactor, it was led through two condensers. Here, the water vapour was condensed and returned to the reactor, and the gas was passed through an acidic wash and a water wash to absorb volatile and basic degradation products. The length of the experiments varied from 21 - 42 days, depending on temperature and oxygen concentration, and samples were taken out from the glass reactor and analyzed with intervals between 3 - 6 days. The components that were measured and used for the models developed in this study are MEA, formate, HEF, HEI, oxalic acid, BHEOX, HEPO, HEA, and HEGly. The compound names, abbreviations and CAS-numbers for these chemical compounds are given in Table 2.1.<sup>[5;7]</sup> The experiments were performed with four different  $O_2$ -concentrations (6%, 21%, 49% and 98%) at three different temperatures (55 °C, 65 °C, 75 °C). An overview of the experiments and their respective labels is given in Table 2.2.<sup>[5]</sup>

 Table 2.2: Overview of the oxidative degradation experiments used in the models, the conditions they were conducted at and their respective labels.<sup>[5]</sup>

$\mathrm{T} \; [^{\circ}\mathrm{C}] \; / \; \mathrm{O}_{2} [\%]$	6	21	49	98
55	A1	A2-I, A2-II	A3	A4
65	B1	B2-II	B3	Β4
75	C1	C2	C3	C4

Because of experimental difficulties, some of the experimental data was not included further in the modelling and data fitting. This applies to experiment B2-I and experiment A2-III. In experiment B2-I, there was a significant water loss resulting in deviations in the mass balance. A water loss will result in higher concentrations of the measured components. This also applies to experiment C2. A correction for water loss was done, and it was decided that experiment C2 would be included in the modelling. Experiment A2-I, A2-II and A2-III were performed at the same conditions, but the results measured from experiment A2-III did not coincide with experiments A2-I and A2-III. It was therefore decided to exclude the results from experiment A2-III in the optimization.

From the experimental results of the study performed by Vevelstad et al. (2016), there was a trend of increased degradation rate with higher temperatures and oxygen concentrations. There is a more significant increase in the degradation rate with increasing temperature than increasing oxygen concentration in the gas phase. This also applies to MEA, where an increased degradation rate was observed with increasing temperature for all oxygen concentrations.

For all oxygen levels, the concentration and the rate of formation of the primary degradation products, formate and oxalic acid, was increasing with increasing temperatures. The concentration levels of oxalic acid are much smaller than for formate, and according to Rooney et al. (1998), this is believed to be because oxalic acid is formed in more steps than formate and the path of formation for oxalic acid is less favorable.<sup>[20]</sup>

HEGly and HEPO are major degradation compounds found in pilot plants.<sup>[12]</sup> A trend was seen where the highest concentration levels of HEGly occurred

when the oxygen content was lowest, and it decreases with increasing oxygen concentrations. Therefore, it is believed that HEGly is consumed as the reactant in another reaction dependent on oxygen.<sup>[5]</sup> The suggested simplified mechanism describing the formation of HEPO from MEA and HEGly is shown in Equation 2.11.<sup>[18]</sup> The formation rate of HEPO was not affected by the oxygen levels. As mentioned, HEPO is a major degradation compound, but in the experiments performed by Vevelstad et al. (2016), the formation of HEPO observed was low compared to what is generally found in pilot plant samples, indicating that the experiments were not able to capture the typical behaviour of HEPO.<sup>[5]</sup>

HEF, HEA and BHEOX are believed to be formed from the reaction between MEA and different acids. The suggested reaction mechanism for HEF is shown in Equation 2.4, where MEA and formate  $(HCOO^{-})$  react and HEF and water is formed. HEF formation is believed to be rapid, and the formation rate increases with increasing oxygen levels.<sup>[5]</sup> The reaction for the formation of HEA is shown in Equation 2.10, where HEA is formed from MEA reacting with acetic acid. HEA was produced in much lower amounts than HEF, about 10% of the amount. HEA had similar behaviour as the other degradation compounds, where the concentrations increased with increasing temperatures and oxygen levels.<sup>[5;18]</sup> The reaction for the formation of BHEOX is shown in Equation 2.8, where MEA reacts with oxalic acid. The measured amounts of BHEOX and oxalic acid are low, and this is because these components are formed after several reaction steps. The concentration of BHEOX also increased with increasing oxygen levels, but it seems to go through a maximum after 3-15 days. This might be because BHEOX decomposes at higher temperatures. BHEOX is therefore not a major degradation compound as it will decompose in stripper conditions.<sup>[5;18]</sup>

The suggested formation reaction for HEI is shown in Equation 2.6. HEI is formed from MEA and primary degradation compounds. The measured concentration levels are around the same as the concentration of HEGly. Therefore, it is an important degradation compound. The formation rate of HEI was similar to many of the other degradation products, favoured by high temperatures and oxygen levels.<sup>[5]</sup>

The study observed that the accelerated degradation experiments performed at 98 % oxygen could not easily be extrapolated to what happens at 6 % oxygen. The experiments performed at higher oxygen levels will not easily represent the situation in an industrial amine absorption plant, where the oxygen levels are

around 3-11 % regarding products formed and the reaction rates.<sup>[5]</sup> However, to optimize a model as much as possible, it is favourable to have as much data as possible. When developing a machine learning model, a large amount of data retrieved under various conditions is good for parameter optimization.

#### 2.2 Thermal degradation

Thermal degradation occurs in the stripper and reboiler of an absorption-based  $\rm CO_2$ -capture plant. Thermal degradation mechanisms describe the irreversible reactions between MEA and  $\rm CO_2$  without any oxygen present, and degradation rates are affected by parameters such as temperature, T, and  $\rm CO_2$ -loading,  $\alpha$ .<sup>[21]</sup> Thermal degradation of MEA in the presence of  $\rm CO_2$  has been studied since the 1950s.<sup>[16]</sup> Several degradation products have been identified, and the main products are 2-oxazolidone (OZD), HEEDA and HEIA. More research has been done on thermal degradation of MEA, and it is more understood than oxidative degradation. Several models on thermal degradation have also been developed in earlier work. The methodology, relevant results, and reaction equations from a study performed by Davis (2009) are presented in the following section.

#### 2.2.1 Thermal Degradation of Aqueous Amines Used for CO<sub>2</sub>-Capture

Davis (2009) conducted the thermal degradation experiments at the University of Texas, and the experimental data used in this study is retrieved from this thesis. The experiments were run for 56 days at two different temperatures, 120 °Cand 135 °C, 3 different  $CO_2$ -loadings, 0.2, 0.4 and 0.5 moles of  $CO_2$  per mole of MEA, and three different initial MEA concentrations 6.58, 4.9 and 2.88 kmol/m<sup>3</sup>.<sup>[6]</sup> An overview of the experiments conducted, their respective labels and the conditions they were conducted in is given in Table 2.3.

The experiments were performed in stainless steel tubes with endcaps. The tubes were loaded with MEA solution and closed. There must be no leaks from the tubes because then the experiment has to be discarded. The tubes were then placed in an oven and heated to the correct temperatures. Samples were taken and analyzed every seven to fourteen days for the eight weeks the experiment was run. The components that were measured during the experiments were MEA, HEEDA, HEIA, and TriHEIA. The compound names, abbreviations and CAS-numbers of the chemical compounds are given in Table 2.1.<sup>[6;7;22]</sup>

	$C_{MEA,0}[kmol/m^3]$ / $\alpha$ [mol $CO_2/mol$ MEA]	0.2	0.4	0.5
120 °C	6.58	E1	E2	E3
	4.9	E4	E5	E6
	2.88	$\mathrm{E7}$	E8	E9
135 °C	6.58	F1	F2	F3
	4.9	F4	F5	F6
	2.88	F7	F8	F9

 Table 2.3: Overview of thermal degradation experiments, the conditions they were conducted at and their respective labels. <sup>[6]</sup>

Since the experimental data used in this thesis is from Davis (2009), the suggested mechanisms from his publications were also the focus. The suggested reaction equations for the formation of HEEDA, HEIA and TriHEIA from MEA is shown in Equation 2.12 - 2.17. Here, OZD and MEA trimer are known intermediate products, as it is found in small amounts in thermal degradation experiments.<sup>[6;22]</sup>

$$2MEA + CO_2 \leftrightarrows MEACOO^- + MEAH^+$$
 (2.12)

$$MEACOO^{-} + MEAH^{+} \leftrightarrows OZD + MEA + H_{2}O \qquad (2.13)$$

$$MEA + OZD \leftrightarrows HEEDA + CO_2 \tag{2.14}$$

$$\text{HEEDA} + \text{CO}_2 \leftrightarrows \text{HEIA} + \text{H}_2\text{O} \tag{2.15}$$

$$\text{HEEDA} + \text{OZD} \leftrightarrows \text{MEAtrimer} + \text{CO}_2 \tag{2.16}$$

$$MEAtrimer + CO_2 \leftrightarrows TriHEIA + H_2O \tag{2.17}$$

In the reaction equations, HEIA is formed from HEEDA and not the other way around, which is suggested in other publications on thermal degradation, such as Polderman et al. (1955).<sup>[23]</sup> In a publication done by Gary and Rochelle (2009),

this was researched further. Two reactors were filled with  $CO_2$ -loaded HEEDA, one with a solution of HEEDA and MEA, and one with HEIA and MEA was placed in ovens at 135°C. When analyzing the solutions later, it was found that in the reactors containing  $CO_2$ -loaded HEEDA and MEA, HEEDA converted rapidly to HEIA. On the other hand, in the reactor containing HEIA and MEA, the conversion to HEEDA was not seen until very long hold times.<sup>[16;24]</sup> This leads us to believe that the reaction presented in Equation 2.15 where HEIA is formed from HEEDA, is reasonable.

In the analysis of the solvent, it was found that the rates of formation of the thermal degradation compounds had a direct correlation with temperature, increasing amine concentration, and increasing concentration of  $CO_2$ . The most substantial dependency was on the temperature, and the results showed that the rate would double for every 7 °C increase in temperature.<sup>[6]</sup>

### 2.3 Machine learning

Machine learning is a subset of artificial intelligence. The objective of machine learning is to emulate how a biological brain processes information. This enables a system to be able to learn from data by analyzing it and eventually improving itself.

Today, ML is a part of a human's daily life. Possible applications of ML are inventory predictions, recruitment, or marketing. An example of a common interaction between humans and machine learning from day to day is targeted ads. When one searches for something on the Internet or is in a specific target group, relevant ads appear on social media and other web pages. This is because the company making the ad has an ML algorithm designed to target specific audiences. Another example of machine learning in marketing is contextual relevance. For example, the algorithm identified that ads for chocolate had more impact on consumers in the afternoon than in the morning, so the ads for a specific chocolate product was run more in the afternoon. This saves the company money used for marketing and increases the popularity of the product. Machine learning has improved many fields and has allowed companies to become more strategic and effective than before.<sup>[25]</sup> Rather than doing complicated programming, a machine learning model enables a system to learn from data and often simplifies a complex program code. However, ML is not a simple process, but because of the fast-developing capabilities of today's computers, its popularity has increased more and more.

## 2.3.1 Paradigms of machine learning

Machine learning has three different paradigms; supervised learning, unsupervised learning and reinforcement learning.

Supervised learning is based on training with a labelled and established set of data. In that way, supervised learning can find patterns in a dataset and apply them to the intended process. With the understanding of how a dataset is classified, a machine learning model can distinguish between millions of animals based on images and descriptions of the given animals. Machine learning in supervised systems often uses a mapping method, such as a decision tree and logistic regression where an input, x, produces an output, y.<sup>[15;26]</sup>

In unsupervised learning, the data is not labelled. The intention is to understand the meaning of the data by using algorithms that find patterns or clusters and classify the data based on them. Examples are in social media, where large amounts of unlabeled data are generally hard to classify. Unsupervised learning is built upon assumptions about the data, such as structural, combinatorial and probabilistic properties.<sup>[15;26]</sup>

In reinforcement learning, there is no correct output for a given input. Instead, the system learns through trial and error. The training data in reinforcement learning gives only an indication of what is the correct output. If the system gives an incorrect output, it will try again to find a correct output, and when a series of correct outputs has been given, the understanding of the system of the data will be reinforced.<sup>[15;26]</sup>

In this project, the machine learning models that have been developed are based on supervised learning with a single hidden layer and is called a supervised shallow neural network. In the following section, artificial neural networks and the theory behind supervised shallow neural networks is presented.

#### 2.3.2 Artificial neural networks

An artificial neural network (ANN) is the part of a computing system that we would want to analyze and process information similarly to the human brain. Learning in this method happens through iteration. Deep learning uses neural networks in several hidden layers, while shallow neural networks only have one hidden layer. Artificial neural networks are explained in more detail in this section. The procedure for making a supervised shallow neural network model with the Deep Learning Toolbox from MATLAB R2019a is presented in Subsection 3.4. Artificial neural networks were first proposed by Warren McCullough and Walter Pitts in 1944.<sup>[27]</sup> An ANN is a nonlinear vector of functions that takes in a vector of inputs and weight parameters and provides a vector of outputs. An ANN has the general form shown in the equation below.<sup>[4]</sup>

$$\underline{\hat{Y}} = \Omega(\underline{X};\underline{\omega}) \tag{2.18}$$

Where  $\Omega$  is a vector of nonlinear functions,  $\underline{X}$  is a vector of input variables, and  $\underline{\omega}$  is a set of weight variables. This gives the predicted vector of output variables,  $\hat{Y}$ .<sup>[4]</sup>

In Figure 2.2 the  $\Omega$ -function is illustrated and shows the training process of a single layer feed-forward neural network (FFNN). The system in the figure has three input variables, four neurons in a single hidden layer, and two output variables. Because the information only flows in one direction, forward, it is called a forward propagation model. A single layer FFNN is the same as a supervised shallow neural network. The loss function compares the predicted output variables,  $\hat{Y}$ , with the experimental or modelled values,  $\underline{Y}^e$  and calculates the error. If the system does not meet a predetermined tolerance or the performance is not satisfactory, a backpropagation signal is sent, and the process is repeated until the predictions of the output variables stop improving or the tolerance is met.<sup>[4]</sup>

The Equations 2.19 - 2.23 describe the operations that occur in pre-processing of the input data before the hidden layer, what happens in the hidden layer and the post-processing of the predicted output data. The variables  $\underline{x}_n$ ,  $\underline{x}_A$ ,  $\underline{x}_B$ ,  $x_C$ ,  $y_A$ ,  $y_B$ ,  $y_C$ ,  $\underline{b}_1$ ,  $\underline{b}_2$ ,  $\underline{I}$  and  $\underline{O}^T$  together form the weight parameter  $\underline{\omega}$ from Equation 2.18. The five equations together form the vectors of nonlinear functions,  $\Omega$ , from Equation 2.18.  $\underline{Z}$  is the result of a sigmoid transformation of the normalized input variables and  $\underline{a}$  is the result of a linear transformation of

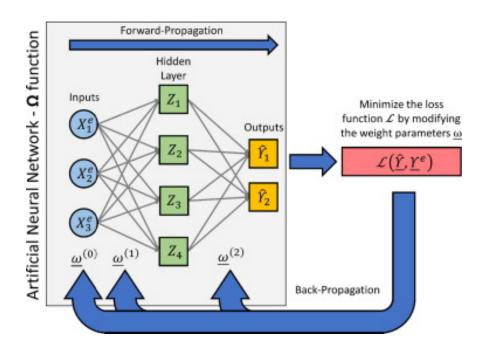


Figure 2.2: Schematic of a feed-forward neural network trained by a back propagation algorithm.<sup>[4]</sup>

the vector  $\underline{Z}$ . All the equations and a more detailed explanation of them is given below. Example code is given in the appendix in Section C.

The hidden layer is a transformation of the input vector,  $\underline{X}$ , to a vector  $\underline{Z}$ , as seen in Figure 2.2. Before the transformation, the vector of input variables is normalized with the following equation.

$$\underline{x_n} = (\underline{X} - \underline{x_A}) \cdot * \underline{x_B} + x_C \tag{2.19}$$

Where  $\underline{x_n}$  is the vector of normalized input variables,  $\underline{X}$  is the vector of input variables and  $\underline{x_A}$ ,  $\underline{x_B}$  and  $x_C$  are constants or matrices of constants generated by MATLAB. .\* is used to do an element-wise multiplication. The sigmoid transformation usually happens through a sigmoid symmetric transfer function, which is a hyperbolic tangent function. This function is shown in Equation 2.20. The matrix  $\underline{Z}$  represents the result of the sigmoid transformation of the normalized variables.

$$\underline{Z} = tansig(\underline{n}) = 2./(1 + e^{-2\underline{n}}) - 1$$
(2.20)

where  $\underline{n}$  is a simplification of the expression below,

$$\underline{n} = \underline{b_1} * Q + \underline{I} * \underline{x_n} \tag{2.21}$$

Here tansig is mathematically equivalent to tanh with small numerical differences between the two, but the tansig function runs faster with MATLAB. In neural networks, the shape of the transfer function is not emphasized. However, speed is important for effective models.<sup>[28]</sup> <u> $b_1$ </u> is the bias of the hidden layer, and <u>I</u> is the hidden layer weight matrix. <u>Q</u> is the number of samples in the dataset. ./ is used to do an element-wise right division.

Afterwards, the vector  $\underline{Z}$  together with the weight parameters  $\underline{b}_2$  and  $\underline{O}^T$  are transformed with a linear transformation function.<sup>[4]</sup> The linear transformation function is shown below.

$$\underline{a} = \underline{b}_2 * \underline{Q} + \underline{O}^T * \underline{Z} \tag{2.22}$$

Where  $\underline{b_2}$  is the bias of the output layer, and  $\underline{O}^T$  is the output layer weight matrix. Finally, to get the vector of predicted output variables,  $\underline{\hat{Y}}$ , the data is un-normalized with the following equation.

$$\underline{\hat{Y}} = \left(\frac{\underline{a} - y_C}{y_B}\right) + y_A,\tag{2.23}$$

where  $y_A$ ,  $y_B$ , and  $y_C$  are constants that MATLAB generates.

# 3 Methodology

All the models presented in this report have a basis in experimental data. The data for oxidative degradation is from work done by Vevelstad et al. (2016), and the data for thermal degradation is from work done by Davis (2009). In this chapter, the methodology of the thesis is described. The method used for developing machine learning models and the different ways of presenting the results, the simplifications and assumptions are presented.

The models that were made in this report are based on the rate of reaction for each component. When using reaction rates, the problem is transformed from requiring a neural network with feedback to a feedforward neural network. Therefore, the data had to be treated and transformed from experimental concentration measurements to the experimental reaction rate for each component. This was done with the following equation.

$$r_{C,n}^{e} = \frac{\Delta c^{e}}{\Delta t} = \frac{c_{C,n+1}^{e} - c_{C,n}^{e}}{t_{C,n+1} - t_{C,n}}$$
(3.1)

 $\Delta c^e$  is the change in experimental concentration of the component over the time interval,  $\Delta t$ .  $r_{C,n}^e$  is the experimental reaction rate for each of the components, C, and n is the measurement number.  $c_{C,n}^e$  is the experimental concentration of the component, and  $t_{C,n}$  is the time the measurement was made. This equation measures the change in the concentration of the compounds over time and is a commonly used equation for calculating reaction rates.<sup>[29]</sup> The rate of reaction was used as an output in the machine learning models.

After developing the machine learning models, a modelled rate is obtained by running the experimental input data through the ML model. This modelled rate was used to find the modelled concentrations of the components at the different measurement points. The modelled concentration,  $c_{C,n+1}^{mod}$  was calculated by reversing Equation 3.1. The equation is shown below.

$$c_{C,n+1}^{mod} = r_{C,n}^{mod}(t_{C,n+1} - t_{C,n}) + c_{C,n}^{mod}$$
(3.2)

 $r_{C,n}^{mod}$  is the modelled reaction rate for each of the components, C, at measurement n.

Several methods were tried to find the optimal fit, the best way to recreate the experimental data, and optimizing the parameters. This included varying the number of inputs of the machine learning models and how the concentrations were calculated from the modelled rates.

## 3.1 Oxidative degradation models

An evaluation of the raw data from the oxidative degradation experiments has been done. The results showed a significant difference in the measured values between the different analytical methods that analyzed the data. As mentioned in Section 2.1.2, this was because of some experimental difficulties. The results from experiment A2-III did not coincide with experiment A2-I and A2-II, even though the three experiments were performed under the same conditions. The data from experiment A2-III was therefore not included further. Experiment B2-I had a significant water loss, which resulted in a higher measured concentration of MEA, and this data was also not used in any further research or development of a model.<sup>[5]</sup>

The first modelling method that was tried out was a machine learning model with 3 inputs and one output. The inputs of the model were the experimental MEA-concentration, oxygen concentration, and temperature. The output was the calculated rate of reaction for one of the nine different components. Thus, nine ML models were created, one for each one of the chemical components.

The second ML model that was developed had 10 inputs and one output. The 10 inputs were temperature, oxygen concentration and the concentrations of eight of the nine components. The only component not included was oxalic acid because the measured concentrations from experiment A2-I were missing or too uncertain to include in the results. Therefore, oxalic acid was excluded as an input in the model. This was to include as much data as possible in the modelling of the reaction rates. However, the oxalic acid model had 11 inputs because the data for oxalic acid was included as an input. The output of the models was the rate of reaction of each of the different components. Also here, nine ML models were developed.

A few methods of calculating the modelled concentrations were tried out. The first method was to use the instantaneous rate, which is the rate at which a reaction is proceeding at a specific time.<sup>[29]</sup> The other method was to use the average rate of each experiment as the reaction rate,  $r_{C,n}$ , assuming the rate is independent of the concentration levels of the degradation compounds. This was done to simplify the model and to attempt to make it more user-friendly. The goal was to develop a model that can be applied in different chemical absorption plants to indicate how the facility's components will degrade over time and how fast the degradation happens at the given conditions used in that specific plant.

### **3.2** Thermal degradation models

There was less available experimental data from the experiments performed by Davis (2009). Some measurements for the different degradation products were not available because of experimental difficulties and uncertainties. Two models were developed for predicting the rates of thermal degradation. The first model had 3 inputs and one output. The inputs were temperature, MEA-concentration and  $CO_2$ -concentration, and the output was the experimental reaction rate calculated with Equation 3.1. Also here, one model was developed for each of the four degradation compounds.

The second model that was developed used all the experimental data as input. In total, there were 6 inputs, temperature, MEA-concentration and  $CO_2$ concentration, in addition to the concentration of HEIA, HEEDA and TriHEIA. Where experimental points were unavailable, the NaN (not a number) function in MATLAB was used for these values.

### **3.3** Assumptions and simplifications

As described in Section 2.1.2, there was some water loss that occurred in the duration of the oxidative degradation experiments. This resulted in concentration measurements that were too high and also some concentration jumps in the measured data. When the reaction rate of MEA was calculated with Equation 3.1, there were some positive values for the rate, indicating that MEA had been formed during the experiments. For the thermal degradation experiments, the same issues were seen with positive values for the reaction rates for MEA. These positive values were not wanted when developing the model. This is because, in this thesis, it is assumed that MEA is not formed, only consumed in oxidative and thermal degradation. Therefore, it was decided that the positive values for the reaction rate of MEA would not be included when developing the machine learning models that modelled the reaction rates of MEA. When making the

plots of the results, all the experimental data was included again.

After the ML models were developed, all experimental data, including the removed points before developing the model, were run through the model. This was to obtain as many reaction rates as possible to have more modelled predictions to compare with the experimental data. There was a problem with underprediction in the plotted results for MEA from the 3 input model with instantaneous rate. To avoid this, the data points or experiments where there were concentration jumps were removed altogether. Therefore, the plotted curve for the 3 input model with instantaneous rate is not included in many of the figures, or the first measurement point is missing, and the plot starts at the second measurement point. An example is Figure 4.2, where the ML model with three inputs and instantaneous rate, which is the purple line, starts at the second measurement point.

The average of the modelled rate was used when calculating the modelled concentration of the degradation products for one of the models. This assumes that the rate is independent of the concentration of MEA and results in a linear trend for the concentration curves. From previous research, it is seen that this is often not the case, as the concentration often has exponential growth, and the concentration will flatten out after reaching a maximum or react further and form other components.<sup>[5]</sup> Therefore, the concentration was also calculated by using the instantaneous rate to compare the two methods.

The density is assumed to be constant for the duration of the experiments. The density was measured at the beginning and end of every experiment. The change in density was around 1 % for all experiments, so it can be assumed that it does not significantly impact the results.

## 3.4 Developing a supervised shallow neural network model

Training a machine learning model is analogous to doing polynomial fitting, only that the optimization equations are more complex. In this section, the steps and considerations for making a supervised shallow neural network model are presented. Example MATLAB code is given in the appendix in Section C.

Before training the model with a dataset, one first has to choose what fraction of the data will be used for training, validation and testing. The data used for training will fit the model. The validation dataset is held back from the model and used to evaluate and further fit the model. The testing dataset is for evaluating the fit of the final model compared to the training dataset.<sup>[30]</sup>

Then the number of neurons in the hidden layer is chosen. The more neurons there are in the hidden layer, the more computation is needed to solve the problem. The network often needs many neurons in the hidden layer to give an appropriate model for more complicated problems. The fitting performance of the model is then evaluated. If the model is overfitted, there are too many neurons in the hidden layer. This will result in a model that is too well fitted to the specific dataset, so its ability to generalize is negatively affected. When the model has not learned enough from the training data, its predictions are unreliable and not generalized. This is known as underfitting and will result in the model not capturing the dominant trend of the data.<sup>[31]</sup> If the model is overfitted or underfitted, it will cause problems when introducing new data to it. When finding the optimal number of neurons in the hidden layer where the model is not overfitted or underfitted, a trial and error method is a common approach.

There are two main optimization methods available in MATLAB's deep learning toolbox. Levenberg-Marquardt (LM) backpropagation algorithm or the Bayesian Regularization (BR) backpropagation algorithm. When the neural network is moderate-sized, LM is the fastest method.<sup>[32]</sup> The BR algorithm typically requires more time, but it has good generalization and prediction qualities and is a combination of the LM optimization method and Bayesian interpolation method. The BR algorithm can give good results for noisy or small datasets.<sup>[33]</sup>

Finally, the model can be trained with the chosen data and conditions. The goal is for the correlation coefficient, R, to be close to 1, which indicates a close relationship between the output and target variables.<sup>[4]</sup>

If the correlation coefficient is not optimal, the neural network can be retrained several times to see if the results improve. Each time the model is retrained, different solutions are obtained, and the outputs will therefore change even though the inputs are the same. One can often improve the accuracy of a model by retraining it several times.<sup>[34]</sup>

The models developed in this thesis are shallow neural network models with a single hidden layer. The number of neurons in the hidden layer was varied from model to model to optimize the fit. An example model with 3 inputs, four neurons in the hidden layer and one output is illustrated in Figure 3.1. Here one can see that there is one hidden layer and one output layer. The sigmoid transformation of the input data happens in the hidden layer, and the linear transformation of the output variables happens in the output layer. The w and b represent the weight matrices and the biases, respectively.

For the machine learning models model in this thesis, the optimization method used was Bayesian Regularization with three or four neurons in the hidden layer, depending on the dataset. The number of neurons is determined by the complexity of the problem, not by the amount of data. However, the amount of data constrains the number of neurons that can be used. Because there was not a lot of data available, the percentage of data used for validation and testing was chosen to be 5-10 %, so most of the data would be used for training. This was to optimize the fitting and predictions of the models.

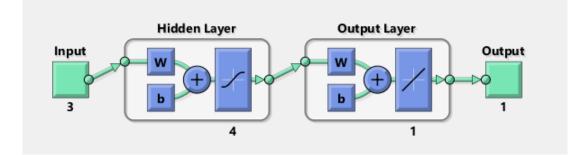


Figure 3.1: Flow sheet of the setup of a supervised shallow neural network with three input variables, four neurons in the hidden layer, one output layer and one output variable. The figure is from MATLAB.

## 3.5 Statistical analysis methods

Statistical analysis can be a helpful tool to help uncover patterns and trends in a dataset. In this thesis, the deviations that were calculated are average absolute relative deviation (AARD) and absolute average deviation (AAD). The AARD calculates the absolute average relative deviation between each data point in the dataset and the model prediction and tells how much each data point deviates from the mean of the data. AAD calculates the average absolute deviation between each data point in the dataset and the model prediction. The AARD was calculated with the following equation.

$$AARD = \frac{1}{N} \sum \left| \frac{c_{C,n}^e - c_{C,n}^{mod}}{c_{C,n}^e} \right| * 100\%$$
(3.3)

N is the number of values in the dataset,  $c^e$  is the experimental value of component C at measurement point n, and  $c^{mod}$  is the modelled value of component C in the measurement point n. The AD was calculated with the following equation,

$$AAD = \frac{1}{N} \sum |c_{C,n}^{e} - c_{C,n}^{mod}|$$
(3.4)

# 4 Results and discussion

In this section, the main results and findings are presented and discussed. Also, a review of the advantages and disadvantages of the models, methods and assumptions made is done.

## 4.1 Oxidative degradation

In the following subsections, the experimental results from the oxidative degradation models are presented and discussed. Each degradation compound is discussed separately, and a comparison of the developed models is made. For each of the oxidative degradation components, some representative results are given. All other figures are given in the appendix in Subsection A.

Table 4.1 and 4.2 gives the mean AAD and AARD values of all experiments (A1-C4) for each one of the components for the three different ML-models. The complete tables with the AAD and AARD for each one of the experiments are given in the appendix in Subsection A.

Table 4.1: Mean AAD for experiment A1-C4 for each one of the components. (1) AAD between the experimental values and the model with 3 inputs and average rate.(2) AAD between experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs and instantaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
MEA	0.362	0.127	0.127
Formate	0.044	0.024	0.047
Oxalic acid	0.002	0.001	0.002
HEGly	0.003	0.001	0.002
HEPO	0.053	0.010	0.041
HEF	0.014	0.006	0.010
HEA	0.041	0.025	0.035
BHEOX	0.001	0.001	0.002
HEI	0.005	0.001	0.002

Table 4.2: Mean AARD for experiment A1-C4 for each on of the components. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs and instantaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
MEA	6.96	2.46	2.55
Formate	35.9	12.5	34.6
Oxalic acid	30.8	10.3	10.8
HEGly	18.1	6.56	11.5
HEPO	16.9	4.89	12.6
HEF	19.5	11.6	15.0
HEA	11.1	10.5	10.4
BHEOX	62.5	22.4	58.1
HEI	19.0	19.2	13.8

### 4.1.1 MEA

The modelling results for MEA is shown in Figure 4.1 and 4.2. The rest of the figures are given in the appendix in Subsection A.1.

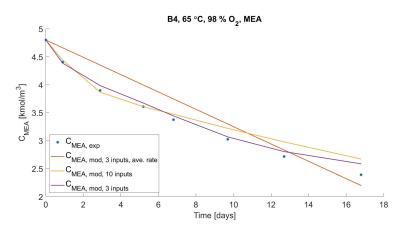


Figure 4.1: The figure shows the plotted results from experiment B4 for MEA conducted at 65°C and with 98% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 or 11 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

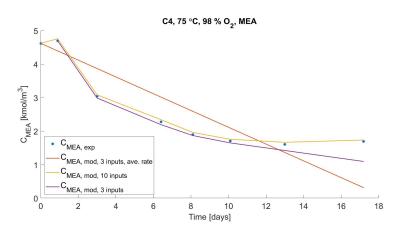


Figure 4.2: The figure shows the plotted results from experiment C4 for MEA conducted at 75°C and with 98% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 or 11 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

In Figure 4.1 experiment B4 is plotted. The experiment was performed at 65 °C with 98 % oxygen. One can see that all of the ML models have been able to predict the experimental data trend. The red line, which is the ML model with 3 inputs and average rate, is linear for all of the experiments. For the time span of the plot, the red curve has a reasonable development because the endpoint of the ML model is similar to the last experimental point. However, the experimental data has a curved shape, indicating that the degradation rate decreases over time. This is in accordance with the expected trend and what earlier research has shown. This trend will not be seen from the linear curve, where a constant degradation rate is assumed. Therefore, this model will have a limited validity range. The two other curves, the yellow and purple ones, have a decrease in degradation rate with time, and if the same trends continue, it seems as though these two curves will have a reasonable development over time.

Figure 4.2 shows the results from experiment C4, which was performed at 75 °C with 98% oxygen. Here, MEA degrades faster than in experiment B4, which is expected as the solvent degrades faster with increasing temperature. In this plot, the yellow and purple curves are similar to the curves in plot B4, where the degradation rate decreases with time. It seems that the ML models for most of the plots developed for MEA have captured the general trend for the data well.

The values for the AAD and AARD are shown in the appendix in Table B.1 and B.2. The AAD seems to increase with increasing temperature for the 3 input model, with some exceptions. This is probably because the reaction rate of MEA decreases faster with higher temperatures, and therefore has a more concave shape as the temperature and oxygen concentration increases. The 3 input model with average rate is linear and will not follow the same trend, so the AAD is expected to increase with increasing temperatures. From Table 4.1, it is seen that the mean AAD is lower for the model with 10 inputs than the model with 3 inputs and average rate. Several of the AADs for the 3 input model with instantaneous rate is missing because of missing modelled reaction rates. For the included values, results are promising, and the mean AAD is similar to the 10 input model. For the 10 input model, the AADs are good and steadily low for all the calculated values. This coincides with the plotted results from the ML model, which seemed to follow the experimental values well. The mean AARD is 6.96%for the 3 input model with an average rate, with a minimum value of 0.892% and a maximum value of 24.34%. For the 10 input model, the mean AARD is 2.46%with a minimum value of 0.761% and a maximum of 5.688%. For experiment B1, the AARD for the 3 input model with average rate deviates significantly from the experimental values. For the 3 input model with simultaneous rate, the mean value is similar to the 10 input model. The AARDs are low for all three models, but a simultaneous rate improves the fit, as seen in the plots and the deviations.

Because there were concentration jumps in the experimental data for MEA, values were removed from the data in the model with 3 inputs. This was done so that the data would have a decreasing concentration trend for the whole duration of the experiments. The ML models were then trained with this data. This was to support the assumption that MEA is only consumed, not formed, for the whole duration of the experiments, from the suggested reaction mechanisms for oxidative degradation. This is seen in Figure 4.2, where the purple line has one less experimental point than the other plots. This has altered the results compared to using the experimental data directly. However, if the concentration of MEA increased and decreased during the experiments, this would not make sense because MEA is not being formed in an absorber or simulated absorber conditions, only consumed. For the model with ten inputs, these experimental data points were not removed. As seen in Figure 4.2, the yellow curve does a jump in the beginning before decreasing in concentration for the remaining duration

of the experiment. This could indicate that the 10 input model is overfitted or is sensitive to outliers in the dataset.

The model with 3 and 10 inputs are similar in many cases. It seems like the model with ten inputs improved the overall fit of the model. This indicates that the degradation rate is not only dependent on the MEA-concentration; it is also dependent on the other degradation products that are formed.

#### 4.1.2 Formate and oxalic acid

Selected results for formate are shown in Figure 4.3 and 4.4. These are the plotted results from experiment A1 and C4. The remaining plots are given in the appendix in Subsection A.2. In the ML model with three inputs, zero-values were removed from the data before training the model. In the model with 10 inputs, this was not done.

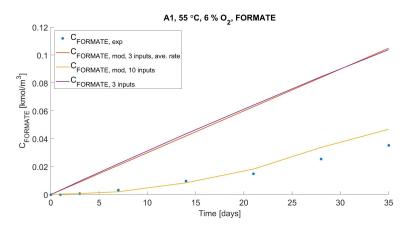


Figure 4.3: The figure shows the plotted results from experiment A1 for formate conducted at 55°C and with 6%  $O_2$ . The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

The results of the ML model for formate are generally good. The values for the modelled reaction rates of the 3 input model were close to constant. This resulted in a concentration profile for the 3 input model with the instantaneous rate to be similar to the 3 input model with average rate. From the figures, it is seen that they are both close to linear. A similar linear trend for the 3 input models is seen for all the experiments. The trend of the experimental data is also linear, and it seems as though the ML model with 3 inputs has captured this linear trend well.

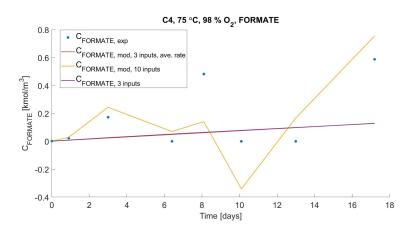


Figure 4.4: The figure shows the plotted results from experiment C4 for formate conducted at 75°C and with 98% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

From Figure 4.4 one can see that the yellow line, which is the 10 input model, has noticeable step changes in the reaction rate. Some experiments had zeros in the experimental data, such as in experiment C4, and these were not removed before training. This seems to have caused disturbances and shows that the ML model with ten inputs is sensitive to outliers in the dataset.

From reported results, the concentration levels and the reaction rate of formate are expected to increase for the whole duration of the experiments.<sup>[5]</sup> From the results, this trend is seen for most of the experiments. In experiment B3, C3 and C4, the concentration either decreases or has zeros where the concentration could not be measured, giving a negative rate for some points. This causes disturbances in the ML model with 10 inputs. Except for these outliers, the concentration has an increasing trend. When it comes to the reaction rate, the increase is linear for the model with 3 inputs. For the model with 10 inputs, the reaction rate has an even increase for many of the plots, and for other plots, it has a steeper growth.

From Table 4.1 it is seen that the mean AAD for formate is low for all ML models, and the AAD for the 10 input model is the lowest. From the mean AARD of formate in Table 4.2, there is a significant difference in the AARD for the 10 input model (12.5%) and the 3 input model with average (35.9%) and simultaneous rate (34.6%). This coincides with what is seen from the plotted results, where the 10 input model more easily follows the experimental data points than both of the plotted lines from the 3 input model, thus deviating more from the mean of the data.

The plotted results from experiment B2-II and C2 for oxalic acid are shown in Figure 4.5 and 4.6. The remaining plots are given in the appendix in Subsection A.3.

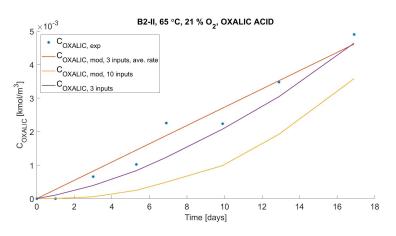


Figure 4.5: The figure shows the plotted results from experiment B2-II for oxalic acid conducted at 65°C and with 21% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 11 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

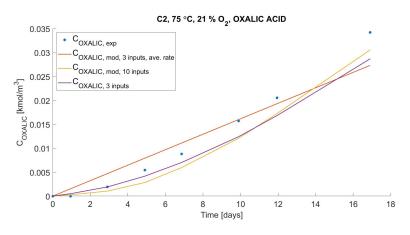


Figure 4.6: The figure shows the plotted results from experiment C2 for oxalic acid conducted at 75°C and with 21% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 11 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

From the results, one can see that the fit is suitable for all the plots. In Figure 4.5 the red line has a very nice development, and the same applies to the purple line. The yellow line, the 11 input model, is underpredicted, meaning that it

predicts too low values. This can be because, in the experimental data, the first two values are zero. As also seen from the formate results, the 10 or 11 input model is sensitive to outliers and zero-values in the dataset. In Figure 4.6 all three curves have a good fit. The yellow and purple lines have a curved shape, which follows the pattern of the experimental data points. It seems like these curves will have a reasonable development over time.

It seems as though the fit improves with increasing temperature and oxygen concentration. When looking at the order of magnitude, the concentration levels are around 10 times larger for the experiments performed at 55 °C and 75 °C, so an error is more visible for the experiments performed at lower temperatures than the higher ones. When looking at Table 4.1 with the mean AAD, the average absolute deviation is very low for all models. This indicates that the fit is good for both the ML models, and errors are more visible for the lower temperatures in the graphs. From Table 4.2 with the AARD, the mean is much higher for the 3 input model with the average rate (30.8%), with the highest value being 153.1%for A2-II, than the models with simultaneous rates with 11 inputs (10.3%) and 3 inputs (10.8%). This indicates that the modelled rates from the models with simultaneous rates follow the experimental data better than with an average rate. A reason for high AARD values can be because the order of magnitude for oxalic acid is relatively low, as mentioned earlier. Therefore, the absolute average relative deviation will be more visible because a deviation from the mean of the data will make a more significant difference when the concentration levels are lower.

### 4.1.3 HEGly and HEPO

The results from the plots of experiment A2-II and C2 for HEGly are shown in Figure 4.7 and 4.8. The remaining plots are given in the appendix in Subsection A.4.

HEGly is a major degradation compound found in pilot plants, and it has a strong temperature dependency. From the results of the ML models, there is an apparent increase in the concentration levels of HEGly with increasing temperature. There is also a decrease in the concentration levels with increasing oxygen content, coinciding with the expected development from research.<sup>[5]</sup> This indicates that ML models have been able to capture the general trend of the data.

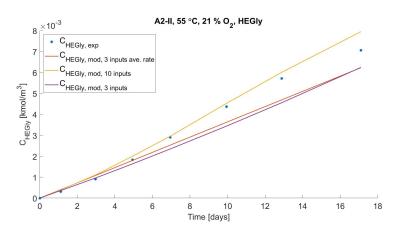


Figure 4.7: The figure shows the plotted results from experiment A2-II for HEGly conducted at 55°C and with 21% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

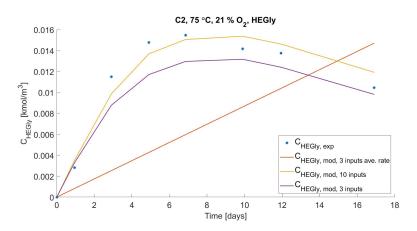


Figure 4.8: The figure shows the plotted results from experiment C2 for HEGly conducted at 75°C and with 21%  $O_2$ . The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

For Figure 4.8 one can see a decrease in the concentration after around 6 days. From the theory, HEGly is believed to be consumed as the reactant in other reactions.<sup>[5]</sup> This is more visible for the highest temperature in the experimental data, and the ML models seem to follow a similar trend. Also, the red line, plotted with the average reaction rate, will have a limited validity range because it has a linear development the whole time, and HEGly is expected to decrease or stagnate in concentration levels. For the results for 55 °C and the experiments done with 6 % oxygen for 65 and 75 °C, the results show a linear trend, similar to Figure 4.7. This is because the reactions with HEGly as an intermediate are believed to be reached faster for higher temperature and oxygen levels, and the decrease in HEGly concentration is therefore not observed at the lower temperature and oxygen levels.

Figure 4.9, 4.10 and 4.11 show the results from the ML models of experiment A1, B1 and C3 for HEPO. The remaining figures are given in the appendix in Subsection A.5. The majority of the results have a good fit, similar to B1 in Figure 4.10.

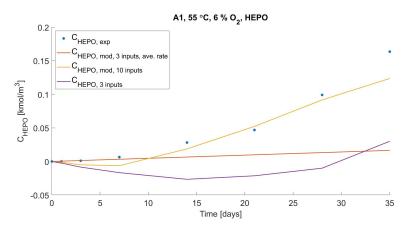


Figure 4.9: The figure shows the plotted results from experiment A1 for HEPO conducted at 55°C and with 6% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

For almost all cases, the two models gave very similar results. For experiment C3, in Figure 4.11 it is seen that the 10 input model is sensitive to concentration jumps in the experimental data and outlier points. The model with 3 inputs has a better-adjusted fit. The exception is Figure 4.9 where the 3 input model gives negative values and low average rates. This may be because the first few data points of the experimental data are low, and this seems to affect the modelled rates a lot.

Lab-scale experiments do not seem to capture HEPO's behaviour in pilot plants,<sup>[5]</sup> therefore, experimental data from pilot plants or larger scale plants is needed for models to be applicable to an industrial plant. However, since the models seemed to easily capture the trends of the lab-scale experimental data for HEPO, this is promising also for a model developed based on data from a pilot or a large-scale capture plant.

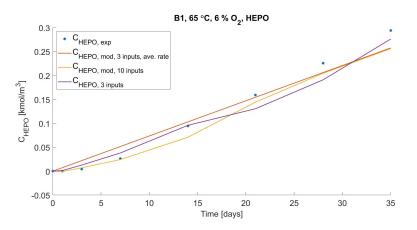


Figure 4.10: The figure shows the plotted results from experiment B1 for HEPO conducted at 65°C and with 6% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

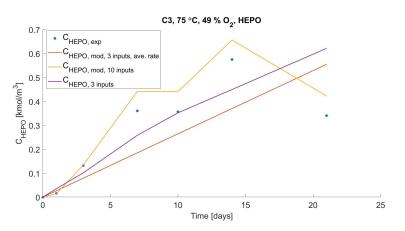


Figure 4.11: The figure shows the plotted results from experiment C3 for HEPO conducted at 75°C and with 49% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

The mean AAD, as seen in Table 4.1, for both HEGly and HEPO are the smallest for the 10 input models for both components. The values for the AAD are around 10 times higher for all models for HEPO than HEGly, and this is believed to be because HEPO is formed in more significant concentrations than HEGly, and this will have a greater impact on the absolute average deviations. The mean AARD for HEGly and HEPO, as seen in Table 4.2, have a similar pattern, where they are highest for the 3 input model with average rates (18.1% and 16.9%) than the models with simultaneous rates with 10 inputs (6.56 and 4.89%) and 3 inputs (11.5 % and 12.6%). This is again because the model with an average rate will have a linear development. The two other plotted lines will curve and thus follow the development of the experimental data more accurately.

#### 4.1.4 HEF, HEA and BHEOX

The result from HEA experiment C3 is shown in Figure 4.12, and the result from HEF experiment C4 is shown in Figure 4.13. Both of these plots give a general idea of how the plotted results of all the experiments turned out. The remaining plots for HEF and HEA are given in the appendix in Subsection A.6 and A.7.

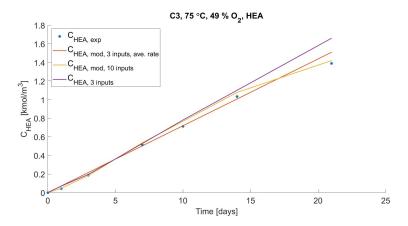


Figure 4.12: The figure shows the plotted results from experiment C3 for HEA conducted at 75°C and with 49% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

For both HEF and HEA, the fit is good, although there are few outlier plots. The models tend to overpredict and underpredict the concentrations, but this also applies to several other degradation compounds. HEA has a similar trend as the formate compound. The model with three inputs and average rate and the model with three inputs and instantaneous rate are similar and follow an almost identical path. From Table 4.1 and 4.2 with the mean AAD and AARD, the values follow the trends that have also been seen for most of the other compounds, where the deviations are lower for the model with 10 inputs than the model with 3 inputs.

Figure 4.14 and 4.15 show the results of experiment B4 and C3 for BHEOX. The results were more varying than many of the plotted results for other compounds. The remaining plots are given in the appendix in Subsection A.8.

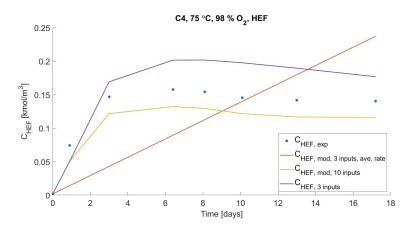


Figure 4.13: The figure shows the plotted results from experiment C4 for HEF conducted at 75°C and with 98% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

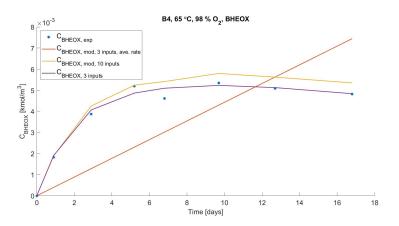


Figure 4.14: The figure shows the plotted results from experiment B4 for BHEOX conducted at 65°C and with 98% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

It is observed that the measured experimental concentrations of BHEOX are low for all the experiments. From theory, it is known that BHEOX is not a major degradation product. It is formed from oxalic acid, which is produced through several and often non-favoured reaction steps.<sup>[5]</sup> The concentration development will therefore be low. Because the concentrations levels are low, an error will be more visible, as seen from other components with low concentration levels. From Table B.16 the values for the AARD are high for many of the experiments. Nevertheless, from Table B.15 it is seen that the AAD between each data point and

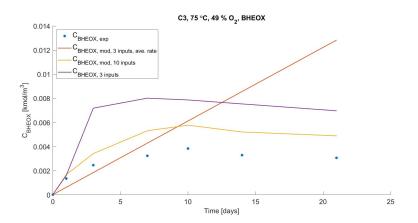


Figure 4.15: The figure shows the plotted results from experiment C3 for BHEOX conducted at 75°C and with 49% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

the model prediction is low for all the values. From Figure 4.14 the inaccuracy of the plotted red line with average, constant rate of reaction is also very visible.

#### 4.1.5 HEI

Figure 4.16 and 4.17 show the results from experiment A1 and B4 for HEI, respectively. The remaining plots are given in the appendix in Subsection A.9.

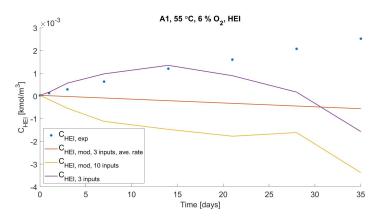


Figure 4.16: The figure shows the plotted results from experiment A1 for HEI conducted at 55°C and with 6% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

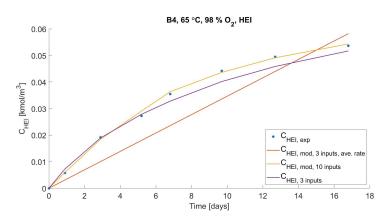


Figure 4.17: The figure shows the plotted results from experiment B4 for HEI conducted at 65°C and with 98% O<sub>2</sub>. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

Experiment B4 has a positive development and flattens out after some time, and this is also representative of many of the other plots. All the ML models have a good development. As expected, the red line, with average, constant reaction rate, is not as accurate as the models with instantaneous rates. From Table B.18 one can see that the average absolute relative deviation is 20.05 % for the red line, 1.479 % and 4.281 % for the yellow and purple line, respectively. The AARD for the red line is larger than the other models, indicating that it is not as accurate, as also seen from the figure. The absolute average deviation, seen in Table B.17 is also larger for the model with average rate than the other two models. The fit for the 3 input model and 10 input model with instantaneous rates are similar, and they follow the experimental data points well.

For experiment A1 all the curves have a negative development over time. The purple line, which is the model with three inputs and instantaneous rate, has a positive development in the beginning before becoming negative after about 15 days. One of the reasons for the inaccuracies shown in Figure 4.16 could be caused by the discrepancy in the order of magnitude of the experimental data. The order of magnitude varies substantially for the experimental data, which will influence the modelled rate. The experimental values for A1 are low, impacting the results notably. The experimental values are low for the other experiments conducted at 55°C, but it seems only to have affected A1.

### 4.1.6 Comparison of the models

Two machine learning models describing the oxidative degradation of MEA have been developed in this thesis. The first model was trained with 3 inputs (MEAconcentration, temperature and  $O_2$ -concentration) and one output (the calculated experimental reaction rate of a component). The modelled rates were obtained from this model, and the modelled concentrations were calculated in two different ways, one with the average of the modelled rates, so a constant rate, and one with the instantaneous rate.

From the results, it was seen that the plotted line with average rate is linear, and it will therefore have a limited validity range. From previous experiments and research, the degradation rates for MEA and reaction rates for the degradation products are expected to decrease with time. When there is less MEA, there will also be less formation of degradation products. Therefore, the linear model will not be valid over time. Therefore it is not relevant to assume a constant reaction rate. From the plotted line with instantaneous rate, it is seen that the results improve substantially, and the curves have better accuracy and behaviour, with some exceptions.

A second model was proposed to see if there was a dependency between the reaction rates of MEA and the degradation products. In addition to the three inputs from the first model, the experimental concentrations of formate, HEF, HEI, BHEOX, HEGly, HEA and HEPO were also inputs. Oxalic acid was not included as an input because the data from experiment A2-I was not available. In the ML model for oxalic acid, all available data were included in the model. For many of the results, the extra inputs seemed to give an improved fit. Looking at the AAD and AARD for the experiments, the error is lowest for the 10 input models in all cases. Because of improved results and lower deviations for the 10 input model, there is an indication that there is a dependency between the degradation compounds.

It seems like the model with 10 inputs will give the most accurate results. This indicates that the more data is available, the better. In machine learning, a model will have better predictions if more data is available. More experimental data could help improve the performance of the ML model. However, it is also seen that the 10 input model is sensitive to outliers in the dataset. A screening of the data and removal of apparent outliers could improve the fit of the model.

One of the goals of this thesis was to see if machine learning can model the oxidative degradation of MEA and the formation of degradation products in an acceptable way. It could also be interesting to see if there is a possibility of developing a model that could be applied in different  $CO_2$ -capture plants. The model is data-driven and requires experimental data from many degradation compounds to obtain the modelled rates and accurate predictions. A model that only requires plant conditions and kinetics as inputs would be optimal. Further understanding of the chemical reactions and how conditions of the plant affect the degradation is needed for this to be possible.

## 4.2 Thermal degradation

In this section, a selection of the plotted results is shown. The rest of the results are given in the appendix in Subsection B. Table 4.3 and 4.4 gives the mean AAD and AARD values from both of the ML models for each one of the components for all experiments (E1-F9). The tables of AAD and AARD for each experiment is given in the appendix in Subsection B.

Table 4.3: Mean AAD for all experiments (E1-E9) for each one of the thermal degradation components. (1) AAD between the experimental values and the ML model with 3 inputs. (2) AAD between the experimental values and the model with 6 inputs.

Compound	AAD $(3)$	AAD $(6)$
MEA	0.235	0.153
HEIA	0.027	0.020
HEEDA	0.012	0.034
TriHEIA	0.015	0.003

Table 4.4: Mean AARD for all experiments (E1-E9) for each one of the thermal degradation components. (1) AARD between the experimental values and the ML model with 3 inputs. (2) AARD between the experimental values and the model with 6 inputs.

Compound	AARD (1) [%]	AARD (2) [%]
MEA	5.3	3.8
HEIA	14.0	11.4
HEEDA	28.9	16.4
TriHEIA	38.8	7.7

#### 4.2.1 Modelling results

Figure 4.18 shows the plotted results for experiment E6 for MEA at 120°C and a  $CO_2$ -loading of 0.5. Figure 4.19 shows the plotted results for experiment F6 for HEEDA at 135°C and a  $CO_2$ -loading of 0.5. Figure 4.20 shows the plotted results for experiment F6 for HEIA at 135°C and a  $CO_2$ -loading of 0.5. Figure 4.21 shows the plotted results for experiment E6 for TriHEIA at 120°C and a  $CO_2$ -loading of 0.5. All the experiments had an initial MEA concentration of 4.9 kmol/m<sup>3</sup>. The figures show the concentration of MEA plotted against time. The experimental data points are the blue dots in the plot. The red line is the ML model with 3 inputs and one output, and the yellow line is the ML model with 6 inputs and one output. The remaining plots are given in the appendix in Subsection B.1, B.2, B.3 and B.4.

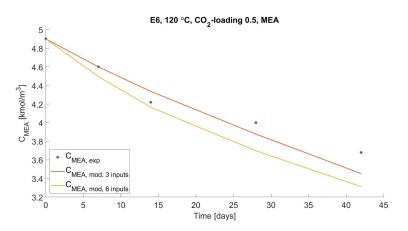


Figure 4.18: The figure shows the plotted results from experiment E6 for MEA conducted at  $120^{\circ}$ C and with a CO<sub>2</sub>-loading of 0.5. The blue dots are the experimental datapoints, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

From the thermal degradation models for MEA, a good fit is observed for most of the experiments. The curves have the expected development, a decreasing reaction rate with time, and a decreasing concentration of MEA over time. For many of the experiments, the model with three inputs and six inputs had similar fits. The model with six inputs gave slightly better results for some of the cases, but all in all, there is not a significant difference. Figure 4.18 represents the results well and is a good indication of how most of the plots for MEA turned out. From Table 4.4 with the mean AARD, the observations from the plotted results are confirmed, as the model with 6 inputs has a lower mean AARD (3.8%) than the 3 input model (5.3%).

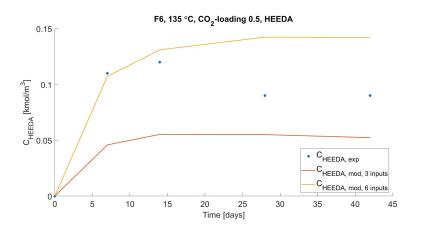


Figure 4.19: The figure shows the plotted results from experiment F6 for HEEDA conducted at 135°C and with a CO<sub>2</sub>-loading of 0.5. The blue dots are the experimental datapoints, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

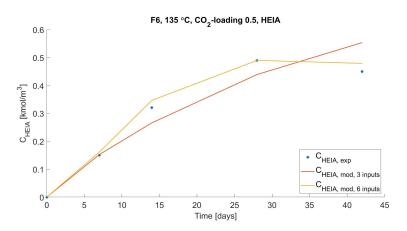


Figure 4.20: The figure shows the plotted results from experiment F6 for HEIA conducted at  $135^{\circ}$ C and with a CO<sub>2</sub>-loading of 0.5. The blue dots are the experimental datapoints, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

For several of the experiments, some of the data points were not available for HEIA, HEEDA and TriHEIA. Therefore, for some of the experiments, the ML models are not complete or not available. For all of the measured compounds, it is seen that the model captures the trend of the data relatively well, but there is also too little experimental data to make an optimal model. However, compared to the amount of available data, the results are promising.

For HEEDA and HEIA, the trends have, for the majority of the results, an increasing reaction rate in the beginning before it starts to decrease after some time. This applies mainly to HEEDA, where almost all the curves have a concave

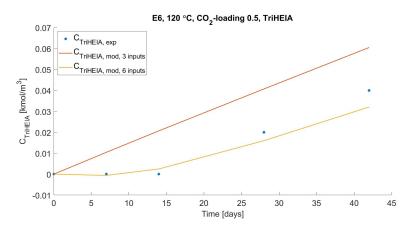


Figure 4.21: The figure shows the plotted results from experiment E6 for TriHEIA conducted at 120°C and with a CO<sub>2</sub>-loading of 0.5. The blue dots are the experimental datapoints, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

shape. The results for HEIA are primarily linear, but the curves are more concave shaped with increasing temperature. As mentioned in Subsection 2.2.1, HEIA is believed to be formed from HEEDA, which could explain the decrease in the concentration levels of HEEDA over time. For HEIA, this conversion is not as rapid. HEIA does react further in the system, but this is more visible at higher temperatures.<sup>[6;24]</sup>

The accuracy of the TriHEIA results varies significantly. Some of the plotted lines have increasing trends, some of the lines have decreasing trends, some are linear, and some are curved. Figure 4.21 shows one of the plotted results that had a reasonable development of the curves. The yellow line, which is the model with 6 inputs, has a much better fit than the red line, which is the model with 3 inputs. Because data was missing in the datasets, it has caused disturbances in the models' ability to capture a trend. From the mean AARD in Table 4.4, it is significantly smaller for the 6 input model (7.7%) compared to the 3 input model (38.8%).

#### 4.2.2 Comparison of the models

It is observed that the ML model with 6 inputs gives an improved trend. The model follows the experimental data points better than the 3 input model for most models. The model with 6 inputs was made because, as for the oxidative degradation model, it was interesting to see if there was any correlation between the concentration levels of the degradation compounds.

The AAD and AARD are lower or similar for the model with six inputs than for the model with three inputs for most of the cases, as seen in the tables in Subsection B in the appendix. This indicates that the fit of the second model is better than the first one and that there is a correlation between the different degradation compounds.

Models of thermal degradation have already been developed. These models are mechanistic and often complex. A machine learning model can potentially simplify such a model while still giving good model predictions if there is enough data. If one has an accurate mechanistic model available, many data points could be generated and used to make a relatively simple ML model. For the model developed in this thesis, only experimental data was used. There was not much data available, so the model is too simple to give satisfactory and accurate predictions. However, the model that was developed shows potential. If more data were available, the model would improve substantially.

# 4.3 Characteristics of the machine learning models

There are several advantages and disadvantages in the developed models, the chosen modelling approach, and the simplifications and assumptions that were made. In this subsection, this will be discussed further.

One of the main characteristics of the machine learning models is that they are data-driven. Hence, they require a significant amount of experimental data. The inputs of the model are experimental concentrations from experiments performed in lab scale. To recreate or make a similar model to be used in predictive analysis of degradation that can be applied to  $CO_2$ -capture plants, it would require similar experiments to be performed on a larger scale. Application to a larger scale would require further adaptations.

The predictions of the models are not generalized due to their data-driven nature, leading to a variation in the quality of the results. Within the same experiment, some of the plotted results have a good trend, and some results have a trend that does not follow the trend of the experimental data. This indicates that there is a lack of generalization in the model.

The developed models are empirical, so reaction equations or equations of state have not been taken into account. The models are based purely on experimental data. A mechanistic approach with kinetic knowledge, experimental data performed at a broader period, and different conditions would help make the model more generalized. However, in a mechanistic model, we extrapolate data measured from experiments and assume that the information available is valid. With both an empirical and a mechanistic approach to modelling degradation, with the current data and knowledge available, an ML model will not be applicable in a larger time scale before more research is done on a larger time frame and a broader understanding of oxidative degradation. Also, the experiments performed are done with increased speed and higher oxygen levels than usual in a large scale plant, so what is seen from the results may not be what is the expected development in an industrial plant.

One advantage of developing a simple machine learning model such as the ones in this thesis is that it helps smoothen the data. Smoothening data is a way to identify and eliminate outliers in a dataset and recognize patterns in a dataset.<sup>[35]</sup> This method is ideal when developing a predictive model. It can help find suitable patterns, and it is a good start, as it can find trends in the dataset. Identifying outliers and finding patterns in a dataset is helpful if a mechanistic model is to be developed in the future.

When developing the ML models describing oxidative and thermal degradation, it was seen that outliers in the dataset were easier to identify. If one had a lot more experimental data, the pattern and trends of the different degradation products and MEA would be easier to spot. The model was able to find a correlation between the different components because an improvement of the models was seen when more inputs were included. This smoothening of the data, as mentioned earlier, can be helpful when developing a predictive model. It will be easier to fit a mechanistic model when the expected development of the degradation is known. When it comes to a thermal degradation model, the mechanisms and the process is more well known, so it would be easier to develop a machine learning model that can predict the degradation over a wider time frame. Much research is still needed for oxidative degradation, but the ML models developed is a promising start. With more research and understanding of oxidative degradation, the predictive abilities of the ML models are expected to improve.

Measures can be taken to improve the models' generalization abilities. Including more parameters can help make the model more accurate. The model is only based on experimental data, so including kinetic information into the neural network could be helpful. Another measure that can be taken is to include even more experimental data from experiments conducted at the same or other conditions. This will improve the learning abilities of the ML model.

The equation used to calculate the rate is a common way of calculating the reaction rate for a compound. Because of the large amount of available experimental data, this method was a good basis for further calculations and the development of a model. However, it has the drawback that the numerical derivative may provide additional uncertainties. Nevertheless, the method used seems to give adequate modelled reaction rates and a satisfying result for most of the experiments.

Several modelled rates for the experiments gave an uneven fit, and it seems that the model is sensitive to outliers in the dataset. In the model developed with 3 inputs, obvious outlier points were removed before developing the ML models, but all data was included in the model with 10 inputs. Therefore, some of the modelled results from the 10 input model are uneven when there were zero-points or concentration jumps in the dataset. Something that could improve the machine learning models would be to conduct several parallels for the experiments, making it easier to identify outliers points in the experimental data.

When removing outliers in the experimental data, the results are altered to get a better fit, and the results obtained may not be similar to reality. However, the data was removed because it had some underlying issues and did not represent what wanted to be measured. If the concentration profile of MEA did not decrease for the whole duration of the experiments, this would not coincide with what is known from theory and previous research; that MEA is not formed, only consumed, in oxidative and thermal degradation. It seems as this is a reasonable assumption to make. If more data had been included in the model, the ML model would identify the outliers in the datasets more efficiently. Therefore, when considering the size of the available datasets, removing the obvious outliers in the experimental data is further supported as something that will optimize the model's parameters.

The results showed that assuming an average degradation rate for the degradation compounds will limit the model's validity range. For MEA, as an example, the concentration will decrease rapidly and eventually go below zero. As has been mentioned earlier, the expected development of the concentration is not linear. However, for many of the modelled results, the model's predictions with a linear rate were good. For a short interval of time, it can therefore be ok to assume a linear reaction rate.

### 5 Conclusion

The objective of this work was to see if there was potential for using machine learning to model the oxidative and thermal degradation of MEA. Machine learning models have been developed by modelling the reaction rates of MEA and known degradation compounds. The data used for the modelling is experimental data from experiments performed at lab-scale. The experiments were conducted by Vevelstad et al. (2016) and Davis (2009). The modelled degradation rates were used to calculate the concentration profiles of the components, and the modelled concentrations were compared to the experimental values.

From the results of the oxidative degradation modelling, it is seen that the results are generally good. For the oxidative degradation model with three inputs, the modelled concentration was calculated in two different ways. The first method used the average of the modelled rates to calculate the concentrations, resulting in a linear curve. However, for MEA and the degradation compounds, a linear development will not be relevant over a longer time frame; thus, the validity range will be limited. Therefore, the simultaneous rate was also used to calculate the concentrations. This improved the model predictions and provided concentration profiles and trends closer to what was seen in the experimental data. The second model developed used all the available ten or eleven parameters as an input. This was to see if the machine learning model would find a correlation between the measured degradation compounds. This model improved the fit for many of the plotted results, and the curves seem to follow the experimental data points more accurately than the model with three inputs. However, the results show that the second model is more sensitive to outliers or zero-values than the first model, thus having more outlier plots than seen from the 3 input model.

More understanding of the chemical reactions and effect of the conditions used are needed to improve the oxidative degradation modelling. In addition, more experimental data could also improve the prediction abilities of the model. Nevertheless, the results from the modelling are promising, and there is potential for making a model that can predict oxidative degradation in a chemical absorption plant.

There was less experimental data available for thermal degradation than for oxidative degradation, but still, the results show potential. Also here two models were developed. The first model had three inputs, and the second model used all the available six parameters as inputs. The fit improved for the 6 input model, and the curves seem to follow the experimental data points better than for the model with three inputs.

Thermal degradation is, as mentioned, better understood than oxidative degradation. Therefore, to improve the predictions of the thermal degradation model, one could include more existing experimental data. Also, it would be interesting to develop a mechanistic model in addition to the empirical model since the reactions and products formed are more well known.

One of the main characteristics of the models is that they are data-driven and require experimental data. This can be disadvantageous, and it will be challenging to apply the models to other plants because it would require experimental data from each specific plant performed at its given conditions for the model to give good model predictions. To make an ML model that would not require experimental data, only parameters such as initial concentration of the solvent, temperature, oxygen concentration and  $CO_2$ -loading would simplify the modelling and make the models more applicable to a larger variety of industrial plants. Furthermore, from the results, outliers in the data are more easily identified. This is, as mentioned, called smoothening of data and can help identify outliers and patterns in the dataset. This is one of the advantages of making a simple model such as the ones developed in this thesis.

There is still much work to do on both models, and as mentioned, more research and understanding of the degradation process is needed to improve the models. Also, understanding how oxidative and thermal degradation is connected is essential if a model describing both processes in an industrial plant can be developed. However, the developed models in this thesis have potential, and they are a good start and basis for further work.

## 6 Further work

The results presented in this thesis are promising and show great potential for further modelling of oxidative and thermal degradation with machine learning. However, some issues were observed with the chosen modelling approach. In this chapter, some recommendations and suggestions that could improve the models' prediction abilities and ideas that would be interesting to implement in a future model are given.

The developed models in this thesis are empirical, and as mentioned earlier, the validity range is low. Therefore, there is a need for more experimental data to increase the validity range and accuracy of the models. It will also be beneficial if this experimental data is from experiments conducted for a wider time interval and at a large variety of conditions.

As mentioned in the introduction of this thesis, the ultimate goal of this work would be to make a model that ties oxidative and thermal degradation together. The models developed in this thesis describing either the oxidative or thermal degradation of MEA will not be applicable to a large scale plant because both oxidative and thermal degradation will occur in the system. For this model to have good prediction abilities, there is a need to understand how these two types of degradation are connected and affect each other. A model that could describe the two types of degradation could help understand the process further and potentially save the plant money and reduce yearly expenses connected to the degradation of the solvent. As of now not, such a model is not likely to be developed any time soon, but it is a fascinating idea.

The models developed in this thesis are supervised, shallow neural network models. Another approach would be deep learning, meaning having several hidden layers in the neural network. Deep learning is even more complex than shallow neural and can generalize and recognize patterns in data even better than shallow neural networks.<sup>[15]</sup> The method is complicated and would require research, but it has the potential to improve the results substantially.

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# Appendix

# A Figures

## A Oxidative degradation

#### A.1 MEA

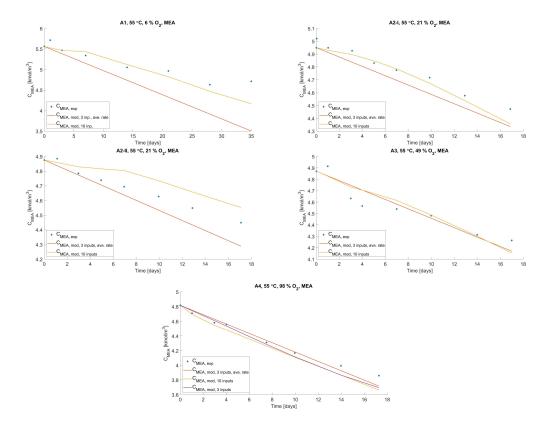


Figure A.1: Plotted results for experiment A1, A2-I, A2-II, A3 and A4 done at 55°C for MEA. The blue dots are the experimental datapoints, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

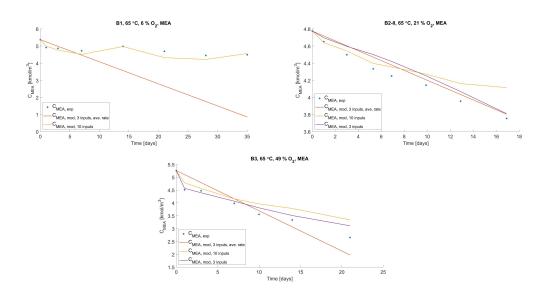


Figure A.2: Plotted results for experiment B1, B2-II and B3 done at 65°C for MEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

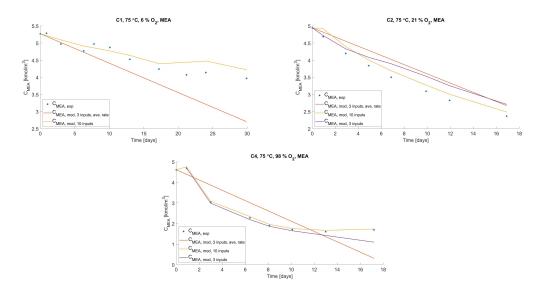


Figure A.3: Plotted results for experiment C1, C2 and C4 done at 75°C for MEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.2 Formate

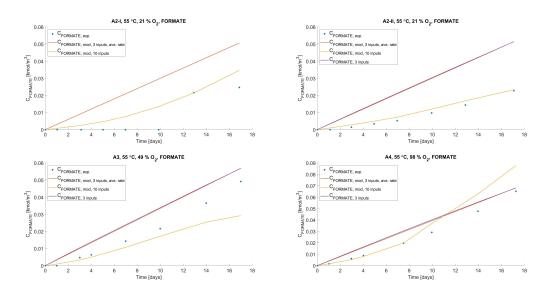


Figure A.4: Plotted results for experiment A2-I, A2-II, A3 and A4 done at 55°C for formate. The blue dots are the experimental data points, and the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, the purple line is the ML-model with 3 inputs with instantaneous rate.

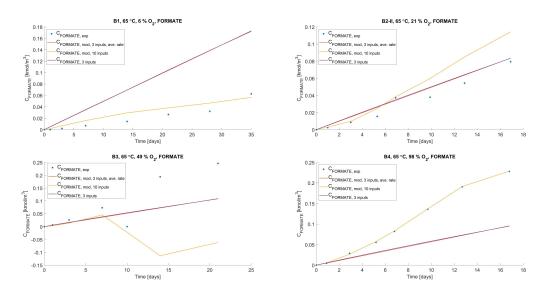


Figure A.5: Plotted results for experiment B1, B2-II, B3, B4 done at 65°C for formate. The blue dots are the experimental data points, and the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, the purple line is the ML-model with 3 inputs with instantaneous rate.

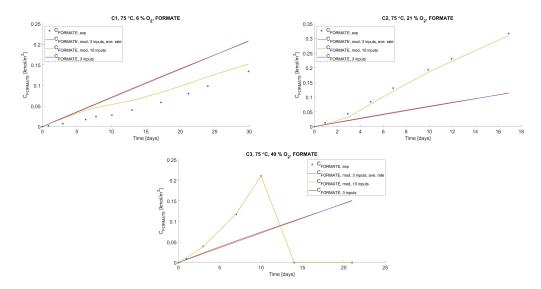


Figure A.6: Plotted results for experiment C1, C2 and C3 done at 75°C for formate. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.3 Oxalic acid

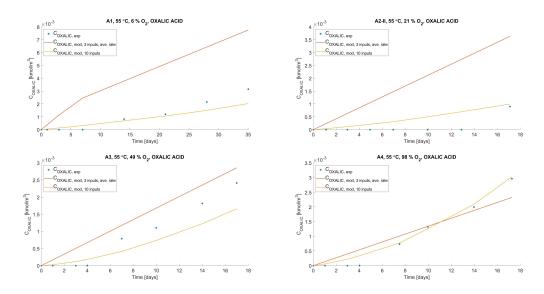


Figure A.7: Plotted results for experiment A1, A2-II, A3 and A4 done at 55°C for oxalic acid. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 11 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

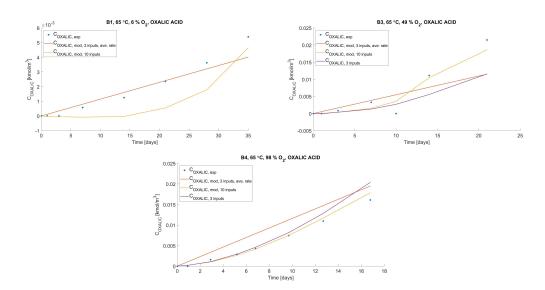


Figure A.8: Plotted results for experiment B1, B3 and B4 done at 65°C for oxalic acid. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 11 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

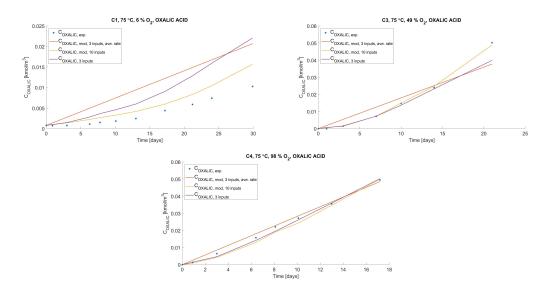


Figure A.9: Plotted results for experiment C1, C3 and C4 done at 75°C for oxalic acid. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 11 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.4 HEGly

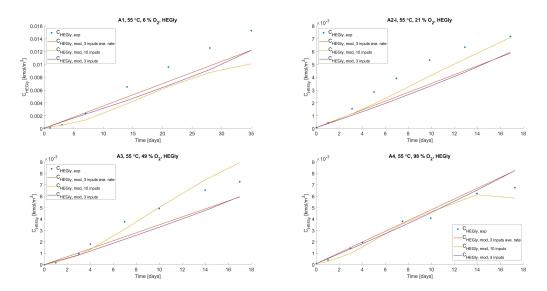


Figure A.10: Plotted results for experiment A1, A2-I, A3 and A4 done at 55°C for HEGly. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

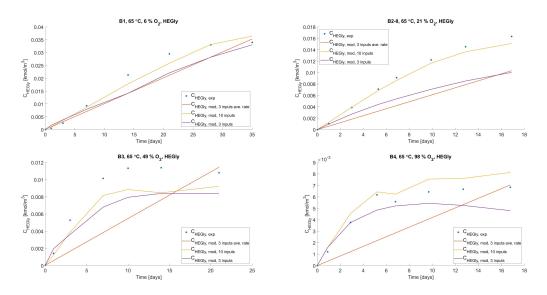


Figure A.11: Plotted results for experiment B1, B2-II, B3 and B4 done at 65°C for HEGly. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

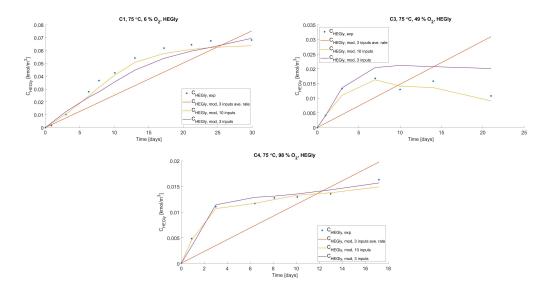


Figure A.12: Plotted results for experiment C1, C3 and C4 done at 75°C for HEGly. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.5 HEPO

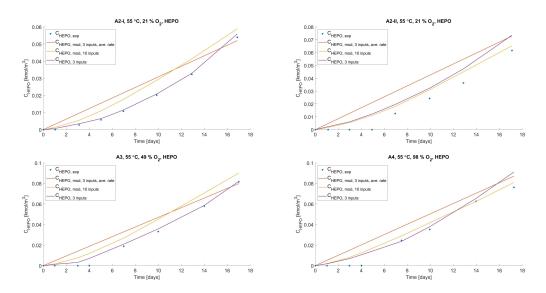


Figure A.13: Plotted results for experiment A2-I, A2-II, A3 and A4 done at 55°C for HEPO. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

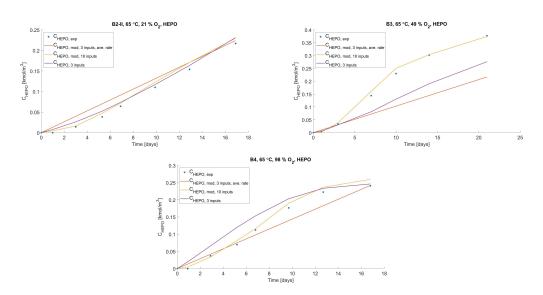


Figure A.14: Plotted results for experiment B2-II, B3 and B4 done at 65°C for HEPO. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

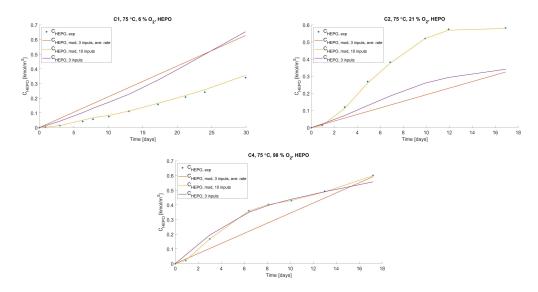


Figure A.15: Plotted results for experiment C1, C2 and C4 done at 75°C for HEPO. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.6 HEF

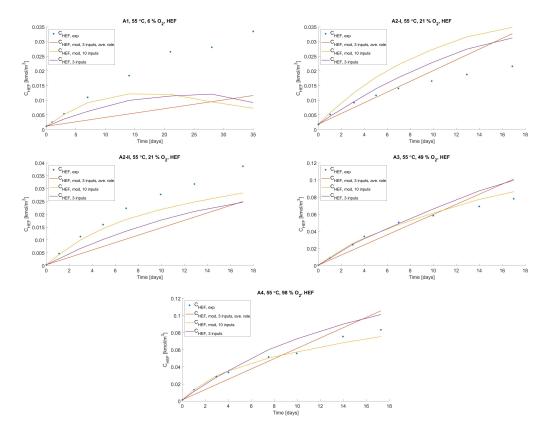


Figure A.16: Plotted results for experiment A1, A2-I, A2-II, A3 and A4 done at 55°C for HEF. The blue dots are the experimental data points, the red line is the MLmodel with 3 inputs and average reaction rate, the yellow line is the MLmodel with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

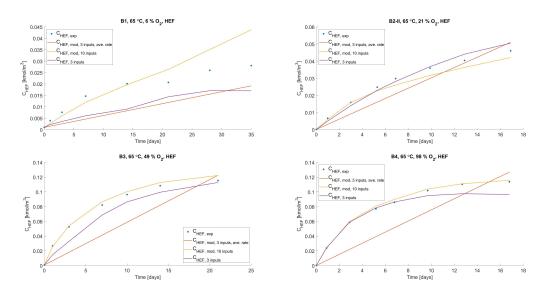


Figure A.17: Plotted results for experiment B1, B2-II, B3 and B4 done at 65°C for HEF. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

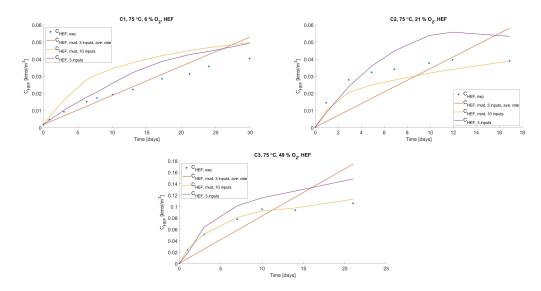


Figure A.18: Plotted results for experiment C1, C2 and C3 done at 75°C for HEF. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.7 HEA

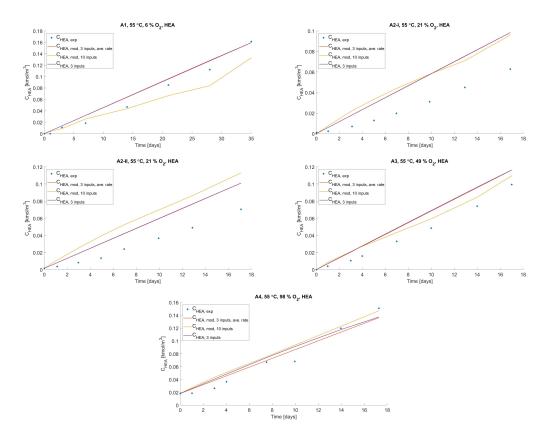


Figure A.19: Plotted results for experiment A1, A2-I, A2-II, A3 and A4 done at 55°C for HEA. The blue dots are the experimental data points, the red line is the MLmodel with 3 inputs and average reaction rate, the yellow line is the MLmodel with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

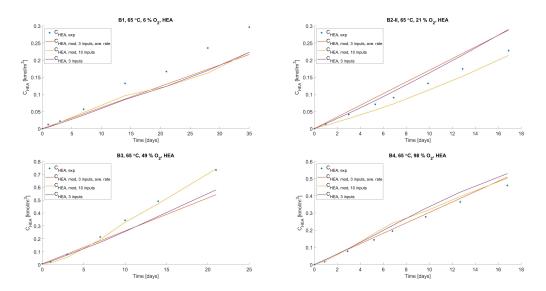


Figure A.20: Plotted results for experiment B1, B2-II, B3 and B4 done at 65°C for HEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

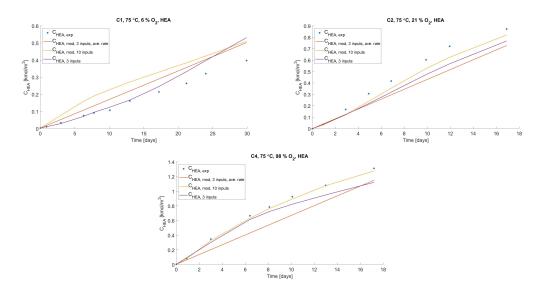


Figure A.21: Plotted results for experiment C1, C2 and C4 done at 75°C for HEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.8 BHEOX

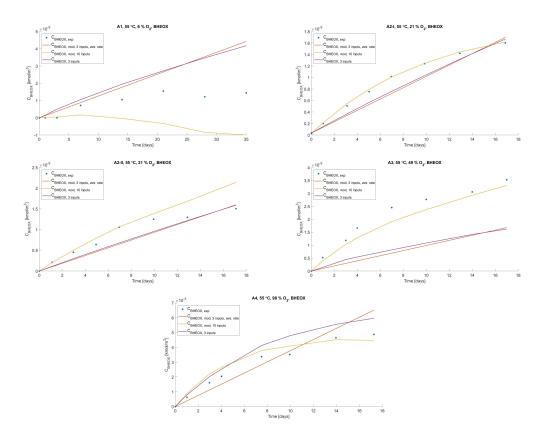


Figure A.22: Plotted results for experiment A1, A2-I, A2-II, A3 and A4 done at 55°C for BHEOX. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the MLmodel with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

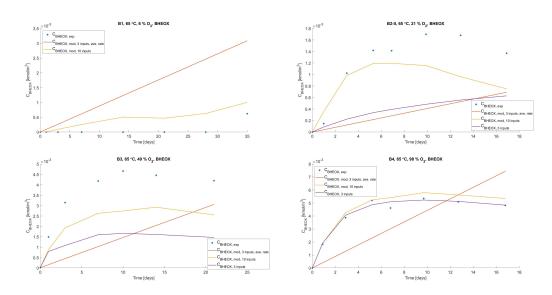


Figure A.23: Plotted results for experiment B1, B2-II, B3 and B4 done at 65°C for BHEOX. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

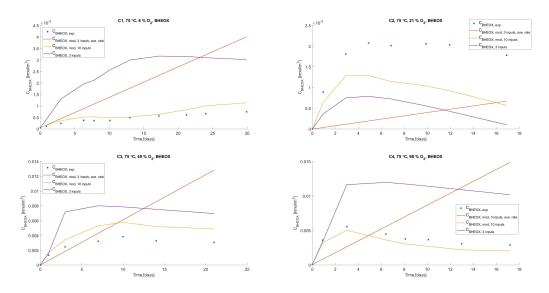


Figure A.24: Plotted results for experiment C1, C2, C3 and C4 done at 75°C for BHEOX. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

#### A.9 HEI

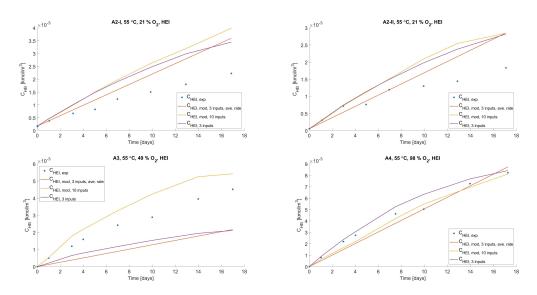


Figure A.25: Plotted results for experiment A2-I, A2-II, A3 and A4 done at 55°C for HEI. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

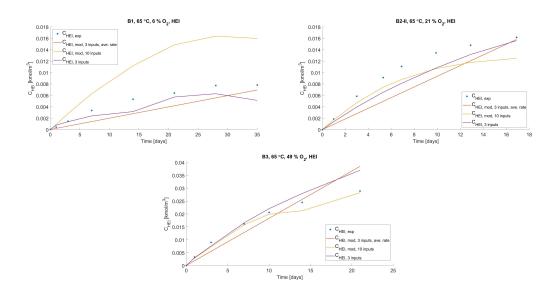


Figure A.26: Plotted results for experiment B1, B2-II and B3 done at 65°C for HEI. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

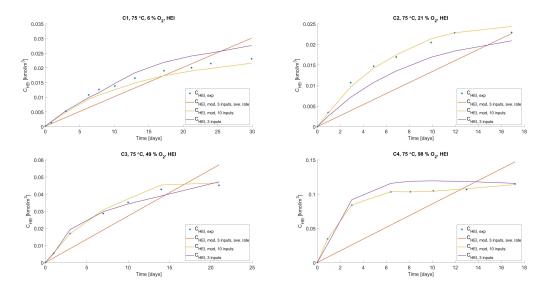


Figure A.27: Plotted results for experiment C1, C2, C3 and C4 done at 75°C for HEI. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs and average reaction rate, the yellow line is the ML-model with 10 inputs, and the purple line is the ML-model with 3 inputs with instantaneous rate.

### **B** Thermal degradation

#### B.1 MEA

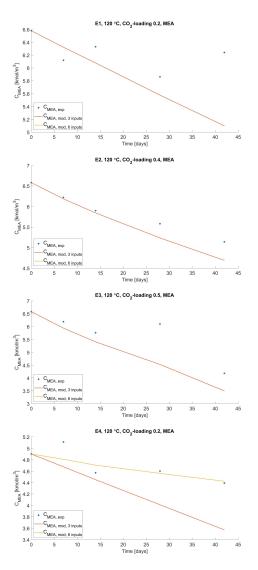


Figure A.28: Plotted results for experiment E1, E2, E3 and E4 done at 120°C for MEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

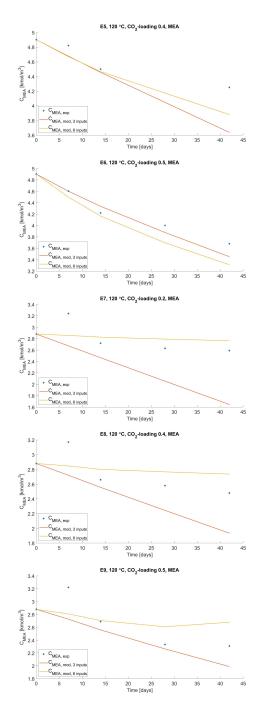


Figure A.29: Plotted results for experiment E5, E6, E7, E8 and E9 done at 120°C for MEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

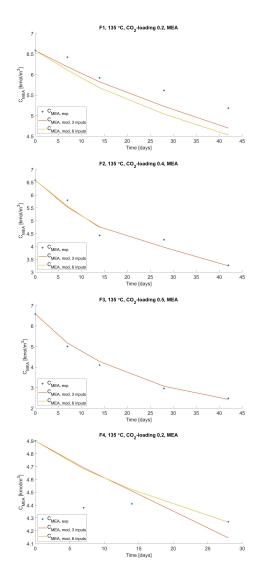


Figure A.30: Plotted results for experiment F1, F2, F3 and F4 done at 135°C for MEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

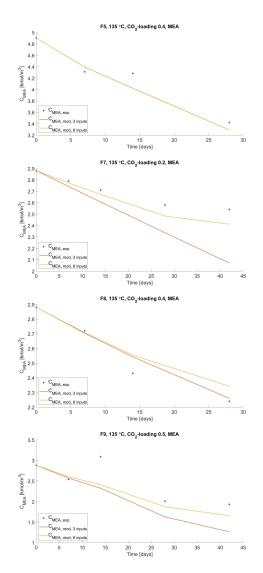


Figure A.31: Plotted results for experiment F5, F7, F8 and F9 done at 135°C for MEA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

#### B.2 HEEDA

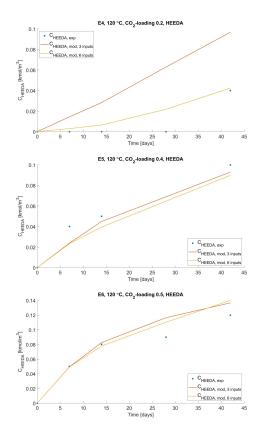


Figure A.32: Plotted results for experiment E4, E5 and E6 done at 120°C for HEEDA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

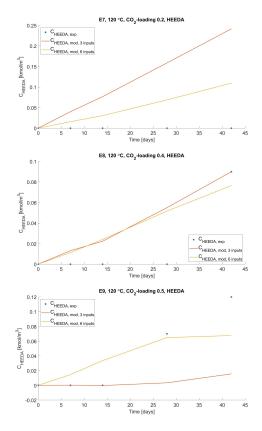


Figure A.33: Plotted results for experiment E7, E8 and E9 done at 120°C for HEEDA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

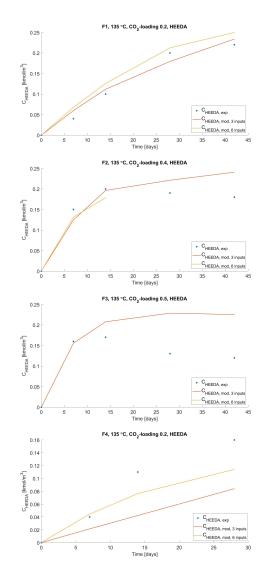


Figure A.34: Plotted results for experiment F1, F2, F3 and F4 done at 135°C for HEEDA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

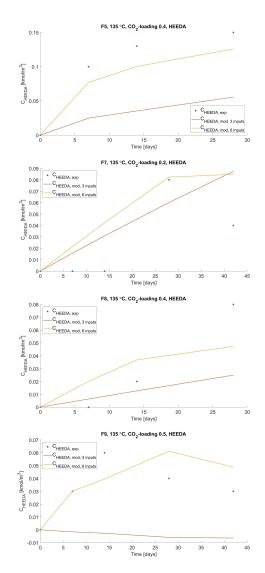


Figure A.35: Plotted results for experiment F5, F7, F8 and F9 done at 135°C for HEEDA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

#### B.3 HEIA

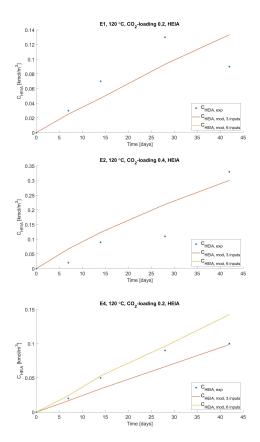


Figure A.36: Plotted results for experiment E1, E2, E3 and E4 done at 120°C for HEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

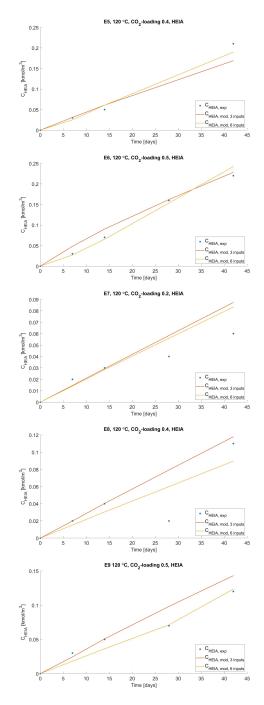


Figure A.37: Plotted results for experiment E5, E6, E7, E8 and E9 done at 120°C for HEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

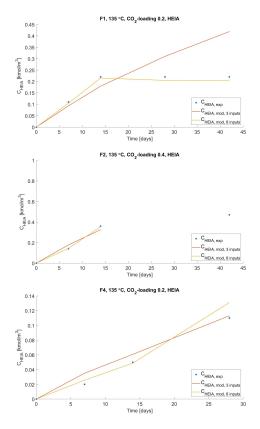


Figure A.38: Plotted results for experiment F1, F2, F3 and F4 done at 135°C for HEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

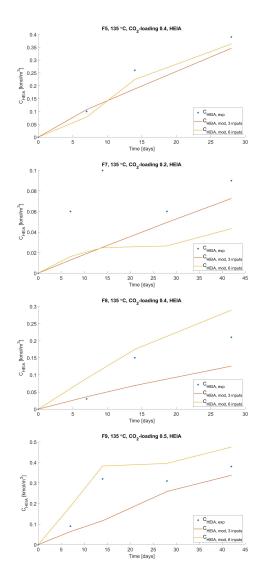


Figure A.39: Plotted results for experiment F5, F7, F8 and F9 done at 135°C for HEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

#### B.4 TriHEIA

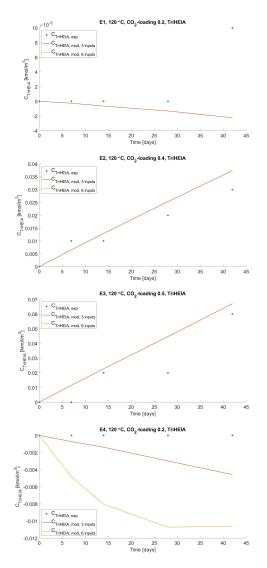


Figure A.40: Plotted results for experiment E1, E2, E3 and E4 done at 120°C for TriHEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

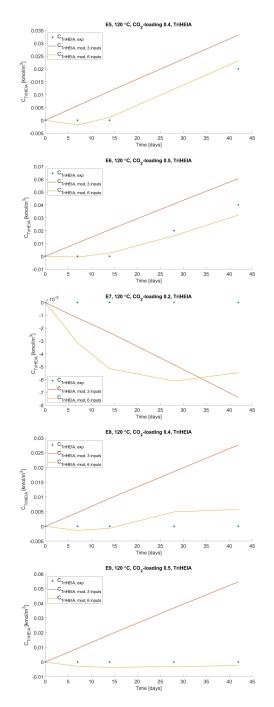


Figure A.41: Plotted results for experiment E5, E6, E7, E8 and E9 done at 120°C for Tri-HEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

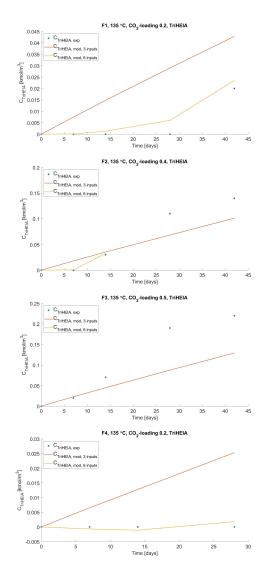


Figure A.42: Plotted results for experiment F1, F2, F3 and F4 done at 135°C for TriHEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

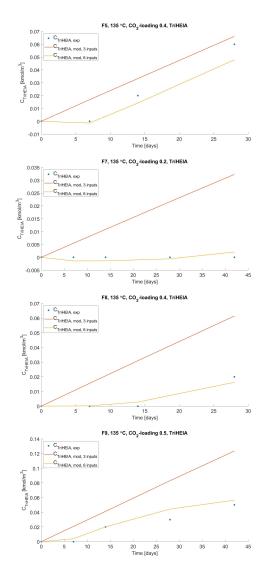


Figure A.43: Plotted results for experiment F5, F7, F8 and F9 done at 135°C for TriHEIA. The blue dots are the experimental data points, the red line is the ML-model with 3 inputs, and the yellow line is the ML-model with 6 inputs.

# B Tables with AAD and AARD

### A Oxidative degradation

Table B.1: AAD for MEA. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.419	0.149	-
A2-I	0.077	0.038	-
A2-II	0.065	0.072	-
A3	0.065	0.066	-
A4	0.043	0.069	0.057
B1	1.307	0.132	-
B2-II	0.078	0.115	0.095
B3	0.312	0.299	0.159
B4	0.255	0.113	0.071
C1	0.422	0.161	-
C2	0.349	0.158	0.252
C3	0.741	0.223	-
C4	0.571	0.048	-

Table B.2: AARD for MEA. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	7.350	2.610	-
A2-I	1.538	0.761	-
A2-II	1.322	1.480	-
A3	1.313	1.344	-
A4	0.892	1.436	1.175
B1	24.34	2.471	-
B2-II	1.640	2.414	1.989
B3	5.938	5.688	3.014
B4	5.325	2.359	1.480
C1	7.977	3.053	-
C2	7.059	3.188	5.095
C3	13.65	4.108	-
C4	12.16	1.031	-

Table B.3: AAD for formate. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between the experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.030	0.003	0.030
A2-I	0.135	0.004	-
A2-II	0.014	0.001	0.014
A3	0.007	0.005	0.007
A4	0.006	0.006	0.006
B1	0.049	0.008	0.049
B2-II	0.006	0.012	0.006
B3	0.051	0.097	0.051
B4	0.052	0.001	0.051
C1	0.040	0.018	0.041
C2	0.007	0.007	0.080
C3	0.068	0.001	0.673
C4	0.158	0.145	0.158

Table B.4: AARD for formate. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	84.41	9.257	85.86
A2-I	54.68	17.70	-
A2-II	61.14	6.208	61.93
A3	13.97	10.84	14.46
A4	8.737	9.030	9.328
B1	78.66	12.52	78.92
B2-II	7.472	15.70	7.742
B3	20.84	39.56	20.72
B4	22.68	0.443	22.37
C1	29.70	13.56	30.34
C2	25.47	2.331	25.16
C3	32.41	0.470	31.95
C4	26.93	24.75	26.95

Table B.5: AAD for oxalic acid. (1) AAD between the experimental values and the model
with 3 inputs and average rate. (2) AAD between the experimental values and
the model with 11 inputs. (3) AAD between the experimental values and the
model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.0025	0.0003	_
A2-II	0.0014	0.0002	-
A3	0.0004	0.0003	-
A4	0.0003	0.0001	-
B1	0.0004	0.0008	-
B2-II	0.0003	0.0009	0.0003
B3	0.0030	0.0013	0.0029
B4	0.0026	0.0005	0.0010
C1	0.0055	0.0017	0.0039
C2	0.0022	0.0021	0.0020
C3	0.0040	0.0004	0.0018
C4	0.0012	0.0015	0.0010

Table B.6: AARD for oxalic acid. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 11 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	78.16	10.11	-
A2-II	153.1	27.49	-
A3	17.04	12.51	-
A4	9.022	3.669	-
B1	6.697	14.84	-
B2-II	5.172	18.56	6.222
B3	13.87	6.179	13.70
B4	16.02	2.819	6.189
C1	53.37	16.72	38.22
C2	6.397	6.273	5.881
C3	7.989	0.893	3.626
C4	2.514	3.119	2.057

Table B.7: AAD for HEGly. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between the experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.0013	0.0020	0.0015
A2-I	0.0009	0.0005	0.0010
A2-II	0.0004	0.0002	0.0005
A3	0.0008	0.0005	0.0010
A4	0.0004	0.0003	0.0004
B1	0.0031	0.0015	0.0030
B2-II	0.0038	0.0005	0.0031
B3	0.0030	0.0015	0.0020
B4	0.0017	0.0007	0.0008
C1	0.0105	0.0030	0.0050
C2	0.0055	0.0009	0.0015
C3	0.0064	0.0011	0.0038
C4	0.0032	0.0004	0.0007

Table B.8: AARD for HEGly. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	8.705	13.00	10.02
A2-I	12.26	7.391	13.39
A2-II	5.796	3.268	6.661
A3	11.06	6.904	12.29
A4	5.636	5.182	5.520
B1	9.139	4.421	8.873
B2-II	22.99	2.844	19.16
B3	26.32	13.21	17.95
B4	25.58	9.898	11.96
C1	15.32	4.354	7.019
C2	35.63	5.989	9.494
C3	38.09	6.633	22.59
C4	19.34	2.233	4.128

Table B.9: AAD for HEPO. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between the experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.037	0.010	0.050
A2-I	0.006	0.004	0.001
A2-II	0.013	0.005	0.007
A3	0.009	0.008	0.002
A4	0.011	0.005	0.005
B1	0.015	0.013	0.013
B2-II	0.018	0.008	0.009
B3	0.075	0.007	0.054
B4	0.014	0.009	0.023
C1	0.141	0.007	0.122
C2	0.178	0.004	0.147
C3	0.107	0.048	0.081
C4	0.059	0.001	0.017

Table B.10: AARD for HEPO. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	22.6	6.31	30.7
A2-I	10.3	8.00	1.25
A2-II	21.0	8.69	11.9
A3	11.5	9.51	2.63
A4	14.3	6.33	6.63
B1	5.08	4.39	4.43
B2-II	8.25	3.76	4.29
B3	19.9	1.84	14.4
B4	5.94	3.61	9.49
C1	41.4	2.12	35.9
C2	30.7	0.64	25.3
C3	18.7	8.25	14.0
C4	9.87	0.15	2.76

Table B.11: AAD for HEF. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between the experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.011	0.008	0.009
A2-I	0.003	0.006	0.004
A2-II	0.009	0.004	0.007
A3	0.008	0.003	0.007
A4	0.008	0.003	0.008
B1	0.007	0.005	0.006
B2-II	0.005	0.002	0.002
B3	0.024	0.003	0.009
B4	0.023	0.002	0.005
C1	0.004	0.010	0.006
C2	0.010	0.005	0.009
C3	0.023	0.003	0.020
C4	0.052	0.022	0.034

Table B.12: AARD for HEF. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	31.61	25.28	26.48
A2-I	13.08	28.42	16.26
A2-II	22.49	9.982	18.10
A3	10.49	4.218	8.450
A4	9.811	3.160	9.321
B1	25.60	16.24	23.05
B2-II	10.94	5.119	4.341
B3	20.63	2.764	8.217
B4	20.05	1.479	4.281
C1	8.845	25.57	14.23
C2	24.72	11.75	22.27
C3	22.14	2.545	18.74
C4	32.86	13.69	21.74

Table B.13: AAD for HEA. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between the experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.008	0.011	0.008
A2-I	0.016	0.017	0.016
A2-II	0.016	0.024	0.016
A3	0.012	0.008	0.013
A4	0.009	0.010	0.010
B1	0.031	0.031	0.033
B2-II	0.025	0.013	0.021
B3	0.064	0.013	0.059
B4	0.016	0.025	0.032
C1	0.053	0.083	0.032
C2	0.098	0.050	0.077
C3	0.032	0.023	0.066
C4	0.016	0.018	0.074

Table B.14: AARD for HEA. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	5.05	7.08	5.18
A2-I	25.8	27.0	25.9
A2-II	23.2	34.1	23.4
A3	12.3	8.55	12.6
A4	5.77	6.76	6.61
B1	10.4	10.4	11.0
B2-II	11.1	5.83	9.04
B3	8.69	1.82	7.99
B4	3.57	5.51	6.98
C1	13.2	21.1	7.94
C2	11.3	5.78	8.83
C3	2.28	1.68	4.74
C4	12.0	1.37	5.63

Table B.15: AAD for BHEOX. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between the experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.0010	0.0010	0.0010
A2-I	0.0001	0.0000	0.0001
A2-II	0.0002	0.0002	0.0002
A3	0.0012	0.0002	0.0011
A4	0.0005	0.0004	0.0006
B1	0.0011	0.0003	-
B2-II	0.0008	0.0003	0.0008
B3	0.0020	0.0012	0.0020
B4	0.0020	0.0004	0.0002
C1	0.0012	0.0002	0.0017
C2	0.0013	0.0007	0.0011
C3	0.0028	0.0013	0.0031
C4	0.0044	0.0007	0.0056

Table B.16: AARD for BHEOX. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	62.97	65.15	64.15
A2-I	8.386	1.121	7.144
A2-II	11.40	11.39	10.28
A3	34.19	6.884	32.29
A4	10.97	7.645	13.02
B1	181.9	47.37	-
B2-II	47.56	18.93	44.44
B3	42.64	25.93	42.61
B4	29.78	6.599	2.974
C1	166.1	20.18	234.7
C2	63.16	34.63	53.78
C3	73.57	33.82	81.93
C4	79.23	11.70	100.3

Table B.17: AAD for HEI. (1) AAD between the experimental values and the model with 3 inputs and average rate. (2) AAD between the experimental values and the model with 10 inputs. (3) AAD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AAD $(1)$	AAD $(2)$	AAD $(3)$
A1	0.0013	0.0023	0.0009
A2-I	0.0004	0.0007	0.0006
A2-II	0.0003	0.0004	0.0004
A3	0.0012	0.0007	0.0011
A4	0.0004	0.0003	0.0004
B1	0.0014	0.0045	0.0011
B2-II	0.0025	0.0018	0.0016
B3	0.0030	0.0010	0.0021
B4	0.0067	0.0006	0.0018
C1	0.0028	0.0012	0.0018
C2	0.0049	0.0056	0.0027
C3	0.0065	0.0011	0.0015
C4	0.0278	0.0004	0.0088

Table B.18: AARD for HEI. (1) AARDD between the experimental values and the model with 3 inputs and average rate. (2) AARD between the experimental values and the model with 10 inputs. (3) AARD between the experimental values and the model with 3 inputs with simultaneous rate.

Experiment	AARD (1) [%]	AARD (2) [%]	AARD (3) [%]
A1	49.91	91.54	37.24
A2-I	19.59	30.42	25.74
A2-II	16.83	24.55	22.61
A3	27.47	15.49	23.93
A4	4.887	3.798	4.754
B1	17.31	57.14	13.44
B2-II	15.48	11.35	9.824
B3	10.41	3.438	7.412
B4	12.45	1.110	3.404
C1	12.16	5.084	7.948
C2	21.33	2.427	11.90
C3	14.47	2.587	3.284
C4	24.21	0.368	7.677

## **B** Thermal degradation

Table B.19: AAD for MEA. (1) AAD between the experimental values and the ML model with 3 inputs. (2) AAD between the experimental values and the model with 6 inputs.

Experiment	AAD $(1)$	AAD 6 (2)
E1	0.38	-
E2	0.18	-
E3	0.57	-
E4	0.39	0.10
E5	0.20	0.14
E6	0.09	0.17
$\mathrm{E7}$	0.47	0.17
E8	0.29	0.18
E9	0.20	0.21
F1	0.24	0.36
F2	0.18	-
F3	0.10	-
F4	0.13	0.10
F5	0.12	0.12
F6	0.11	0.09
F7	0.17	0.06
F8	0.04	0.06
F9	0.37	0.23

Experiment	AARD (1) [%]	AARD (2) [%]
E1	5.7	-
E2	2.7	-
E3	8.7	-
E4	7.7	2.0
E5	4.1	2.8
E6	1.9	3.4
$\mathrm{E7}$	14.4	5.1
E8	9.1	5.7
E9	6.3	6.7
F1	3.7	5.4
F2	2.8	-
F3	1.6	-
F4	2.7	2.1
F5	2.4	2.4
F6	2.1	1.8
F7	6.0	2.0
F8	1.3	2.1
F9	12.0	7.5

Table B.20: AARD for MEA. (1) AARD between the experimental values and the ML model with 3 inputs. (2) AARD between the experimental values and the model with 6 inputs.

Experiment	AAD $(1)$	AAD $(2)$
E1	0.02	_
E2	0.04	-
E4	0.01	0.01
E5	0.01	0.01
E6	0.01	0.01
E7	0.01	0.01
E8	0.01	0.01
E9	0.01	0.01
F1	0.07	0.01
F4	0.01	0.01
F5	0.03	0.02
F6	0.04	0.01
F7	0.03	0.04
F8	0.04	0.04
F9	0.06	0.07

Table B.21: AAD for HEIA. (1) AAD between the experimental values and the ML model with 3 inputs. (2) AAD between the experimental values and the model with 6 inputs.

Experiment	AARD (1)[%]	AARD (2)[%]
E1	16.6	-
E2	13.3	-
E4	8.82	11.1
E5	6.28	4.28
E6	4.45	3.29
$\mathrm{E7}$	17.3	15.6
E8	12.3	13.6
E9	9.60	5.03
F1	31.4	3.82
F4	6.58	6.32
F5	7.93	5.44
F6	8.61	2.74
F7	30.0	39.8
F8	20.4	19.4
F9	17.0	17.9

Table B.22: AARD for HEIA. (1) AARD between the experimental values and the ML model with 3 inputs. (2) AARD between the experimental values and the model with 6 inputs.

Experiment	AARD (1)	AAD $(2)$
E4	0.03	0.01
E5	0.01	0.01
E6	0.01	0.01
$\mathrm{E7}$	0.10	0.04
E8	0.02	0.02
E9	0.03	0.02
F1	0.01	0.02
F2	0.02	-
F3	0.05	-
F4	0.04	0.02
F5	0.07	0.02
F6	0.04	0.02
F7	0.02	0.02
F8	0.02	0.02
F9	0.04	0.01

Table B.23: AAD for HEEDA. (1) AAD between the experimental values and the ML model with 3 inputs. (2) AAD between the experimental values and the model with 6 inputs.

Experiment	AARD (1) [%]	AARD (2) [%]
E4	81.2	16.8
E5	7.04	9.30
${ m E6}$	7.69	7.17
$\mathrm{E7}$	-	-
E8	20.1	22.3
E9	28.6	17.6
F1	5.99	8.69
F2	12.1	-
F3	29.9	-
F4	25.4	13.1
F5	44.1	12.8
F6	33.6	19.7
F7	28.5	27.8
F8	21.5	21.8
F9	58.9	20.2

Table B.24: AARD for HEEDA. (1) AARD between the experimental values and the ML model with 3 inputs. (2) AARD between the experimental values and the model with 6 inputs.

Experiment	AAD $(1)$	AAD $(2)$
E1	0.00	-
E2	0.00	-
E3	0.01	-
E4	0.00	0.01
E5	0.01	0.00
E6	0.01	0.00
$\mathrm{E7}$	0.00	0.00
E8	0.01	0.00
E9	0.00	0.01
F1	0.01	0.00
F2	0.02	-
F3	0.04	-
F4	0.01	0.00
F5	0.01	0.00
F6	0.01	0.00
F7	0.01	0.00
F8	0.02	0.00
F9	0.03	0.01

Table B.25: AAD for TriHEIA. (1) AAD between the experimental values and the ML model with 3 inputs. (2) AAD between the experimental values and the model with 6 inputs.

Experiment	AARD (1) [%]	AARD (2) [%]
E1	29.0	-
E2	12.7	-
E3	15.3	-
E4	-	-
E5	37.7	7.68
E6	36.2	7.50
E7	-	-
E8	-	-
E9	-	-
F1	74.1	11.0
F2	14.8	-
F3	20.1	-
F4	-	-
F5	15.1	7.99
F6	9.76	1.36
F7	-	-
F8	110	8.37
F9	67.4	10.0

Table B.26: AARD for TriHEIA. (1) AARD between the experimental values and the ML model with 3 inputs. (2) AARD between the experimental values and the model with 6 inputs.

# C MATLAB code

In this chapter, some example code from the modelling in MATLAB is given.

### A MATLAB code oxidative degradation

#### A.1 Example: HEPO 3 input model data file

```
clear
 1
   clc
2
   close all
3
 4
   DOT = [
\mathbf{5}
6
   5.560000000 \ 6 \ 328.15
\overline{7}
   5.711823131 \ 6 \ 328.15
8
   5.465229927 6 328.15
9
   5.341912612 \ 6 \ 328.15
10
   5.052484218 6 328.15
11
   4.963055823 \ 6 \ 328.15
12
   4.631034815 6 328.15
13
   4.712075773 6 328.15
14
15
   4.95
                  21
                       328.15
16
   4.948427315 21
                       328.15
17
   4.925410918 21
                       328.15
18
   4.830016762 21
                       328.15
19
   4.774658871 21
                       328.15
20
   4.716091961 21
                       328.15
21
   4.576204533 21
                       328.15
22
   4.472071886 21
                       328.15
23
24
   4.875
                  21
                       328.15
25
   4.737944046 21
                       328.15
26
   4.692972306 21
                       328.15
27
   4.626608838 21
                       328.15
^{28}
   4.548468095 21
29
                       328.15
   4.448673133 21
                       328.15
30
^{31}
   4.87
                  49
                       328.15
32
   4.56647853
                  49
                       328.15
33
   4.539215368 49
                       328.15
34
```

```
4.479785934 49
                      328.15
35
   4.313389169 49
                      328.15
36
   4.263836337 49
                      328.15
37
38
   4.817
                 98
                      328.15
39
   4.55720619
                 98
                      328.15
40
   4.311055911 \ 98
                      328.15
41
   4.167074428 98
                      328.15
42
   3.991948363 98
                      328.15
43
   3.859212836 98
                      328.15
44
45
   5.37
                 6 \ 338.15
46
   4.911035228 6 338.15
47
   4.863074058 6 338.15
48
   4.716951419 6 338.15
49
   4.974640781 6 338.15
50
   4.690677151 \ \ 6 \ \ 338.15
51
   4.446093649 6 338.15
52
   4.492912239 \ 6 \ 338.15
53
54
   4.775
                 21
                      338.15
55
   4.651566177 21
                      338.15
56
   4.498363888 21
                      338.15
57
   4.334036235 21
                      338.15
58
   4.249692067 21
                      338.15
59
   4.142513473 21
                      338.15
60
   3.955865155 21
                      338.15
61
   3.753967639 21
                      338.15
62
63
   5.26
                 49
                      338.15
64
   4.506904135 49
                      338.15
65
   4.470774185 49
                      338.15
66
   3.980779552 49
                      338.15
67
   3.555425284 49
                      338.15
68
   3.337613545 49
                      338.15
69
   2.651222746 49
                      338.15
70
71
   4.798
                 98
                      338.15
72
   4.405681764 98
                      338.15
73
   3.896320554 98
                      338.15
74
   3.606477896 98
                      338.15
75
   3.373334889 98
                      338.15
76
   3.022642215 98
                      338.15
77
   2.714667974 98
                      338.15
78
```

```
2.387096959 98
                       338.15
79
80
    5.27
                  6 348.15
81
    5.2879338 6 348.15
82
    4.974793126 \ 6 \ 348.15
83
    4.769646356 6 348.15
84
    4.97394122 \quad 6 \quad 348.15
85
    4.870772163 \ 6 \ 348.15
86
    4.526150579 6 348.15
87
    4.238312461 6 348.15
88
    4.069101956 6 348.15
89
    4.139477397 \ 6 \ 348.15
90
    3.968698224 6 348.15
91
92
    4.944
                  21
                       348.15
93
    4.690061157 21
                       348.15
94
    4.196898229 21
                       348.15
95
    3.836553249 21
                       348.15
96
    3.499202912 21
                       348.15
97
    3.0930167 21
                    348.15
98
    2.824493483 21
                       348.15
99
    2.362609886 21
                       348.15
100
101
    5.06
                       348.15
                  49
102
    5.428108647 49
                       348.15
103
    4.165642573 49
                       348.15
104
                       348.15
    3.434605249 49
105
    3.129162546 49
                       348.15
106
    3.139614905 49
                       348.15
107
    2.045924558 49
                       348.15
108
109
    4.62
                  98
                       348.15
110
    4.69620739
                       348.15
                  98
111
    3.041796127 98
                       348.15
112
    2.276859458 98
                       348.15
113
    1.896128731 98
                       348.15
114
    1.704424298 98
                       348.15
115
    1.601117644 98
                       348.15
116
    1.693475041 98
                       348.15
117
118
    ];
119
120
121
122
```

123	TEDO I
124	m rHEPO = [
125	0
126	0
127	5.4500 E-04
128	1.3625 E-03
129	3.1143E-03
130	2.6471 E-03
131	7.4743E-03
132	9.1871E-03
133	6.0729 E-03
134	
135	
136	$0.0000 \text{E}{+00}$
137	1.3015 E-03
138	1.6010E-03
139	2.5832E-03
140	3.2332E-03
141	3.9625 E-03
142	5.4721 E-03
143	8.8939E-03
144	
145	
146	$0.0000 \text{E}{+00}$
147	6.2460 E- 03
148	3.9194E-03
149	4.0720 E-03
150	5.9992 E- 03
151	7.2398E-03
152	
153	
154	$0.0000 \mathrm{E}{+00}$
155	6.2479 E-03
156	4.8167 E-03
157	6.1967E-03
158	7.8763E-03
159	4.9998 E-03
160	
161	
162	$0.0000 \mathrm{E}{+00}$
163	6.9940E-03
164	4.3770 E-03
165	6.8378E-03
166	4.1261E-03

167

```
6.1547E-03
168
169
    0.0000E+00
170
    2.1800E-03
171
    5.4500E-03
172
    9.8100E-03
173
    9.1871E-03
174
    9.4986E-03
175
    9.8100E-03
176
    1.1367E-02
177
178
179
    0.0000E + 00
180
    7.0850\mathrm{E}{\text{-}}03
181
    1.0426E-02
182
    1.6350E-02
183
    1.5260 \text{E-}02
184
    1.4533E-02
185
    1.5805E-02
186
    1.3824E-02
187
188
189
    4.3600E-03
190
    1.4715E-02
191
    2.7523E-02
192
    2.8703E-02
193
    1.7985E-02
194
    1.0744E-02
195
    -8.0971E-03
196
197
198
    0.0000E+00
199
    1.8530E-02
200
    1.4217E-02
201
    2.6569E-02
202
    2.2176E-02
203
    1.5260 \text{E-}02
204
    4.5195E-03
205
    2.6585E-04
206
207
208
    3.6333E-03
209
    5.1905E-03
210
```

8.5879E-032111.0173E-022127.5826E-032131.2403E-022141.1160E-022151.2535E-022161.2068E-022171.6627 E-022181.7258E-02219220 221222 1.2974E-02223 5.4801E-027.4791E-022245.8104E-022254.5633E-02226 2.5921E-022271.4741E-03228 -4.6728E-03229 2302311.5260 E-02232 5.8315E-022335.7225E-02234-1.4533E-03 2355.4773E-02236 -3.3634E-02 237-3.1143E-04 238 239 240241 2.4222E-027.0071E-022425.6103E-022432.5006E-022441.3625E-022452.1800E-022462.5693E-022479.2650E-03248249]; 250

### A.2 Example: HEPO 10 input model data file

```
clear
1
   clc
2
   close all
3
4
\mathbf{5}
   Input = [
6
7
8
   5.560000000 \ 6 \ 328.15
                           0.00000000 0.001167320 2.675430E-05
9
       0.0000000000
                      0.0000671596
                                     0.0000000000
                                                     0.0000000000
   5.711823131 \ 6 \ 328.15
                           0.00000000 0.002559941 1.248930E-04
10
      0.0000000000
                      0.0001175670
                                     0.0000000000
                                                     0.0000000000
   5.465229927 6 328.15
                           0.000680503 0.005370319 2.856530E-04
11
      0.0000000000
                     0.0006050160
                                     0.0109000000
                                                     0.0010900000
   5.341912612 \ 6 \ 328.15
                           0.003139448 0.010990578 6.256630E-04
12
       0.0007168170
                      0.0023474270
                                     0.0185300000
                                                     0.0065400000
   5.052484218 6 328.15
                           0.009611549 0.018399819 1.200369E-03
13
      0.0010491140
                      0.0065098750
                                     0.0468700000
                                                     0.0283400000
   4.963055823 6 328.15
                           0.014842849 0.026519892 1.598068E-03
14
                      0.0095921610
      0.0015486010
                                     0.0850200000
                                                     0.0468700000
   4.631034815 6 328.15
                           0.025515765 0.028028314 2.078502E-03
15
       0.0012141410
                      0.0125694890
                                     0.1122700000
                                                     0.0991900000
   4.712075773 6 328.15
                           0.035207176 0.033447441 2.524977E-03
16
                      0.0152543180
       0.0014406820
                                     0.1613200000
                                                     0.1635000000
17
   4.95
                    328.15
                             0.00000000 \ 0.001851997 \ 0.000178362
                21
18
                                     0.0000000000
      0.0000340580
                      0.0000839496
                                                     0.0000000000
   5.020220179 21
                    328.15
                             0.00000000 \ 0.00178473
                                                        0.000160533
19
      0.0000283829
                      0.0000755579
                                     0.0011554000
                                                     0.0000000000
   4.948427315 21
                    328.15
                             0.00000000 \ 0.005171952 \ 0.000384133
20
       0.0001990110
                      0.0004456920
                                     0.0024198000
                                                     0.0000000000
   4.925410918 21
                    328.15
                             0.000000000 \ 0.009195184 \ 0.000672327
21
                      0.0015442440
                                     0.0069869000
                                                     0.0027250000
       0.0005078140
   4.830016762 21
                    328.15
                             0.00000000 \quad 0.011668854 \quad 0.000827321
22
      0.0007555360
                      0.0028527350
                                     0.0128838000
                                                     0.0057770000
23
   4.774658871 21
                    328.15
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       0.0010163460
                      0.0039148910
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                                                     0.0107910000
   4.716091961 21
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                      0.0053328910
                                     0.0309996000
                                                     0.0201650000
   4.576204533 21
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      0.0014205660
                      0.0063456700
                                     0.0449407000
                                                   0.0322640000
```

```
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                                                   0.0539550000
27
   4.875 21
              328.15
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                                     0.0000000000
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                     0.0003112740
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                                                    0.0000000000
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                                     0.0081750000
                                                    0.0000000000
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31
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                    0.0018302860
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                                                    0.0000000000
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                                                    0.0125350000
   4.626608838 21
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33
                                     0.0366567000
       0.0012492030
                     0.0043706960
                                                    0.0243070000
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                     0.0057104280
                                     0.0489083000
                                                    0.0362970000
   4.448673133 21
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                                                    0.0615850000
36
   4.87
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              328.15
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                     0.0000000000
                                     0.0000000000
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                                                    0.00000000000
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                                                    0.0187436400
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   4.55720619
                98
                    328.15
49
```

```
0.0019537200
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                                                    0.0244301700
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                                                    0.0351753900
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                                     0.1196351300
                                                    0.0625736300
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                                                       0.008224628
53
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                                     0.1508309300
                                                    0.0762128000
54
   5.37
         6 338.15
                    0.00000000 0.000987732 2.68E-05
                                                         0.0000000000
55
      0.0000419748
                      0.0000000000
                                     0.0000000000
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56
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                                                    0.0000000000
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                                                    0.0043600000
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                                     0.1318900000
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                                                    0.2256300000
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62
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                                     0.2964800000
                                                    0.2943000000
63
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   4.775 \ 21
              338.15
64
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      0.0000000000
                      0.0000000000
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                                     0.0130800000
                                                    0.0000000000
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                                                    0.0381500000
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                     0.0090912710
                                     0.0904700000
                                                    0.0643100000
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                      0.0122200100
                                     0.1318900000
                                                    0.1100900000
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   3.955865155 21
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70
                                     0.1744000000
                                                    0.1536900000
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                             0.079352092 \quad 0.046067145 \quad 0.016157756
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71
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      0.0013697710
                     0.0163208270
                                                    0.2169100000
```

72

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0.00000000 0.000729575 4.46E-05 0.0000170290
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73
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                                     0.0000000000
   4.506904135 49
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                             0.006615347 0.026706538 0.003270701
74
       0.0014918510
                      0.0014261630
                                     0.0207100000
                                                     0.0043600000
   4.470774185 49
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                             0.026190101 0.052578019 0.008962048
75
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                                                     0.0337900000
       0.0031438780
   3.980779552 49
                     338.15
                             0.073265974 0.082179843 0.016144102
76
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                     0.0101425040
                                    0.2147300000
                                                    0.1438800000
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77
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                                     0.3433500000
                                                     0.2299900000
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79
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80
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81
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82
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                                                    0.0697600000
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                                                    0.2223600000
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                                                        0.053636501
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91
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         0.0016983290
                        0.0109000000
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92
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                                                    0.0141700000
   4.769646356 6 348.15
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       0.0003785790
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                                     0.0763000000
                                                    0.0425100000
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                           0.027835989 \quad 0.019368704 \quad 0.013838528
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                                     0.1079100000
       0.0003751830
                                                    0.0752100000
```

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                                                      0.1111800000
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                            0.058853583 \ 0.02856616
                                                       0.018999795
97
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                                      0.2147300000
                                                      0.1580500000
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                            0.080063623 0.031285096 0.02005575
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                                                      0.2081900000
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                            0.098401549 0.03574572
                                                       0.021491243
99
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                      0.0675194400
                                      0.3215500000
                                                      0.2419800000
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                                                      0.3400800000
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102
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                       0.0000000000
                                      0.0000000000
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103
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                                      0.0372322200
                                                      0.0123802200
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                              0.043611634 0.027905986 0.010699939
104
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                                                      0.1198117100
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                                      0.3057537200
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                                                      0.3822771700
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                                      0.6028288600
                                                      0.5209208100
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                              0.231152006 \quad 0.039631362 \quad 0.022839995
108
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                       0.0137465540
                                      0.7213609100
                                                      0.5739863700
   2.362609886 21
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                              0.317002761 \quad 0.038941214 \quad 0.022911482
109
                                      0.8719389600
                                                      0.5813068100
       0.0017821280
                       0.0104450210
110
   5.06 \quad 49 \quad 348.15
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                                                             0.0000113527
111
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                       0.0000000000
                                      0.0000000000
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112
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                       0.0041540550
                                      0.0425100000
                                                      0.0152600000
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113
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                                      0.1863900000
                                                      0.1318900000
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                              0.117476598 0.077818173 0.028731141
114
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                       0.0167908450
                                      0.5112100000
                                                      0.3607900000
   3.129162546 49
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                              0.210658429 0.095263758 0.035233162
115
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                                      0.7117700000
                                                     0.3564300000
                              0.00000000 \ \ 0.093712041 \ \ 0.042779156
   3.139614905 49
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116
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                                                      0.5755200000
   2.045924558 49
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117
       0.0030540700
                       0.0108002800
                                      1.3875700000
                                                      0.3400800000
118
                       0.000937345 0.001784652 0.000224485 0.0000624397
   4.62
               348.15
          98
119
```

```
0.0000839496
                       0.0043600000
                                       0.0000000000
   4.69620739
                 98
                      348.15
                               0.022051269 0.074199559 0.034610012
120
                       0.0048735330
                                        0.0817500000
                                                        0.0218000000
        0.0036129080
   3.041796127 98
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                               0.172964598 0.146832164 0.084022431
121
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                       0.0110850240
                                        0.3477100000
                                                        0.1689500000
                      348.15
                               0.00000000 \ \ 0.157442729 \ \ 0.103384565
   2.276859458 98
122
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                       0.0117188830
                                        0.6649000000
                                                        0.3597000000
   1.896128731 98
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                               0.482465869 \quad 0.154192835 \quad 0.103471215
123
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                       0.0127843360
                                        0.7848000000
                                                        0.4022100000
   1.704424298 98
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124
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                       0.0129858550
                                        0.9232300000
                                                        0.4294600000
   1.601117644 98
                      348.15
                               0.00000000 \ 0.141684896 \ 0.106773968
125
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                       0.0135823620
                                        1.0801900000
                                                        0.4926800000
                               0.587886570 \quad 0.140393582 \quad 0.114854416
   1.693475041 98
                      348.15
126
       0.0028949970
                       0.0163160820
                                        1.3123600000
                                                        0.6005900000
127
128
129
    ];
130
131
    Output = [
132
133
134
    0.0000000000
135
    0.0005450000
136
   0.0013625000
137
   0.0031142857
138
    0.0026471429
139
   0.0074742857
140
    0.0091871429
141
    0.0060728571
142
143
   0.0000000000
144
   0.0000000000
145
   0.0013015236
146
   0.0016010072
147
   0.0025832045
148
   0.0032331942
149
   0.0039624681
150
    0.0054721360
151
    0.0088938779
152
153
    0.0000000000
154
   0.0000000000
155
```

0.00000000001560.00624595151570.00391942731580.00407199861590.0059992408160 0.0072397679161 1620.00000000001630.00000000001640.0000000000 1650.00624788001660.0048167100167 0.0061966500 168 0.00787634001690.0049998300170171 0.00000000001720.0000000000 1730.00000000001740.00699403661750.00437705001760.00683776491770.00412608001780.0061546622179180 0.00000000001810.0021800000182 0.0054500000183 0.00981000001840.00918714291850.0094985714186 0.0098100000 187 0.0113671429188 189 0.0000000000 190 0.0070850000191 0.0104260870192 0.01635000001930.01526000001940.0145333333195 0.0158050000196 0.0138243902197 198 0.0043600000199

0.0147150000200 0.0275225000201 0.0287033333202 0.0179850000203 0.0107442857204-0.0080971429205206 0.0000000000 2070.01853000002080.0142173913209 0.02656875002100.02217586212110.0152600000212 0.00451951222130.0002658537214215 0.00363333332160.00519047622170.0085878788218 0.01017333332190.0075826087220 0.01240344832210.01115952382220.0125350000223 0.0120678571224 0.01662711862250.0172583333226 227 0.0129744498228 229 0.05480080090.0747910299230 0.05810370772310.04563348042320.0259210434233 0.0014741120234-0.0046728307235236 0.01526000002370.05831500002380.0572250000239 -0.00145333332400.0547725000241-0.0336342857242-0.0003114286243

```
244
    0.0242222222
245
_{246} 0.0700714286
    0.0561029412
247
   0.0250058824
248
_{249} 0.0136250000
    0.0218000000
250
    0.0256928571
251
_{252} 0.0092650000
253
   ];
254
```

## A.3 Example: HEPO machine learning model

```
function [y1] = myNeuralNetworkFunction(x1)
1
2 %MYNEURALNETWORKFUNCTION neural network simulation function.
  %
3
4 % Auto-generated by MATLAB, 21-Apr-2021 09:25:18.
5 %
6 \% [y1] = myNeuralNetworkFunction(x1) takes these arguments:
7 \% x = Qx10 matrix, input #1
8 % and returns:
  \% y = Qx1 matrix, output #1
9
  % where Q is the number of samples.
10
11
  %#ok<∗RPMT0>
12
13
  % = ____ NEURAL NETWORK CONSTANTS =
14
15
16 % Input 1
17 x1 step1.xoffset = [1.601117644;6;328.15;0;0.000112242;0;0;0;0;0];
_{18} x1 step1.gain =
      [0.486534490569793; 0.0217391304347826; 0.1; 3.40201682103403;
  12.7120943825719; 17.4133487388069; 359.766065713431; 29.2977263221159;
19
  1.44136872374006; 3.33005877553739];
20
  x1 step1.ymin = -1;
21
22
23 % Layer 1
_{24} b1 =
      [-0.47872977914236120034; 1.2786511101914832533; -1.4971016117307271998];
25 IW1 1 = [0.94312394416852174395 - 0.11206548441644094416
      0.93660825264448477334 1.1552573135201360532
```

```
0.38025026570939007842 \quad 0.43469722227676665938
       0.0035921397008878458608 - 0.66351598580508719394
       0.64149606969172934257
       -0.69253155682261591242; -0.70454721456875890606
       -0.81997983357239812019 -3.079652332314779084
       -2.9685322158861500164 -1.352191162043323347
       1.8328410582875043211 - 2.2127753394987017543
       -0.38577084088525881445 -1.8441903839229920603
       0.040932223018159220873; 1.185659753415429174
       -0.13202324897596046105 0.83415606577463041749
       1.4506475481156042573 \quad -0.027705190520301407192
       1.5835386691143724658 \quad \text{-}0.64379756074347771477}
       -0.46884830722346726439 0.76142373903767690546
       -2.0915975087964815415;
26
27 % Layer 2
_{28} b2 = -2.084601385894188752;
  LW2 1 = [2.7470944772556880054 \ 1.0168490111870966963]
29
       -3.4723638174334068296;
30
  % Output 1
31
_{32} y1 step1.ymin = -1;
<sup>33</sup> y1 step1.gain = 18.4458766749488;
   y1 step1.xoffset = -0.0336342857;
34
35
   \% = SIMULATION =
36
37
   % Dimensions
38
  Q = size(x1,1); \% samples
39
40
  % Input 1
41
_{42} x1 = x1';
   xp1 = mapminmax apply(x1, x1 step1);
43
44
  % Layer 1
45
   a1 = tansig apply (repmat (b1, 1, Q) + IW1 1*xp1);
46
47
  % Layer 2
48
   a2 = repmat(b2, 1, Q) + LW2_1*a1;
49
50
51 % Output 1
y_1 = mapminmax\_reverse(a2, y1\_step1);
_{53} y1 = y1';
54 end
```

```
55
   \% =
       — MODULE FUNCTIONS —
56
57
  % Map Minimum and Maximum Input Processing Function
58
   function y = mapminmax apply(x, settings)
59
  y = bsxfun(@minus,x,settings.xoffset);
60
   y = bsxfun(@times, y, settings.gain);
61
   y = bsxfun(@plus, y, settings.ymin);
62
   end
63
64
  % Sigmoid Symmetric Transfer Function
65
  function a = tansig apply(n, )
66
   a = 2 ./ (1 + exp(-2*n)) - 1;
67
   end
68
69
  % Map Minimum and Maximum Output Reverse - Processing Function
70
  function x = mapminmax reverse(y, settings)
71
  x = bsxfun(@minus, y, settings.ymin);
72
  x = bsxfun(@rdivide, x, settings.gain);
73
x = bsxfun(@plus, x, settings.xoffset);
   end
75
```

### A.4 Example: Obtaining modelled rates 3-input model

```
clear
1
  clc
2
  close all
3
  \% Experiment #1, A1
4
5
<sup>6</sup> %Inputs [Time [days], O2-concentration [%], Temperature [K]]
7 X1 = [
s 5.560000000 6 328.15
  5.711823131 \ 6 \ 328.15
9
_{10} 5.465229927 6 328.15
11 5.341912612 6 328.15
12 5.052484218 6 328.15
13 4.963055823 6 328.15
14
  4.631034815 6 328.15
   4.712075773 6 328.15
15
16
17
   ];
18
19 %Output: rHEF [kg/kmol]?
```

```
Y1 = [
20
   0
^{21}
   5.4500E-04
22
   1.3625E-03
23
   3.1143E-03
24
   2.6471 \text{E-}03
25
   7.4743E-03
26
   9.1871E-03
27
   6.0729 E - 03
^{28}
29
   ];
30
31
32
   \% Experiment #2, A2-I
33
34
    X2 = [
35
   4.95
                  21
                      328.15
36
   5.020220179 21
37
                       328.15
   4.948427315 21
                      328.15
38
   4.925410918 21
                      328.15
39
   4.830016762 21
                       328.15
40
   4.774658871 21
                      328.15
41
   4.716091961 21
                      328.15
42
   4.576204533 21
                       328.15
43
   4.472071886 21
                      328.15
44
45
46
   ];
47
48
   Y2 = [
49
50
   0
   0
51
   1.3015E-03
52
   1.6010E-03
53
   2.5832E-03
54
   3.2332E-03
55
   3.9625E-03
56
   5.4721E-03
57
   8.8939E-03
58
59
60
61
   ];
62
63
```

```
\% Experiment #3, A2-II
64
65
   X3 = [
66
   4.875
                 21
                      328.15
67
   4.884367008 21
                      328.15
68
   4.784768453 21
                      328.15
69
   4.737944046 21
                      328.15
70
   4.692972306 21
                      328.15
71
   4.626608838 21
                       328.15
72
   4.548468095 21
                      328.15
73
   4.448673133 21
                      328.15
74
75
76
   ];
77
78
   Y3 = [
79
   0
80
81
   0
82
   0
   6.2460 E-03
83
   3.9194E-03
84
   4.0720E-03
85
   5.9992E-03
86
   7.2398E-03
87
88
    ];
89
90
   % Experiment #4, A2-III
91
92
93
   \% Experiment #5, A3
94
95
   X5 = [
96
   4.87
                 49
                      328.15
97
   4.914460858 49
                      328.15
98
   4.632419663 49
                      328.15
99
   4.56647853
                      328.15
                 49
100
   4.539215368 49
                      328.15
101
   4.479785934 49
                      328.15
102
   4.313389169 49
                      328.15
103
   4.263836337 49
                      328.15
104
   ];
105
106
107 Y5 = [
```

```
0
108
    0
109
    0
110
    6.2479 E - 03
111
    4.8167 E-03
112
    6.1967 E-03
113
    7.8763E-03
114
    4.9998E-03
115
116
117
118
119
    ];
120
121
    \% Experiment #6, A4
122
123
    X6 = [
124
    4.817
                   98
125
                        328.15
    4.709764828 98
                        328.15
126
    4.579582871 98
                        328.15
127
    4.55720619
                        328.15
128
                   98
    4.311055911 98
                        328.15
129
    4.167074428 98
                        328.15
130
    3.991948363 98
                        328.15
131
    3.85921283698
                        328.15
132
133
134
    ];
135
136
    Y6 = [
137
138
    0
    0
139
    0
140
    6.9940 E-03
141
    4.3770E-03
142
    6.8378E-03
143
    4.1261E-03
144
    6.1547E-03
145
146
147
    ];
148
149
    \% Experiment #7, B1
150
151
```

```
X7 = [
152
    5.37
                   6 338.15
153
    4.911035228 \ \ 6 \ \ 338.15
154
    4.863074058 \ \ 6 \ \ 338.15
155
    4.716951419 6 338.15
156
    4.974640781 \ 6 \ 338.15
157
    4.690677151 \ 6 \ 338.15
158
    4.446093649 \ 6 \ 338.15
159
    4.492912239 \ 6 \ 338.15
160
161
    ];
162
163
    Y7 = [
164
    0
165
    2.1800E-03
166
    5.4500E-03
167
    9.8100E-03
168
    9.1871E-03
169
    9.4986E-03
170
    9.8100E-03
171
    1.1367E-02
172
173
174
175
    ];
176
177
    % Experiment #8, B2-I
178
179
    \% Experiment #9, B2-II
180
181
182
    X9 = [
    4.775
                   21
                        338.15
183
    4.651566177 21
                        338.15
184
    4.498363888 21
                        338.15
185
    4.334036235 21
                        338.15
186
    4.249692067 21
                        338.15
187
    4.142513473 21
                        338.15
188
    3.955865155 21
                        338.15
189
    3.753967639 21
                        338.15
190
191
192
193
    ];
194
195 Y9 = [
```

```
0
196
    7.0850E-03
197
    1.0426E-02
198
    1.6350E-02
199
    1.5260E-02
200
    1.4533E-02
201
    1.5805E-02
202
    1.3824E-02
203
204
205
    ];
206
207
    % Experiment 10, B3
208
209
   X10 = [
210
    5.26
                   49
                        338.15
211
    4.506904135 49
                        338.15
212
213
    4.470774185 49
                        338.15
214
    3.980779552 49
                        338.15
    3.555425284 49
                        338.15
215
    3.337613545 49
216
                        338.15
    2.651222746 49
                        338.15
217
218
219
    ];
220
221
    Y10 = [
222
    4.3600E-03
223
    1.4715E-02
224
    2.7523E-02
225
226
    2.8703E-02
    1.7985E-02
227
    1.0744\mathrm{E}{\text{-}}02
228
    -8.0971E-03
229
230
231
232
233
234
    ];
235
    \% Experiment #11, B4
236
237
    X11 = [
238
    4.798
                   98
                       338.15
239
```

```
4.405681764 98
                       338.15
240
    3.896320554 98
                       338.15
241
    3.606477896 98
                       338.15
242
    3.373334889 98
                       338.15
243
    3.022642215 98
                       338.15
244
    2.714667974 98
                       338.15
245
    2.387096959 98
                       338.15
246
247
    ];
248
249
    Y11 = [
250
    0
251
    1.8530E-02
252
   1.4217 E-02
253
    2.6569E-02
254
    2.2176E-02
255
    1.5260 E-02
256
    4.5195E-03
257
    2.6585E-04
258
259
    ];
260
261
    \% Experiment #12, C1
262
263
    X12 = [
264
    5.27
                  6 \ 348.15
265
    5.2879338 6 348.15
266
    4.974793126 \ 6 \ 348.15
267
    4.769646356 6 348.15
268
    4.97394122 \quad 6 \quad 348.15
269
270
    4.870772163 \ 6 \ 348.15
    4.526150579 6 348.15
271
    4.238312461 \ 6 \ 348.15
272
    4.069101956 6 348.15
273
    4.139477397 \ 6 \ 348.15
274
    3.968698224 6 348.15
275
276
    ];
277
278
    Y12 = [
279
    3.6333E-03
280
    5.1905E-03
281
    8.5879E-03
282
283 1.0173E-02
```

```
7.5826E-03
284
    1.2403E-02
285
    1.1160E-02
286
    1.2535E-02
287
    1.2068E-02
288
    1.6627E-02
289
    1.7258E-02
290
291
292
    ];
293
294
    \% Experiment #13, C2
295
296
    X13 = [
297
    4.944
                  21
                       348.15
298
    4.690061157 21
                       348.15
299
    4.196898229 21
                       348.15
300
    3.836553249 21
                       348.15
301
    3.499202912 21
                       348.15
302
    3.0930167\ 21\ 348.15
303
    2.824493483 21
                       348.15
304
    2.362609886 21
                       348.15
305
306
307
    ];
308
309
    Y13 = [
310
    1.2974E-02
311
    5.4801E-02
312
   7.4791E-02
313
314
    5.8104E-02
    4.5633E-02
315
    2.5921E-02
316
    1.4741E-03
317
    -4.6728E-03
318
319
320
    ];
321
322
    \% Experiment #14, C3
323
324
    X14 = [
325
    5.06
                  49
                       348.15
326
327 5.428108647 49
                       348.15
```

```
4.165642573 49
                       348.15
328
    3.434605249 49
                       348.15
329
    3.129162546 49
                       348.15
330
    3.139614905 \ 49
                       348.15
331
    2.045924558 49
                       348.15
332
333
334
    ];
335
336
    Y14 = [
337
    1.5260 \text{E-}02
338
    5.8315E-02
339
    5.7225E-02
340
    -1.4533E-03
341
    5.4773E-02
342
    -3.3634E-02
343
    -3.1143E-04
344
345
346
347
348
    ];
349
350
    \% Experiment #15, C4
351
352
   X15 = [
353
    4.62
                  98
                       348.15
354
    4.69620739 98
                       348.15
355
    3.041796127 \ 98
                       348.15
356
    2.276859458 98
                       348.15
357
    1.896128731 98
                       348.15
358
    1.704424298 98
                       348.15
359
    1.60111764498
                       348.15
360
    1.693475041 98
                       348.15
361
362
363
    ];
364
    Y15 = [
365
    2.4222E-02
366
    7.0071E-02
367
    5.6103E-02
368
    2.5006E-02
369
    1.3625E-02
370
371 2.1800E-02
```

2.5693E-023729.2650E-03373374]; 375376Yc = [377378 $HEPO_ML(X1)$ 379 $HEPO_ML(X2)$ 380  $HEPO_ML(X3)$ 381 $HEPO_ML(X5)$ 382383  $HEPO_ML(X6)$  $HEPO_ML(X7)$ 384 $HEPO_ML(X9)$ 385 $HEPO_ML(X10)$ 386  $HEPO_ML(X11)$ 387 $HEPO_ML(X12)$ 388 $HEPO_ML(X13)$ 389  $HEPO_ML(X14)$ 390 $HEPO_ML(X15)$ 391392 393 394];

1	A1 = [
2	
3	0
4	1
5	3
6	7
7	14
8	21
9	28
10	35
11	%42
12	
13	];
14	
15	A2I = [
16	
17	0.00
18	0.03
19	1.03
20	3.12
21	5.03
22	6.97
23	9.87
24	12.92
25	16.88
26	%21.03
27	1.
28	];
29	A2II = [
30 31	
32	0
33	1.1181
34	2.9653
35	4.9375
36	6.9444
37	9.9479
38	12.8924
39	17.1076
40	%20.9167
41	

# A.5 Example: Oxidative degradation time measurements

42	
43	];
44	
45	A3 = [
46	
47	0
48	1
49	3
50	4
51	7
52	10
53	14
54	17
55	%21
56	
57	];
58	
59	A4 = [
60	
61	0
62	1.0278
63	2.9757
64	4.0174
65	7.5104
66	9.9653
67	13.9722
68	17.2778
69	%21.1944
70	
71	];
72	
73	B1 = [
74	
75	
76	
77	
78	
	14
	21
	28
	35
83	%42
84	
85	];

86	
87	B2II = [
88	
89	0
	1
91	3
92	5.3
93	6.9
94	9.9
95	12.9
96	16.9
90 97	%21
	/021
98	
99	1.
100	];
101 102	B3 = [
103 104	0
	1
106	3
107	7
108	10
109	14
110	21 %28
111	/028
112	1.
113	];
114	
	B4 = [
$116 \\ 117$	0
117	0.9
	2.9
	5.2
	6.8
122	9.7
	12.7
124	16.8
	%20.9
126	
127	];
128	1 /
	C1 = [
••	i.

130	
131	0
132	0.9
133	3
134	6.3
135	7.8
136	10.1
137	13
138	17.2
139	21.2
140	24
141	29.9
142	%35.9
143	
144	];
145	
146	C2 = [
147	
148	0
149	0.9542
150	2.9146
151	4.909
152	6.859
153	9.8972
154	11.9444
155	16.9104
156	%19.909
157	
158	
159	];
160	
161	C3 = [
162	
163	0
	1
165	3
	7
167	10
	14
169	21
	%28
171	
172	];
173	

### A.6 Example: Plotting 3-input model

```
clear
 1
   clc
^{2}
   close all
3
   TIME
4
\mathbf{5}
6
   A1HEPO = [
7
   0.0000000000
                    0.0000000000
8
   0.0000000000
                    0.0004716359
9
   0.0010900000
                    0.0014149078
10
   0.0065400000
                    0.0033014516
11
   0.0283400000
                    0.0066029031
12
   0.0468700000
                    0.0099043547
13
   0.0991900000
                    0.0132058063
14
   0.1635000000
                    0.0165072579
15
16
17
   ];
^{18}
19
   A2IHEPO = [
^{20}
^{21}
   0.0000000000
                    0.0000000000
22
   0.0000000000
                    0.0000813013
^{23}
   0.0000000000
                    0.0031608962
^{24}
   0.0027250000
                    0.0096086439
25
   0.0057770000
                    0.0154792755
26
```

```
0.0107910000
                   0.0214567691
27
   0.0201650000
                   0.0303854385
^{28}
   0.0322640000
                   0.0397886734
29
   0.0539550000
                   0.0519958794
30
31
32
33
^{34}
   ];
35
36
   A2IIHEPO = [
37
38
   0.0000000000
                   0.0000000000
39
   0.0000000000
                   0.0047597572
40
   0.0000000000
                   0.0126232967
^{41}
   0.0000000000
                   0.0210189618
42
   0.0125350000
                   0.0295623449
43
   0.0243070000
                   0.0423482592
44
   0.0362970000
                   0.0548830102
45
   0.0615850000
                   0.0728271373
46
47
48
   ];
49
50
   A3HEPO = [
51
52
   0.0000000000
                   0.0000000000
53
   0.0000000000
                   0.0046974149
54
   0.0000000000
                   0.0140922447
55
   0.0000000000
                   0.0187896597
56
   0.0187436400
                   0.0328819044
57
   0.0331937700
                   0.0469741491
58
   0.0579803700
                   0.0657638088
59
   0.0816093900
                   0.0798560536
60
61
   ];
62
63
   A4HEPO = [
64
65
   0.0000000000
                   0.0000000000
66
   0.0000000000
                   0.0051775459
67
   0.0000000000
                   0.0149900986
68
   0.0000000000
                   0.0202376658
69
   0.0244301700
                   0.0378336648
70
```

```
0.0351753900
                    0.0502002317
71
   0.0625736300
                    0.0703850037
72
   0.0762128000
                    0.0870369746
73
74
75
    ];
76
77
   B1HEPO = [
78
79
   0.0000000000
                    0.0000000000
80
   0.0000000000
                    0.0073584875
81
   0.0043600000
                    0.0220754625
82
   0.0261600000
                    0.0515094126
83
   0.0948300000
                    0.1030188252
84
   0.1591400000
                    0.1545282378
85
   0.2256300000
                    0.2060376504
86
   0.2943000000
                    0.2575470631
87
88
89
90
91
    ];
92
93
   B2IIHEPO = [
94
95
   0.0000000000
                    0.0000000000
96
   0.0000000000
                    0.0132478325
97
   0.0141700000
                    0.0397434975
98
   0.0381500000
                    0.0702135123
99
   0.0643100000
                    0.0914100443
100
   0.1100900000
                    0.1311535418
101
   0.1536900000
                    0.1708970393
102
   0.2169100000
                    0.2238883693
103
104
105
106
    ];
107
108
   B3HEPO = [
109
110
   0.0000000000
                    0.0000000000
111
   0.0043600000
                    0.0103306534
112
   0.0337900000
                    0.0309919601
113
   0.1438800000
                    0.0723145737
114
```

```
0.2299900000
                    0.1033065338
115
    0.3019300000
                    0.1446291473
116
    0.3771400000
                    0.2169437210
117
118
    ];
119
120
    B4HEPO = [
121
122
    0.0000000000
                    0.0000000000
123
    0.0000000000
                    0.0129557024
124
    0.0370600000
                    0.0417461523
125
    0.0697600000
                    0.0748551697
126
    0.1122700000
                    0.0978875296
127
    0.1765800000
                    0.1396336819
128
    0.2223600000
                    0.1828193567
129
    0.2408900000
                    0.2418397789
130
131
132
133
134
    ];
135
136
    C1HEPO = [
137
138
    0.0000000000
                    0.0000000000
139
    0.0032700000
                    0.0188858549
140
    0.0141700000
                    0.0629528497
141
    0.0425100000
                    0.1322009844
142
    0.0577700000
                    0.1636774092
143
    0.0752100000
                    0.2119412606
144
    0.1111800000
                    0.2727956820
145
    0.1580500000
                    0.3609296716
146
    0.2081900000
                    0.4448668045
147
    0.2419800000
                    0.5036227976
148
                    0.6274300686
    0.3400800000
149
150
151
152
153
    ;
154
    C2HEPO = [
155
156
    0.0000000000
                    0.0000000000
157
    0.0123802200
                    0.0183351820
158
```

```
0.1198117100
                     0.0560047385
159
    0.2689749400
                     0.0943276131
160
    0.3822771700
                      0.1317973310
161
    0.5209208100
                     0.1901770732
162
    0.5739863700
                     0.2295145125
163
    0.5813068100
                      0.3249373942
164
165
166
    ];
167
168
    C3HEPO = [
169
    0.0000000000
                     0.0000000000
170
    0.0152600000
                     0.0264356179
171
    0.1318900000
                     0.0793068538
172
    0.3607900000
                      0.1850493256
173
    0.3564300000
                     0.2643561794
174
    0.5755200000
                     0.3700986512
175
    0.3400800000
                      0.5551479767
176
177
178
    ];
179
180
    C4HEPO = [
181
182
    0.0000000000
                      0.0000000000
183
    0.0218000000
                     0.0309656578
184
    0.1689500000
                     0.1032188594
185
    0.3597000000
                     0.2202002334
186
    0.4022100000
                     0.2786909204
187
    0.4294600000
                     0.3475034933
188
    0.4926800000
                      0.4472817241
189
    0.6005900000
                     0.5917881273
190
191
192
    ];
193
194
    a = figure();
195
196
    subplot(2,3,1)
197
    hold on
198
    \operatorname{plot}(A1, A1 \operatorname{HEPO}(:, 1), '*')
199
    \operatorname{plot}(A1, A1 \operatorname{HEPO}(:, 2), '-')
200
    xlabel('Time [days]')
201
    ylabel('C_{HEPO} [kmol/kg]')
202
```

```
legend({ 'C_{HEPO, exp}}', 'C_{HEPO, mod}' }, 'Location', 'southeast')
203
    title ('A1, 55 \land circC, 6 % O 2, HEPO')
204
205
    subplot(2,3,2)
206
    hold on
207
    plot(A2I, A2IHEPO(:,1), '*')
208
    plot(A2I, A2IHEPO(:, 2), '-')
209
    xlabel('Time [days]')
210
    ylabel('C {HEPO} [kmol/kg]')
211
    legend({ 'C_{HEPO, exp}}', 'C_{HEPO, mod}' }, 'Location', 'southeast')
212
    title ('A2-I, 55 \ circC, 21 % O 2, HEPO')
213
214
    subplot (2,3,3)
215
   hold on
216
    plot(A2II, A2IIHEPO(:,1), '*')
217
    plot(A2II, A2IIHEPO(:,2), '-')
218
    xlabel('Time [days]')
219
    ylabel('C {HEPO} [kmol/kg]')
220
    legend({ 'C_{HEPO, exp} ', 'C_{HEPO, mod} '}, 'Location', 'southeast')
221
    title ('A2-II, 55 \circC, 21 % O 2, HEPO')
222
223
    subplot(2,3,4)
224
    hold on
225
    plot(A3, A3HEPO(:, 1), '*')
226
    plot(A3, A3HEPO(:, 2), '-')
227
    xlabel('Time [days]')
228
    ylabel('C {HEPO} [kmol/kg]')
229
    legend({ 'C_{HEPO, exp} ', 'C_{HEPO, mod} '}, 'Location', 'southeast')
230
    title ('A3, 55 \circC, 49 % O 2, HEPO')
231
232
    subplot(2,3,5)
233
   hold on
234
    plot(A4, A4HEPO(:,1), '*')
235
    \operatorname{plot}(A4, A4\operatorname{HEPO}(:, 2), '-')
236
    xlabel('Time [days]')
237
    ylabel('C {HEPO} [kmol/kg]')
238
    legend({ 'C {HEPO, exp} ', 'C {HEPO, mod} '}, 'Location', 'southeast')
239
    title ('A4, 55 \circC, 98 % O 2, HEPO')
240
241
    b = figure();
242
243
244
    subplot(2,2,1)
245
   hold on
246
```

```
plot (B1, B1HEPO(:,1), '*')
247
    plot(B1, B1HEPO(:, 2), '-')
248
    xlabel('Time [days]')
249
    ylabel('C_{HEPO} [kmol/kg]')
250
    legend({ 'C {HEPO, exp} ', 'C {HEPO, mod} '}, 'Location', 'southeast')
251
    title ('B1, 65 \circC, 6 % O 2, HEPO')
252
253
    subplot(2,2,2)
254
    hold on
255
    plot(B2II, B2IIHEPO(:,1), '*')
256
    plot (B2II, B2IIHEPO(:,2), '-')
257
    xlabel('Time [days]')
258
    ylabel('C_{HEPO} [kmol/kg]')
259
    legend({ 'C_{HEPO, exp}}', 'C_{HEPO, mod}' }, 'Location', 'southeast')
260
    title ('B2-II, 65 \circC, 21 % O 2, HEPO')
261
262
    subplot(2,2,3)
263
    hold on
264
    plot(B3, B3HEPO(:, 1), '*')
265
    plot(B3, B3HEPO(:, 2), '-')
266
    xlabel('Time [days]')
267
    ylabel('C {HEPO} [kmol/kg]')
268
    legend({ 'C_{HEPO, exp}}', 'C_{HEPO, mod}' }, 'Location', 'southeast')
269
    title ('B3, 65 \circC, 49 % O 2, HEPO')
270
271
   subplot(2,2,4)
272
    hold on
273
    plot(B4, B4HEPO(:,1), '*')
274
    plot(B4, B4HEPO(:, 2), '-')
275
    xlabel('Time [days]')
276
    ylabel('C_{HEPO} [kmol/kg]')
277
    legend({ 'C {HEPO, exp} ', 'C {HEPO, mod} '}, 'Location', 'southeast')
278
    title('B4, 65 \circC, 98 % O 2, HEPO')
279
280
    c = figure();
281
282
283
    subplot (2,2,1)
284
   hold on
285
    plot(C1, C1HEPO(:, 1), '*')
286
    \operatorname{plot}(C1, C1 \to C1 \to C(:, 2), '-')
287
   xlabel('Time [days]')
288
    ylabel('C_{HEPO} [kmol/kg]')
289
290 legend({ 'C_{HEPO, exp}}', 'C_{HEPO, mod}' }, 'Location', 'southeast')
```

```
title('C1, 75 \circC, 6 % O_2, HEPO')
291
292
    subplot (2,2,2)
293
    hold on
294
    \operatorname{plot}(C2, C2HEPO(:, 1), '*')
295
    plot(C2, C2HEPO(:, 2), '-')
296
    xlabel('Time [days]')
297
    ylabel('C {HEPO} [kmol/kg]')
298
    legend({ 'C_{HEPO, exp}}', 'C_{HEPO, mod}' }, 'Location', 'southeast')
299
    title ('C2, 75 \ circC, 21 % O_2, HEPO')
300
301
    subplot (2,2,3)
302
    hold on
303
    \operatorname{plot}(C3, C3HEPO(:, 1), '*')
304
    plot(C3, C3HEPO(:, 2), '-')
305
    xlabel('Time [days]')
306
    ylabel('C {HEPO} [kmol/kg]')
307
    legend({ 'C {HEPO, exp} ', 'C {HEPO, mod} '}, 'Location', 'southeast')
308
    title ('C3, 75 \ \ CircC, 49 % O_2, HEPO')
309
310
    subplot(2,2,4)
311
    hold on
312
    plot(C4, C4HEPO(:,1), '*')
313
    plot(C4, C4HEPO(:, 2), '-')
314
    xlabel('Time [days]')
315
_{316} ylabel ('C_{HEPO} [kmol/kg]')
s17 legend({ 'C {HEPO, exp} ', 'C {HEPO, mod} '}, 'Location', 'southeast')
318 title ('C4, 65 \circC, 98 % O_2, HEPO')
```

# **B** MATLAB code thermal degradation

```
clear
1
   clc
2
   close all
3
4
5 DOT = [
\mathbf{6}
   393 6.58
                0.2
\overline{7}
   %393 6.12 0.2
8
   393 6.33
                0.2
9
   \%393 5.86 0.2
10
   393 6.24
                0.2
11
^{12}
13 393 6.58
                0.4
   393 6.22
                0.4
14
   393 \ 5.9 \ 0.4
15
   393 5.58
                0.4
16
   393 5.14
                0.4
17
^{18}
   393 6.58
               0.5
19
   393 6.19
                0.5
20
   \%393 5.76 0.5
^{21}
   393 \ 6.1 \ 0.5
22
   393 \ 4.18 \ 0.5
23
24
   \%393 \quad 4.9 \quad 0.2
25
   393 5.11
26
                0.2
   \%393 4.57 0.2
27
   393 \ 4.6 \ 0.2
^{28}
   \%393 4.39 0.2
29
30
   393 \ 4.9 \ 0.4
31
   393 \ 4.82 \ 0.4
32
   393 \ 4.5 \ 0.4
33
   \%393 4.25 0.4
34
35
   393 \ 4.9 \ 0.5
36
   393 \ 4.6 \ 0.5
37
   393 \ 4.22 \ 0.5
38
39 393 4 0.5
```

```
393 \ 3.68 \ 0.5
40
^{41}
   \%393 2.88 0.2
42
   393 3.24
               0.2
43
   393 \ 2.72
               0.2
44
   393 2.63
               0.2
45
   \%393 2.59 0.2
46
47
   \%393 2.88 0.4
^{48}
   393 3.17
               0.4
49
   393 2.66
               0.4
50
   393 2.58
               0.4
51
   %393 2.48 0.4
52
53
   \%393 2.88 0.5
54
   393 \ 3.22
               0.5
55
   393 2.69
               0.5
56
   393 2.33
               0.5
57
   \%393 2.31 0.5
58
59
   408 6.58
               0.2
60
   408 6.42
               0.2
61
   408 5.92
               0.2
62
   408 5.61
               0.2
63
   408 5.18
               0.2
64
65
   408 6.58
               0.4
66
   408 5.8 0.4
67
   408 4.43
               0.4
68
   408 4.26
               0.4
69
   408 3.27
70
               0.4
71
   408 6.58
               0.5
72
   408 \ 5 \ 0.5
73
   408 4.09
               0.5
74
   408 2.95
               0.5
75
   408 2.48
               0.5
76
77
   408 \ 4.9 \ 0.2
78
   408 4.41
               0.2
79
   408 4.27
               0.2
80
81
   408 4.31
               0.4
82
   408 \ 4.28
               0.4
83
```

84	408 3	3.42	0.4			
85						
86	408 4	4.9	0.5			
87	408 4	4.05	0.5			
88	408 3	3.46	0.5			
89	408 2	2.69	0.5			
90	408 2	2.42	0.5			
91						
92	408 2	2.88	0.2			
93	408 2	2.79	0.2			
94	408 2	2.71	0.2			
95	408 2	2.58	0.2			
96	408 2	2.54	0.2			
97						
98						
99	408 2	2.88	0.4			
100	408 2	2.72	0.4			
101	408 2	2.43	0.4			
102	408 2	2.24	0.4			
103						
104	408 2	2.88	0.5			
105	%408	2.54	0.5			
106	408 3	3.09	0.5			
107	408 2	2.01	0.5			
108	408 1	1.93	0.5			
109						
110						
111						
112	];					
113						
114	rMEA	= [				
115						
116	-0.065714286					
117	%0.03					
118	-0.033571429					
119	% 0.027142857					
120	-0.03	28571	43			
121						
122						
123		14285				
124	-0.045714286					
125		28571	-			
126		14285				
127	-0.01	92857	14			

128 129-0.055714286130-0.061428571131% 0.024285714132-0.137142857133 -0.016428571134135136137%0.03-0.077142857138139% 0.002142857-0.015140 % 0.000714286141142143-0.011428571144-0.045714286145-0.008928571146%0.004285714147148149-0.042857143150-0.054285714151-0.015714286152-0.022857143153-0.012857143154155156157%0.051428571-0.074285714158-0.006428571159-0.002857143160% 0.002142857161 162163% 0.041428571164-0.072857143165-0.005714286166-0.007142857167 %0.025168169170 171 %0.048571429

-0.075714286172-0.025714286173-0.001428571174% 0.005714286175176-0.022857143177-0.071428571178-0.022142857179-0.030714286180 -0.034285714181 182183 -0.111428571184 -0.195714286185-0.012142857186-0.070714286187 -0.037142857188189 190 -0.225714286191-0.13 192-0.081428571193 -0.033571429194-0.045195196 197-0.074285714198 -0.01199 -0.0275200201 202 -0.004285714203-0.061428571204-0.0375205206 207-0.121428571208 -0.084285714209-0.055210-0.019285714211-0.049285714212213214-0.012857143215

```
-0.011428571
216
    -0.009285714
217
    -0.002857143
218
    -0.015714286
219
220
221
    -0.022857143
222
    -0.041428571
223
    -0.013571429
224
    -0.078214286
225
226
227
    -0.048571429
228
    \% 0.078571429
229
    -0.077142857
230
    -0.005714286
231
    -0.031428571
232
233
234
    ];
235
```

## B.2 Example: MEA 6 input model data file with all inputs and outputs

```
clear
1
   clc
2
   close all
3
\mathbf{4}
   Input = [
\mathbf{5}
6
   393 \ 6.58
               0.2 \ 6.58
                          NaN 0
                                         0
7
               0.2 6.12
   393 6.12
                          NaN 0.03
                                       0
8
   393 6.33
               0.2 6.33
                          NaN 0.07
                                       0
9
                          NaN 0.13
   393 5.86
               0.2 5.86
                                       0
10
               0.2 \ 6.24
   393 \ 6.24
                          NaN 0.09
11
                                       0.01
                0.2 5.78 NaN 0.15
   %393
         5.78
                                         0.01
12
^{13}
               0.4 \ 6.58
                          NaN 0
                                          0
14
   393 \ 6.58
   393 6.22
               0.4 6.22
                          NaN 0.02
                                       0.01
15
   393 5.9
                0.4 \ 5.9
                                NaN 0.09 0.01
16
   393 \ 5.58
               0.4 \ 5.58
                          NaN 0.11
                                       0.02
17
               0.4 \ 5.14
                           NaN 0.33
   393 5.14
                                       0.03
18
  %393 4.87 0.4 4.87 NaN 0.41
                                         0.05
19
```

```
20
   393 6.58
               0.5 \ 6.58
                          NaN NaN
                                          0
^{21}
   393 6.19
                           NaN NaN
                                          0
               0.5 \ 6.19
22
   393 5.76
               0.5 \ 5.76
                           NaN NaN
                                          0.02
23
   393 6.1
                 0.5 \ 6.1
                                NaN NaN
                                          0.02
^{24}
   393 4.18
               0.5 4.18
                          NaN NaN
                                          0.06
25
   %393 3.95 0.5 3.95 NaN NaN
                                           0.09
26
27
   393 \ 4.9
                  0.2 \ 4.9
                                          0
                                                   0
                                0
^{28}
   393 5.11
               0.2 \ 5.11
                           0
                                     0.02
                                            0
29
   393 \ 4.57
               0.2 4.57
                           0
                                     0.05
                                            0
30
   393 \ 4.6
                 0.2 \ 4.6
                                0
                                          0.09
                                                 0
^{31}
   393 4.39
               0.2 4.39
                           0.04
                                   0.1
                                            0
32
   %393 4.4
                    0.2 \ 4.4
                                   0.08
                                          0.13
                                                0
33
34
   393 4.9
                  0.4 4.9
                                0
                                          0
                                                   0
35
   393 \ 4.82
               0.4 4.82
                           0.04 0.03
                                          0
36
                                0.05 0.05
   393 4.5
                  0.4 \ 4.5
                                              0
37
   393 4.25
               0.4 4.25
                           0.1
                                     0.21
                                            0.02
38
   \%393 4.31 0.4 4.31 0.12
                                   0.35 \quad 0.03
39
40
   393 4.9
                 0.5 \ 4.9
                                0
                                          0
                                                   0
41
   393 4.6
                  0.5 \ 4.6
                                0.05
                                        0.03
                                              0
42
   393 4.22
               0.5 \ 4.22
                           0.08
                                  0.07
                                          0
43
   393 4
                  0.5 4
                                0.09
                                        0.16
                                              0.02
44
   393 3.68
               0.5 \ 3.68
                           0.12
                                   0.22
                                          0.04
45
                                          0.3
   \%393 \quad 3.5
                    0.5 \ 3.5
                                   0.12
                                                    0.06
46
47
   393 2.88
               0.2 2.88
                                     0
                                               0
                           0
48
   393 \ 3.24
               0.2 3.24
                           0
                                     0.02
                                            0
49
   393 2.72
               0.2 2.72
                           0
                                     0.03
                                            0
50
   393 2.63
               0.2 2.63
                           0
                                     0.04
                                            0
51
   393 2.59
               0.2 \ 2.59
                           0
                                     0.06
                                            0
52
   %393 2.62
                0.2 2.62
                              0.17
                                     0.03
                                            0
53
54
   393 2.88
               0.4 2.88
                                               0
                           0
                                     0
55
   393 3.17
               0.4 3.17
                           0
                                     0.02
                                            0
56
   393 2.66
               0.4 2.66
                           0
                                     0.04
                                            0
57
   393 \ 2.58
                                     0.02
               0.4 \ 2.58
                           0
                                            0
58
   393 2.48
               0.4 2.48
                                   0.11 0
                           0.09
59
   \%393 2.83 0.4 2.83
                                     0.2
                                               0.02
                              0.07
60
61
                                               0
   393 2.88
               0.5 2.88
                           0
                                     0
62
   393 \ 3.22
               0.5 \ 3.22
                           0
                                     0.03 0
63
```

```
0.05 0
    393 2.69
               0.5 \ 2.69
                           0
64
    393 2.33
                0.5 \ 2.33
                            0.07
                                   0.07 0
65
    393 2.31
                0.5 \ 2.31
                            0.12
                                   0.12
                                         0
66
    %393 2.39 0.5 2.39 0.12
                                    0.17 \quad 0
67
68
    408 6.58
                0.2 \ 6.58
                           0
                                     0
                                              0
69
    408 6.42
                0.2 \ 6.42
                            0.04
                                   0.11
                                        0
70
    408 5.92
                0.2 5.92
                            0.1
                                     0.22 0
71
    408 5.61
                0.2 \ 5.61
                            0.2
                                     0.22
                                            0
72
    408 5.18
                0.2 5.18
                            0.22
                                   0.22
                                          0.02
73
    %408 4.7
                    0.2 \ 4.7
                                   0.26
                                          0.28
                                                 0.05
74
75
    408 6.58
                0.4 \ 6.58
                           0
                                     0
                                              0
76
    408 5.8
                0.4 \ 5.8
                                0.15 0.14
                                              0
77
    408 4.43
                0.4 \ 4.43
                           0.2
                                     0.36
                                            0.03
78
    408 4.26
                0.4 4.26
                            0.19 NaN
                                            0.11
79
    408 3.27
                0.4 \ 3.27
                            0.18
                                     0.47
                                            0.14
80
    %408 2.75 0.4 2.75 0.16
                                    NaN
                                             0.25
81
82
    408 \ 6.58
                0.5 \ 6.58
                           0
                                     0 0
83
    408 5
                  0.5 \ 5
                                0.16 NaN 0.02
84
    408 4.09
                0.5 \ 4.09
                           0.17 NaN 0.07
85
                            0.13 NaN 0.19
    408 \ 2.95
                0.5 \ 2.95
86
    408 2.48
                0.5 \ 2.48
                            0.12 NaN 0.22
87
    %408 1.85 0.5 1.85 0.09 NaN 0.3
88
89
                                                   0
    408 4.9
                  0.2 4.9
                                0
                                          0
90
    408 4.38
                0.2 \ 4.38
                            0.04
                                   0.02
                                          0
91
    408 4.41
                0.2 4.41
                            0.11
                                          0
                                   0.05
92
    408 4.27
                0.2 4.27
                            0.16
                                   0.11
                                          0
93
    \%408 \quad 3.5
                    0.2 \ 3.5
                                   0.18
                                          0.19
                                                 0.03
94
95
    408 4.9
                  0.4 \ 4.9
                                                   0
                               0
                                          0
96
    408 4.31
                0.4 \ 4.31
                            0.1
                                     0.1
                                              0
97
    408 4.28
                0.4 \ 4.28
                            0.13
                                   0.26
                                          0.02
98
    408 3.42
                0.4 \ 3.42
                            0.15
                                   0.39
                                          0.06
99
                 0.4 \ 2.37 \ 0.13
    \%408 	2.37
                                    0.61 0.13
100
101
                                          0
    408 \ 4.9
                  0.5 \ 4.9
                              0
                                                   0
102
    408 4.05
                0.5 \ 4.05
                           0.11
                                   0.15
                                          0
103
    408 3.46
                0.5 \ 3.46
                            0.12
                                   0.32
                                          0.04
104
    408 2.69
                0.5 \ 2.69
                            0.09
                                   0.49
                                          0.1
105
    408 2.42
                0.5 \ 2.42
                            0.09
                                   0.45
                                          0.17
106
   \%408 1.73 0.5 1.73 0.08 0.5
                                              0.19
107
```

```
108
    408 2.88
                0.2 2.88
                            0
                                      0
                                               0
109
    408 2.79
                0.2 2.79
                            0
                                      0.06 0
110
    408 2.71
                0.2 \ 2.71
                            0
                                      0.1
                                               0
111
    408 2.58
                0.2 \ 2.58
                            0.08
                                   0.06 0
112
    408 \ 2.54
                0.2 \ 2.54
                            0.04
                                   0.09
                                         0
113
    %408 2.32 0.2 2.32 0.06
                                     0.12 0.02
114
115
    408 2.88
                0.4 \ 2.88
                            0
                                      0
                                               0
116
                0.4 \ 2.72
    408 2.72
                            0
                                      0.03
                                             0
117
    408 2.43
                0.4 \ 2.43
                            0.02
                                   0.15
                                          0
118
    408 \ 2.24
                0.4 \ 2.24
                            0.08
                                   0.21
                                         0.02
119
    %408 0.05 0.4 0.05 0
                                        0.36 0
120
121
    408 2.88
                0.5 2.88
                            0
                                      0
                                               0
122
    408 2.54
                0.5 \ 2.54
                            0.03
                                   0.09
                                          0
123
    408 \ 3.09
                0.5 \ 3.09
                            0.06
                                   0.32
                                          0.02
124
    408 2.01
                0.5 \ 2.01
                            0.04
                                   0.31
                                           0.03
125
    408 1.93
                0.5 \ 1.93
                            0.03
                                   0.38
                                          0.05
126
    \%408 1.49 0.5 1.49 0.05 0.37 0.07
127
128
    ];
129
130
    Output MEA = [
131
132
    -0.065714286
133
    0.03
134
    -0.033571429
135
    0.027142857
136
    -0.032857143
137
138
139
    -0.051428571
140
    -0.045714286
141
    -0.022857143
142
    -0.031428571
143
    -0.019285714
144
145
146
    -0.055714286
147
    -0.061428571
148
    0.024285714
149
    -0.137142857
150
    -0.016428571
151
```

1521530.03154-0.0771428571550.002142857156-0.0151570.000714286158159160-0.011428571161 -0.045714286162163 -0.0089285710.004285714164165166-0.042857143167 -0.054285714168-0.015714286169 -0.022857143170-0.0128571431711721730.051428571174-0.074285714175-0.006428571176-0.0028571431770.002142857178179180181 0.041428571-0.072857143182 -0.005714286183-0.0071428571840.0251851861870.048571429188 -0.075714286189-0.025714286190-0.001428571191 0.005714286192193 194-0.022857143195

-0.071428571196-0.022142857197-0.030714286198-0.034285714199 200201-0.111428571202 -0.195714286203-0.012142857204-0.070714286205-0.037142857206207 208 -0.225714286209-0.13 210-0.081428571211-0.033571429212-0.045 213214215216-0.0742857140.004285714217-0.01 218-0.0275219220 221-0.084285714222-0.004285714223 -0.061428571224-0.0375225226 227 -0.121428571228-0.084285714229 -0.055 230 -0.019285714231-0.049285714232 233 234-0.012857143235-0.011428571236 -0.009285714237-0.002857143238 -0.015714286239

240241-0.022857143242-0.041428571243-0.013571429244-0.078214286245246247-0.0485714292480.078571429249-0.077142857250-0.005714286251-0.031428571252253254255]; 256257258 $Output\_HEEDA = [$ 259260NaN 261NaN 262NaN 263264NaN NaN 265266NaN 267NaN 268NaN 269270NaN NaN 271272NaN 273NaN 274NaN 275NaN 276NaN 2772780 2790 2800 2810.002857143282  $_{283}$  0.002857143

```
0.005714286
372
    0.004285714
373
    -0.002857143
374
    0.004285714
375
376
    0.002857143
377
    0.01
378
    0.001428571
379
    0.015714286
380
    0.005714286
381
382
383
   NaN
    NaN
384
   NaN
385
    NaN
386
    NaN
387
388
    0.002857143
389
    0.004285714
390
    0.002857143
391
    0.000714286
392
    0.002142857
393
394
    0.004285714
395
    0.002857143
396
    0.005714286
397
    0.01
398
399
    0.004285714
400
    0.005714286
401
    0.006428571
402
    0.004285714
403
    0.005714286
404
405
    0.002857143
406
    0.001428571
407
    0.000714286
408
    0.001428571
409
    -0.002142857
410
411
    0.002857143
412
    0.002857143
413
    -0.001428571
414
415 0.006428571
```

416	0.006428571
417	
418	0.004285714
419	0.002857143
420	0.001428571
421	0.003571429
422	0.003571429
423	
424	0.015714286
425	0.015714286
426	0
427	0
428	0.004285714
429	
430	0.02
431	0.031428571
432	NaN
433	NaN
434	NaN
435	
436	NaN
437	NaN
438	NaN
439	NaN
440	NaN
441	
442	0.002857143
443	0.004285714
444	0.004285714
445	0.002857143
446	
447	0.014285714
448	0.022857143
449	0.009285714
450	0.007857143
451	
452	0.021428571
453	0.024285714
454	0.012142857
455	-0.002857143
456	0.003571429
457	0.000
458	0.008571429
459	0.005714286

```
-0.002857143
460
    0.002142857
461
    0.002142857
462
463
    0.004285714
464
    0.017142857
465
    0.004285714
466
    0.005357143
467
468
    0.012857143
469
    0.032857143
470
471
    -0.000714286
    0.005
472
    -0.000714286
473
474
475
    ];
476
477
    Output_TriHEIA = [
478
479
480
    0
    0
481
    0
482
    0.000714286
483
    0
484
485
    0.001428571
486
    0
487
    0.000714286
488
    0.000714286
489
    0.001428571
490
491
492
    0
    0.002857143
493
    0
494
    0.002857143
495
    0.002142857
496
497
    0
498
    0
499
    0
500
    0
501
    0
502
503
```

## B.3 Example: MEA machine learning model

```
1 function [y1] = myNeuralNetworkFunction(x1)
2 %MYNEURALNETWORKFUNCTION neural network simulation function.
3 %
4 % Auto-generated by MATLAB, 14-Apr-2021 13:37:58.
5 %
6 \% [y1] = myNeuralNetworkFunction(x1) takes these arguments:
7 \% x = Qx3 matrix, input #1
8 % and returns:
9 % y = Qx1 matrix, output #1
10 % where Q is the number of samples.
11
12 %#ok<*RPMT0>
13
14 % ==== NEURAL NETWORK CONSTANTS ====
15
16 % Input 1
17 x1\_step1.xoffset = [393; 1.93; 0.2];
_{18} x1 step1.gain =
       [0.13333333333333333; 0.43010752688172; 6.666666666666666];
  x1 step1.ymin = -1;
19
20
21 % Layer 1
_{22} b1 =
       [-1.5746388810380491652; 0.021319806190481817992; -0.020786658904295585854];
23 IW1 1 = [0.51181388799705329617 \ 0.88690316085691345283
      0.72902402194927262702; 0.12431852575192366139\\
       -0.032181772504924176237
      0.13507381922287772791; -0.1237962766908106832
      0.032913040483900299349 - 0.1346362178511378016;
24
25 % Layer 2
{}_{26} \quad b2 \; = \; -0.30807497583435677901;
  LW2 1 = \begin{bmatrix} -1.1547236028974714461 & 0.21763249586769245481 \end{bmatrix}
27
      -0.21695040679872487632;
28
29 % Output 1
_{30} y1 step1.ymin = -1;
y1_step1.gain = 8.91719742383058;
_{32} y1 step1.xoffset = -0.225714286;
33
```

```
= SIMULATION =
   \% =
34
35
  % Dimensions
36
  Q = size(x1,1); \% samples
37
38
  % Input 1
39
   x1 = x1';
40
   xp1 = mapminmax apply(x1, x1 step1);
41
42
   % Layer 1
43
   a1 = tansig_apply(repmat(b1, 1, Q) + IW1_1*xp1);
44
45
   \% Layer 2
46
   a2 = repmat(b2, 1, Q) + LW2_{1*a1};
47
48
  % Output 1
49
   y1 = mapminmax_reverse(a2, y1_step1);
50
   y1 = y1';
51
   end
52
53
   % — MODULE FUNCTIONS —
54
55
  % Map Minimum and Maximum Input Processing Function
56
   function y = mapminmax apply(x, settings)
57
   y = bsxfun(@minus,x,settings.xoffset);
58
   y = bsxfun(@times, y, settings.gain);
59
   y = bsxfun(@plus,y,settings.ymin);
60
   end
61
62
  % Sigmoid Symmetric Transfer Function
63
   function a = tansig_apply(n, )
64
   a = 2 ./ (1 + exp(-2*n)) - 1;
65
   end
66
67
  % Map Minimum and Maximum Output Reverse - Processing Function
68
   function x = mapminmax reverse(y, settings)
69
   x = bsxfun(@minus, y, settings.ymin);
70
x = bsxfun(@rdivide, x, settings.gain);
  x = bsxfun(@plus,x,settings.xoffset);
72
   end
73
```

1	clear
2	clc
3	close all
4	
5	TE1 = [
6	
	0
	7
	14
10	28
11	42
12	
13	];
14	
15	TE2 = [
16	
17	0
	7
19	14
20	28
21	42
22	
23	];
24	
25	TE3 = [
26	
27	0
28	7
29	14
30	28
31	42
32	
33	];
34	
35	TE4 = [
36	
37	
38	
	14
	28
41	42
	·

## B.4 Example: Thermal degradation time measurements

86	
87	0
88	7
89	14
90	28
91	42
92	
93	];
94	
95	TF1 = [
96	
97	0
98	7
99	14
100	28
101	42
102	
103	];
104	_
105	$\mathrm{TF2} = [$
106	
107	0
108	7
109	14
110	28
111	42
112	
113	];
114	F
115	$\mathrm{TF3}=[$
116	
117	0
118	7
119	14
120	28
121	42
122	1
123	];
124	
125	TF4 = [
126	0
127	0
128	7
129	14

130	28
131	
132	
133	];
134	
135	$\mathrm{TF5}~=~[$
136	
137	0
138	7
139	14
140	28
141	
142	
143	];
144	
145	$\mathrm{TF6}~=~[$
146	
147	0
148	7
149	14
150	28
151	42
152	
153	];
154	
155	$\mathrm{TF7}~=~[$
156	
157	0
158	7
159	14
160	28
161	42
162	
163	];
164	
165	TF8 = [
166	
167	
	7
	14
170	28
171	
172	];
173	

174	$\mathrm{TF9}~=~[$
175	
176	0
177	7
178	14
179	28
180	
181	
182	];

## B.5 Example: MEA all plots

```
clear
1
  clc
\mathbf{2}
  close all
3
4 THERMAL TIME
   set(groot, 'defaultLineLineWidth',1.5)
5
6
  E1_MEA = [
\overline{7}
8
         6.58
                                     NaN
9
  6.12
         6.32204413541079
                                   NaN
10
   6.33
         6.07707514441802
                                   NaN
11
   5.86
        5.57619058091935
                                   NaN
12
   6.24
        5.09801931107691
                                   NaN
13
14
   ];
15
16
  E2 MEA = [
17
18
         6.58
                                   NaN
19
   6.22
                                   NaN
        6.18559155445716
20
   5.9
          5.84324777271713
                                     NaN
21
   5.58
        5.23441267993921
                                    NaN
22
         4.68797130426874
   5.14
                                    NaN
^{23}
^{24}
25
26
   ];
27
  E3_MEA = [
^{28}
29
   6.58
         NaN
30
   6.19
        5.94051797054882
                                    NaN
31
```

```
5.76
         5.40443449133772
                                    NaN
32
   6.1
           4.52486957379720
                                      NaN
33
         3.49611022224730
   4.18
                                    NaN
34
35
36
   |;
37
38
   E4 MEA = [
39
40
           4.9000000000000 4.900000000000
   4.9
41
   5.11
         4.67649471407249
                            4.80723428252824
42
   4.57
         4.45022190942435
                             4.70490356923068
43
   4.6
           4.01086561950235
                             4.56114697744983
44
   4.39
         3.57085979685593 4.42265975947287
45
46
47
   ];
^{48}
49
   E5 MEA = [
50
51
   4.9
           52
   4.82
         4.67540906123845
                            4.66951855276596
53
   4.5
           4.45526678842533 4.46580084023358
54
         3.63738307488669
                             3.88034300379937
   4.25
55
56
57
   1;
58
59
   E6 MEA = \begin{bmatrix} \end{bmatrix}
60
61
           4.9
                               62
           4.60023747267246
                               4.49596766314742
   4.6
63
   4.22
         4.33527562923556
                           4.16467568838407
64
   4
           3.87697366706872
                               3.69689137793502
65
         3.45294779708397
   3.68
                            3.31295891335673
66
67
   ];
68
69
  E7 MEA = \begin{bmatrix} 1 \\ 1 \end{bmatrix}
70
71
   2.88
         72
   3.24
         2.67393240901055
                             2.85672646120665
73
   2.72
         2.46550949324481
                             2.82645111877345
74
                             2.79250474939521
         2.05535443589185
   2.63
75
```

```
1.64628704830735
                            2.76430194262755
   2.59
76
77
78
   ];
79
80
   E8 MEA = [
81
82
   2.88
         83
   3.17
         2.72061891964655
                            2.84739912154367
84
   2.66
         2.55599258751855
                            2.80016288836989
85
   2.58
         2.24416593767766
                            2.76670703440018
86
   2.48
         1.93467240134749
                            2.73639533530704
87
88
89
   ];
90
91
   E9 MEA = [
^{92}
93
   2.88
         94
   3.22
         2.72594167323439
                            2.80753429791252
95
   2.69
         2.55844862117512
                            2.70469436348007
96
   2.33
         2.26301421161241
                            2.60754032847966
97
   2.31
         1.98787801077467
                            2.67862289030410
98
99
100
   ];
101
102
   F1 MEA = [
103
104
         6.58
105
   6.42
         6.18702716254070
                            6.10856294981150
106
   5.92
         5.82041179169698
                            5.67624756030738
107
         5.22435799969755
                            5.03817065938236
   5.61
108
   5.18
         4.69502930546699
                            4.52735323726988
109
110
111
112
   ];
113
   F2 MEA = \begin{bmatrix} 1 \\ 1 \end{bmatrix}
114
115
   6.58
         116
                              5.56676534573707
   5.8
           5.53573764260373
117
   4.43
         4.76109975395887
                            4.73554349398986
118
         3.96872448871623
   4.26
                            NaN
119
```

```
3.24492012237961
                              3.06178197261633
   3.27
120
121
122
    ];
123
124
   F3 MEA = [
125
126
                              6.580000000000000
   6.58
          127
   5
            5.17008173688541
                                        NaN
128
    4.09
          4.26796404266877
                                     NaN
129
   2.95
          3.06568105880457
                                     NaN
130
   2.48
          2.42487440577308
                                     NaN
131
132
133
    ];
134
135
   F4 MEA = [
136
137
            4.9000000000000 4.9000000000000
    4.9
138
    4.38
          4.69125808400730
                              4.68124062587235
139
    4.41
          4.51003328670225
                              4.52132915491829
140
    4.27
          4.14488399032678
                              4.26665642021020
141
142
143
    ];
144
145
   F5 MEA = [
146
147
   4.9
            4.900000000000 4.900000000000
148
    4.31
          4.39391281665650
                              4.39253637308310
149
    4.28
          4.02222187017508
                              4.01999361833809
150
   3.42
          3.29064500283009
                              3.28968517917833
151
152
153
    ];
154
155
   F6 MEA = [
156
157
    4.9
            158
    4.05
          4.03273798583193
                              4.12638924272244
159
   3.46
          3.44356801399938
                              3.59273497603730
160
          2.58356341111304
                              2.79414101129343
   2.69
161
   2.42
          2.03499094323044
                              2.28416922077770
162
163
```

```
164
    ];
165
166
    F7 MEA = [
167
168
           2.88
169
    2.79
           2.74221500427992
                                 2.77244804738971
170
    2.71
           2.60600805555225
                                 2.67224245747956
171
           2.33627346581151
                                 2.48263217518174
    2.58
172
    2.54
           2.07065752021148
                                 2.41139839015401
173
174
175
    ];
176
177
    F8 MEA = \begin{bmatrix} 1 \\ 1 \end{bmatrix}
178
179
    2.88
           180
    2.72
           2.70461576344569
                                 2.70808554773775
181
    2.43
           2.54246944408620
                                 2.55423090042582
182
    2.24
           2.25978439727425
                                 2.34214994344376
183
184
    ];
185
186
   F9 MEA = \begin{bmatrix} 1 \\ 1 \end{bmatrix}
187
188
    2.88
           189
    2.54
           2.57263639632440
                                 2.60774051495939
190
    3.09
           2.32216481565399
                                 2.40855536716565
191
    2.01
           1.62635372590170
                                 1.87356587912771
192
    1.93
           1.26440243863403
                                 1.65582517046464
193
194
    ];
195
196
197
    AD E1 3 = \text{mean}(\text{abs}(\text{E1 MEA}(:,1) - \text{E1 MEA}(:,2)))
198
    AD E1 6 = \text{mean}(\text{abs}(\text{E1 MEA}(:,1) - \text{E1 MEA}(:,3)))
199
200
    AD E2 3 = \text{mean}(\text{abs}(\text{E2 MEA}(:,1) - \text{E2 MEA}(:,2)))
201
    AD_E2_6 = mean(abs(E2_MEA(:,1) - E2_MEA(:,3)))
202
203
    AD_E3_3 = mean(abs(E3_MEA(:,1) - E3_MEA(:,2)))
204
    AD_E3_6 = mean(abs(E3_MEA(:,1) - E3_MEA(:,3)))
205
206
   AD_E4_3 = mean(abs(E4_MEA(:,1) - E4_MEA(:,2)))
207
```

```
AD E4 6 = \text{mean}(\text{abs}(\text{E4 MEA}(:,1) - \text{E4 MEA}(:,3)))
208
209
     AD E5 3 = \text{mean}(\text{abs}(\text{E5 MEA}(:, 1) - \text{E5 MEA}(:, 2)))
210
     AD\_E5\_6 = mean(abs(E5\_MEA(:,1)-E5\_MEA(:,3)))
211
212
     AD E6 3 = \text{mean}(\text{abs}(\text{E6 MEA}(:, 1) - \text{E6 MEA}(:, 2)))
213
     AD E6 6 = mean ( abs (E6 MEA(:,1) - E6 MEA(:,3) ) )
214
215
     AD E7 3 = \text{mean}(\text{abs}(\text{E7 MEA}(:,1) - \text{E7 MEA}(:,2)))
216
     AD E7 6 = \text{mean}(\text{abs}(\text{E7 MEA}(:,1) - \text{E7 MEA}(:,3)))
217
218
     AD E8 3 = \text{mean}(\text{abs}(\text{E8 MEA}(:,1) - \text{E8 MEA}(:,2)))
219
     AD E8 6 = \text{mean}(\text{abs}(\text{E8 MEA}(:,1) - \text{E8 MEA}(:,3)))
220
221
     AD E9 3 = \text{mean}(abs(E9 \text{ MEA}(:,1) - E9 \text{ MEA}(:,2)))
222
     AD E9 6 = \text{mean}(\text{abs}(\text{E9 MEA}(:,1) - \text{E9 MEA}(:,3)))
223
224
     AD F1 3 = \text{mean}(\text{abs}(\text{F1 MEA}(:, 1) - \text{F1 MEA}(:, 2)))
225
     AD F1 6 = \text{mean}(\text{abs}(\text{F1 MEA}(:,1) - \text{F1 MEA}(:,3)))
226
227
     AD F2 3 = \text{mean}(\text{abs}(\text{F2 MEA}(:,1) - \text{F2 MEA}(:,2)))
228
     AD F2 6 = \text{mean}(\text{abs}(\text{F2 MEA}(:,1) - \text{F2 MEA}(:,3)))
229
230
     AD F3 3 = \text{mean}(\text{abs}(F3 \text{ MEA}(:, 1) - F3 \text{ MEA}(:, 2)))
231
     AD F3 6 = \text{mean}(\text{abs}(F3 \text{MEA}(:,1) - F3 \text{MEA}(:,3)))
232
233
     AD F4 3 = \text{mean}(\text{abs}(\text{F4 MEA}(:,1) - \text{F4 MEA}(:,2)))
234
     AD_F4_6 = mean(abs(F4_MEA(:,1) - F4_MEA(:,3)))
235
236
     AD F5 3 = \text{mean}(\text{abs}(\text{F5 MEA}(:,1) - \text{F5 MEA}(:,2)))
237
     AD_F5_6 = mean(abs(F5_MEA(:,1) - F5_MEA(:,3)))
238
239
     AD F6 3 = \text{mean}(\text{abs}(\text{F6 MEA}(:,1) - \text{F6 MEA}(:,2)))
240
     AD_F6_6 = mean(abs(F6_MEA(:,1) - F6_MEA(:,3)))
241
242
     AD F7 3 = \text{mean}(\text{abs}(\text{F7 MEA}(:,1) - \text{F7 MEA}(:,2)))
243
     AD F7 6 = \text{mean}(\text{abs}(\text{F7 MEA}(:,1) - \text{F7 MEA}(:,3)))
244
245
     AD F8 3 = \text{mean}(\text{abs}(F8 \text{MEA}(:, 1) - F8 \text{MEA}(:, 2)))
246
     AD F8 6 = \text{mean}(\text{abs}(\text{F8 MEA}(:,1) - \text{F8 MEA}(:,3)))
247
248
     AD F9 3 = \text{mean}(\text{abs}(\text{F9 MEA}(:, 1) - \text{F9 MEA}(:, 2)))
249
     AD F9 6 = \text{mean}(\text{abs}(\text{F9 MEA}(:,1) - \text{F9 MEA}(:,3)))
250
251
```

252

AARD E1 3 = mean ( abs ( (E1 MEA(:,1) - E1 MEA(:,2) ) / E1 MEA(:,1) ) \*100 253AARD E1 6 = mean(abs((E1 MEA(:,1)-E1 MEA(:,3))/E1 MEA(:,1)))\*100 254255AARD E2 3 = mean ( abs ( (E2 MEA(:,1) - E2 MEA(:,2) ) / E2 MEA(:,1) ) \*100 256AARD E2 6 = mean(abs((E2\_MEA(:,1)-E2\_MEA(:,3))/E2\_MEA(:,1)))\*100 257258AARD E3 3 = mean ( abs ( (E3 MEA(:,1) -E3 MEA(:,2) ) /E3 MEA(:,1) ) \*100 259260 261AARD E4 3 = mean ( abs ( (E4 MEA(:,1) - E4 MEA(:,2) ) / E4 MEA(:,1) ) \*100 262AARD E4 6 = mean ( abs ( (E4 MEA(:,1) - E4 MEA(:,3) ) / E4 MEA(:,1) ) \*100 263 264 AARD E5 3 = mean ( abs ( (E5 MEA(:,1) - E5 MEA(:,2) ) / E5 MEA(:,1) ) \*100 265AARD E5 6 = mean ( abs ( (E5 MEA(:,1) - E5 MEA(:,3) ) / E5 MEA(:,1) ) ) \*100266 267AARD E6 3 = mean ( abs ( (E6 MEA(:,1) - E6 MEA(:,2) ) / E6 MEA(:,1) ) \* 100 268AARD E6 6 = mean ( abs ( (E6 MEA(:,1) - E6 MEA(:,3) ) / E6 MEA(:,1) ) \*100 269270AARD E7 3 = mean ( abs ( (E7 MEA(:,1) - E7 MEA(:,2) ) / E7 MEA(:,1) ) \*100 271AARD E7 6 = mean ( abs ( (E7 MEA(:,1) - E7 MEA(:,3) ) / E7 MEA(:,1) ) \*100 272273AARD E8 3 = mean ( abs ( (E8 MEA(:,1) - E8 MEA(:,2) ) / E8 MEA(:,1) ) \*100 274AARD E8 6 = mean ( abs ( (E8 MEA(:,1) - E8 MEA(:,3) ) / E8 MEA(:,1) ) ) \*100275276 $AARD_E9_3 = mean(abs((E9_MEA(:,1) - E9_MEA(:,2))/E9_MEA(:,1))) *100$ 277 AARD E9 6 = mean ( abs ( (E9\_MEA(:,1) - E9\_MEA(:,3) ) / E9\_MEA(:,1) ) ) \*100278279AARD F1 3 = mean (abs ((F1 MEA(:,1) - F1 MEA(:,2))/F1 MEA(:,1))) \* 100280 AARD F1 6 = mean (abs ((F1 MEA(:,1) - F1 MEA(:,3))/F1 MEA(:,1))) \* 100281 282 AARD F2 3 = mean(abs((F2 MEA(:,1)-F2 MEA(:,2))/F2 MEA(:,1)))\*100 283  $AARD_F2_6 = mean(abs((F2_MEA(:,1) - F2_MEA(:,3))/F2_MEA(:,1))) * 100$ 284 285AARD F3 3 = mean(abs((F3 MEA(:,1)-F3 MEA(:,2))/F3 MEA(:,1)))\*100 286  $AARD F3 6 = mean(abs((F3_MEA(:,1) - F3_MEA(:,3))/F3_MEA(:,1))) * 100$ 287 288 AARD F4 3 = mean(abs((F4 MEA(:,1)-F4 MEA(:,2))/F4 MEA(:,1)))\*100 289  $AARD \ F4_6 = mean(abs((F4_MEA(:,1) - F4_MEA(:,3))/F4_MEA(:,1))) * 100$ 290 291 AARD F5 3 = mean (abs ((F5 MEA(:,1) - F5 MEA(:,2))/F5 MEA(:,1))) \*100 292 293 294AARD F6 3 = mean (abs ((F6 MEA(:,1) - F6 MEA(:,2))/F6 MEA(:,1))) \*100 295

```
AARD F6 6 = mean(abs((F6 MEA(:,1)-F6 MEA(:,3))/F6 MEA(:,1)))*100
296
297
    AARD F7 3 = mean ( abs ( (F7 MEA(:,1) - F7 MEA(:,2) ) / F7 MEA(:,1) ) ) *100
298
    AARD_F7_6 = \operatorname{mean}(\operatorname{abs}((F7\_MEA(:,1) - F7\_MEA(:,3))/F7\_MEA(:,1))) * 100
299
300
    AARD F8 3 = mean (abs ((F8 MEA(:,1) - F8 MEA(:,2))/F8 MEA(:,1))) *100
301
    AARD F8 6 = mean ( abs ( (F8_MEA(:,1) - F8_MEA(:,3) ) / F8_MEA(:,1) ) ) *100
302
303
    AARD F9 3 = mean(abs((F9 MEA(:,1)-F9 MEA(:,2))/F9 MEA(:,1)))*100
304
    AARD F9 6 = mean (abs((F9 \text{ MEA}(:,1) - F9 \text{ MEA}(:,3))/F9 \text{ MEA}(:,1))) * 100
305
306
307
    a = figure();
308
309
    hold on
310
    plot(TE1, E1 MEA(:, 1), '*');
311
    plot(TE1, E1 MEA(:, 2), '-');
312
    plot(TE1, E1 MEA(:,3), '-');
313
    xlabel('Time [days]');
314
    ylabel('C {MEA} [\text{kmol/m}^3]');
315
    legend ('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
316
        inputs } ', 'Location ', 'southwest ');
    title ('E1, 120 \setminus circC, CO 2-loading 0.2, MEA');
317
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
318
319
    b = figure();
320
321
    hold on
322
    plot(TE2, E2 MEA(:, 1), '*');
323
    plot(TE2, E2 MEA(:, 2), '-');
324
    plot (TE2, E2 MEA(:, 3), '-');
325
    xlabel('Time [days]');
326
    ylabel('C {MEA} [\text{kmol/m}^3]');
327
    legend('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
328
        inputs } ', 'Location ', 'southwest ');
    title ('E2, 120 \setminus circC, CO 2-loading 0.4, MEA');
329
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
330
331
    c = figure();
332
333
    hold on
334
    plot(TE3, E3 MEA(:, 1), '*');
335
    plot (TE3, E3 MEA(:, 2), '-');
336
    plot(TE3, E3_MEA(:,3), '-');
337
```

```
xlabel('Time [days]');
338
    ylabel('C {MEA} [\text{kmol/m}^3]');
339
   legend ('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
340
       inputs } ', 'Location ', 'southwest ');
    title ('E3, 120 \ circC, CO 2-loading 0.5, MEA');
341
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
342
343
   d = figure();
344
345
   hold on
346
   plot(TE4, E4 MEA(:, 1), '*');
347
   plot(TE4, E4 MEA(:, 2), '-');
348
   plot(TE4, E4 MEA(:,3), '-');
349
   xlabel('Time [days]');
350
   ylabel('C {MEA} [\text{kmol/m}^3]');
351
   legend('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
352
       inputs } ', 'Location ', 'southwest ');
    title ('E4, 120 \ circC, CO 2-loading 0.2, MEA');
353
    set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
354
355
   e = figure();
356
357
   hold on
358
    plot(TE5, E5 MEA(:, 1), '*');
359
    plot(TE5, E5 MEA(:, 2), '-');
360
   plot (TE5, E5_MEA(:,3), '-');
361
   xlabel('Time [days]');
362
   ylabel('C_{\text{MEA}} [ kmol/m^3 ] ' );
363
   legend ('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
364
       inputs } ', 'Location ', 'southwest ');
    title ('E5, 120 \circC, CO_2-loading 0.4, MEA');
365
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
366
367
    f = figure();
368
369
   hold on
370
    plot(TE6, E6 MEA(:, 1), '*');
371
    plot(TE6, E6 MEA(:, 2), '-');
372
   plot (TE6, E6 MEA(:, 3), '-');
373
   xlabel('Time [days]');
374
   ylabel('C_{\text{MEA}} [ kmol/m^3 ] ' );
375
   legend('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
376
       inputs } ', 'Location ', 'southwest ');
   title ('E6, 120 \setminus circC, CO 2-loading 0.5, MEA');
377
```

```
set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
378
379
    g = figure();
380
381
    hold on
382
    plot(TE7, E7 MEA(:, 1), '*');
383
    plot(TE7, E7 MEA(:, 2), '-');
384
    plot(TE7, E7 MEA(:,3), '-');
385
    xlabel('Time [days]');
386
    ylabel('C {MEA} [\text{kmol/m}^3]');
387
    legend ('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
388
       inputs } ', 'Location ', 'southwest ');
    title ('E7, 120 \land circC, CO 2-loading 0.2, MEA');
389
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
390
391
    h = figure();
392
393
    hold on
394
    plot(TE8, E8 MEA(:,1), '*');
395
    plot(TE8, E8 MEA(:,2), '-');
396
    plot(TE8, E8 MEA(:,3), '-');
397
    xlabel('Time [days]');
398
    ylabel('C {MEA} [\text{kmol/m}^3]');
399
    legend ('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
400
        inputs } ', 'Location ', 'southwest ');
    title('E8, 120 \circC, CO_2-loading 0.4, MEA');
401
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
402
403
    i = figure();
404
405
    hold on
406
    plot (TE9, E9 MEA(:,1), '*');
407
    plot(TE9, E9 MEA(:, 2), '-');
408
    plot(TE9, E9 MEA(:,3), '-');
409
    xlabel('Time [days]');
410
    ylabel('C {MEA} [\text{kmol/m}^3]');
411
    legend('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
412
       inputs } ', 'Location ', 'southwest ');
    title ('E9, 120 \land circC, CO_2-loading 0.5, MEA');
413
    set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
414
415
    j = figure();
416
417
   hold on
418
```

```
plot(TF1, F1 MEA(:, 1), '*');
419
    plot(TF1, F1 MEA(:, 2), '-');
420
    plot(TF1, F1 MEA(:,3), '-');
421
    xlabel('Time [days]');
422
    ylabel('C {MEA} [\text{kmol/m}^3]');
423
    legend('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
424
       inputs } ', 'Location ', 'southwest ');
    title ('F1, 135 \land circC, CO 2-loading 0.2, MEA');
425
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
426
427
    k = figure();
428
429
    hold on
430
    plot(TF2, F2 MEA(:,1), '*');
431
    plot(TF2, F2 MEA(:, 2), '-');
432
    plot(TF2, F2 MEA(:,3), '-');
433
    xlabel('Time [days]');
434
    ylabel('C {MEA} [\text{kmol/m}^3]');
435
    legend ('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6}
436
       inputs } ', 'Location ', 'southwest ');
    title ('F2, 135 \ circC, CO 2-loading 0.4, MEA');
437
    set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
438
439
    1 = figure();
440
441
    hold on
442
    plot(TF3, F3 MEA(:,1), '*');
443
    plot(TF3, F3_MEA(:,2), '-');
444
    plot(TF3, F3 MEA(:,3), '-');
445
    xlabel('Time [days]');
446
    ylabel('C_{\text{MEA}} [ kmol/m^3 ] ' );
447
    legend('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
448
       inputs } ', 'Location ', 'southwest ');
    title ('F3, 135 \land circC, CO 2-loading 0.5, MEA');
449
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
450
451
452
   m = figure();
453
454
    hold on
455
    plot(TF4, F4_MEA(:,1), '*');
456
    plot(TF4, F4_MEA(:,2), '-');
457
    plot(TF4, F4 MEA(:,3), '-');
458
   xlabel('Time [days]');
459
```

```
ylabel('C_{MEA} = [kmol/m^3]');
460
   legend('C {MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
461
       inputs } ', 'Location ', 'southwest ');
    title('F4, 135 \circC, CO_2-loading 0.2, MEA');
462
    set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
463
464
465
   n = figure();
466
467
   hold on
468
   plot (TF5, F5 MEA(:,1), '*');
469
   plot (TF5, F5 MEA(:, 2), '-');
470
   plot (TF5, F5 MEA(:,3), '-');
471
   xlabel('Time [days]');
472
   ylabel('C {MEA} [\text{kmol/m}^3]');
473
   legend('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
474
       inputs } ', 'Location ', 'southwest ');
   title ('F5, 135 \ circC, CO 2-loading 0.4, MEA');
475
   set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
476
477
478
   o = figure();
479
480
   hold on
481
   plot(TF6, F6 MEA(:,1), '*');
482
   plot(TF6, F6_MEA(:,2), '-');
483
   plot(TF6, F6 MEA(:,3), '-');
484
   xlabel('Time [days]');
485
   ylabel('C {MEA} [\text{kmol/m}^3]');
486
   legend ('C {MEA, exp}', 'C {MEA, mod, 3 inputs}', 'C {MEA, mod, 6
487
       inputs } ', 'Location ', 'southwest ');
   title ('F6, 135 \land circC, CO 2-loading 0.5, MEA');
488
    set(findall(gcf, '-property', 'FontSize'), 'FontSize', 18);
489
490
491
   p = figure();
492
493
   hold on
494
   plot(TF7, F7_MEA(:,1), '*');
495
   plot(TF7, F7 MEA(:, 2), '-');
496
   plot(TF7, F7 MEA(:,3), '-');
497
   xlabel('Time [days]');
498
   ylabel('C {MEA} [\text{kmol/m}^3]');
499
   legend('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
500
```

```
inputs } ', 'Location ', 'southwest ');
    title ('F7, 135 \land circC, CO 2-loading 0.2, MEA');
501
    set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
502
503
   q = figure();
504
505
   hold on
506
   plot (TF8, F8 MEA(:,1), '*');
507
   plot (TF8, F8 MEA(:, 2), '-');
508
   plot(TF8, F8_MEA(:,3), '-');
509
   xlabel('Time [days]');
510
   ylabel('C {MEA} [\text{kmol/m}^3]');
511
   legend('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
512
       inputs}', 'Location', 'southwest');
    title ('F8, 135 \land circC, CO 2-loading 0.4, MEA');
513
    set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
514
515
   r = figure();
516
517
   hold on
518
   plot (TF9, F9 MEA(:,1), '*');
519
   plot(TF9, F9 MEA(:, 2), '-');
520
   plot(TF9, F9_MEA(:,3), '-');
521
   xlabel('Time [days]');
522
   ylabel('C_{\text{MEA}} [ kmol/m^3 ] ' );
523
   legend('C_{MEA, exp}', 'C_{MEA, mod, 3 inputs}', 'C_{MEA, mod, 6
524
       inputs } ', 'Location ', 'southwest ');
    title ('F9, 135 \ circC, CO_2-loading 0.5, MEA');
525
   set(findall(gcf, '-property', 'FontSize'), 'FontSize',18);
526
```



