Abstract

Atlantic salmon (*Salmo salar*) is the main fish species harvested from aquaculture, making up a total of 93,9% of Norway's total fish production. Expansion of aquaculture has over the last few years proved difficult due to environmental and geographical challenges, and alternative production methods are being investigated. Recirculating aquaculture systems (RAS) has proved to be a viable alternative but has faced problems with acute mortality events suspected to be caused by hydrogen sulfide. Hydrogen sulfide is produced by oxidation of sulfate, and a proposed possible solution this problem is to desalinate seawater with a nanofiltering membrane, specifically designed to remove sulfate.

The aim of this thesis was to study the effects a nanofiltering membrane has on the composition of seawater and see if sulfur content can be removed without changing other key parameters. Over the course of 13 weeks samples where taken at 10 different points on two RAS. One with nanofiltered inlet water and one with a combination of seawater and freshwater to serve as control. These samples where then measured for pH, salinity and conductivity, and analyzed by ICP-MS, IC and UV-vis.

The main objective of this thesis was to find the effiency of sulfate removal by nanofiltering membrane, investigated by analysis with ICP-MS and IC. Sulfur content had a reduction of 93,37 % measured by ICP-MS and had a reduction of 85,85% when compared to a control. The second objective was to see the effect on water quality parameters as well as other key ions. pH saw an increase by 1,41 % before and after nanofilter, but there was no significant difference between treated water an control. There was a 60,13 % reduction of salinity and 56,83 % reduction of conductivity after nanofiltration, but no significant difference when compared to control. Magnesium, silicone, potassium, calsium, bromide and strontium all saw a reduction after treatment, with magnesium, silicone, calsium and strontium having a lower concentration when compared to control, while potassium and bromide had a higher concentration.

Overall, this work demonstrated that use of nanofiltering membrane can achieve a large reduction of sulfur content, while keeping salinity, pH and conductivity unchanged in comparison to control. However, there were some observed changes in other ions, and further investigations are needed to determine the effects this has on health and wellbeing of Atlantic Salmon.

Sammendrag

Atlanterhavslaks (*Salmo salar*) er den største fiskearten som produseres i akvakulturnæringen, og representerer 93,39% av Norges totale fiskeproduksjon. Utvidelse av akvakulturdrift har i løpet av de siste årene vært problematisk, grunnet miljøhensyn og geografiske utfordringer. Resirkulerende akvakultur anlegg (RAS) has vist seg å være et godt alternativ, men har over de siste årene møtt på problemer med akutte massedødstilfeller hvor det mistenkes at hydrogen sulfid had spilt en stor rolle. Hydrogen sulfid oppstår etter oksidasjon av sulfat, og en spekulert løsning til dette problemet er å avsalte saltvann med et nanofilter som er spesifikt designet til å redusere sulfatinnhold.

Bakgrunnen denne oppgaven var å studere effekten nanofiltering har på komposisjonen av saltvann, og undersøke hvorvidt svovelinnhold kan reduseres uten at andre viktige vannkvalitetsparametere blir endret. I løpet av 13 uker ble det hentet ut prøver fra 2 ulike RAS anlegg. En av disse med nanofiltrert inntaksvann, og en med kombinasjon av saltvann og ferskvann som kontroll. Disse prøvene ble målt for pH, salinitet og konduktivitet, og analysert med ICP-MS, IC og UV-Vis.

Hovedformålet var å finne hvor effektiv nanofiltering kan fjerne svovelinnhold, som ble undersøkt med ICP-MS og IC. Det ble funnet en 93,37% reduksjon av svovel etter nanofiltering, og en 85,85% reduksjon sammenlignet med kontroll. Det andre formålet med oppgaven var å undersøke effekten på viktige vannkvalitetsparametere, samt undersøke effect på viktige ioner. pH økte med 1,41% etter nanofiltering, men det ble ikke funnet en signifikant forskjell sammenlignet med kontroll. Salinitet og konduktivitet ble redusert med henholdsvis 60,13 % og 56,83%, men det ble heller ikke her funnet en signifikant forskjell sammenlignet med kontroll. Magnesium, silitsium, kalsium, brom og strontium hadde alle en reduksjon etter nanofiltering, hvor magnesium, silitsium kalsium og brom hadde en observer lavere konsentrasjon sammenlignet med kontroll, og kalsium og brom hadde en observer høyere konsentrasjon.

Dette arbeidet demonstrerte at bruk av nanofilter kan oppnå en høy reduksjon av svovelinnhold uten å påvirke vannkvalitetsparametere som pH, salinitet og konduktivitet. Det var forøvrig observer endring i andre ioner, og det behøves mer forskning for å finne ut av hvordan dette kan påvirke helsen og velværet til Atlanterhavslaks.

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Table of contents

1	Int	rodu	ction	10	
	1.1	Air	ns and objectives	11	
2	Re	circu	lating aquaculture system	12	
	2.1	Wa	ter quality parameters	13	
	2.1	.1	pH	13	
	2.1	.2	Salinity	13	
	2.1	.3	H ₂ S, its accumulation and harmful effects on Atlantic salmon	14	
3	Na	nofil	tration	16	
4	Ma	teria	ls and experimental method	21	
	4.1	Set	up of nanofiltering membrane at Sunndalsøra	21	
	4.2	Sar	npling method	24	
	4.3	ICP-MS			
	4.4	IC .		25	
	4.5	UV	Z-Vis	27	
	4.6	Sta	tistics	27	
	4.6	.1	Averages	27	
	4.6	.2	Standard deviation	28	
	4.6	.3	Mann-Whitney-U test	28	
5	Re	sults	and discussion	29	
	5.1	The	e effects of nanofiltering membrane on pH, salinity and conductivity	29	
	5.1	.1	рН		
	5.1	.2	Salinity and conductivity	32	
	5.2	Eff	ect of nanofiltering membrane on elemental composition	33	
	5.2	.1	Efficiency on sulfur removal measured by ICP-MS and IC	33	
	5.2	.2	Other ions of importance	39	
	5.3	UV	/-vis	41	

5.3.1 Outliers
5.4 Further work
6 Conclusion
References
A.1 All measurements of pH, salinity and conductivity
A.2 Measurements done by ICP-MS for magnesium, silicone, sulfur, potassium, calsium,
bromide and strontium
A.3 All measured values of sulfate measured by IC-Analysis
A.3 All measurements of absorbance at 254 nm for each sampling point and date by UV-Vis

List of figures

Figure 2.1 Flow through system compared with a recirculating aquaculture system. (Lekang,O.
Aquaculture engineering (p. 285))
Figure 3.1 Graphical demonstration of the process behind general membrane separation (Graphics from: Droas, M. 2019)
Figure 3.2 The four different classes of membrane separations, with pore sizes, operation pressures and an overview of types of compound that can be retained or separated. (Graphics provided by Akvafresh, 2020)
Figure 3.3 Representation of the selective PA layer and the microporous support layer of a thin film composite membrane. (Graphics from: Pinnau, I. 2000
Figure 3.4 Preparation of NF membrane by immersion precipitation. (Graphics altered from: Jye, L. and Ismail, A. 2019)
Figure 3.5 Demonstration of the electrostatic structure of LBL NF membranes. (Graphics altered from Jye, L. and Ismail, A 2019)
Figure 3.6 Configuration of a spiral-wound membrane. (Graphics from: Rackley.S 2008) 20
Figure 3.7 Configuration of a hollow fibre module. (Graphics from: Rackley.S. 2008)
Figure 4.1 Picture of the same type of NF membrane installed at Sunndalsøra. (Picture provided by Akvafresh)
Figure 4.2 Process flow diagram for RAS 1 with sampling points 1-6
Figure 4.3 Process flow diagram for RAS 2 with sampling points 7-10
Figure 4.4 Essential components found in an ion chromatograph with a typical output graph. (Graphics from Worden, R. 2005)
Figure 5.1 Measured pH of feed(<i>NF</i> , <i>in</i>), permeate(<i>NF</i> , <i>out</i>), treated water(<i>RAS1</i>) and control(<i>RAS2</i>) plotted for each sampling date
Figure 5.2 Box plot of measured pH, where sample points 1-4 represents feed(<i>NF</i> , <i>in</i>), permeate(<i>NF</i> , <i>out</i>), treated water(<i>RAS1</i>) and control(<i>RAS2</i>) respectively
Figure 5.3 and 5.4 Measured conductivity (left) and salinity (right) for feed(NF , in), permeate(NF , out), treated water($RAS1$) and control($RAS2$) plotted for each sampling date 32
Figure 5.5 Box plot of salinity of feed(1), permeate(2), treated water(3) and control(4)31

Figure 5.6 Box plot of conductivity of feed(1), permeate(2), treated water(3) and control(4) 32
Figure 5.7 Measured sulfur concentration [µg/l] for NF,in, NF,out, RAS1 and RAS2 from
11.03.20 until 10.07.20, found by ICP-MS
Figure 5.8 Box plot of elemental sulfur concentration of feed(1), permeate(2)
Figure 5.9 Box plot of elemental sulfur concentration of treated water(1) and control(2) 32
Figure 5.10 Concentration of sulfate measured by IC and converted to sulfur for each sample
date, bompared to ICP-MS measured sulfur concentration represented as lines
Figure 5.11 Box plot comparing distribution of sulfur measured by ICP-MS(1,3) and measured
by IC (2,4)
Figure 5.12 A comparison of average elemental composition for magnesium, silicone,
potassium, calsium, bromide and strontium for each sample point
Figure 5.13 Measured absorbance plotted against each date for NF, in, NFout, RAS1 and RAS2

List of tables

Table 2.1 Summary of major ion composition found in seawater altered to mg/L (Byrne et al 2021)
Table 4.1 An overview of each sampling point taken with name, description, and comment. 22
Table 5.1 Summary of each measured parameter with calculated difference presented in associated units and in percentage, between feed and permeate and between treated water and control. 29
Table 5.2 Descriptive values of pH, salinity and conductivity for NF, in, NF, out, RAS1 and RAS2
Table 5.3 An investigation to determine if there was a significant difference of pH, salinity or conductivity before and after the nanofilter (<i>NF</i> , <i>in/NF</i> , <i>out</i>) and between treated and untreated water in RAS phase (<i>RAS1/RAS2</i>). A Mann-Whitney-U test with null hypothesis H_0 : $P(x_i>y_j) = 0,5$ versus alternative hypothesis H_1 : $P(x_i>y_j) \neq 0,5$ was used
Table 5.4 Descriptive values of elemental sulfur concentration determined by ICP-MS [μ/L] for <i>NF</i> , <i>in</i> , <i>NF</i> , <i>out</i> , <i>RAS1</i> and <i>RAS2</i> 34
Table 5.5 An investigation to determine if there was a significant difference in concentration of elemental sulfur before and after the nanofilter (<i>NF</i> , <i>in</i> / <i>NF</i> , <i>out</i>) and between treated and untreated water in RAS phase (<i>RAS1/RAS2</i>). A Mann-Whitney-U test with null hypothesis H ₀ : $P(x_i>y_j) = 0,5$ versus alternative hypothesis H ₁ : $P(x_i>y_j) \neq 0,5$ was used
Table 5.6 Descriptive values of elemental sulfur concentration [mg/L] for RAS1 and RAS2 measured by IC
Table 5.7 An investigation to determine if there was a significant difference in concentration of sulfur between treated and untreated water in RAS phase (<i>RAS1/RAS2</i>) measured by IC, and if there was a significant difference between sulfur measured by ICP-MS and sulfur measured by IC. A Mann-Whitney-U test with null hypothesis H_0 : $P(x_i>y_j) = 0.5$ versus alternative hypothesis H_1 : $P(x_i>y_j) \neq 0.5$ was used
Table 5.8 Calculated differences of Mg, Si, K, Ca, Br and SR between NFin/NFout andRAS1/RAS2, with significance.39
Table 5.9 Descriptive values of measured absorbance for NF, in, NF, out, RAS1 and RAS242

Acronyms, abbreviations and symbols

RAS	Recirculating aquaculture system					
NF	Nanofiltration					
SRB	SRB Sulfate reducing bacteria					
TFC	Thin film composite membrane					
LBL	Layer-by-layer					
PE	Polyelectrolyte					
SW	Spiral Wound					
HF	Hollow-fibre					
ICP-MS	Inductively coupled plasma mass spectrometry					
IC	Ion Chromatrography					
UV-vis	Ultraviolet-visible spectroscopy					
Ι	Intensity					
Т	Transmittance					
А	Absorbance					
С	Concentration					
3	Molar absorption coefficient					
d	Path length					

 σ Standard deviation

1 Introduction

In 2019 the farming of Atlantic salmon (Salmo Salar) represented 93,9% of Norway's total aquaculture where a total of 1 364 044 tonnes were produced (Statistics Norway 2020), making Norway the biggest producer worldwide (Iversen et.al 2020). Aquaculture is an important part of Norwegian culture and economy, and it is estimated that there is room to increase total revenue by up to 6 times (Ministry of Trade, Industry and Fisheries 2014-2015). To achieve this there needs to be innovation in method of production, since ocean fisheries are facing both environmental and area challenges (Olaussen, J. 2018). One possible solution is a recirculating aquaculture system (RAS), where the outlet water from the fish tanks is recycled and reintroduced into the system, instead of being released into recipient water body done in conventional flow-through-systems (FTS). (Lekang, O. 2020 p. 257). RAS provides several benefits. Re-use of water will limit the demand for new water, making it possible to establish production in otherwise geologically challenging areas. Reduction of new water needed will also reduce energy costs and cleaning costs, since the overall body of water that needs to be treated is less. Lastly, a RAS can work around a poor water supply. Access to fresh water can be difficult and costly, and in RAS this can be bypassed by either combining freshwater and seawater, or perhaps desalinating seawater.

Still, there are some challenges. Operating RAS is still more energy-intensive than ocean fisheries and establishing a production site will require a high investment cost. There is also a problem with accumulation of waste products. Organic matter and particles from uneaten feed, feces and bacteria will cause gill irritation and stress (Chiam,C.K. et. Al. 2011) and build-up of ammonia, CO₂ and hydrogen sulfide (H₂S) can all cause harm and potential mortality events (Lekang, O. 2020 p. 264-26). Therefore, each RAS needs to install proper water treatment components further increasing the overall establishment cost. Hydrogen sulfide is the main suspect of many acute mortality events where feedwater has been a combination of saltwater and freshwater. Saltwater has a naturally high sulfate content (2700 mg/L, freshwater around 2 mg/L)(Boyd,C. 2014), and H₂S is a product of sulfate reduction (Holmer, M. and Storkholm,P. 2001). A solution to this problem is still up for debate.

1.1 Aims and objectives

This master thesis is a part of a collaboration project between Nofima, Akvafresh and NTNU called Akvafresh, where the aim is to investigate the effects of using a nanofiltering membrane to desalinate saltwater used as feed water in RAS. More specifically, the objectives were to see if:

- Sulfate content can be reduced by nanofiltration to levels below 15 mg/L.
- Salinity will be kept at approximately 12 ‰
- Document effects on health and fitness, as well as documenting new water composition

For this thesis the aim was to document the effects of nanofilteration on water composition, specifically on pH, salinity, conductivity, and the changes in key ions. Two RAS provided by Nofima at the Nofima Centre for Recirculation in aquaculture where compared. One with desalinated water by nanofilter provided by Akvafresh, and one with combination water that served as a control. A full project description is included in appendix A.5.

2 Recirculating aquaculture systems

In RAS, the main principle is to recycle outlet water from the fish tank continuously instead of discarding it in a more conventional FTS, demonstrated in figure 2.1. Since FTS requires a steady water supply a lot of energy and cost is spent in temperature control, and choice of location becomes limited. RAS provides a different approach to aquaculture. With a constant recycling process total water consumption is reduced, decreasing energy costs at the same time. RAS is also preferable in implementation, as it can be designed to work with freshwater, brackish water and seawater (Lekang,O. 2020 p.267). Since it is a recirculating system, it does require a thorough water treatment, as there are many components that when accumulated can cause harmful effects.

Large particles, usually accumulating from untouched fish feed and feces, can cause harm to gills (Pedersen et al 2011) as well as being substrates for unwanted bacteria (Attramadal et al 2012). These are removed by a mechanical filter. Due to respiration, there will be a build-up of CO_2 throughout the life cycle of the fish. Long term exposure to high levels of CO_2 will have a negative effect on growth and fitness (Aslam et al 2019), as well as impacting pH. Therefore, control of CO_2 is usually done by a degasser where CO_2 rich water flows from the top of a stripping tower, while air flows the opposite direction from the bottom. This crosscurrent maximises fluid surface allowing CO_2 to escape and can reintroduce oxygen to the system if needed.

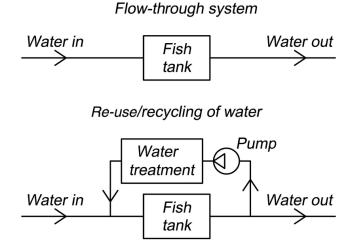


Figure 2.1 Flow through system compared with a recirculating aquaculture system. (Lekang,O. Aquaculture engineering (p. 285))

Last point of treatment is the removal of total-ammonia-nitrogen (TAN). TAN is the product of the protein metabolism and is secreted from the gills of the fish. When dissolved in water, TAN is present as both ammonia and ammonium. Ammonia is toxic and will with increased levels cause harmful effect (Iwama et al 1998). Therefore, TAN is commonly removed by utilizing a biofilter. A biofilter is a bed of media where bacteria grow to form a biological layer called a biofilm (Molleda et al 2008). The layer is populated by two groups of nitrifying bacteria, Nitrosomas and Nitrobacter, which will concrete ammonium to nitrite to nitrate. A simplification of this is given in equation 2.1. Efficiency of biofiltration depends primarily on temperature and pH, where optimal conversion happens between a pH of 7 and 9 (Noble et al 2018).

$$NH_3 \xrightarrow{Nitrosomas} NO_2^- \xrightarrow{Nitrobacter} NO_3$$
 (2.1)

2.1 Water quality parameters

To ensure optimal growth conditions a RAS must adhere to many water quality parameters. This thesis will focus mainly on pH, salinity, and ion composition based on recommended values for Atlantic salmon.

2.1.1 pH

pH is an important parameter to monitor, as it will not only affect the efficiency of nitrification in biofilter, but will also have an effect on aluminium dissolved in water (Lydersen, E. 1990) Under alkaline conditions aluminium will have to toxic effect on Atlantic salmon (Poleo,A., and Hytterød,S. 2003), but under acidic conditions inorganic monomeric Al species will occur which is considered to be the most toxic to Atlantic salmon. The recommended pH levels according to the Norwegian Food Safety Authority is between 6,2 and 7,8, however if optimal nitrification is also a priority pH should be between 7,0 and 7,8.

2.1.2 Salinity

Salinity is defined as the mass in grams of salts in 1 kg of seawater, with major ion compositions given in table 2.1 (Byrne et al 2014). It affects other parameters like ammonia, dissolved oxygen, efficiency of nitrification in biofilter as well as efficiency of removal of CO_2 (Noble et al 2018), and it is recommended to have levels around 12 ‰ for cost-efficient production (Ytrestøyl et al. 2014)

Major ion composition, seawater (mg/L)						
Chlorine 18 980						
Sodium	10 556					
Sulphate	2 649					
Magnesium	1 262					
Calcium	400					
Potassium	380					
Bicarbonate	140					
Bromide	65					
Borate	26					
Strontium	13					
Fluoride	1					
Silicate	1					
Iodide	<1					
Others	-					
Total dissolved solids 34 483						

Table 2.1 Summary of major ion composition found in seawater altered to mg/L (Byrne et al 2021)

To achieve optimal growth conditions in RAS it is important that the water provides the right ion composition, as many ions play an important part in fish metabolism and can only be accessed through gill intake. Magnesium acts as an activator of cofactors in enzyme systems (El-Mowafi, A. 1998), calcium is important for cellular signalling (Clapham,D. 2007) and potassium is important in maintenance of cellular volume and generation of nerve impulses (Kalantarian et al 2013). Keeping track of these ions is therefore an important part of a RAS process, to provide optimal growth condition and fish welfare.

2.1.3 Hydrogen sulfide, its accumulation and harmful effects on Atlantic salmon

Hydrogen Sulfide (H₂S) has been a much-debated topic in the salmon farming industry as of late, being the main suspect of several mass mortality events that has happened in RAS. Is is highly toxic to Atlantic salmon, and when digested it will cause respiratory failure (Forgan, L. and Donald, J. 2016). Sulfur is an essential element for life and is found in both seawater and freshwater in the form of either dissolved sulfate or sedimentary minerals. Sulfate mostly comes from the degradation of sulfur-containing rocks, or from the oxidation of organic sulphur found in decomposition of living things and waste products (Holmer, M. and Storkholm, P. 2001).

Concentration of sulfate in freshwater and seawater differ widely however, where concentrations are around 2 mg/L and 2700 mg/L respectively (Boyd,C. 2014).

H₂S is mostly made through sulfate reducing bacteria (SRB), found in anaerobic slime layers called biofilms. Biofilms are common in nature and grow at the water/solid interface in most biological systems (King et al 2008). It consists of essentially two layers: An aerobic top layer and an anaerobic bottom layer. The top layer consists of nitrifying bacteria (Schramm et al 2000) that converts ammonia and ammonium released from the fish into nitrate. The bottom layer is where SRB are found, and it is here that H₂S is created. There are multiple bacterial species involved in reduction of sulphate, mainly Sporovibrio desulfuricans and Desulfovibrio delsulfuricans. These bacteria are strictly anaerobic and use organic substances as electron donors and sulphate as electron acceptor, making conversion possible only when both sulphate and organic substances are available. The biofilm pathway starts with the nitrifying bacteria, that will convert all available anomia and ammonium in the water to nitrate, where nitrate is stored in the top layer structure keeping the anaerobic biofilm separated from the water. In the bottom layer two things are happening. Firstly, organic material and sulphate is converted into H₂S. Secondly, H₂S together with nitrate found in the upper layer is converted back to sulfate. This process will keep circulating until there is no more nitrate containing compounds left in the water. Once this happens the bottom layer of the biofilm will keep converting nitrate, but this time the structural integrity of the upper layer will be weakened until it disappears. This will release the underlying H₂S found in the bottom layer, which in large enough quantities could be harmful and even lethal to the fish.

Combatting the H₂S problem has been at the forefront of the RAS industry for many years, and different solutions have been proposed. According to Langeteig (2019) one possible solution to keeping levels of H₂S low is having sufficient levels of nitrate in the water to keep the biofilm at steady state. Since nitrate levels depends on the amount of ammonia and ammonium, which stems from feed and fish waste, the natural occurrence will fluctuate. Therefore, it is important to monitor nitrate concentrations and add a nitrate source when needed. This will prevent the bottom layer of the biofilm from degrading the upper layer, keeping the H₂S safely trapped.

Another suggested solution is to keep vigorous cleaning routines. Since biofilms occur on all surfaces, not only in the biofilter, but the idea also that removing the biofilm with sanitizers could be a possible solution. However, according to Schramm et al (2000), this could potentially eliminate beneficial nitrifying bacteria, which are essential to remove harmful build-up of ammonia. Some aspects of the system will need regular cleaning, depending on the system

design. Some areas of a RAS are more susceptible to "dead-zones", where a biofilm build up can get out of control. These zones are usually a result of bad circulation due to sharp corners or non-uniform water flow (Portz et al 2006) and will need further monitoring. An argument can be made that designing a RAS with a uniform flow in mind.

The removal of sulfate from inlet water is another approach. H_2S is seen mostly accumulating in RAS where inlet water has been partly or mainly seawater. Using freshwater would be beneficial since it is naturally low on sulfate, but it could prove to be difficult since access to freshwater is geographically restricted. However, a new solution of removing sulfate from seawater could be favourable. This would assure both low concentration of H_2S and easy access to inletwater, as saltwater is much more readily available than freshwater. This can be achieved by nanofiltration, a membrane separation process.

2 Nanofiltration

A membrane separation is defined as a thin sheet, film, or layer, which selectively separates components based on size or chemical attributes between two phases of either liquid, gas or vapor (Saleh, T. and Gupta, K. 2016). A typical membrane will have inlet for the compound that is getting separated (feed), an outlet for separated substance (permeate) and an outlet for the retained substance (retentate) showed in figure 2.1 (Droas, M. 2019).

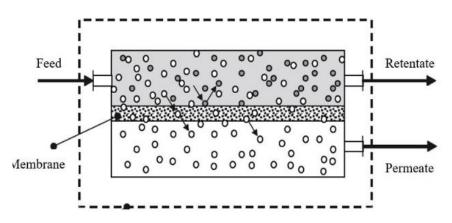


Figure 3.1 Graphical demonstration of the process behind general membrane separation (Graphics from: Droas, M. 2019)

Nanofiltration (NF) is the fourth class of pressure-driven membranes born after microfiltration (MF), ultrafiltration (UF) and reverse osmosis (RO) (Jye, L. and Ismail, A 2019). The different classes are defined by what kind of compounds they can separate based on size, chemical attribute, or operating pressure gradient, demonstrated in figure 3.2. There are three different

transport mechanisms at work in a NF membrane. Diffusion convection and electrostatic interactions. Diffusion is the transport of a compound between areas of high and low concentrations through a concentration gradient, convection is transport of a group of molecules through flow, and electrostatic interactions are movement caused by electrical charges. When selecting and designing a membrane separation process, all three of these transport mechanisms must be considered when choosing category and materials of the membrane.

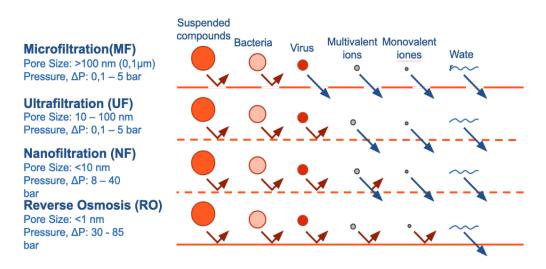


Figure 3.2 The four different classes of membrane separations, with pore sizes, operation pressures and an overview of types of compound that can be retained or separated. (Graphics provided by Akvafresh, 2020)

There are currently three main methods to synthesize NF membranes: (1) Poly amide thin film composite membrane (TFC), (2) single-step phase inversion and (3) layer-by-layer (LBL). An TFC synthesized membrane is an ultrathin selective poly amide (PA) layer, formed over the surface of a microporous support membrane. This creates what is known as a thin-film composite membrane (TFC). In brief, a microporous membrane made of either polysufone or polyethersulfone is treated with an amine monomer. This will start the formation of the PA layer, where the amine monomer is now fused to the top of the support membrane. The support is only there for mechanical strength, the separation is determined by the PA layer (Pinnau, I. 2000). The performance of the THC membrane, performance will vary with particle sizes, hydrophilicity, charge properties and pore channels of the materials used.

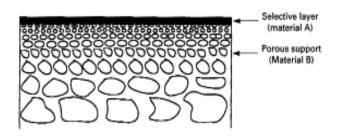


Figure 3.3 Representation of the selective PA layer and the microporous support layer of a thin film composite membrane. (Graphics from: Pinnau, I. 2000

The phase inversion method transforms a polymer solution from a liquid state to a solid state. This can be achieved several different ways. Immersion of polymer in bath of non-solvent, hot polymer solution casted over a chilled film, exposing the polymer to a vapour of a non-solvent, or evaporating a solvent from a polymer solution. The cheapest and therefore the most common option is the immersion method, demonstrated in figure 3.4.

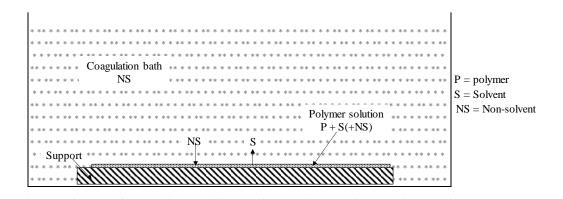


Figure 3.4 Preparation of NF membrane by immersion precipitation. (Graphics altered from: Jye, L. and Ismail, A. 2019).

The last method of preparation is LBL, where an alternating electrostatic absorption of cationic and anionic polyelectrolytes is applied to the surface of a porous supporting membrane. (Jye, L. and Ismail, A 2019). For each step the surface will absorb the polyelectrolyte (PE) and get a charge, and each layer will have alternating charges built up, leading to a PE complex stabilized by strong electrostatic forces, demonstrated in figure 3.5.

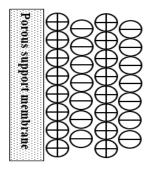


Figure 3.5 Demonstration of the electrostatic structure of LBL NF membranes. (Graphics altered from Jye, L. and Ismail, A 2019)

Two main materials are used for NF membranes in general, polymers and ceramics. Polyethylene, polyvinyl chloride, and polypropylene are generally sought after due to their low cost but are not ideal in conditions that are either high temperature or suscepted to high backwash pressure. Ceramic membranes are generally more thermally, mechanically, and chemically stable (Mulder,M. 1996), however they are more prone to breakage than polymeric membranes. There are many different materials suitable for a ceramic membrane, but the most common ones are aluminium oxide (Al₂O₃), titanium dioxide (TiO₂) and zirconium dioxide (ZrO₂).

There are in general two different modules for application of a NF membrane, the spiral wound (SW) and the hollow-fiber (HF) module (Rackley, S. 2018). A SF module consist of several membranes envelops surrounding a central collecting tube. Each envelope is built up by a feed spacer, the first membrane, a permeate spacer, the second membrane and finally the last feed spacer, sealing the envelope on three sides. This is demonstrated in figure 3.6.

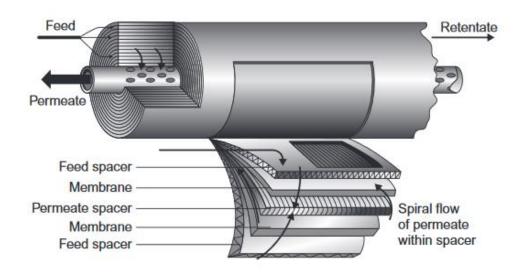


Figure 3.6 Configuration of a spiral-wound membrane. (Graphics from: Rackley.S 2008)

A HF module is built up by stacks of fibres in a closed pressure vessel, where permeate either passes out of the fibres or into them, demonstrated in figure 3.7. A HF module is more mechanically stable and is preferred under high pressure conditions.

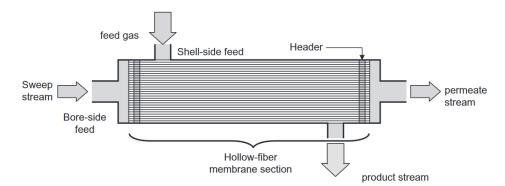


Figure 3.7 Configuration of a hollow fibre module. (Graphics from: Rackley.S. 2008)

Nanofiltration of seawater can give brackish water with different salinity and ion composition based on the choice of membrane material. This makes it an interesting technology for production of intake water for production of post smolt in RAS. As nanofiltration removes divalent ions to a larger extent than monovalent ions, the resulting ion composition is different than what is obtained by mixing seawater and freshwater to a given salinity. Sulfate, being a large and charged ion, can effectively be held back by a NF membrane. By removing sulfate from the intake water, the risk of developing H2S in RAS is lowered. Mixing seawater and freshwater can release toxic metals bound to organic matter in freshwater. This is avoided by producing the intake water with nanofiltration of seawater. In addition, nanofiltration is a good biological barrier, keeping unwanted bacteria and virus out of the RAS. This makes a NF membrane a viable solution to the H_2S problem. By choosing the right membrane material, synthesis and module, a NF membrane can be designed to remove sulfate and NaCl from saltwater, giving a RAS site a new inlet water that does not need to be mixed with freshwater to meet recommended water quality levels. This includes a sulfate concentration that is lower than that of brackish water.

4 Materials and experimental method

4.1 Setup of nanofiltering membrane at Sunndalsøra

A NF membrane supplied by Akvafresh was installed to desalinate saltwater feed in one RAS system at The Nofima Centre for Sustainable Aquaculture in Sunndalsøra. The membrane was a combination of two different polyamide spiral wound membranes, one with an open structure designed for high sulfate rejection and one with a denser structure aimed lower the final salinity to 12‰. Specific design parameters belong to Akvafresh and will not be disclosed.



Figure 4.1 Picture of the same type of NF membrane installed at Sunndalsøra. (Picture provided by Akvafresh)

From 11.03.30 until 10.06.03, samples were taken from 10 different locations at two different RAS sites. One with the installed NF membrane to desalinate seawater (RAS1), and one where inlet water was a combination of sea water and fresh water that served as a control (RAS2). A process flow diagram for each RAS is given in figure 4.2 and 4.3, with a summary of sample points and descriptions given in table 4.1.

Sampling point	Name	Decription/Comment			
RAS 1					
1	NF,in	Saltwater feed into NF membrane			
2	NF,out (1)	Permeate after NF membrane			
3	NF,out (2)	Permeate after NF membrane. Sampled to			
		investigate possible trace metals from a metal valve			
4	RAS1, Tank(A) Fish tank sidewall drain 1				
5	RAS1, Tank(B) Fish tank sidewall drain 2				
6	RAS1, Sump Sump				
RAS 2					
7	7 RAS2, Tank(C) Fish tank sidewall drain 3				
8	RAS2, Tank(D) Fish tank sidewall drain 4				
9	RAS2, Sump	Sump			
10	10 FW Makeup water into biofilter				

Table 4.1 An overview of each sampling point taken with name, description, and comment.

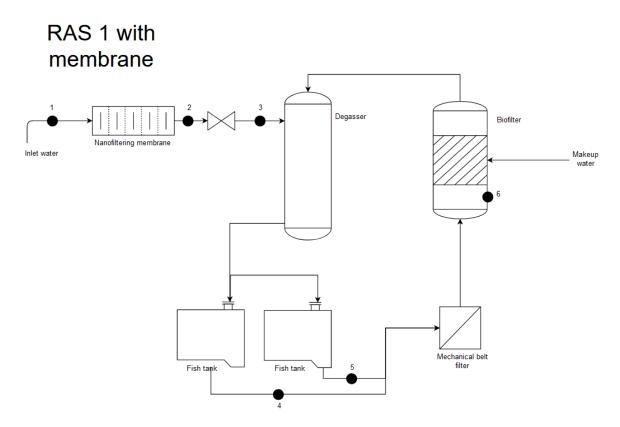


Figure 4.2 Process flow diagram for RAS 1 with sampling points 1-6

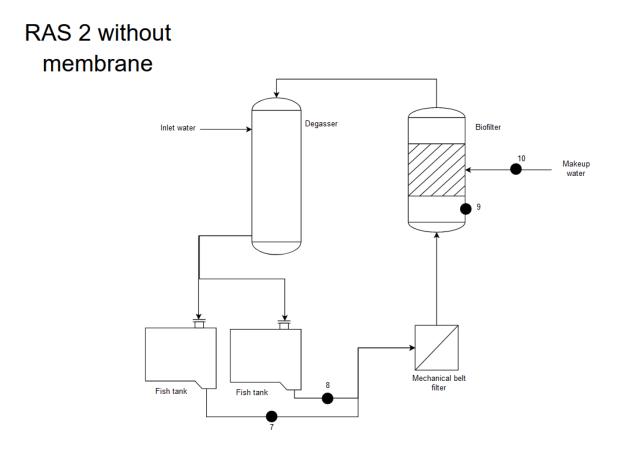


Figure 4.3 Process flow diagram for RAS 2 with sampling points 7-10

4.2 Sampling method

Each component used in the sampling process is listed in table 4.2. Sampling was done by May Britt Mørkedal at The Nofima Centre for Sustainable Aquaculture in Sunndalsøra.

For each sample point a large container was first cleaned with sample water three times, then filled and brought back to the laboratory. Here it was tested for pH, salinity, and conductivity with MultiLine 3620 IDS. Before distribution to centrifugal test tubes, the syringe and test tube were washed 3 times with water from sample point. Then, 15 mL of sample water was extracted with filter attached to the syringe. Filtrated sample water was then used to wash the test tube, making sure to close the lid and shake thoroughly before emptying the test tube. After washing the filter was detached and kept clean, and 30 mL sample water was taken. The filter was then reapplied, and 10 mL sample water was filtrated to two centrifugal test tubes, where one test tube received 3 drops of concentrated nitric acid. Test tubes treated with nitric acid where later used in ICP-MS analysis, and test tubes without were used in IC analysis. Lastly, another 30 mL sample water was extracted with the syringe and transferred to a glass test tube. These samples were used in UV-Vis analysis.

Equipment	
Syringe	Dispisable, two-piece without needle, PP barrel and PE
	piston. Product number WVR 613-2033
Syringe filter	PES membrane, 25 mm diameter, 0,2 µm pore size.
	Product number vWR 514-0074
Centrifugal test tube	Polypropylene, metal free, 15 mL.
Glass test tube	Prewashed and sertified, 40 mL borosilicate,
	polypropylene/PTFE/Silicone septa. cork. Phoenix
	product number 9-102-3
Concentrated nitric acid	Ultra pure grad; Pro Analyses destilled with Milestone
	SubPure

 Table 4.2 Overview of equipment used when sampling from RAS at The Nofima Centre for Sustainable Aquaculture in Sunndalsøra.

4.3 ICP-MS

Inductively coupled plasma mass spectrometry (ICP-MS) is a combination of an inductively couple's plasma (ICP) spectrometer and a mass spectrometer (MS), capable of detecting elements at a very low concentration below ppt (SeQuant 2007). The ICP converts the atom of the element into 2 ions, which are then detected by the MS. In short, the plasma is produced by heating argon gass with a radiofrequency generating coil to a high temperature (6000K - 10000K). The plasma decomposes the sample into 2 ions, which are then extracted and lead into the MS which separates the ions based on their mass/charge ratio (m/z). The intensity of the signal is directly proportional to the concentration of the sample element.

Determination of elemental composition was done by ICP-MS in two batches. The first was conducted by Syverin Lierhagen, with samples from 11.03.20 to 15.04.20 using Agilent 8900 triple quadrupole ICP-MS. The second was conducted by Anica Simic, with samples from 22.04.20 to 10.06.20 using Agilent 8800 triple quadrupole ICP-MS. In total, 27 elements were analyzed, with 7 elements chosen for further investigation by this thesis. The elements included are sulfur, magnesium, potassium, calcium, bromide, silicon, and strontium. Sulfur was chosen as it is the main point of investigation for this thesis. Magnesium, potassium, and calcium were selected as they play an important part in fish metabolism. High concentrations of chloride can interfere with ICP-MS and was therefore not analyzed. Bromide shares similar qualities and was chosen to give some insight to nanofiltration effects on chloride. Silicone was chosen due to the addition of silica compounds in RAS2 to reduce aluminum concentration. Lastly, strontium was chosen due to it being a major seawater ion.

4.4 IC

Ion chromatography separates mixtures into their component ions (Worden, R. 2005). This separation takes place on polymers with columns, where choice of column has a major impact on the results. Before getting injected into the main column, the mixture will pass through a guard column that contains similar materials as the main one. For separation to occur the mixture component needs to exist in a stationary phase and a mobile phase, where the mobile phase is the ionic solution that travel through the system at a constant rate and pressure. Since the mobile phase is conductive, a suppressor is needed to better see the response of low-level components, by removing high conductivity ions from the mobile phase and replacing them with low conductivity ions. To create a stable mobile phase, it is important to utilize an eluent

generator for consistent transportation of sample ions. A representation of the IC system is given in figure 4.4.

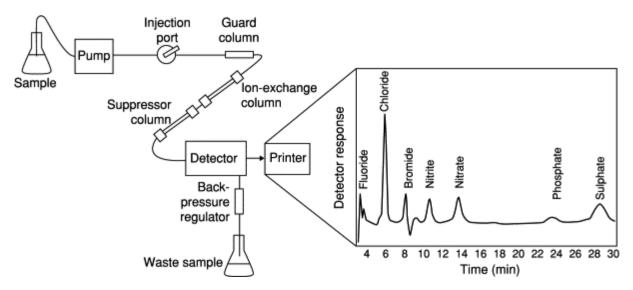


Figure 4.4 Essential components found in an ion chromatograph with a typical output graph. (Graphics from Worden, R. 2005)

Analysis by IC was done with a Methrom 940 Professional IC Vario, with a Metrohm Metrosep A Supp 7 – 250/4.0 column and 3,5 mM Na₂CO₃ used as anion eluent. Analysis was done at 45° C at a 0,700 mL/min flow, with certified calibration standards given in table 4.2. Samples from RAS1 was diluted 1:10, and RAS2 was diluted 1:50 due to high concentration of chlorine.

Table 4.3 An overview of standard solutions used to make a calibration curve for IC with product number listed for each ion.

IC Standards						
Ion	Product number					
Fluoride	77365-100 mL					
Bromide	43147-100 mL					
Nitrate	74246-100 mL					
Nitrite	67276-100 mL					
Phosphate	38364-100 mL					
Sulfate	90071-100 mL					

4.5 UV-Vis

Ultraviolet-visible spectroscopy (UV-vis) is the observation of the absorption of electromagnetic radiation in the UV and visible regions of the spectrum. (Atkins,P. 2010 p.228-229). It measured intensity of light passing through a sample (I) and compares it to the intensity of no sample (I₀). The ratio between these two (I/I₀) is called transmittance, and from transmittance you can calculate absorption (A) as $-\log(T)$. There is a linear relationship of light absorbed (A) and the concentration of substance of the sample (d), called the Lambert-Beer-Law, where absorbance is given in equation 4.1.

$$A = \mathcal{E} * c * d \tag{4.1}$$

Where \mathcal{E} is the molar absorption coefficient (M⁻¹cm⁻¹) unique for each sample and d is the optical path length (cm) of cuvette used in analysis. UV-vis can be a useful tool for measuring a number of organic compounds in a given sample. An increase of compounds with aromatic rings, hydroxyl groups or carboxylic acid, as well as an increase of conjugate double bonds will have increased absorption.

Shimadzu UV mini 1240 was used to measure absorbance at 254 nm with a 1cm quartz cuvette. The cuvette was washed prior to sample measurement with Milli-Q water, followed by a wash with sample solution to be analyzed.

4.6 Statistics

4.6.1 Averages

To better compare treated water (RAS1) to control (RAS2), averages were made from 3 different sample points from each system, where RAS1 is given in equation 4.2 and RAS2 is given in equation 4.3.

$$RAS1 = \frac{RAS1, Tank(A) + RAS1, Tank(B) + RAS1, Sump}{3}$$
(4.2)

$$RAS1 = \frac{RAS2,Tank(C) + RAS2,Tank(D) + RAS2,Sump}{3}$$
(4.3)

4.6.2 Standard deviation

Standard deviation was calculated using equation 4.4, to better describe the variation of the dataset.

$$\sigma = \sqrt{\frac{1}{n-1} \sum_{i=1}^{n} (X_i - \bar{X})^2}$$
(4.4)

where σ is the standard deviation, n is the number of samples and X is the sample value.

4.6.3 Mann-Whitney-U test

The Mann-Whitney-U test is a version of the independent samples t-Test, that can be performed on ranked or ordinal data (Ruxton). This test will compare the mean of the two populations, and the null hypothesis states that the probability is 50% that a randomly drawn member from the first population will have a higher rank than a member from the other population. This is done by first assigning each value a rank based on value. The highest value is rank 1, the second highest rank 2 and so on. U value is then calculated from equation 4.5.

$$U = \sum_{i=1}^{n} \sum_{j=1}^{m} S(X_i Y_i)$$
(4.5)

Where S is 1 if Y<X, $\frac{1}{2}$ if Y=X and 0 if Y>x. Calculated U is then compared to critical value, and null hypothesis is rejected if U<U_{crit}.

Assumptions made prior to performing Mann-Whitney-U are as follows:

- 1. Samples are of one dependent variable measured at the continuous level.
- 2. Samples consists of two categorical, independent groups
- 3. There is no relationship between observed effect between the groups
- 4. Samples are not normally distributed
- 5. The overall distribution of the samples follows the same general shape

5 Results and discussion

This chapter summarizes and presents the results from all conducted experiments, to investigate the effect of the nanofiltration membrane. Investigations on the relationship between feed and permeate and between treated water and control was done for each parameter. A summary of the results is given in table 5.1. Each parameter will be discussed further in their own separate section. Sample points discussed in this chapter are *NF*,*in* (feed), *NF*,*out* (permeate), *RAS1*(treated water) and *RAS2*(control).

Table 5.1 Summary of each measured parameter with calculated difference presented in associated units and in percentage, between feed and permeate and between treated water and control.

Parameter			Difference	%	Mean		Difference
	Feed	Permeate			RAS1	RAS2	
pН	7,940	8,060	0,120	1,511 %	7,71	7,680	-0,030
Salinity (‰)	32,210	12,840	-19,370	-60,137 %	12,07	11,970	-0,100
Conductivity (mS/cm)	49,800	21,500	-28,300	-56,827 %	12,07	20,390	8,320
S (mg/L)	857,310	56,850	-800,460	-93,369 %	26,55	308,500	281,950
SO4(2-) (mg/L)	-	-			30,14	212,980	182,840
Mg+ (mg/L)	119,980	338,500	218,520	182,130 %	269,68	293,980	24,300
Ca2+ (mg/L)	398,550	126,400	-272,150	-68,285 %	95,93	141,200	45,270
K+ (mg/L)	318,670	157,990	-160,680	-50,422 %	125,29	118,250	-7,040
Br- (mg/L)	69,520	30,580	-38,940	-56,013 %	27,13	23,970	-3,160
Si4+ (mg/L)	0,160	0,100	-0,060	-37,500 %	0,14	4,300	4,160
Sr- (mg/L)	7,375	2,170	-5,205	-70,576 %	0,169	2,568	2,399
Absorbance	0,023	0,017	-0,006	-26,087 %	0,051	0,049	-0,002

5.1 The effects of nanofiltering membrane on pH, salinity, and conductivity

Descriptive values for pH, salinity and conductivity are given in table 5.2, with results from test of significance given in table 5.3 and all measured values are given in appendix A.1. Comparing permeate and feed there is a significant difference in all three parameters. However, this is not the case when comparing treated water with control, where none of the parameters was proven to be significantly different. Therefore, this section is further divided to discuss each individual parameter.

	Sample					Standard
	point	Average	Median	Min	Max	deviation
pН	NF, in	7,945	7,938	7,872	8,046	0,043
	NF, out	8,057	8,061	7,918	8,131	0,052
	RAS1	7,706	7,680	7,373	7,942	0,150
	RAS2	7,680	7,706	7,275	7,876	0,124
Salinity [%]	NF, in	32,208	33,800	12,900	34,200	5,579
	NF, out	12,842	12,000	10,300	33,800	4,236
	RAS1	12,067	12,100	11,300	12,800	0,383
	RAS2	11,972	12,000	11,300	12,700	0,386
Conductivity	NF, in	49,800	52,250	21,800	53,000	8,450
[mS/cm]	NF, out	21,497	20,500	13,330	52,200	6,623
	RAS1	12,067	20,450	0,021	21,600	3,334
	RAS2	20,387	20,350	19,270	21,500	0,610

Table 5.2 Descriptive values of pH, salinity and conductivity for NF, in, NF, out, RAS1 and RAS2

Table 5.3 An investigation to determine if there was a significant difference of pH, salinity or conductivity before and after the nanofilter (*NF*,*in*/*NF*,*out*) and between treated and untreated water in RAS phase (*RAS1/RAS2*). A Mann-Whitney-U test with null hypothesis H₀: $P(x_i>y_j) = 0,5$ versus alternative hypothesis H₁: $P(x_i>y_j) \neq 0,5$ was used.

Parameter	Sample point	Mann-whitney U	Z-value	P-value	Reject Ho
pH	Nf,in/Nf,out	17,000	-3,463	0,001	Yes
	RAS1/RAS2	689,500	-0,710	0,478	No
Salnity	Nf,in/Nf,out	8,000	-3,937	0,000	Yes
	RAS1/RAS2	640,500	-1,208	0,227	No
Conductivity	v Nf,in/Nf,out	7,000	-3,767	0,000	Yes
	RAS1/RAS2	661,000	-0,636	0,525	No

5.1.1 pH

Figure 5.1 demonstrates the differences in pH for feed, permeate, treated water and control. A box plot was generated to inspect the distribution further. Data shows a difference in averages of feed and permeate of 0,112. It is a small but significant increase and puts pH above recommended levels of 6,2-7,8. One possible reason for this increase could be the nanofilter retained a small amount of bicarbonate (HCO₃⁻) and carbonate (CO₃²⁻). As discussed earlier in section 3, the design of the nanofilter can allow for a partial diffusion of some multivalent ions, depending on size on charge. This small increase is only temporary, as there was no significant difference in pH between treated water and control throughout the experiment.

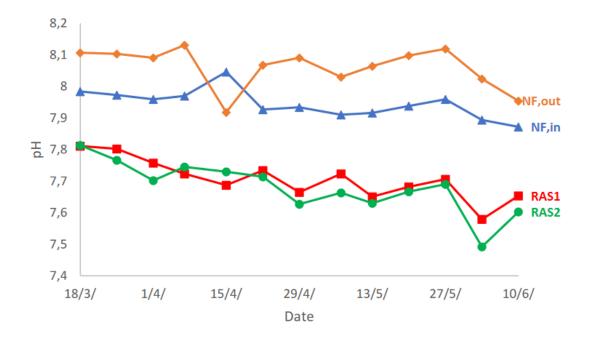


Figure 5.1 Measured pH of feed(*NF*,*in*), permeate(*NF*,*out*), treated water(*RAS1*) and control(*RAS2*) plotted for each sampling date.

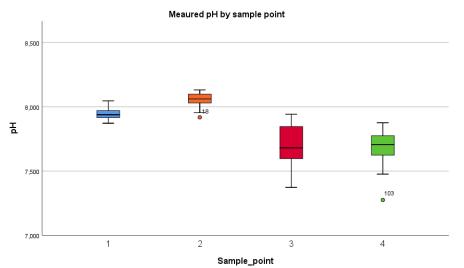


Figure 5.2 Box plot of measured pH, where sample points 1-4 represents feed(*NF*,*in*), permeate(*NF*,*out*), treated water(*RAS1*) and control(*RAS2*) respectively.

5.1.2 Salinity and conductivity

Figure 5.3 and 5.4 demonstrates the differences in salinity and conductivity for feed, permeate, treated water and control. Box plots were generated to inspect the distribution further. As with pH, there was a significant difference between both salinity and conductivity levels of feed compared to permeate. This is to be expected, as the nanofilter can be designed to retain ions of certain size and charge. A decrease in salinity points to a decrease in ions such as Mg^{2+} , Ca^{2+} , K^+ and SO_4^{2-} , which would also decrease conductivity due to the lack of charged ions. This will be investigated further in the results from the IC-PMS and IC analysis. When comparing treated water to control there is no significant difference, which means the treated water will achieve the same water quality standard as the currently used brackish water.

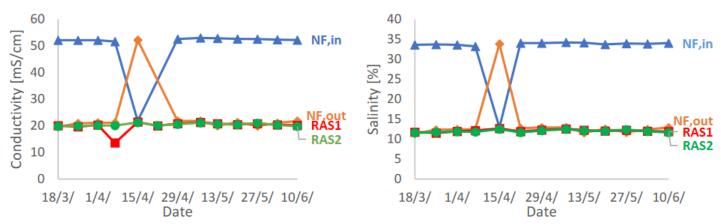


Figure 5.3 and 5.4 Measured conductivity (left) and salinity (right) for feed(*NF*,*in*), permeate(*NF*,*out*), treated water(*RAS1*) and control(*RAS2*) plotted for each sampling date.

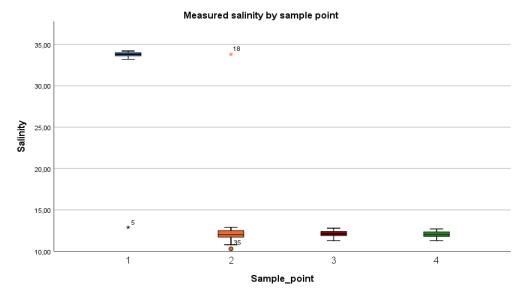


Figure 5.5 Box plot of salinity of feed(1), permeate(2), treated water(3) and control(4).

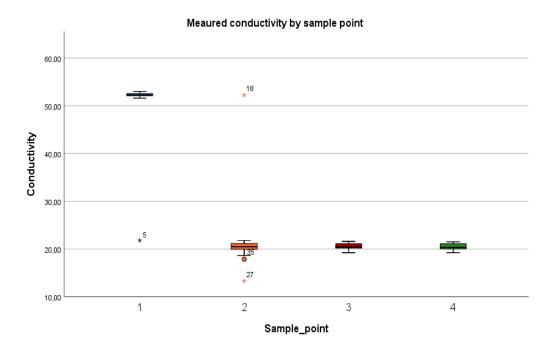


Figure 5.6 Box plot of conductivity of feed(*1*), permeate(2), treated water(*3*) and control(*4*).

5.2 Effect of nanofiltering membrane on elemental composition

Determination of elemental composition was done by ICP-MS. In total, 27 elements were analyzed, with 7 elements chosen for further investigation by this thesis. The elements included are sulfur, magnesium, potassium, calcium, bromide, silicon, and strontium.

5.2.1 Efficiency on sulfur removal measured by ICP-MS and IC

Reduction of sulfur was the main point of interest. As discussed in section 2.1.3, reducing total sulfur content will limit accumulation of harmful H_2S , and was one of the key design aspects of the nanofiltering membrane. Elemental composition data from ICP-MS analysis is visualized in figure 5.7 with data given in appendix A.2, together a generated box plot shown in figures 5.8 with accompanying descriptive values given in table 5.4 and statistical parameters given in table 5.5. In both point of comparison there was a significant decrease in sulfur, with a 93% reduction of average from feed to permeate, and a 91% reduction between the average of treated water and control, implying that the specific nanofilter design is working as intended. When observing the box plots, there are two points of interest. *NF,in* and *NF,out* again seem to line up better with their counterparts, observable both in the figure and at outliers in the box plot.

There is also a high standard deviation for *NF*,*in*, *NF*,*out* and RAS2. Measured concentration of sulfur is not approximating a linear trend, having higher values between 22.04.20 before it evens out after 27.05.20. It follows that all subsequent sample points experience the same rise in value, since they are all part of an almost closed loop system with *NF*,*in* as inlet water.

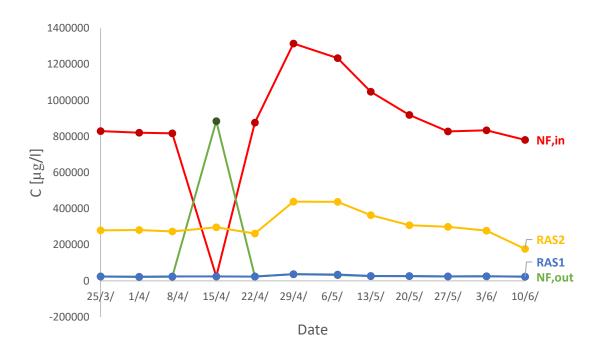


Figure 5.7 Measured sulfur concentration [µg/l] for *NF*,*in*, *NF*,*out*, *RAS1* and *RAS2* from 11.03.20 until 10.06.20, found by ICP-MS.

Table 5.4 Descriptive values of elemental sulfur concentration determined by ICP-MS $[\mu/L]$ for
NF, in, NF, out, RAS1 and RAS2.

Sample					Standard
point	Average	Median	Min	Max	deviation
NF, in	857 313,26	831 792,81	24 369,73	1 314 804,22	280 015,85
NF, out	56 851,39	23 473,44	19 432,89	884 867,28	162 437,51
RAS1	26 554,83	24 586,29	16 859,89	39 823,53	5 363,53
RAS2	308 498,41	282 085,68	252 342,05	460 536,91	61 581,16

Table 5.5 An investigation to determine if there was a significant difference in concentration of elemental sulfur before and after the nanofilter (*NF*,*in/NF*,*out*) and between treated and untreated water in RAS phase (*RAS1/RAS2*). A Mann-Whitney-U test with null hypothesis H₀: $P(x_i>y_j) = 0.5$ versus alternative hypothesis H₁: $P(x_i>y_j) \neq 0.5$ was used.

Sample point M	lann-whitne y U	Z-value	P-value	Reject Ho
Nf,in/Nf,out	16,000	-3,768	0,000	Yes
RAS1/RAS2	16,000	-7,842	0,000	Yes

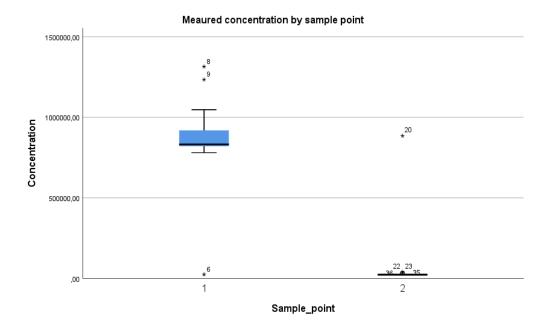


Figure 5.8 Box plot of elemental sulfur concentration of feed(*1*) and permeate(2)

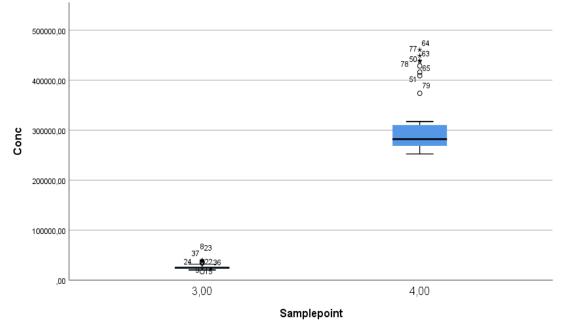


Figure 5.9 Box plot of elemental sulfur concentration of treated water(*3*) and control(*4*).

As discussed in section 2.1.3 sulfur found in seawater is present as different compounds. An IC analysis was done to investigate the percentage of sulfur compound present as sulfate. Results from this analysis is represented graphically in figure 5.10 with values in appendix A.3 where measured sulfate has been divided by 3 to convert to sulfur mass (Fang et al. 2015) and compared to ICP-MS data. A box plot was generated to further investigate distribution of data, with descriptive statistical values given in table 5.6. To further investigate the relationships between IC and ICP-MS data, tests of significance were performed on three levels; (1) Between *RAS1* and *RAS2* measured by IC, (2) between *RAS1* measured by IC and ICP-MS and (3) between *RAS2* measured by IC and ICP-MS, with values in table 5.7.

Results from IC analysis was highly volatile, with a range of 447,29 mg/L for *RAS1* and 2385 mg/L for *RAS2*. High concentration of chloride is known to be challenging in IC analysis (Anes et al. 2019) and may have interfered with the IC quantification of sulfate. This highly suggests that there was an issue with dilution, where samples were not diluted to the extent required to limit interference. There is however an observable trend, where there is a significant difference between *RAS1* and *RAS2*. This mirrors the results from the ICP-MS analysis, providing further support that nanofiltration was efficient at removing sulfate.

36

It is expected that the elemental sulfur found in the samples is mainly sulfate. As discussed in section 2.1.3 H_2S will only occur in the anaerobic layer of the biofilm if it has access to sulfate, and with the overall sulfate reduction the connected H_2S concentration can also be expected to be low. This would be further proved by comparing elemental concentration to ion concentration, but there was found no significant difference between the two and therefore no definitive conclusion can be made on H_2S concentration in the RAS site.

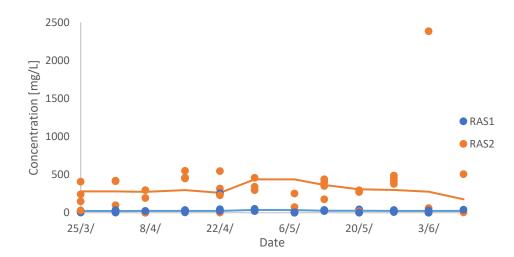


Figure 5.10 Concentration of sulfate measured by IC and converted to sulfur for each sample date, compared to ICP-MS measured sulfur concentration represented as lines.

Table 5.6 Descriptive values of elemental sulfur concentration [mg/L] for <i>RAS1</i> and <i>RAS2</i> measured
by IC.

Sample point	Average	Median	Min	Max	Standard deviation
RAS1	28,65	25,21	0,64	258,13	39,61
RAS2	317,88	297,59	0,14	2 385,47	364,88

Table 5.7 An investigation to determine if there was a significant difference in concentration of sulfur between treated and untreated water in RAS phase (*RAS1/RAS2*) measured by IC, and if there was a significant difference between sulfur measured by ICP-MS and sulfur measured by IC. A Mann-

Test	Mann-whitney U	Z-value	P-value	Reject Ho
RAS1/RAS2	350,000	-4,962	0,000	Yes
IC				
RAS1/RAS1	794,000	-1,127	0,260	No
IC/ICP-MS				
RAS2/RAS2	909,500	-0,130	0,897	No
IC/ICPMS				

Whitney-U test with null hypothesis H_0 : $P(x_i>y_j) = 0,5$ versus alternative hypothesis H_1 : $P(x_i>y_j) \neq 0,5$ was used.

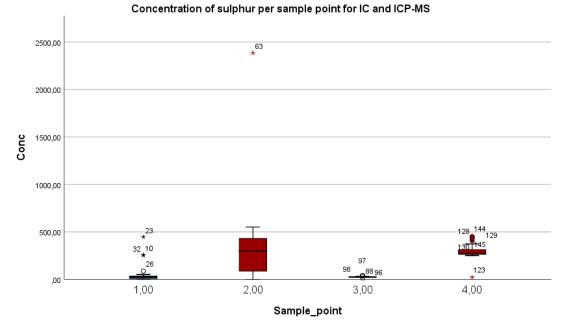


Figure 5.11 Box plot comparing distribution of sulfur measured by ICP-MS (1,3) and measured by IC (2,4)

5.2.2 Other ions of importance

Results from ICP-MS analysis for magnesium, silicone, potassium, calcium, bromide, and strontium is given in figure 5.12, with a summary of important calculated data given in table 5.7.

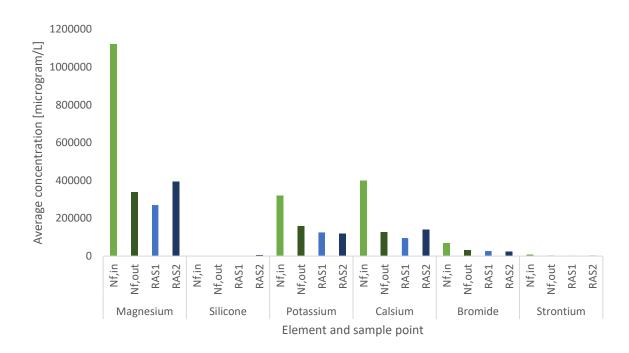


Figure 5.12 A comparison of average elemental concentration for magnesium, silicone, potassium, calsium, bromide and strontium for each sample point

Table 5.8 Calculated	differences o	of Mg, Si,	K, Ca	, Br and SF	R between	NFin/NFout and	RAS1/RAS2,
with significance.							

Element				Aver	ages (m	icrogram/	L]		
	Nf,in	Nf,out	Diff	р		RAS1	RAS2	Diff	р
Mg	1 119 975,385	338 495,357	69,	78 %	0,000	269 680,829	392 977,279	-45,72 %	0,000
Si	156,571	96,214	38,	55 %	0,006	137,046	4 304,506	-3040,91 %	0,000
к	318 667,237	157 989,286	50,4	42 %	0,011	125 286,404	118 249,977	5,62 %	0,053
Ca	398 551,093	126 398,362	68,2	29 %	0,000	95 932,881	141 204,582	-47,19 %	0,000
Br	69 519,866	30 583,869	56,	01%	0,000	27 128,016	23 966,663	11,65 %	0,000
Sr	7 374,622	2 170,228	70,	57 %	0,000	1 689,781	2 568,321	-51,99 %	0,000

Before nanofilter, magnesium levels were found to be the highest out of the selected ions, and amount decreased in the order of Ca, K, Br, Sr, and Si respectively. This fits with expected values presented in section 2.1.2. All ions investigated had a significant decrease after nanofiltration.

When comparing treated water to control a few things are apparent. There is a higher concentration of magnesium, silicone, calcium, and strontium in control, where inlet water is a mixture between saltwater and seawater. As discussed earlier, Mg, Ca and Sr are all major ions of seawater, and to achieve lower concentrations of these ions require further dilution with freshwater, which might not be ideal when considering other water quality parameters. Silicon is much higher in RAS2 than in RAS1. When looking at data from Appendix A.2, freshwater (FW) samples have a very high concentration of silicon compared to other sampling points. This is caused by the addition of silica-compounds to inlet freshwater to reduce the harmful effects of aluminum compounds.

Bromine and potassium had higher concentrations in RAS 1. Increase in potassium was not significant, and it is likely that treated water will have the same concentration of potassium as untreated water. A higher bromine concentration is caused by filtration, where the nanofilter did not reduce bromine enough to be equal to that of brackish water. This could however provide some insight to overall concentration of chlorine. Chlorine was excluded from analysis by ICP-MS, due to the high concentration it has in seawater and the potential to cause interference with other measurements, but since chlorine and bromine share similar qualities as monovalent ions, it can be assumed that the NF membrane will reduce Cl to a similar extent.

The effect of this change in ion composition was not studied, therefore it is not known what kind of effect this will have on fish welfare. As discussed in section 2.1.2, magnesium, calcium and potassium all play important parts in fish metabolism. Since magnesium and calcium had an overall decrease this could effect the overall fitness of the fish, but it is unknown if this effect would prove to be harmful over time. There was found an increase of potassium almost at a 5% level of significance, but here it is also unknown if this effect would prove to be either beneficial or harmful to the fish.

5.3 UV-vis

UV-vis analysis was performed to investigate if nanofiltration had an impact on accumulation of organic matter. Measured values and calculations are given in appendix A.4.

There was an average reduction of 28% percent absorbance in desalinated water, indicating that larger organic compounds did not permeate the membrane. No significant difference was found between RAS1 and RAS2. Data from test of significance is given in table 5.8. There was an overall increase in absorbance for all datapoints, demonstrated in figure 5.13

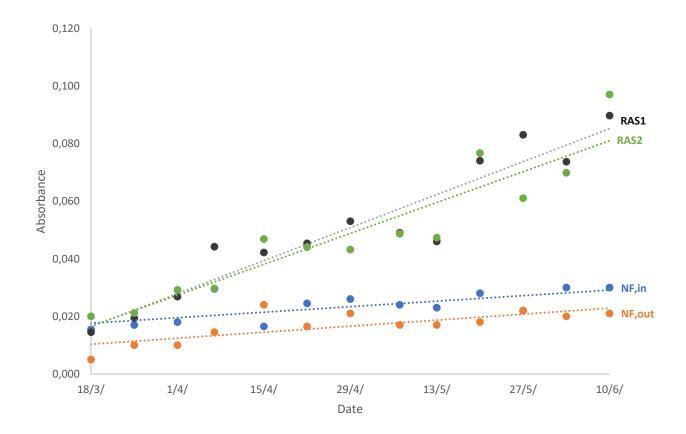


Figure 5.13 Measured absorbance plottet against each date for NF, in, NF, out, RAS1 and RAS2.

All points of measurement has an linear increase in absorbance over time, a smaller one for NF, in and NF, out, and a quite substantial one for RAS1 and RAS2. In total, 130 samples were analyzed using the same quartz cuvette, and contamination seems likely to be the cause of this increase, but this would not explain the difference in rate of increase between all four sample points. If contamination was the only issue, one would expect that increase of absorption would happen at the same rate for all sample points. However, RAS1 and RAS2 increase at a much

higher rate. One possible explanation of this is fish waste. Throughout the experiment salmon lived in the tanks, consuming feed, and excreting waste. Over time it is expected that particle waste in fish tanks will increase overall, making it likely that the steady increase of absorbance is due to fish waste and uneaten fish food.

Table 5.9 Descriptive values of measured absorbance for NF, in, NF, out, RAS1 and RAS2

Sample point	Average	Median	Min	Max	Standard de viation
NF, in	0,023	0,024	0,016	0,030	0,005
NF, out	0,017	0,017	0,005	0,022	0,005
RAS1	0,051	0,049	0,015	0,090	0,024
RAS2	0,049	0,050	0,020	0,097	0,022

Table 5.10 An investigation to determine if there was a significant difference in absorption between treated and untreated water in RAS phase (*RAS1/RAS2*) measured by UV-VIS. A Mann-Whitney-U test with null hypothesis H_0 : $P(x_i>y_j) = 0.5$ versus alternative hypothesis H_1 : $P(x_i>y_j) \neq 0.5$ was used.

Sample point	Mann-whitne y U	Z-value	P-value	Reject Ho
Nf,in/Nf,out	33,000	-2,646	0,007	Yes
RAS1/RAS2	701,000	-0,595	0,552	No

5.3.1 Outliers

At 15.04.20 there is two points of interest, where it appears that values of *NF*, *in* and *NF*, *out* has a better fit within their counterpart's dataset than within their own. This trend of outliers is consistent in all points of measurements, making it likely that an error with labelling of samples has occurred. The outliers will therefore have an effect on statistical parameters, making it likely that means, medians, minimum values, maximum values and standard deviations are skewed for *NF*, *in* and *NF*, *out* and that measured significance between the two sample points is somewhat lower.

5.4 Further work

This thesis could only focus on a select few ions, and there are many elements left to investigate. Since there was a difference in elemental composition between the treated water and the untreated water, it would be interesting to see what kind of long term effects this would have on fish welfare, growth and survivability.

More testing is needed with IC. Current dataset does not give a conclusive answer to the relationship between sulfate and elemental sulfur measured by ICP-MS and would be an important parameter to figure out for future investigation on sulfurs behavior in RAS. For a future analysis of samples with IC, a higher dilution is recommended.

There is a method that directly measures H_2S concentration (Langeteig, S. 2019), by utilizing the Diffusive Gradients in Thin films (DGT) instrument. Access to directly measured H_2S would provide a great benefit into the investigation on desalination of water, by giving a more detailed and accurate description of the sulfur equilibrium.

Since this thesis only performed a UV-Vis analysis, there can only be made general assumption on the concentration of organic compounds. A future research with a TOC and DOC analysis could be interesting, as it could give a more detailed picture on the specific parameters of the nanofiltering membrane and its effect on different organic compounds.

It will be interesting going forward what will be the optimal solution to the H_2S problem. This thesis has not taken cost into consideration, and there is therefore no final conclusion to be made on what is the optimal solution. Using a nanofiltering membrane has been proved to be an adequate alternative, but there is yet to be done a cost analysis comparing nanofiltration to optimizing tank design or adding nitrate to keep a healthy biofilm.

6 Conclusion

Desalination of saltwater proved to be an effective method for removal of sulfate, removing 93% of all sulfur compounds. When comparing treated water against control, treated water had on average 91 % less sulfur and 86 % less sulfate. In theory, this would lead to a drastic reduction in the amount of H₂S produced making desalination with nanofiltration a very viable alternative in RAS. The nanofiltering membrane did decrease the pH, salinity, and conductivity of the inlet, but there was no significant difference when compared to control, providing further evidence that this treatment method will not have any harmful effects on water quality.

Nanofiltered feed water had a reduction in magnesium, silicone, potassium, calcium, bromide, and strontium in inlet water. When comparing treated water to control there was an increase of bromide, and a reduction of magnesium, silicone, calcium, and strontium. It is not known wether or not this will influence fish welfare, growth, or survivability in the long term.

There was found to be a reduction in organic compounds between feed and permeate water, but no significant difference between treated water and control. The latter two had a steep increase over time compared to the prior two. This is likely due to the natural growth cycle of the fish, where they produce more particle waste as they grow.

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Appendix

A.1 All measurements of pH, salinity and conductivity

Table A.1.1 Water quality parameters pH, salinity and conductivity measurements for each sample point and date.

Date	Sample point	pН	Salinity %	Cond. [mS/sm]	Date	Sample point	pН	Salinity %	Cond. [mS/sm]
18.03.2020	RAS1(A)	7,809	11,9		18.03.2020	RAS1 sump	7,857	11,9	
25.03.2020		7,802	11,3		25.03.2020		7,925		
01.04.2020		7,792	12	,	01.04.2020		7,892		
07.04.2020		7,66		21,1 µS/cm	07.04.2020		7,83		
15.04.2020		7,581	12,7	21,5	15.04.2020		7,84		
22.04.2020		7,72	12,1	20,6	22.04.2020		7,849	12,1	
29.04.2020		7,643	12,5		29.04.2020		7,851	12,4	
07.05.2020		7,76	12,6	21,4	07.05.2020		7,89	12,6	21,3
13.05.2020		7,605	12,3	21	13.05.2020		7,843	12,3	21
20.05.2020		7,606	12	20,5	20.05.2020		7,942	12,1	20,5
27.05.2020		7,628	12,1	20,6	27.05.2020		7,935	12,1	20,6
03.06.2020		7,515	12	20,4	03.06.2020		7,849	12	20,4
10.06.2020		7,618	12,1	20,5	10.06.2020		7,855	12,1	20,5
18.03.2020	RAS1(B)	7,768	11,4	19,55	18.03.2020	RAS2 sump	7,775	11,4	19,56
25.03.2020		7,68	11,9	20,3	25.03.2020		7,803	11,9	20,3
01.04.2020		7,589	11,8	20	01.04.2020		7,71	11,8	20
07.04.2020		7,68	11,5	19,55	07.04.2020		7,812	11,5	19,56
15.04.2020		7,64	12,5	21,1	15.04.2020		7,779	12,4	21,1
22.04.2020		7,632	11,4	19,4	22.04.2020		7,775	11,4	
29.04.2020		7,501	11,9	20,2	29.04.2020		7,7	11,9	20,2
07.05.2020		7,52	12,4	21,1	07.05.2020		7,71	12,4	
13.05.2020		7,504	12		13.05.2020		7,749	12	
20.05.2020		7,497	11,9		20.05.2020		7,841	11,9	
27.05.2020		7,555	12,5		27.05.2020		7,876		1
03.06.2020		7,373	11,9		03.06.2020		7,68		
10.06.2020		7,487	11,4		10.06.2020		7,712	11,4	
18.03.2020	RAS2(C)	7,868	11,9		18.03.2020	FW	7,088		
25.03.2020	10.02(0)	7,815	11,3	19,27	25.03.2020		7,142	0,1	
01.04.2020		7,802	11,3	20,3	01.04.2020		7,077	0,1	
07.04.2020		7,718	12,4		07.04.2020		7,344		
15.04.2020		7,718	12,4	21,1	15.04.2020		7,437	0,1	
22.04.2020		7,713	12,7		22.04.2020		7,437		
29.04.2020		7,698	12,1		29.04.2020		7,082	0,1	
07.05.2020		7,038	12,5		07.05.2020		7,002	0,1	
13.05.2020		7,627			13.05.2020				
20.05.2020		7,627	12,3 12	20,5			7,257	0,1	
					20.05.2020		7,317	0,1	
27.05.2020		7,63	12,1	20,6	27.05.2020		7,301	0	
03.06.2020		7,521	12		03.06.2020		7,25		1.7
10.06.2020	DA (2(D)	7,62	12,1	20,5	10.06.2020		7,94		
18.03.2020	RAS2(D)	7,798	11,4		18.03.2020	Nf,in	7,984		
25.03.2020		7,681	11,9		25.03.2020		7,973		
01.04.2020		7,594	11,8		01.04.2020		7,959	33,6	
07.04.2020		7,706	11,5		07.04.2020		7,97	33,2	
15.04.2020		7,692			15.04.2020		8,046		
22.04.2020		7,654	11,4		22.04.2020		7,927		
29.04.2020		7,484	11,9		29.04.2020		7,934		
07.05.2020		7,54	12,4		07.05.2020		7,91		
13.05.2020		7,514	12		13.05.2020		7,916		1
20.05.2020		7,513	12	20,4	20.05.2020		7,938	33,7	52,6
27.05.2020		7,565	12,5	21,2	27.05.2020		7,959	33,9	52,5
03.06.2020		7,275	11,9	20,2	03.06.2020		7,894	33,8	52,3
10.06.2020		7,476	11,4	19,45	10.06.2020		7,872	34	52,2
18.03.2020	Nf,out(2)	8,058	11,3	13,33	18.03.2020	Nf,out(1)	8,107	11,4	19,61
25.03.2020		8,101	11,9	20,3	25.03.2020		8,103	12,3	20,9
01.04.2020		8,098	12	20,5	01.04.2020		8,091	12,4	21,1
07.04.2020		8,121	12	20,5	07.04.2020		8,131	12,4	21,1
15.04.2020		8,039	12,2	20,8	15.04.2020		7,918	33,8	52,2
22.04.2020		8,054	11,9		22.04.2020		8,068	12,7	
29.04.2020		8,011	11,7		29.04.2020		8,091	12,9	
07.05.2020		8,04	12,5		07.05.2020		8,03		
13.05.2020		8,035	10,3		13.05.2020		8,064		
20.05.2020		8,043	11,9		20.05.2020		8,098		
27.05.2020		8,088	10,8		27.05.2020		8,119		
03.06.2020		8,01	11,6	19,83	03.06.2020		8,024	12,4	2:

48

A.2 Measurements done by ICP-MS for magnesium, silicone, sulfur, potassium, calsium, bromide and strontium

	RAS2,Tank(D)	3/5 339	340/90	100 661	365 061	394 259	355 430		530 521	442 955	424 466	391 678	387 860	334 047		RAS2.Tank(D)	117 622	109 045	119 049	119 698	117 464	127 605	117 976					ı				RAS2,Tank(D)	23 483	22 087	23 162	23 046	22 224	24 134	900 77	- 26 0.02	20 242	20 505	24 772	23 553	21 474															
	RAS2,Tank(C)	3/5 U3U	240 045	1VC COC	373 925	397 109	346 882	526 030	554 549	484 469	435 470	407 734	353 609	325 830		RAS2.Tank(C) RAS2.Tank(D)	116.675	108 517	118 364	120 022	118 575	128 838	114 402									RAS2,Tank(C)	23 158	21 823	23 061	108 22	22 629	24 184	242 12	20 034	COL 02	5/0 TC	25 530	23 647	21 880															
	ŝ	3// 382	280 776	2010.040	362 100	393 068	340 779	501 468	489 679	421 215	384 993	366 505	362 924	213 369			2	112 133	119 562	123 380	116 753	127 742	113 057										22 930	22 302	23 450	23 805	22 253	24 556	21 615 75 616	016 CC	6TC / 7	73 592	24 478	22 475	25 684															
	RAS1, Tank(A) RAS1, Tank(B) RAS2, Sump	22/340	ACC 122	24E 141	268.082	273 469	243 958	376 445	374 742	306 826	277 248	251 079	250 805	233 564		BAS1 Tank(A) BAS1 Tank(B) BAS2 Sump	120 702	120.815	118 565	128 873	138 967	137 558	128 289					,				RAS1, Tank(B) RAS2, Sump	25 304	26 395	25 272	20 023	28 3/4	28 446	26 046	30.842	176 76	22/ 62	27 781	26 194	25 449															
	AS1,Tank(A)	1// 848 774 774	15/ 122	224 000	259 064	270 861	250 414	368 351	352 076	364 080	328 511	285 483	255 364	233 532		AS1.Tank(A)	93 870	120 112	120 555	127 759	131 651	138 119	130 299									RAS1,Tank(A)	19 700	25 758	25 28/	25 25 77 27	2/ 2/2	28 315	26 / 35	30 322	01 940 LC	200 20	27 950	26 922	26 165															
	50	231 861	763716	17C / TZ	257 799	259 917	242 987	376 355	332 831	289 136	255 304	229 186	228 842	242 484	point	8	681		119 229	129 264	133 448	132 825	128 417		-			,				đ	26 933	26 162	25 481	20 833	2/ 421	27 720	26 359	70/ 12	37.1.90	27.165	26 076	25 975	27 052															
Ē		102 127	763716	201 100	257 799	259 917	242 987	376 355	332 831	289 136	255 304	229 186	228 842	242 484	Concentration [microgram/L] per Sample point	VE.out(2) R/			124 686	127 473	124 008	125 060	123 524								Concentration [microgram/L] per Sample point	NF,out(2) R/	24 565	-	26 824 26 FF4	155 92	26 632	26 575	26 2/4	23 003	DET DC	26 800	23 564	25 605	25 443															
[microgram		660.052	258 213	4TH 007	270 985	1 180 276	261 716	379 493	365 278	285 590	266 401	226 379	262 643	222 025	Imicroeram	NF_out(1) NF_out(2)	120346	120 732 -	128 444	127 970	126 882	356 887	124 664	-							[microgram,	NF,out(1)	25 821	25 413	2/ 40/	2/ 340	2/ 065	71 533	20.070	30.970		28 130	25 845	27 912	26 557															
oncentration	NF,in N	1 1 7 7 0 4 C	T 12/ 040	1 005 240	1 070 885	279 478	1 146 470	1 571 700	1 489 143	1 336 768	1 233 129	1 024 922	1 114 172	1 007 004	oncentration	NFin	976	350 560	345 564	344 207	341 451	130 439	358 522							,	oncentration	NF,in N	71 852	70 549	70 456	02 020	095.07	28 072	707 10	102 10	CHE NO	75 331	68 946	67 294	67 932															
agnesium Co	CLU F	4 053	16/ C	000 2	3 441	3 543	3 364	7 908	4 210	3 381	3 518	2 785	3 559		-	EW N	10	2 893	3 050	3 132	2 623	2 691	2 653								Bromide C		274	280	605	328	194	18/	T80	808	0TO	819	746	698	694															
Date	FW	11.03.20	25 03 20	04.04.20	07.04.20	15.04.20	22.04.20	29.04.20	07.05.20	13.05.20	20.05.20	27.05.20	03.06.20	10.06.20 -	Date Po		11 03 20	18.03.20	25.03.20	01.04.20	07.04.20	15.04.20	22.04.20	29.04.20	07.05.20	13.05.20	20.05.20	27.05.20	03.06.20	0.06.20	Date		11.03.20	18.03.20	25.03.20	01.04.20	07.04.20	75.04.20	22.04.20	23.04.20 07.05.20	13.05.20	20.05.20	27.05.20	03.06.20	10.06.20															
	RAS2, Tank(D)	209 293 7EF 846	0T0 CC7	500 1/2	268 699	298 514	264 417	448 858	437 472	373 734	309 199	299 605	298 270	255 728			7 487	796	3 926	4 013	4 853	4 470	4 634		6 902	6 424	5 780	4 081	4 357	3 993		RAS2, Tank(D)	118 050	113 070	155 862	154 896	155 003	155 021	13/ 490	160 070	154 261	146.178	131 227	125 232	114 580		RAS2,Tank(D)	2 496	2 308	2 439	2 403	2 390	2 520	2 283		2 871	2 782	2 798	2 625	2 425
	RAS2, Tank(C) R	268481	232.342	510002	276474	301897	267554	439 163	460537	409 007	316670	317169	270145	253484		RAS2.Tank(C) RAS2.Tank(D)	2 471	2 805	3905	4051	4778	4665	4787	7 242	7 264	7177	5 958	4347	3 888	3 987			118750	111964	155555	120212	152.693	160.063	111011	174 0E2	166 70A	150587	140675	121896	113 230		RAS2, Tank(C) R	2513	2 264	2 365	2372	2 380	2564	2 288	2830	3033	2882	2 9 0 9	2 690	2410
		26/ /35	CTC 202	C 14 202	275 564	290 995	254 615	428 411	415 918	310 236	299 025	282 086	264 770			RAS2.Sump R	401	3 877	4 017	4 2 1 4	4 596	4 403	4 295	7 156	6 684	5 412	4 969	3 814	3 929	295		_	115 492	146 708	159 853	160 444	150 818	153 745	126 /21	67T QCT	1 12 255	128 571	127 767	120 778	73 881		RAS2,Sump R	2 474	2 311	2 435	2 439	2 311	2 591	2 332	2 815	2 730	2 617	2 799	2 681	1 654
	(B)	970 17	22 034	012 22	25 336	25 264	24 552	39 824	38 973	31 842	26 894	26 585	28 513	24 621		RAS1.Tank(B) RA		101	139	141	162	139	62	98	182	235	258	467	288	323		RAS1,Tank(B) RA	73 251	78 980	91 196	104 029	114 25/	113 637	205 305 207 711	115 601	102 240	93 915	84 126	80 017	77 040		RAS1,Tank(B) RA	1 526	1 484	1 357	1557	1 615	1 659	1 528	2 035	1 893	1 809	1 764	1 660	1 677
	A)	16 86U	071 72	00/ 62	25 037	24 973	24 659	36 890	36 480	37 169	36 519	26 298	27 419	24 476		RAS1.Tank(A) RA		100	117	146	153	133	69	282	172	277	262	241	263	340			57 837	79 488	90.462	102 699	110 250	110 903	104 468 108 072	111 060	100 750	965 398	83 086	78 765	76 278		RAS1,Tank(A) RA	1 209	1 473	1 374	1 462	1 575	1 664	15/5	2 00 C	1 966	1 856	1 737	1 724	1 690
		20 288	23 004	046 46	24 368	24 436	23 578	37 946	34 167	26 858	26 488	23 440	23 991	22 870	oint	a	63	139	143	154	160	140	62	98	163	194	224	198	274				70 060	97 715	91 360	105 /42	111 922	109 015	92 /39 117 E1 A	106 070	DVE DOT	85 214	79 625	77 796	87 639	oint		1 573	1 469	1 368	1 539	1 610	1 649	155/	2 022	1 851	1 729	1 715	1 627	1 932
er Sample p	NF,out(2) RAS	19433	73735	21 75 4	23 101	22 503	23 277	34684	31617	23 078	23 763	22579	23764	23 143	er Sample p	NF.out(2) RAS	1		82	67	91	61	117	131	82	64	41	58	79	64	er Sample p	NF,out(2) RAS	64337	-	103 302	16/171	11214/	11/625	9/ 13b	112 260		96.865	72585	81624	80 201	er Sample p	NF,out(2) RAS	1362		1499	1622	1608	1694	15/5	1918	1531	1893	1565	1714	1757
crogram/L] p	6	680.22	234/3	21/10	22 954	884 867	24302	36679	32 805	26519	25873	24158	25516	23 007	crogram/L] p	ut(1) NE.0	17	76	65	73	66	169	62	123	135	78	63	44	56	320	icrogram/L] p	NF,out(1) NF,o	74455		105012			480 790 10F 108				021.02	79 137	88910	72 670	icrogram/L] p		1503	1446	1570	1683	1673	7421	1818	2169	1 865	1867	1717	1 890	1684
ntratio	in NF,out(1)	823 500	820127	100000	817205					1 047 661	919066	827569	834 448	780594	Concentration [microgram/L] per Sample point	in NF.out(1)	113	129	86	06	83	75	156	289	310	235	165	116	144	189	ntratic		403 290		406 505			122070		116064		476.692	376 299	384327	360 202	Concentration [microgram/L] per Sample point		7401	7179	7014	7 055	7 228	1 750	7 104	8804	8 480	8 205	6777	8 0 9 8	8 063
hur		1991	9410 0685	0 505	9324	9837	9377	16023		9 2 3 6		7 996	9360	6 104	Silicone Con		2158	5128	5 408	5 799	7543	7577	7825	8 764	10749	8568	8331	6084	7 680	287	Calsium Con	/ NF,in	7131	10613	10592	10/30	12 142	12 099	14 075	10 005	DC8 D	9706	7 932	9 701	6897	Strontium Con	/ NF,in	65	68	69	73	63	64	64	88	ະ ຮ		57	67	48
Date Su	FW	11.03.20	25.03.20	04 04 20	07.04.20	15.04.20	22.04.20	29.04.20	07.05.20	13.05.20	20.05.20	27.05.20	03.06.20	10.06.20	Date Sil		11 03 20	18.03.20	25.03.20	01.04.20	07.04.20	15.04.20	22.04.20	29.04.20	07.05.20	13.05.20	20.05.20	27.05.20	03.06.20	0.06.20	Date Ca		11.03.20	18.03.20	25.03.20	01.04.20	07.04.20	75.04.20	22.04.20	23.04.20 07.05.20	12.05.20	20.05.20	27.05.20	03.06.20	10.06.20	Date Str	FV	11.03.20	18.03.20	25.03.20	01.04.20	07.04.20	15.04.20	22.04.20	29.04.20 07.05.20			27.05.20	03.06.20	10.06.20

Table A.2.1 Measured concentration for element and each sample point by ICP-MS analysis.

A.3 All measured values of sulfate measured by IC-Analysis

Table A.3 Measured sulfate concentration (mg/L) for each fish tank measured by IC-analysis

Date					C	Concentrat	ion, mg/L					
	RAS	S1,Tank(A)		RA	S2,Tank(C)		RAS	51,Tank(B)		RA	S2,Tank(D)	
25.mar	12	45,16		90,283	459,15		1357,358			1242,831	734,2	
01.apr	105,605	8,17		1259,633			98,882	15,23		1277,554	302,5	
07.apr	5,372	69,48		11,694	593,1		264,246	74,79			901,8	
15.apr	102,97	13,61		1381,601	1399,65		105,455	82,08		1672,786	1369,55	
22.apr		105,65	782,2	10,648	700,51	1663,6	142,075	78,01	766,88		754,31	966,65
29.apr	96,048	159,18		902,894			117,274	68,06		1393,893	1033,85	
07.mai	4,377	63,1			226,8			21,42		0,435	767,35	
13.mai	114,504	89,66		1335,032	1069,45		106,449	69,47		1212,715	538,35	
20.mai		138,43		60,393	827		5,898	12,9		86,365	896,65	
27.mai	106,371	44,5		1485,36	1152,5		107,667	31,6		1389,383	1269,3	
03.jun	32,407	14,6		8,66	7228,7		1,946	93,48		189,187	1,6	
10.jun	126,231									13,487	1539,25	

A.4 All measurements of absorbance at 254 nm for each sampling point and date by UV-Vis

Table A.4 Absorbance measured for each sampling point and date by UV-Vis analysis

					Absorba	nce at 254 n	m			
Dato	NF,in	NF,out(1)	NF,out(2)	FW	RAS1,Sump	RAS2,Sump	RAS1,Tank(A)	RAS2,Tank(C)	RAS1,Tank(B)	RAS2, Tank (D
18.mar	0,016	0,005	0,005	0,015	0,011	0,020	0,015	0,019	0,017	0,024
25.mar	0,017	0,010	0,011	0,017	0,018	0,017	0,020	0,021	0,022	0,020
01.apr	0,018	0,010	0,012	0,020	0,026	0,026	0,026	0,029	0,035	0,02
07.apr	0,030	0,015	0,016	0,021	0,071	0,021	0,025	0,037	0,036	0,033
15.apr	0,017	0,024	0,017	-	0,037	0,039	0,044	0,047	0,059	0,044
22.apr	0,025	0,017	0,018	0,026	0,050	0,044	0,042	0,045	0,043	0,046
29.apr	0,026	0,021	0,020	0,028	0,051	0,048	0,053	0,056	0,037	0,045
07.mai	0,024	0,017	0,017	0,026	0,050	0,041	0,047	0,050	0,048	0,05
13.mai	0,023	0,017	0,019	0,024	0,040	0,050	0,050	0,049	0,047	0,045
20.mai	0,028	0,018	0,018	0,026	0,070	0,076	0,063	0,089	0,069	0,085
27.mai	0,022	0,022	0,021	0,029	0,079	0,061	0,084	0,086	0,059	0,063
03.jun	0,030	0,020	0,019	0,029	0,069	0,074	0,082	0,071	0,067	0,069
10.jun	0,030	0,021	0,022	0,031	0,087	0,109	0,087	0,095	0,101	0,081