

Vortex dislocation mechanisms in the near wake of a step cylinder

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(Received 26 September 2019; revised 13 December 2019; accepted 31 January 2020)

Vortex interactions behind step cylinders with diameter ratio $D/d = 2$ and 2.4 at Reynolds number (Re_D) 150 were investigated by directly solving the three-dimensional Navier–Stokes equations. In accordance with previous studies, three spanwise vortex cells were captured: S-, N- and L-cell vortices. In this paper, we focused on vortex interactions between the N- and L-cell vortices, especially the vortex dislocations and subsequent formations of vortex loop structures. The phase difference accumulation process of every pair of corresponding N- and L-cell vortices and its effects on the vortex dislocations were investigated. We revealed that the total phase difference between N- and L-cell vortices was accumulated by two physically independent mechanisms, namely different shedding frequencies and different convective velocities of these two cells. The second mechanism has never been reported before. The relative importance of these two mechanisms varied periodically in the phase difference accumulation process of every pair of corresponding N- and L-cell vortices. This variation caused the vortex dislocation process and the subsequent formation of the loop structures to change from one N-cell cycle to another. Our long-time observations also revealed an interruption of the conventional antisymmetric vortex interactions between two subsequent N-cell cycles in this wake. Moreover, the trigger value and the threshold value in the phase difference accumulation processes were identified and discussed. Both values contribute to better understanding of the vortex dislocations in this kind of wake flow. Finally, the universality of our discussions and conclusions was investigated.

Key words: vortex interactions, vortex shedding, wakes

1. Introduction

Cylindrical structures are widely used in the marine offshore industry, for example, the hull of a spar platform (Saiful-Islam *et al.* 2012), deep-water risers (Carter & Ronalds 1998), etc. Wake flow behind circular cylinders has been a popular topic

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of investigation for researchers and engineers for decades. It is well known that when the Reynolds number (Re_D) is less than 50, the wake flow around a circular cylinder is laminar and steady, and there is no vortex shedding behind the cylinder (Williamson 1996). For $50 \lesssim Re_D \lesssim 180$, periodic two-dimensional vortex shedding occurs in the wake behind the cylinder. When Re_D exceeds 180, the wake becomes three-dimensional. The well-known mode A and mode B appear at $Re_D = 180\text{--}194$ and $Re_D = 200\text{--}250$, respectively (Williamson 1996). Wake turbulence and shear layer instabilities follow as Re_D further increases.

However, even at $Re_D \lesssim 180$, we can observe three-dimensional cylinder wakes under certain circumstances, such as cylinders with non-uniform inflow, cylinders with varying cross-sections, cylinders with free ends, etc. In these cases, three-dimensionality is triggered by spanwise non-uniformity in either the incoming flow or the configuration itself. Complex three-dimensional wake dynamics appear, such as vortex split, vortex dislocation and oblique shedding. In order to investigate these complex flow phenomena, a single step cylinder becomes an ideal configuration in which geometric complications are removed except for the sudden diameter change.

1.1. Single step cylinder wake

There are two important parameters in the wake flow behind a single step cylinder, i.e. the Reynolds number (Re_D) and the diameter ratio (D/d). The latter, D/d , is the ratio between the large- and small-diameter parts of the step cylinder, while $Re_D = UD/\nu$ (where U represents the uniform inflow velocity, and ν is the kinematic viscosity of the fluid).

The wake of step cylinders with $1.14 < D/d < 1.76$ at $67 < Re_D < 200$ was initially investigated by Lewis & Gharib (1992). They reported two vortex interaction modes: a direct and an indirect mode. The direct mode occurs when $D/d < 1.25$, where two dominating shedding frequencies (f_S and f_L) correspond to vortices shed from the small and large cylinders, respectively. The interactions between these two kinds of vortices take place in a narrow region referred to as the interface. When they are in phase, vortices from the two wake regions connect to each other one by one across the interface. When they are out of phase, the direct connection will be interrupted and at least one half-loop connection between oppositely rotating vortices will appear. The period between two such interruptions is called a beat cycle. In the indirect mode ($D/d > 1.55$), in addition to f_S and f_L , another distinct frequency f_3 (which is referred to as f_N in the present paper) can be detected near the interface behind the large cylinder. This region was first named the modulation zone by Lewis & Gharib (1992). It prevents direct interactions between the vortices with shedding frequency f_S and those with shedding frequency f_L . In the modulation zone, the velocity variation is modulated by the main frequency behind the large cylinder, and an inclined interface was found to occur at a beat frequency ($f_L - f_N$). Lewis & Gharib (1992) found that the vortex interactions in the indirect mode are more complex than in the direct mode.

Based on the three dominating shedding frequencies, Dunn & Tavoularis (2006) identified three types of spanwise vortices: (1) S-cell vortex shed from the small cylinder with the highest shedding frequency f_S , (2) N-cell vortex shed in the modulation zone with the lowest shedding frequency f_N , and (3) L-cell vortex shed from the large cylinder with shedding frequency f_L . The terminologies

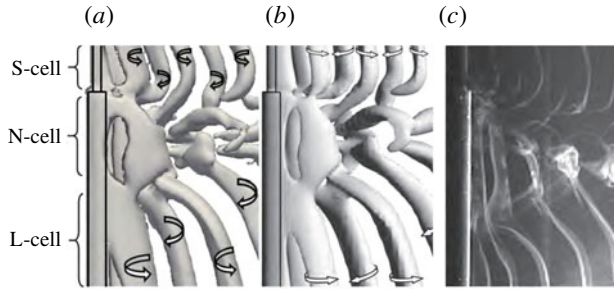


FIGURE 1. Vortex shedding in the wake behind a step cylinder. (a) Isosurfaces of $\lambda_2 = -0.05$ (Jeong & Hussain 1995) from our simulation, at $Re_D = 150$ and $D/d = 2$. (b) Isosurfaces of $Q \approx 2 \times 10^{-3}$ from Morton & Yarusevych (2010b), at $Re_D = 150$ and $D/d = 2$ (image reproduced from Morton & Yarusevych (2010b), with the permission of AIP Publishing). (c) Flow visualization image from Dunn & Tavoularis (2006), at $Re_D = 150$ and $D/d = 1.98$ (image reproduced from Dunn & Tavoularis (2006) with permission from Cambridge University Press).

S-, N- and L-cell were thereafter adopted in many studies (Morton, Yarusevych & Carvajal-Mariscal 2009; Morton & Yarusevych 2010a,b, 2014; Tian *et al.* 2017a,b), and are also used in the present study. The regions where these vortex cells occur are indicated in figure 1(a).

The interactions between different vortex cells in the indirect mode were investigated in the wake behind a single step cylinder with $D/d \approx 2$ and $Re_D \approx 150$, experimentally by Dunn & Tavoularis (2006) and numerically by Morton & Yarusevych (2010b). These studies concluded that the S–N cell boundary (the region between the S- and N-cell vortices) is stable and deflects spanwise into the large cylinder direction. At this boundary, one N-cell vortex always connects to a counter-rotating N-cell mate and an S-cell vortex. The vortex dislocations between the S- and N-cell vortices occur at a beat frequency ($f_S - f_N$) at the S–N cell boundary. During this dislocation process, the half-loop connection between S-cell vortices is dominating. The number of S- and N-cell vortices in a cyclic period (from one dislocation process to the next) is determined by the ratio of the shedding frequencies of these two cells (f_S/f_N).

Unlike the S–N cell boundary, the N–L cell boundary (the region between the N- and L-cell vortices) is unstable. As the phase difference between the N- and L-cell vortices accumulates, in parallel with the appearance of vortex dislocations between N- and L-cell vortices, the shapes and lengths of the N-cell vortices and the position of the N–L cell boundary vary periodically with the beat frequency ($f_L - f_N$). Morton & Yarusevych (2010b) defined these cyclic changes as the N-cell cycle. Tian *et al.* (2017a) further investigated the dislocation processes at the N–L cell boundary. Two new loop structures were identified: the NL-loop (the fake loop) formed between a pair of N- and L-cell vortices with opposite rotating directions, and the NN-loop (the real loop) formed between two subsequent N-cell vortices with opposite rotating directions. In addition, antisymmetric vortex interactions between two adjacent N-cell cycles were reported based on careful observations of the development of these two kinds of loop structures.

When Re_D increases, the wake gradually becomes more complex. However, the three dominating spanwise vortices (S-, N- and L-cell vortices), the vortex dislocation between them and the cyclic variation of the N-cell vortices are still observable in

the wake flow (Morton & Yarusevych 2010*b*). In addition, Morton & Yarusevych (2010*a*, 2014) reported that the duration of the N-cell cycle varies and fits a Gaussian distribution at relatively high $Re_D = 1050$.

Other characteristics of the wake behind a single step cylinder with different diameter ratios and different Reynolds numbers have been discussed in several papers. Ko, Leung & Au (1982), Yagita, Yoshihiro & Matsuzaki (1984), Norberg (1992) and Dunn & Tavoularis (2006) found that the vortex shedding behind the small cylinder was seldom influenced, but the flow behind the large cylinder was strongly affected by the step. When this induced effect becomes strong enough, N-cell vortices appear (Norberg 1992; Dunn & Tavoularis 2006). In addition to the three main vortex cells (S, N and L), two pairs of streamwise vortices (i.e. junction vortices and edge vortices) have also been identified around the step region (Dunn & Tavoularis 2006; Morton *et al.* 2009; Tian *et al.* 2017*b*).

1.2. Vortex dislocation

It is widely accepted that most of the observations mentioned above for the step cylinder are closely related to vortex dislocations. As an interesting physical phenomenon, vortex dislocations have also been investigated in various types of flow, such as in uniform cylinder wakes, mixing layers and nonlinear waves.

The phrase vortex dislocation was first introduced by Williamson (1989) when he observed multiple vortex cells with different shedding frequencies in his experiments of flow past a circular cylinder at $Re_D < 200$. Neighbouring vortex cells are observed to move either in phase or out of phase with each other due to their different shedding frequencies. When these vortex cells move out of phase, at the boundary between them, the contorted ‘tangle’ of vortices appears and looks like dislocations that appear in solid materials. Williamson (1989) defined this kind of flow phenomenon as vortex dislocation. He reported that, at $Re_D = 100$, vortex dislocations occur at the boundary between cells (the end-plate cell of frequency f_e and the single cell of frequency f_L) at a constant beat frequency $f_L - f_e$, accompanied by an obvious minimum amplitude of the velocity fluctuations at the boundary. In addition, by comparing velocity signals from different vortex cell regions, the time trace of phase differences was plotted. Williamson (1992) further investigated the dislocation by adding a small ‘ring’ on a circular cylinder in order to force the dislocation to happen. This study revealed more detailed features of vortex dislocations, such as the vortex dynamics and the effects of vortex dislocations in the wake flow. An interesting long-period characteristic of the vortex dislocation was first reported in McClure, Morton & Yarusevych (2015) by investigating flow past dual step cylinders. They defined the time period between two identical vortex dislocations as the fundamental dislocation cycle. Further investigations of this characteristic in the wake behind the single step cylinder can be found in Tian *et al.* (2019). Vortex dislocations in other types of wakes and mixing layers have been reported by many others. For details, the reader is referred to the works of Gaster (1969), Eisenlohr & Eckelmann (1989) and Dallard & Browand (1993).

1.3. Objectives of the present study

There have been many attempts to describe the vortex dislocations in the step cylinder wake. Previous studies pointed out that it is the accumulation of phase differences that causes the vortex dislocation between different adjacent spanwise vortex cells. However, the investigations of how phase differences accumulate and how they affect the vortex dislocations are still limited.

Williamson (1989) and Lewis & Gharib (1992) experimentally examined the time trace of the phase difference by using probes to monitor velocity signals in different vortex cell regions positioned 10 cylinder diameters downstream. However, at such a location, oblique vortex shedding, complex vortex interactions and the stretching and tilting of the vortices make it difficult to accurately evaluate phase differences. Another interesting phenomenon in the wake flow behind the step cylinder is the cyclic changes of the N-cell vortex, which was defined as the N-cell cycle by Morton & Yarusевич (2010*b*). However, they analysed this phenomenon in a relatively short time period containing only a few N-cell cycles. Whether N-cell cycles have any long-period variations or very low-frequency features is still unknown.

The primary goal of the present numerical study is to thoroughly investigate the mechanisms of phase difference accumulation in the step cylinder wake, and their effect on vortex interactions. Considering that the wake behind the small cylinder part is seldom influenced by the step, and the contributions of the streamwise vortices on the vortex dislocation between the S- and N-cell vortices are unclear, we only focus on the vortex dislocation between the N- and L-cell vortices. To achieve this objective, we analyse the time and space signals of several flow quantities (velocity, vorticity and λ_2) obtained from a direct numerical simulation (DNS) of flow past two different step cylinders with diameter ratios $D/d=2$ and 2.4. In order to change the diameter ratio of the step cylinder, we keep D constant, and change d . These two cases share the same coordinate system, computational method and data analysis process.

First, in §§ 2–5, the flow problem, the numerical settings and analyses of the wake flow field are described in detail based on the $D/d=2$ case. Then, in § 6, the universality of our discussions and conclusions is studied by investigating the $D/d=2.4$ case. Last but not least, we also aim to present a reliable method that can be used to calculate the phase information (φ) and phase difference (Φ) of vortices, since such a method is lacking in the literature. Details of the method are included in appendix A.

2. Flow configuration and computational aspects

2.1. Flow configuration and coordinate system

A sketch of the $D/d=2$ step cylinder geometry is shown in figure 2(*a*), where L and l represent the lengths of the large and small parts of the cylinder, respectively. In figure 2(*b*), the computational domain and coordinate system are shown, where x -, y - and z -directions correspond to the streamwise, cross-flow and spanwise directions, respectively. The origin is located in the centre of the interface between the small and large cylinders. The inlet plane is $10D$ upstream from the centre of the step cylinder, while the outlet plane is $20D$ downstream. The spanwise height of the domain is $45D$, of which the small and large cylinders occupy $15D$ (l) and $30D$ (L), respectively. The width of the domain is $20D$. This domain is larger than that used by Morton & Yarusевич (2010*b*) for the same D/d and Re_D . Boundary conditions applied in the present study are as follows.

- (i) The inlet boundary: uniform velocity profile, $u = U$, $v = 0$, $w = 0$.
- (ii) The outlet boundary: Neumann boundary condition for velocity components ($\partial u/\partial x = \partial v/\partial x = \partial w/\partial x = 0$) and constant zero pressure condition.
- (iii) The other four sides of the computational domain: free-slip boundary conditions (for the two vertical sides, $v = 0$, $\partial u/\partial y = \partial w/\partial y = 0$; for the two horizontal sides, $w = 0$, $\partial u/\partial z = \partial v/\partial z = 0$).
- (iv) The step cylinder surfaces: no slip and impermeable wall.

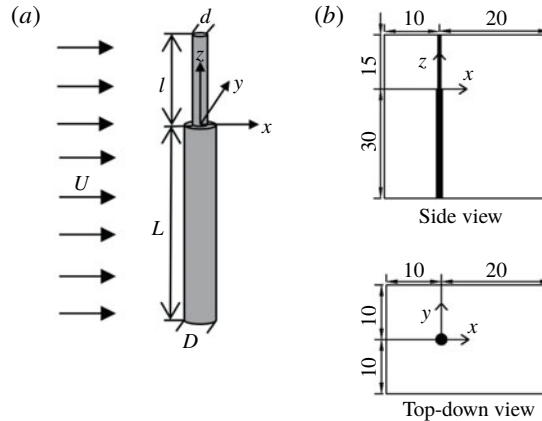


FIGURE 2. (a) A sketch of the step cylinder geometry ($D/d = 2$). (b) Computational domain, origin and coordinate system illustrated from two different viewpoints. The diameter of the large cylinder, D , is the length unit. The origin is located in the centre of the step, i.e. the interface between the small and large cylinders.

2.2. Computational method

For all cases in the present investigation, a thoroughly validated finite-volume-based numerical code MGLT (Manhart 2004) is used to directly solve the incompressible Navier–Stokes equations. The midpoint rule is used to approximate the surface integral of flow variables over the faces of the discrete volumes, leading to second-order accuracy in space. A third-order explicit low-storage Runge–Kutta scheme (Williamson 1980) is used for time integration with a constant time step Δt that ensures a Courant–Friedrichs–Lewy (CFL) number smaller than 0.65. The pressure–velocity coupling is handled by solving a Poisson equation with Stone’s strongly implicit procedure (SIP) (Stone 1968). The same code has recently also been used to investigate other complex flows, such as the spheroid wake (Jiang *et al.* 2016) and the curved cylinder wake (Jiang, Pettersen & Andersson 2019).

All simulations are conducted on a staggered Cartesian mesh, while the solid surface of the step cylinder is handled by an immersed boundary method (IBM) (Peller *et al.* 2006). The computational domain is divided into cubic Cartesian grid boxes, named level-1 boxes. In each of them, $N \times N \times N$ cubic Cartesian grid cells are uniformly distributed. In order to refine the grid regions in which complex flow phenomena take place, such as the regions close to the step cylinder geometry, the region around the ‘step’, the regions where vortex dislocations happen, etc., all the grid boxes (the level-1 boxes) are equally split into eight smaller cubic boxes (the level-2 boxes). In each level-2 box, there are also $N \times N \times N$ cubic grid cells. Hence, the grid resolution on level 2 is two times finer than that on level 1. This splitting process goes on automatically until the finest grid level is reached. The overall properties of the grids for all simulations can be found in table 1. A schematic illustration of the mesh design is shown in figure 3.

2.3. Grid convergence study

Table 2 shows the Strouhal number (St) of the three dominating vortex cells ($St_S = f_S D/U$, $St_N = f_N D/U$ and $St_L = f_L D/U$) behind the step cylinder calculated

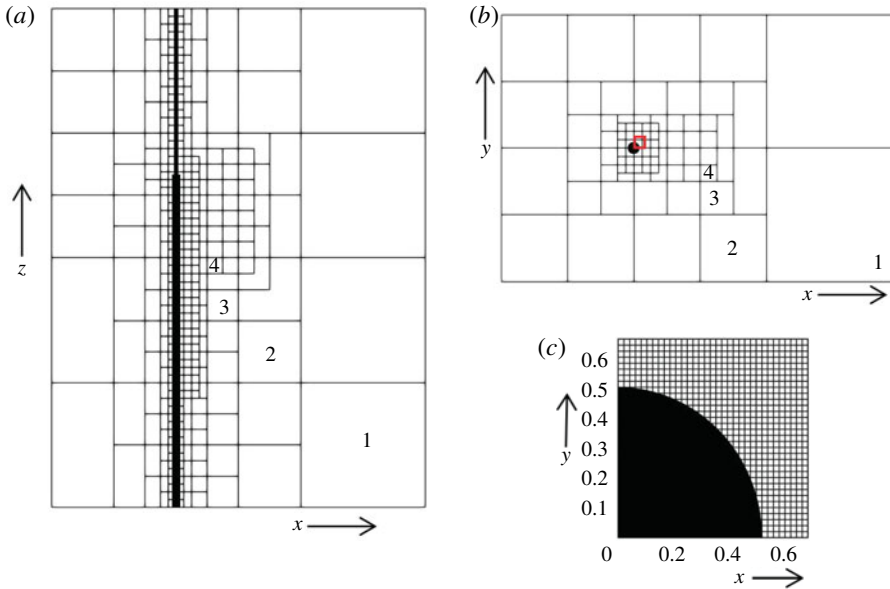


FIGURE 3. An illustration of the multi-level grids: (a) a slice of the computational domain in the x - z plane at $y/D = 0$, and (b) a slice of the computational domain in the x - y plane at $z/D = 0^-$ (at the large diameter D region). Each square represents the slice of a corresponding cubic Cartesian grid box that contains $N \times N \times N$ grid cells. Here, there are five levels of grid boxes, where the first four levels are indicated by numbers. Owing to different minimum grid sizes, different cases have either five or six levels of grid boxes. (c) A zoom-in plot of the grid cells in the step region (red rectangle in panel (b)) for case 2.

Case	Minimum grid cell size, D	Time step, $\Delta t U/D$	Number of grid levels	Number of grid cells in one grid box	Total number of grid cells (million)
1	0.025	0.0080	5	$30 \times 30 \times 30$	30.2
2	0.020	0.0067	5	$36 \times 36 \times 36$	48.8
3	0.015	0.0050	6	$24 \times 24 \times 24$	81.0
4	0.012	0.0040	6	$30 \times 30 \times 30$	173.8

TABLE 1. Detailed mesh information of all $D/d = 2$ cases. The Reynolds number for all cases is $Re_D = UD/\nu = 150$.

by a fast Fourier transform (FFT) of the time series of the streamwise velocity u along a vertical sampling line positioned at $(x/D, y/D) = (0.6, 0.2)$. For these four cases, the differences between St numbers of the same vortex cell are small. In figure 4(a), the distributions of mean streamwise velocity along the line AB (as indicated in inset figure 4(a₁)) for all four cases are plotted to illustrate the flow variation on the ‘step’ just in front of the small cylinder. The curves in figure 4(a) and a zoom-in view in the inset figure 4(a₂) clearly show a convergent tendency from case 1 to case 4, and there are only minor differences between case 3 and case 4. Moreover, figure 4(b) shows time traces of the spanwise velocity (w) in the N-cell

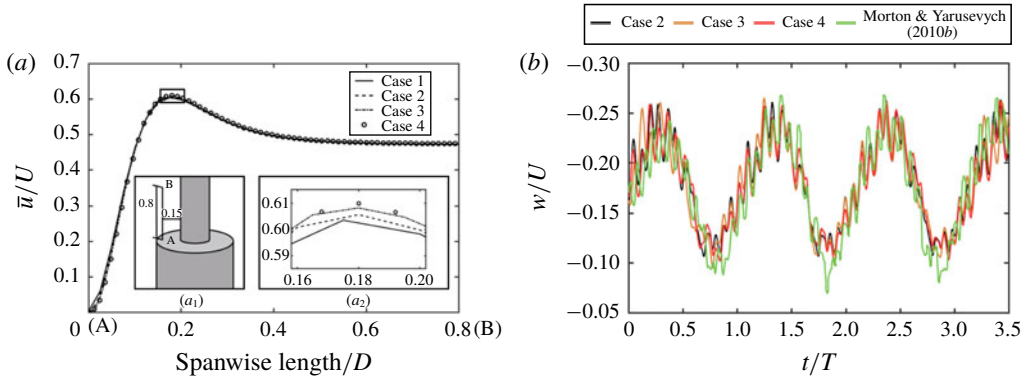


FIGURE 4. (a) Distributions of mean streamwise velocity \bar{u}/U along a sampling line AB in the x - z plane at $y/D=0$. Insets: (a_1) a sketch of the sampling line AB of length $0.8D$, positioned $0.15D$ in front of the small cylinder; and (a_2) a zoom-in plot of the upper part of the curves in panel (a) (black rectangle in panel (a)). (b) Time traces of the spanwise velocity w at point $(x/D, y/D, z/D) = (1, 0, -2.5)$ in the N-cell region. The green line is obtained from Morton & Yarusevych (2010b); T is the period of one N-cell cycle, which is the same time scale as Morton & Yarusevych (2010b) used.

Case	1	2	3	4	Morton & Yarusevych (2010b)	Norberg (1994)
St_S	0.294	0.295	0.290	0.292	0.320	0.297
St_N	0.153	0.153	0.155	0.154	0.157	—
St_L	0.177	0.177	0.178	0.178	0.179	—

TABLE 2. Strouhal numbers of the three dominating vortex cells (S-cell, $St_S = f_S D/U$; N-cell, $St_N = f_N D/U$; and L-cell, $St_L = f_L D/U$) for all cases studied. Results from Morton & Yarusevych (2010b) are from their numerical simulations for a step cylinder with $D/d=2$ at $Re_D=150$. The result from Norberg (1994) is calculated by (2.1), which was derived by Norberg based on laboratory experiments. (Note that, in our cases, St_S is calculated based on the large-cylinder diameter, so a factor 2 should be used when using Norberg's equation.)

formation region where the velocity varies dramatically with time. The fluctuations and the mean values of w from case 3 and case 4 almost coincide. However, the computational cost of case 4 is significantly higher than that of case 3, due to the large number of grid cells and smaller time step. The long-period features of the flow that we will discuss in later sections require exceptionally long simulations (more than $3000D/U$). All discussions are therefore based on data from case 3. Case 4 was run only for a limited time for this convergence test.

2.4. Comparison with previous studies

An overview of the vortical structures in the wake of the step cylinder is illustrated in figure 1(a) by plotting the isosurface of $\lambda_2 = -0.05$ (Jeong & Hussain 1995). By comparing figures 1(a), (b) and (c), one can see that the overall wake structures from the present study compare well with the previous numerical simulations by Morton

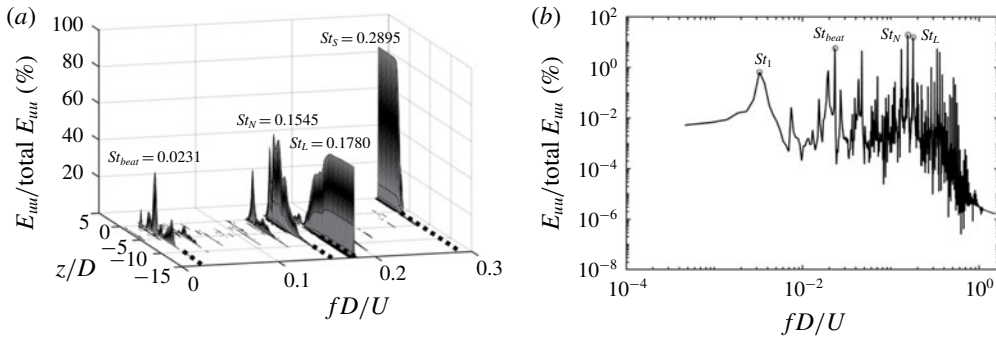


FIGURE 5. (a) Streamwise velocity spectra along a spanwise line behind the step cylinder at $(x/D, y/D) = (0.6, 0.2)$. (b) Power spectrum plotted at position $(x/D, y/D, z/D) = (0.6, 0.2, -4.4)$, in which St_N , St_L , St_{beat} and an exceptionally low-frequency St_1 are marked by small black circles. (Note that there is no S-cell vortex in the wake flow at spanwise position $z/D = -4.4$, so St_S does not show up in this figure.)

& Yarusevych (2010b) and experiments by Dunn & Tavoularis (2006). Behind the step cylinder, as mentioned in § 1, the shedding of S-cell vortices is barely influenced, which makes it reasonable to introduce the correlation derived by Norberg (1994),

$$St = 0.1835 - 3.458/Re + 1.51 \times 10^{-4} Re, \tag{2.1}$$

to validate our St_S . From the data in table 2, we see that St_S from the present study is slightly lower than that from Morton & Yarusevych (2010b), but compares better with the experimental value reported in Norberg (1994). In addition, we have obtained spanwise velocity data from Morton & Yarusevych (2010b) and displayed them in figure 4(b). The match between the present study and Morton & Yarusevych (2010b) is convincing. Based on all these careful comparisons, we believe that the grid resolution in case 3 is good enough to accurately simulate this flow.

3. Features of the present wake flow

Generally, the wake behind the two step cylinders ($D/d = 2$ and 2.4) in the present study are very similar. In order to ease the discussions, only the wake flow behind the $D/d = 2$ case is described in §§ 3–5. The $D/d = 2.4$ case is presented as a justification case in § 6.

3.1. Overview of the flow development

In figure 5(a), the streamwise velocity spectrum is obtained by means of a discrete Fourier transform (DFT) of continuous velocity data along a vertical sampling line parallel to the Z-axis at position $(x/D, y/D) = (0.6, 0.2)$, over a long period of 2500 time units (D/U). As in the previous studies (Dunn & Tavoularis 2006; Morton & Yarusevych 2010b; Tian *et al.* 2017a), the three dominating frequency components ($St_S = f_S D/U$, $St_N = f_N D/U$ and $St_L = f_L D/U$) and the beat frequency ($St_{beat} = f_{beat} D/U$) are dominating.

The vortex structures in the near wake are illustrated by consecutive snapshots of the isosurface of λ_2 in figure 6. The time t is set to $t = t^* - 2378.1D/U$, where t^* is the actual time in the simulation. This applies all through §§ 3–5. All N- and

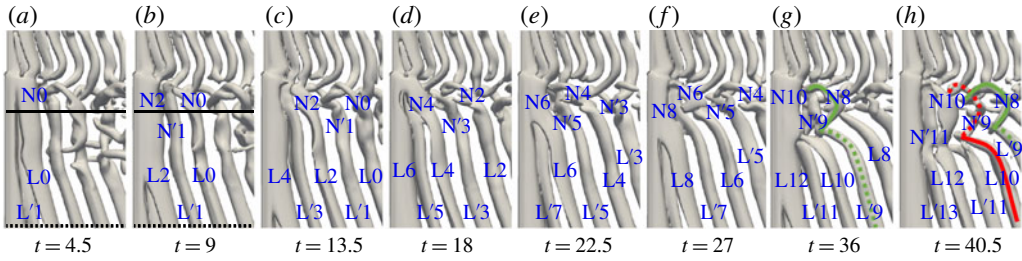


FIGURE 6. Isosurface of $\lambda_2 = -0.05$ showing developments of vortex structures on the $-Y$ side. The time t is set to $t = t^* - 2378.1D/U$ (t^* is the actual time). Solid and dashed curves in panels (g) and (h) indicate the loop structures on the $-Y$ and $+Y$ side, respectively. The red and green curves point to different NL-loop structures. In panels (a) and (b), the black solid line at $z/D = -2.9$ and the black dashed line at $z/D = -14$ indicate the positions of vorticity contours given in figure 9.

L-cell vortices are labelled by a combination of capital letters and numbers: ‘N’ and ‘L’ represent N- and L-cell vortices, respectively, while the number indicates the shedding order. To differentiate vortices shed from different sides of the step cylinder, we use capital letters with primes (N’ and L’) to represent vortices shed from the $+Y$ side; and only capital letters (N and L) to represent vortices shed from the $-Y$ side. In figure 6(a–f), every N-cell vortex has one corresponding L-cell vortex with the same direction of rotation (e.g. N0 and L0; N’1 and L’1, etc.). Owing to different shedding frequencies of N- and L-cell vortices, loop structures appear when corresponding N- and L-cell vortices are out of phase. From figure 6(g,h), loop structures (N8–L’9) and (N’9–L10) form, and are indicated by green and red curves, respectively. Details of the formation processes of those loop structures were described in Tian *et al.* (2017a). Based on the order of their appearances, the green and red curves are named the NL-loop 1 and NL-loop 2, respectively.

Based on long-time observations ($2500D/U$), a schematic topology sketch is shown in figure 7. This will be used to introduce some important concepts. In figure 7, the short and long straight lines represent the N- and L-cell vortices, respectively. Between them, the curved solid lines connect the N-cell vortex and its counterpart L-cell vortex. The dashed curves indicate broken connections that are not able to persist due to dislocations. Detailed visualizations of vortex connections and dislocations in the first N-cell cycle are shown in figure 6. To ease the observation, we only show the connections between the N- and L-cell vortices. The L–L and N–N loops (Tian *et al.* 2017a) are not shown in this figure.

We define the side of the N-cell vortex in an NL-loop structure as the side of the loop itself. For example, the NL-loop N8–L’9 (shown by green curves) in figure 6(g) is identified to form at the $-Y$ side. As shown in figure 7, from the first to the seventh N-cell cycle, the NL-loop 1 (the green curves) appears alternately at the $+Y$ and $-Y$ side between subsequent N-cell cycles. This is what we called the antisymmetric vortex interactions in Tian *et al.* (2017a). However, an unexpected interruption of this antisymmetry is observed between the seventh and eighth N-cell cycles. Figure 7 shows, in both the seventh and eighth N-cell cycles, that the NL-loop 1 appears at the $-Y$ side (green curves connect to black short lines which represent the N-cell vortex on the $-Y$ side). We introduce the term ‘long N-cell cycle’ to identify the uninterrupted series of antisymmetric N-cell cycles. Within one long N-cell cycle,

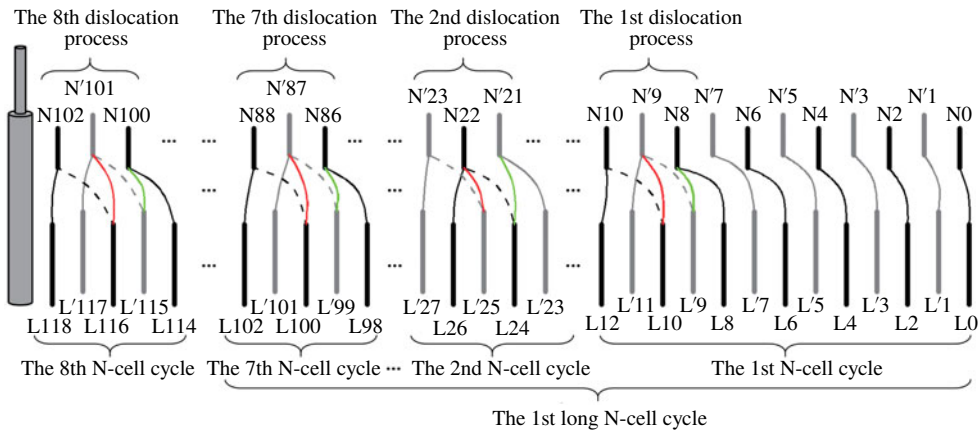


FIGURE 7. Schematic topology sketches illustrating the long-time history of the vortex connection topology and the vortex shedding. The thick black and grey straight lines represent vortices on the $-Y$ and $+Y$ sides, respectively. Only the N- and L-cell vortices are shown by short and long straight lines. The connections between them are depicted by thin solid curves. Black and grey solid curves indicate the connections between an N-cell vortex and its counterpart L-cell vortex. The red and green curves reveal different NL-loop structures (same colour code as used in figure 6). The dashed curves, on the other hand, indicate broken connections that are not able to persist due to dislocations. We define a new term ‘long N-cell cycle’ containing several conventional N-cell cycles, while the conventional N-cell cycle was firstly defined by Morton & Yarusевич (2010b) and adopted also in the present study.

antisymmetric vortex interactions appear between subsequent N-cell cycles. However, at the boundary between two long N-cell cycles, this antisymmetry is interrupted. Our long-time observation covering eight long N-cell cycles shows that there are either seven or eight N-cell cycles in one long N-cell cycle. In fact, an exceptionally low frequency (St_1) is captured in figure 5(b) where a power spectrum at position $(x/D, y/D, z/D) = (0.6, 0.2, -4.4)$ is shown. The value of St_1 is 0.0032, and is around $St_{beat}/7.5$. This coincides well with our observation that one long N-cell cycle contains either seven or eight N-cell cycles. We believe that this low-frequency component is related to the long N-cell cycles. More detailed information on this long-period phenomenon, and the unexpected interruption, will be discussed in § 5. The other visible frequency components in figure 5(b) are combinations of the basic frequency components, i.e. St_S , St_N , St_L and St_1 (Gerich & Eckelmann 1982).

3.2. Necessity of monitoring the phase information of each N- and L-cell vortex

All the interesting physical phenomena, i.e. the formation of NL-loops, the unexpected interruption of the antisymmetry, etc., are directly related to the vortex dislocations in the wake behind the step cylinder. A consensus from the literature (Williamson 1989; Lewis & Gharib 1992; Morton *et al.* 2009) is that vortex dislocations are attributed to different shedding frequencies. In the present configuration, if both N- and L-cell vortices shed regularly, it is natural to directly use f_L and f_N to measure the phase difference (Φ) between N- and L-cell vortices. However, the actual wake flow is more complicated. In figure 8(a,b), we plot time traces of the instantaneous cross-flow velocity v at two locations in the L- and N-cell regions in the symmetry plane. Two

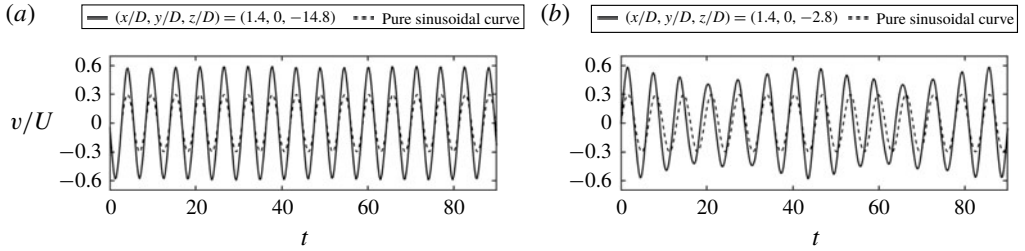


FIGURE 8. Time trace of the oscillating cross-flow velocity v is plotted as the solid line: (a) at the sampling point $(x/D, y/D, z/D) = (1.4, 0, -14.8)$ in the L-cell region, and (b) at the sampling point $(x/D, y/D, z/D) = (1.4, 0, -2.8)$ in the N-cell region. For comparison, pure sinusoidal curves are plotted as dashed lines with frequency f_L in panel (a) and frequency f_N in panel (b); f_L and f_N are calculated by FFT obtained from figure 5.

dashed sinusoidal curves with constant frequencies f_L and f_N are also plotted in figure 8. By comparing figures 8(a) and (b), it is clear that, unlike the regularly shed L-cell vortices, the shedding frequency of the N-cell vortex slightly fluctuates during every N-cell cycle. This was also briefly mentioned by Morton & Yarusyevych (2010b), but not investigated further. The irregularity of the N-cell shedding makes it challenging but necessary to monitor the phase information of every N-cell vortex. Therefore, we developed a method to obtain the phase information (φ) and the phase difference (Φ) of vortices. Details can be found in appendix A.

4. Two different phase difference accumulation mechanisms and their effects on vortex interactions

4.1. Two different phase difference accumulation mechanisms

From figure 6, one can see that both the N- and L-cell vortices are spanwise vortices. This means that the variation of the streamwise distance between corresponding N- and L-cell vortices can reflect the changes in their phase difference (Φ). In the present study, we use the location of the most concentrated spanwise vorticity (ω_z) to indicate the position of the corresponding vortex. In figure 9, we plot instantaneous spanwise vorticity ω_z contours at an (x, y) plane in the N-cell region $z/D = -2.9$ and L-cell region $z/D = -14$. Four black lines indicate the positions of vortices N0 and L0. One can see that from $tU/D = 4.5$ to 9, the streamwise distance between N0 and L0 increases from $1.8D$ ($3.7D - 1.9D$) to $2.3D$ ($7.7D - 5.4D$) as they convect downstream. This means that, even after both N0 and L0 disconnect from the shear layer, as shown in figure 6(a), Φ between them continues to accumulate. By marking the moment when the N-cell vortex just forms as an individual wake-type vortex, we divide the process of Φ accumulation into two parts. Before this moment, Φ between the N- and L-cell vortex is dominated by their different shedding frequencies, called Φ_f . After this moment, Φ is caused by different convective velocities in the N- and L-cell regions, and called Φ_c . Detailed descriptions of monitoring Φ_f and φ can be found in appendix A. Owing to the spatial inhomogeneity of the convective velocity, it is difficult to accurately assess its effect on Φ . Yet, the distributions of mean streamwise velocity (\bar{u}) in different vortex cell regions can roughly indicate the influence.

In figure 10, the spanwise distributions of \bar{u} are plotted at several downstream positions. As shown in figure 10(a), the mean streamwise velocity in the N-cell region

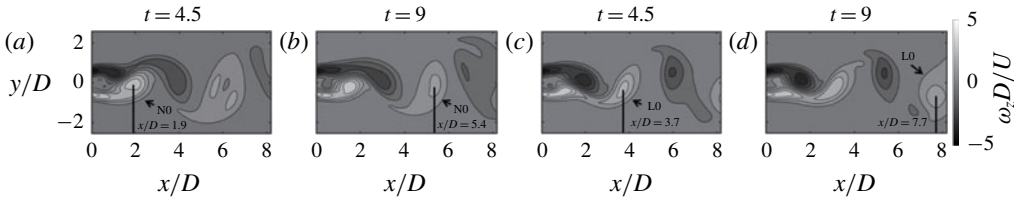


FIGURE 9. Instantaneous spanwise vorticity ω_z ($\omega_z = \partial v / \partial x - \partial u / \partial y$) contour plots in an (x, y) plane in (a,c) the N-cell region $z/D = -2.9$ (black solid line in figure 6(a,b)) and (b,d) in the L-cell region $z/D = -14$ (black dotted line in figure 6(a,b)). By detecting the location of concentrated vorticity, the positions of vortices N'9 and L'9 are marked by black lines. (Note that we have compared the position of the centre of the concentrated vorticity and the centre in the region defined by λ_2 isolines, and confirmed only tiny differences.)

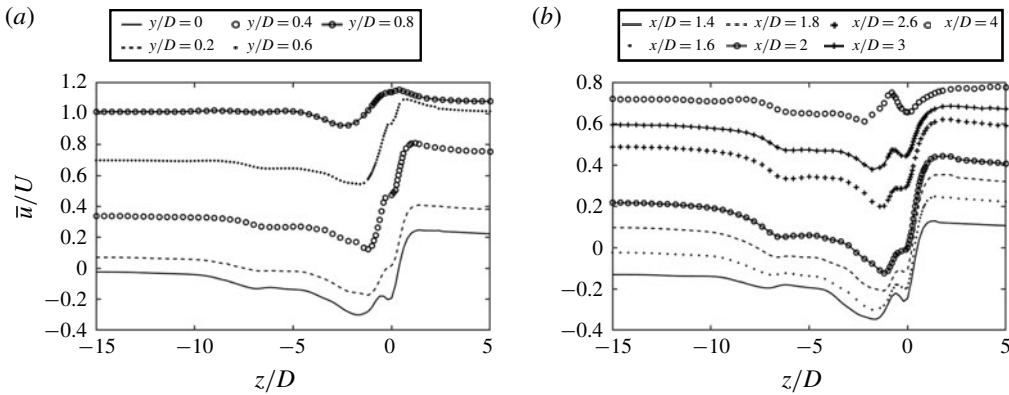


FIGURE 10. (a) Distributions of the mean streamwise velocity (\bar{u}/U) along spanwise lines with the same x -coordinate ($x/D = 1.6$), but for different y -coordinates. (b) Distributions of mean streamwise velocity \bar{u}/U along spanwise lines with different x -coordinates in the symmetry plane ($y/D = 0$).

in the symmetry plane ($y/D = 0$) is nearly $0.2U$ less than that in the L-cell region. At the side plane $y/D = 0.8$, this difference still reaches $0.1U$. From figure 10(b), we see that the difference in mean streamwise velocity is clear until a downstream position $x/D = 4$. In other words, at least until $x/D = 4$ in the wake, the convective velocity distribution is distinctly non-uniform in the spanwise direction. This non-uniformity induces an additional Φ when the vortices convect downstream. We note that this role of the non-uniform convection velocity and its effects have never been addressed before.

4.2. Effects of two phase difference accumulation mechanisms

4.2.1. Differences in formation positions of the NL-loop 1 and NL-loop 2

The formation process of the NL-loop 1 in each N-cell cycle is repetitive. An example of this process is presented in figure 11, where the vortex structures are shown from both $+Y$ and $-Y$ sides of the step cylinder. In figure 11(a,b), and the corresponding zoom-in plots (figure 11f,g), the foot of vortex N8 completely

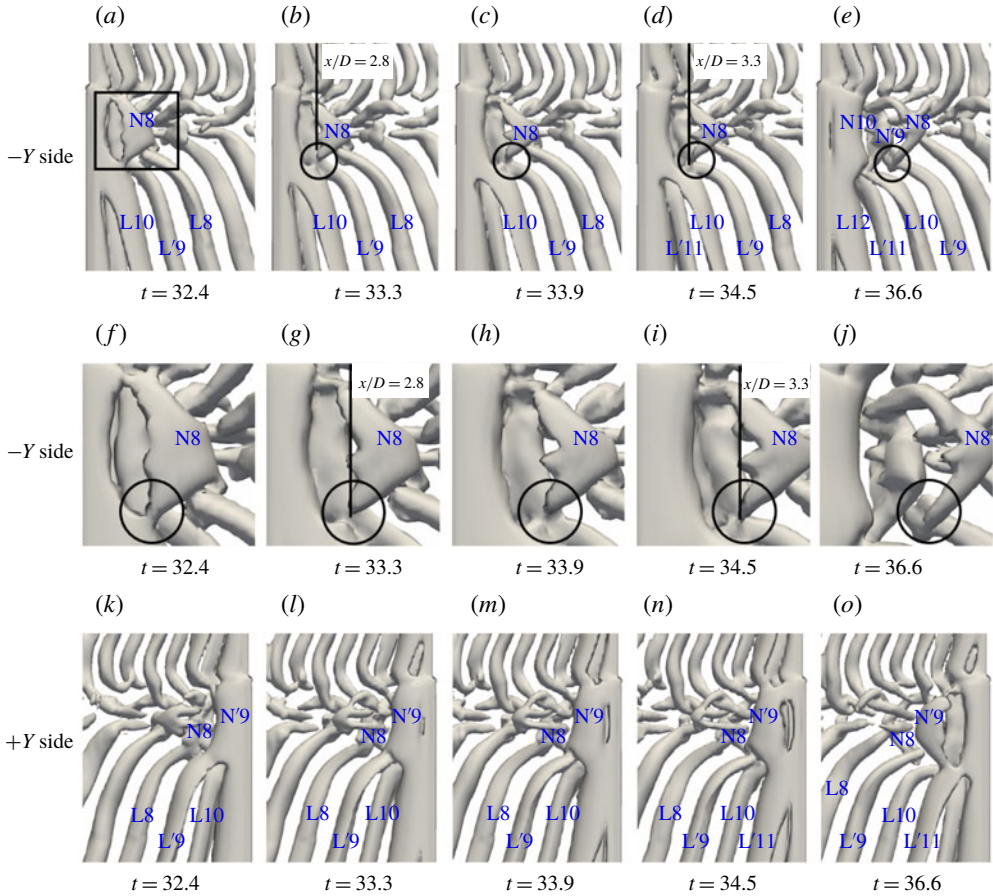


FIGURE 11. The formation process of the NL-loop 1 structure in the first dislocation process (defined in figure 7) is shown from the $-Y$ and $+Y$ sides in (a–e) and (k–o) rows, respectively. In (f–j), zoom-in plots of vortex structures at N-cell region (black rectangle in panel a) are shown. The black circles highlight the position where the NL-loop 1 forms.

disconnects from the shear layer at $x/D=2.8$ (marked by a black line in figure 11(b,g)). At this moment ($tU/D=33.3$) the NL-loop 1 structure has not yet formed, because there is still no direct connection between N8 and L'9. It takes some more time for N8 to convect downstream and eventually develop into the NL-loop 1 with L'9 at $x/D=3.3$ and $tU/D=34.5$. This process is indicated in figure 11(b–e) and the corresponding zoom-in plots (figure 11(g–j)). By following the same process as described in §4.1, we found that from $tU/D=33.3$ to 34.5, the streamwise distance between vortex N'9 and L'9 increases from $5.3D$ to $6.1D$ as they move downstream. When Φ between vortex N'9 and L'9 increases, L'9 gradually disconnects from its counterpart N'9 and forms the NL-loop 1 with N8 (see figure 11k–o).

Unlike the NL-loop 1 structure, which has a distinct formation position, it is difficult to pinpoint where the NL-loop 2 forms. As shown in figure 12(a–e), in the black circle area, it is not clear how the foot of vortex N'9 completely separates from the shear layer and subsequently connects to L10 as they move downstream. The connection between N'9 and L10 forms in the very near wake before N'9

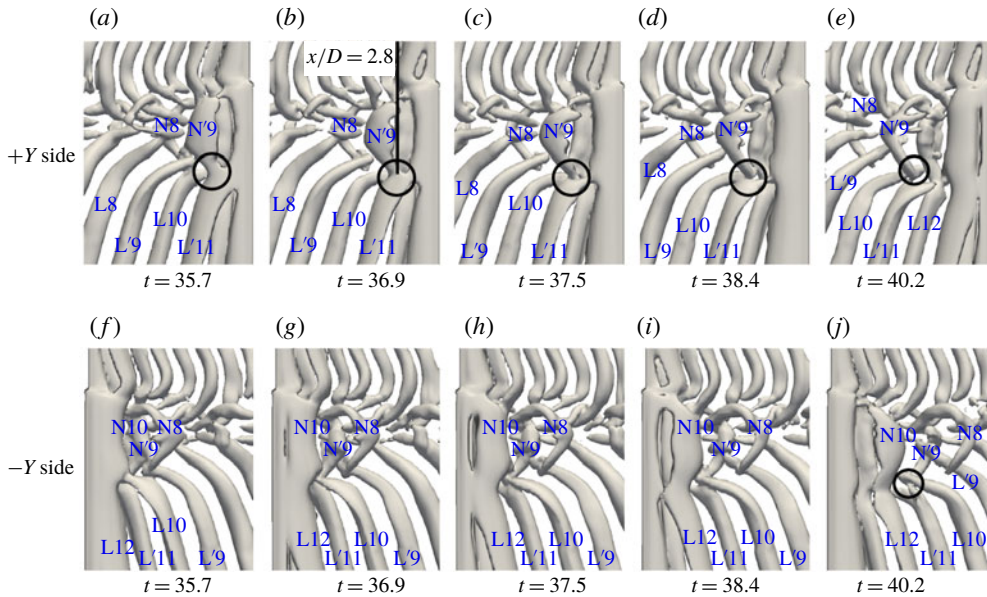


FIGURE 12. The formation process of the NL-loop 2 structure in the first dislocation process is shown from both +Y and -Y sides. The black circles highlight the position where the NL-loop 2 structure is formed.

completely disconnects from the shear layer. In order to compare with the formation process of the NL-loop 1 structure shown in figure 11, we use the same method to monitor the variation of the streamwise distance between vortices N10 and L10. At $tU/D = 36.9$ (the corresponding instantaneous isosurface of the vortex structure is shown in figure 12(g)), the distance between vortex N10 and L10 reaches $5.9D$. This is very close to the distance between N'9 and L'9 at $tU/D = 34.5$ (figure 11n), when L'9 successfully induces N8 to connect to itself and together form the NL-loop 1 structure. At $tU/D = 36.9$, as shown in figure 12(b), the leg of vortex N'9 is at position $x/D = 2.8$. At the same downstream position, the foot of vortex N8 already disconnects from the shear layer, as shown in figure 11(b). It is reasonable to speculate that Φ between N10 and L10 becomes sufficiently large to attract N'9 to connect to L10 before it disconnects from the shear layer. As a consequence, the formation position of NL-loop 2 is not so clear.

The time trace of Φ_f accumulation proves our speculation. By using the method described in appendix A, the time trace of Φ_f accumulation in the first N-cell cycle is shown in figure 13(b). Circles in this figure represent Φ_f of corresponding N- and L-cell vortices, in which the green circle represents Φ_f between N'9 and L'9, and the red circle represents Φ_f between N10 and L10. Eventually, the dislocations of the vortex pairs corresponding to the green and red circles cause formation of the NL-loop 1 structure (N8-L'9) and the NL-loop 2 structure (N'9-L10), respectively.

One can see that the red circle represents a larger Φ_f value than the green one, which means that Φ_f between N10 and L10 is larger than that between N'9 and L'9. Therefore, compared to the vortex pair N10-L10, the vortex pair N'9-L'9 needs a larger contribution of Φ_c to achieve a sufficiently large Φ to trigger the vortex dislocation between them, and the subsequent formation of the NL-loop 1 (N8-L'9). In other words, due to the reduced need of a contribution from Φ_c , the vortex dislocation

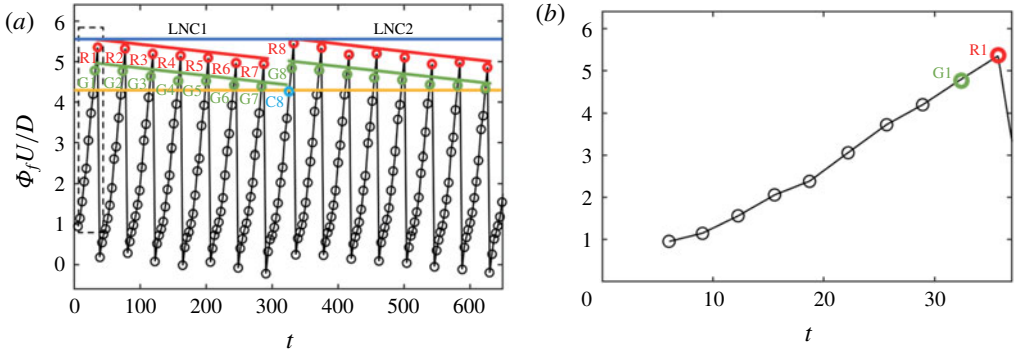


FIGURE 13. (a) Time trace of Φ_f between corresponding N-cell and L-cell vortices in the first (LNC1) and second (LNC2) long N-cell cycles, i.e. from the first to the 15th N-cell cycle. The circles represent Φ_f between an N-cell vortex and its counterpart L-cell vortex. The green and red circles indicate Φ_f , which eventually causes formation of the NL-loop 1 and NL-loop 2 structures, respectively. From the first to the eighth N-cell cycle, the green and red circles are numbered. (b) A zoom-in plot of the time trace of Φ_f in the first N-cell cycle (the black dashed rectangle in panel a). From the left to the right, circles represent Φ_f between the vortex pair N'1–L'1 to the vortex pair N10–L10, respectively. (Note that the detailed calculation processes can be found in appendix A. All detailed data about Φ_f and the longer-time trace of Φ_f are included in the supplementary material, file 1, available at <https://doi.org/10.1017/jfm.2020.110>. The trigger value and the threshold value are estimated based on 55 N-cell cycles, as shown in supplementary file 3.)

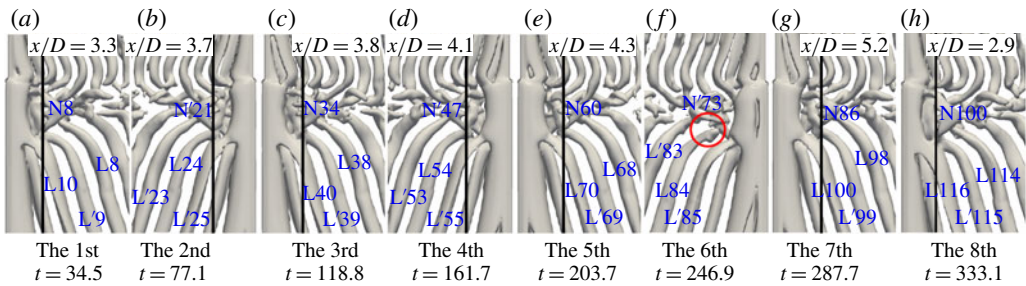


FIGURE 14. The just-formed NL-loop 1 structures in the first to the eighth N-cell cycle are plotted from both the $-Y$ and $+Y$ sides (the first long N-cell cycle consists of the first to the seventh N-cell cycles). The black line marks the formation position of NL-loop 1. The red circle in panel (f) highlights an irregular absence of the NL-loop 1 structure, which will be discussed later.

between N10 and L10 and the subsequent NL-loop 2 (N'9–L10) is formed closer to the cylinder, which causes the unclear formation position.

4.2.2. Variation of formation positions of the NL-loop 1 structures

In figure 14, the NL-loop 1 structures in the first eight N-cell cycles are plotted. The black vertical lines show the positions where the NL-loop 1 structures just form.

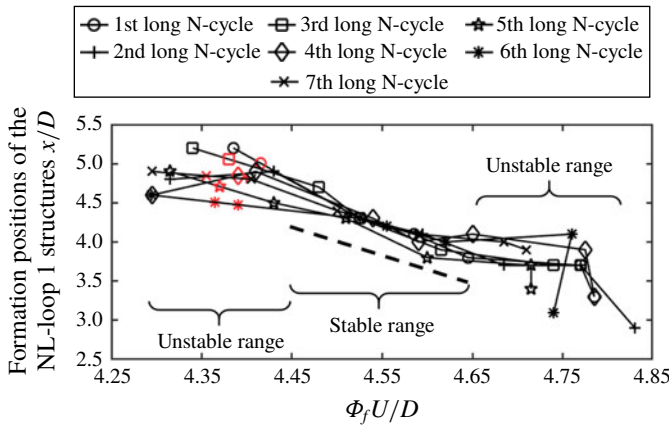


FIGURE 15. Relation between Φ_f and the formation position (x/D) of corresponding NL-loop 1 structures in the first to the seventh long N-cell cycles (52 N-cell cycles are included). Based on the trends of the curves, one stable range and two unstable ranges are identified. A straight dashed line outlines the trend of the stable range. The occasionally absent NL-loop 1 structures in these seven long N-cell cycles are marked by red colour at the expected formation positions, which can be obtained by linear interpolation.

N-cell cycle no.	1	2	3	4	5	6	7
Formation position (x/D)	3.3	3.7	3.8	4.1	4.3	—	5.2
$\Phi_f U/D$	4.485	4.470	4.345	4.275	4.225	4.115	4.085

TABLE 3. Formation positions and Φ_f values that cause the NL-loop 1 structures in the first to seventh N-cell cycle (the first long N-cell cycle). The corresponding vortex structures are shown in figure 14(a–g). In the sixth N-cell cycle, there is a loop formation failure.

Except for the sixth N-cell cycle (figure 14f), the NL-loop 1 structures alternately appear at the +Y and -Y side of the step cylinder from the first to the seventh N-cell cycles (the first long N-cell cycle). The shape and the formation position of the NL-loop 1 structure also vary, as depicted in figure 14(a–h).

In table 3, the relation between the formation positions of the NL-loop 1 structures in the first long N-cell cycle and their Φ_f are presented. One can see that, except for the sixth N-cell cycle, the formation positions move downstream as the corresponding Φ_f decreases. This can easily be ascribed to the already discussed two different phase difference accumulation mechanisms. Formation of the NL-loop 1 structures requires sufficiently large Φ . Since Φ_f decreases, Φ_c must contribute more, which consequently leads to a longer formation time and further downstream formation position. To be more clear, the relations between Φ_f and formation positions of the corresponding NL-loop 1 structures during the first–seventh long N-cell cycles are plotted in figure 15. Generally, except for several irregular points, the formation position shifts downstream as Φ_f decreases. (Note that the appearances of the irregular points will be discussed in § 5.3.)

Based on the discussions above, we conclude that, for the NL-loop structures, Φ is accumulated by the joint influence of different shedding frequencies and different convective velocities

$$\Phi = \Phi_f + \Phi_c. \quad (4.1)$$

As the relative magnitude of Φ_f and Φ_c varies, the formation processes of the NL-loop structures change.

5. Characteristics of the long N-cell cycles

5.1. Trend of Φ_f variation

The time trace of Φ_f accumulation between corresponding N- and L-cell vortices is plotted in figure 13(a). We use green and red circles to indicate Φ_f of the pair of N- and L-cell vortices whose dislocation eventually causes the NL-loop 1 and NL-loop 2, respectively. Two solid lines with the same corresponding colours describe the decreasing tendency in Φ_f of both NL-loop 1 and NL-loop 2 over time.

The gradual decrease of Φ_f in each N-cell cycle can be expressed as

$$S = \alpha \frac{1}{2f_L} - \beta \frac{1}{2f_N}, \quad (5.1)$$

where S (with dimension D/U) is a measure of the phase shift of every vortex pair in one N-cell cycle, as compared to the N-cell cycle before it. In this expression, α and β represent the number of L- and N-cell vortices in one N-cell cycle; and f_L and f_N are the shedding frequencies of L- and N-cell vortices. In the present case, $\alpha = 15$, $\beta = 13$, $f_L D/U = 0.1780$ and $f_N D/U = 0.1545$ (from figure 5), from which we obtain $S = 0.064D/U$. This means that, in one N-cell cycle, the duration of 13 N-cell and 15 L-cell vortices is not exactly the same. Although S has a very small value, after a certain number of N-cell cycles, the accumulated difference becomes large enough to influence the dislocation process. Moreover, by checking figure 13(a) and the supplementary file 1, one can find that from R1 to R7 or from G1 to G7, Φ_f decreases by approximately $0.4D/U$, i.e. Φ_f decreases by around $0.067D/U$ after every N-cell cycle, which is close to the S value from expression (5.1).

It is worth mentioning that the numbers $\alpha = 15$, $\beta = 13$ and $S = 0.064D/U$ are related to the particular configuration studied. For different configurations, i.e. different D/d and Re_D , these numbers in expression (5.1) may vary. But what we observe in figure 13(a) will be a common feature, because it is extremely unlikely to attain an S value exactly equal to zero.

5.2. Interruption of the antisymmetric phenomenon

From figure 14(a–h), one can clearly see that the NL-loop 1 structure alternately appears at the $-Y$ and $+Y$ side of the step cylinder in subsequent N-cell cycles. This is the antisymmetric phenomenon reported in Tian *et al.* (2017a). In the present case, the long-time observation reveals that this antisymmetric phenomenon will be interrupted once in a while. As shown in figure 14(g,h), instead of being antisymmetric, the loop structures in the seventh and eighth N-cell cycles are symmetric. In these two N-cell cycles, both NL-loop 1 structures, i.e. N86–L'99 and N100–L'115, are formed at the $-Y$ side.

This interruption is caused by the decreasing tendency in Φ_f , as we discussed in §5.1. Normally, there are 13 N-cell and 15 L-cell vortices in one N-cell cycle. The

odd number of N-cell vortices causes the antisymmetric phenomenon. However, as shown in figure 13(a), when Φ_f continues to decrease along the green line from G1 to C8, it eventually becomes insufficient in point C8. Even by including the contribution of Φ_c , Φ is still not large enough to induce the formation of the expected NL-loop 1 (N'99–L114). Therefore, in this N-cell cycle, one additional vortex pair shedding is needed to make Φ sufficiently large to induce formation of the NL-loop 1. The additional one pair of N- and L-cell vortices makes the number of N-cell vortices in the eighth N-cell cycle become even, and thereby interrupts the antisymmetric phenomenon. In the supplementary file 3, the time trace of Φ_f between N- and L-cell vortices in the first to the eighth long N-cell cycles (the first to the 55th N-cell cycles) is illustrated.

5.3. Trigger value and threshold value of vortex dislocations

Based on the results from earlier papers (Williamson 1989; Morton & Yarusevych 2010b) and our discussions in §§ 5.2 and 4, it is clear that only when Φ becomes sufficiently large can the vortex dislocation process be triggered. We call this value the ‘trigger value’. Based on (4.1), Φ consists of two parts, Φ_f and Φ_c . Owing to the complexity of Φ_c , an accurate trigger value is hard to obtain, but an approximate value is possible to estimate. As we discussed in § 4, unlike the NL-loop 1 structure, which has a clear formation position, the NL-loop 2 structure forms in the near wake. This makes it hard to define the exact formation position of the NL-loop 2. It means that the Φ_f that induces this NL-loop 2 is very close to the trigger value, and only a modest contribution from Φ_c is needed. Therefore, by considering all the largest Φ_f corresponding to the NL-loop 2 structures, we can draw the blue line in figure 13(a) to approximate the trigger value (around $5.60D/U$).

Besides the trigger value, there is another interesting value of Φ_f that should be noted. As we discussed in § 5.2, when Φ_f continues to decrease from G1 to C8 (figure 13a), the expected formation of the NL-loop 1 (N'99–L118) fails. We can speculate that there is a threshold value for Φ_f , such that when Φ_f becomes less than this value, a vortex dislocation will not occur, even when taking the contribution from Φ_c into account. By connecting all of the smallest values of Φ_f in green (Φ_f inducing the NL-loop 1), the threshold value can be estimated by the yellow line in figure 13(a), with a value around $\Phi_f U/D = 4.30$.

Owing to the complexity of Φ_c , the formation of NL-loop structures becomes quite unstable when Φ_f is close to the trigger value or to the threshold value. As shown in figure 15, one stable Φ_f range and two unstable Φ_f ranges can be identified. A dashed straight line outlines the trend in the stable range ($4.45 \lesssim \Phi U/D \lesssim 4.65$), in which the distribution of markers is concentrated, and the formation position decreases almost linearly as Φ_f increases. Outside this stable range, the tendency becomes unclear. When Φ_f is smaller than $4.45D/U$, i.e. much smaller than the trigger value $5.60D/U$ and close to the threshold value $4.30D/U$, the contribution of Φ_c becomes significant and determines whether the NL-loop 1 is able to be formed or not. Figure 15 shows that, in the unstable range ($4.30 \lesssim \Phi_f U/D \lesssim 4.45$), all NL-loop 1 structures are generated beyond a downstream position $x/D = 4$, i.e. Φ of these NL-loop 1 structures cannot exceed the trigger value upstream of $x/D = 4$. In this situation, how much Φ_c can accumulate downstream of $x/D = 4$ determines whether these NL-loop 1 structures will appear or not. In figure 10(b), we see apparent differences between the convective velocity in the N- and L-cell regions, while these differences diminish as we move downstream. Downstream of $x/D = 4$, the differences become very small.

In other words, the accumulation of Φ_c is modest downstream of $x/D = 4$. Based on the above observation, we can conclude that, for the NL-loop 1 structures with Φ_f in the range $(4.30D/U-4.45D/U)$, their phase differences are around a critical value, and a small variation in Φ_c can influence their formation positions, and even lead to unsuccessful formations. The fact that all the red markers in figure 15, which represent the occasionally absent NL-loop 1 structures, are located in this range also supports this conclusion.

Another unstable range appears when Φ_f corresponding to NL-loop 1 becomes larger than $4.65D/U$, which is close to the approximate level of the trigger value. In this situation, only a small contribution from the convective velocity is needed for NL-loop 1 to form. Meanwhile, as shown in figure 10(b), when x/D is smaller than 3 ($x/D = 1.4, 1.6, 1.8, 2, 3$) the differences between the convective velocities in the N- and L-cell regions are obvious. These differences are able to increase Φ_c rapidly. Variations in the convective velocity could also affect the formation position, and lead to a less clear tendency.

Detailed investigations show that many interesting and important features of vortex dislocation in a step cylinder wake may easily be overlooked if the observation time is too short. In the present case, during one long N-cell cycle, most N-cell cycles need an odd number of N- and L-cell vortices to accumulate sufficient Φ , and to trigger the vortex dislocation, which leads to antisymmetry between subsequent N-cell cycles. However, between two long N-cell cycles, the antisymmetry is interrupted. In our earlier paper (Tian *et al.* 2017a), we did not foresee this interruption, because we tried to conclude that the antisymmetric dislocation process is a result of $f_L/f_{beat} \approx 7.5$, such that two dislocations are needed to compensate for the frequency differences between the N- and L-cells, and that the wake could return to normal one-to-one shedding. However, more detailed observations based on substantially longer simulations show that the small differences (i.e. S in expression (5.1)), which were ignored when we obtain the $f_L/f_{beat} \approx 7.5$ relationship, are continuously accumulating and cause a decreasing tendency in the time trace of Φ_f . This is exactly what causes the interruption of the antisymmetry discussed in this section. We note again that these results require exceptionally long simulations. The value of S is so small that it may easily be ignored in short-term observations. But it turns out to lead to very interesting vortex dislocation phenomena. We mentioned that McClure *et al.* (2015) also reported similar small differences in the vortex dislocations behind a dual step cylinder. However, instead of investigating how different vortex dislocations vary, they focused on when two identical vortex dislocations appear.

6. Investigation on universality

In order to investigate the universality of the two different phase difference accumulation mechanisms and their effects on vortex dislocations, the wake behind a step cylinder with $D/d = 2.4$ at the same $Re_D = 150$ is investigated. All observations are consistent with our findings from the $D/d = 2.0$ case and support our previous discussions and conclusions.

In general, comparing with the wake in the $D/d = 2$ case, the change in D/d brings no fundamental changes. As shown in figure 16, the three dominating frequency components, i.e. St_S , St_N and St_L , and the beat frequency St_{beat} are all captured, similar as in figure 5(a). Moreover, similar non-uniform distributions of the mean streamwise velocity \bar{u} are shown in figure 17. This means that, for the $D/d = 2.4$ case, the differences in convective velocities in the N- and L-cell regions can increase Φ when vortices convect downstream, just as for the $D/d = 2.0$ case.

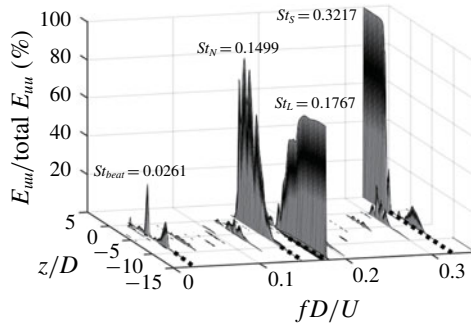


FIGURE 16. Streamwise velocity spectra in the $D/d = 2.4$ case are calculated based on $1200D/U$ continuous velocity data along a vertical sampling line parallel to the Z -axis at position $(x/D, y/D) = (0.6, 0.2)$.

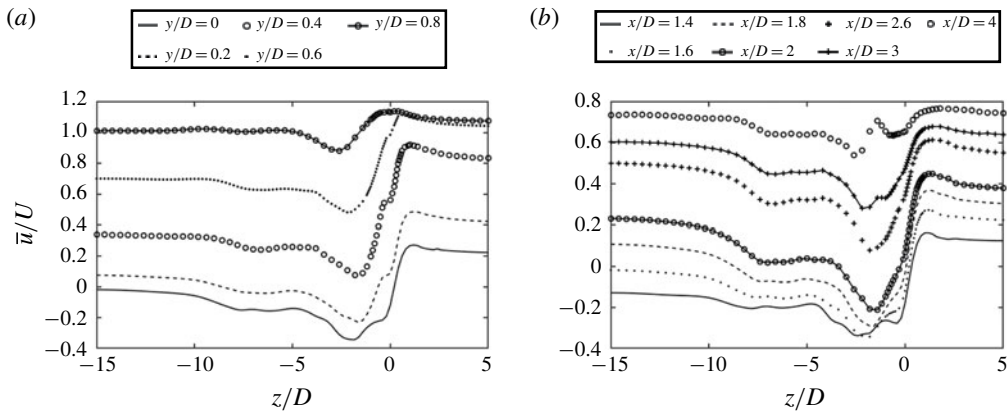


FIGURE 17. Distributions of mean streamwise velocity \bar{u}/U in the $D/d = 2.4$ case.

In figure 18(a,b), the two phase difference accumulation mechanisms (4.1) are examined. As Φ_f decreases along the red and green lines in figure 18(a), larger contributions from Φ_c are needed to make Φ sufficiently large to trigger the vortex dislocation, which makes the formation positions of the NL-loop 1 structures move downstream during two long N-cell cycles, as shown in figure 18(b).

This decreasing tendency in Φ_f corresponding to the NL-loop 1 and NL-loop 2 in figure 18(a) can be explained by (5.1). In figure 18(a), from G1 to G7, Φ_f decreases by $0.52D/U$ ($4.69D/U - 4.17D/U$), i.e. it decreases by around $0.087D/U$ after every N-cell cycle, which is close to the value from (5.1), i.e. $13 \times 1/(2 \times 0.1767U/D) - 11 \times 1/(2 \times 0.1499U/D) = 0.094D/U$. As Φ_f continues to decrease, the expected interruption of the conventional antisymmetry appears in the $D/d = 2.4$ case. The NL-loop 1 structures in seven continuous N-cell cycles are plotted in figure 19(a)–(g). The NL-loop 1 alternately appears at the $-Y$ and $+Y$ side in the first six N-cell cycles, i.e. from the second to the seventh N-cell cycle, from figure 19(a) to (f). But this conventional antisymmetry is interrupted in the seventh and eighth N-cell cycles. In figure 19(f,g), the NL-loop 1 appears at the same side of the step cylinder. Based on the interruption of the antisymmetry, the

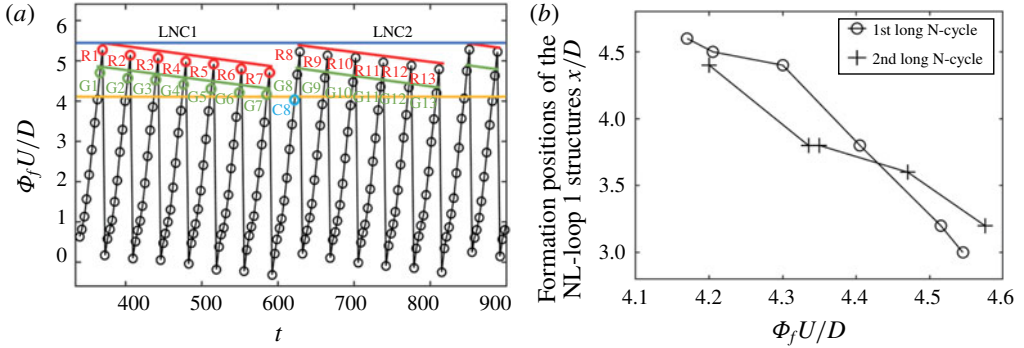


FIGURE 18. (a) Time traces of Φ_f between N-cell and L-cell vortices are plotted in the first and second long N-cell cycles in the $D/d = 2.4$ case. The same annotations as in figure 13 are also used here. (b) Relation between Φ_f and the formation position (x/D) of NL-loop 1 structures in the first and second long N-cell cycles in the $D/d = 2.4$ case (same as in figure 15). (All detailed data about φ and Φ_f are included in the supplementary file 2.)

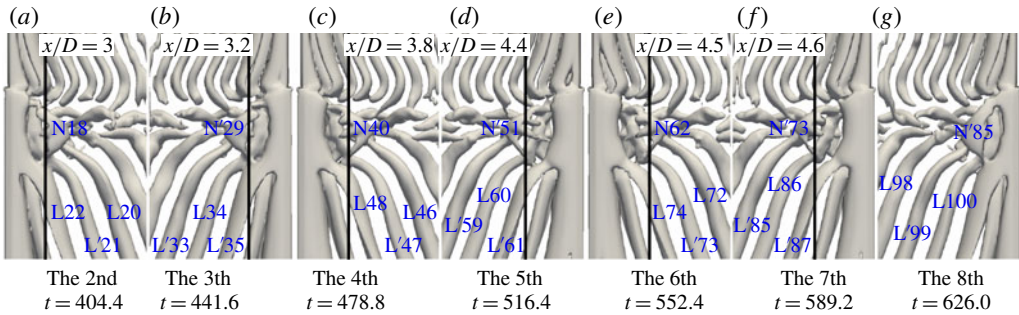


FIGURE 19. From (a) to (g), the NL-loop 1 structures in the second to the eighth N-cell cycles are plotted from both the $-Y$ and $+Y$ side in the $D/d = 2.4$ case. The black line marks the formation position of an NL-loop 1.

long N-cell cycle, the trigger value (blue line) and the threshold value (yellow line) are also indicated in figure 18(a), similar as in the $D/d = 2$ case.

These investigations prove that our discussions and conclusions in §§ 4 and 5 are valid not only in the wake behind the step cylinder $D/d = 2$ case, but also in other D/d cases.

7. Conclusions

We use DNS to investigate vortex interactions, especially the vortex dislocations between the N- and L-cell vortices, in the near wake behind two single step cylinders with diameter ratio $D/d = 2$ and 2.4 at $Re_p = 150$. Our results in the $D/d = 2$ case show good agreement with previous studies (Dunn & Tavoularis 2006; Morton & Yarusevych 2010b; Tian *et al.* 2017a), with respect to the three dominating spanwise vortices (i.e. S-, N- and L-cell vortices), vortex dislocations occurring at the N-L cell boundaries, loop structures (NL-loop 1 and NL-loop 2) appearing

during the dislocation processes, and antisymmetric phenomena between subsequent N-cell cycles. In addition, the numerical results provide more detailed information on how the phase difference (Φ) between the corresponding N- and L-cell vortices is accumulated and finally triggers the formation of vortex dislocations and concomitant NL-loop structures. A phase difference accumulation mechanism is identified for the first time, i.e. $\Phi = \Phi_f + \Phi_c$. We have clearly identified that there are two qualitatively different physical factors contributing to the accumulation of Φ : one is different shedding frequencies (Φ_f), the other is varying convective velocities in the different vortex cell regions (Φ_c). While Φ_f is relatively well known, the contribution from convective velocity Φ_c has never been examined before.

Based on the new understanding of the phase difference accumulation mechanism, we manage to obtain a clearer insight into various phenomena during the dislocation process. Most importantly, the variations of the formation position of the NL-loop 1 and NL-loop 2, and the irregularity of the NL-loop 1 formation, have been fully explained. For a pair of N- and L-cell vortices, as Φ_f decreases, Φ_c must contribute more to ensure a sufficiently large Φ (we refer to it as the trigger value) that can trigger the vortex dislocations. This makes the formation position of the corresponding NL-loop structure move downstream.

Moreover, the long-time trace of the accumulation of Φ_f clearly shows cyclic trends, which are caused by minute differences accumulated during each N-cell cycle (as indicated by S in expression (5.1)). Owing to the accumulation of this difference, the antisymmetric phenomenon, reported in Tian *et al.* (2017a), will be cyclically interrupted when Φ_f decreases below a certain value. We refer to this value as the threshold value. The long N-cell cycle is defined based on this phenomenon. Finally, in §6, the universality of our discussions and conclusions is justified by investigating the $D/d = 2.4$ case.

The identification of the phase difference accumulation mechanism, explanations of the formation positions of the NL-loops and observations of the long-period characteristics offer a deeper and more complete understanding of the vortex dislocation phenomenon in the wake behind a step cylinder.

Although all investigations in the present paper are based on single step cylinders at Reynolds number 150, the N- and L-cell vortices and their vortex dislocations were observed in other step cylinder cases with $1.55 < D/d < 2$ at $67 < Re_D < 1100$ (Norberg 1992; Dunn & Tavoularis 2006; Morton & Yarusевич 2010a,b). In these cases, due to the abrupt change in diameter, vortex shedding frequencies and convective velocities are different in N- and L-cell regions. With these two mechanisms present in the flow, we believe that our discussions and conclusions are also valid for the above-mentioned cases. We anticipate that the phase difference accumulation mechanism we report here also exists in other wake flows that contain several adjacent spanwise vortices. In addition, the method we have developed to obtain the phase information and phase differences of vortices may also be applicable in other wake flows.

Acknowledgements

Computing resources were granted by the Norwegian Research Council (Program for Supercomputing, nn9191k). C.T. would like to thank the China Scholarship Council (CSC) for financial support.

Declaration of interests

The authors report no conflict of interest.

Supplementary material

Supplementary material is available at <https://doi.org/10.1017/jfm.2020.110>.

Appendix A. The method used to obtain the phase information and phase difference of vortices

In order to perform detailed investigations on how the phase difference between corresponding N- and L-cell vortices accumulates and triggers the vortex dislocation, we need a reliable method to obtain the phase information (φ) and the phase difference (Φ) of the wake vortices. According to Green & Gerrard (1993) and Griffin (1995), the end of the vortex formation region coincides with the location where the vortex strength becomes maximum. By monitoring the time traces of the strength of a vortex and the corresponding vorticity distribution along a centreline at $y/D = 0$, we found that in the present low-Reynolds-number case the time instant when the vortex strength reaches its maximum coincides with the instant at which the corresponding largest ω_z appears at the centreline. A detailed example is shown in supplementary file 4. Based on this feature, the ‘shed position’ of a vortex is defined as the position where the corresponding largest ω_z appears at the centreline. Moreover, φ of one vortex is defined as the time instant when the corresponding ω_z reaches its maximum at the sampling point. At a downstream sampling point, Φ between a pair of N- and L-cell vortices is the time difference between the time instants when they pass this sampling point:

$$\Phi = \varphi_N - \varphi_L. \quad (\text{A } 1)$$

Ideally, we monitor φ_N and φ_L at the shed position of the N- and L-cell vortex, respectively. Then, by using equation (A 1), Φ can be obtained. However, there are two challenges:

- (i) Only when both the N- and L-cell vortex are monitored at the same downstream position can we get Φ between them without taking the effects from the convective velocity into account. Owing to different shedding frequencies, the shedding positions of the N- and L-cell vortices are different. Moreover, the fluctuations in the shedding frequencies of N-cell vortices, as discussed in § 3.2, make the situation even more complicated.
- (ii) In the L-cell region, due to the oblique shedding, the phases of the L-cell vortices vary when the sampling point shifts in the spanwise direction.

The general process developed to overcome these two challenges is as follows. (1) Find the regular shedding regions of the N- and L-cell vortices. (2) Monitor shed positions of the N- and L-cell vortices, and find the suitable sampling positions for both of them. (3) Develop a method to minimize effects of the oblique shedding in the L-cell region. The complete process of obtaining Φ in the $D/d = 2$ case is described in the following.

A.1. Selection of the sampling region and the signal variable

The root mean square (r.m.s.) values of the spanwise vorticity ω_z in a part of the N-cell region ($-3.2 < z/D < -2.4$) and the L-cell region ($-18.8 < z/D < -15.8$) are plotted in figure 20. From figure 20(a), one can see that, except for the lowest curve (at $z/D = -2.4$), the trends of the other five curves are the same. Especially at position $z/D = -2.8$ and -2.9 , the r.m.s. values coincide, as presented in the zoom-in view

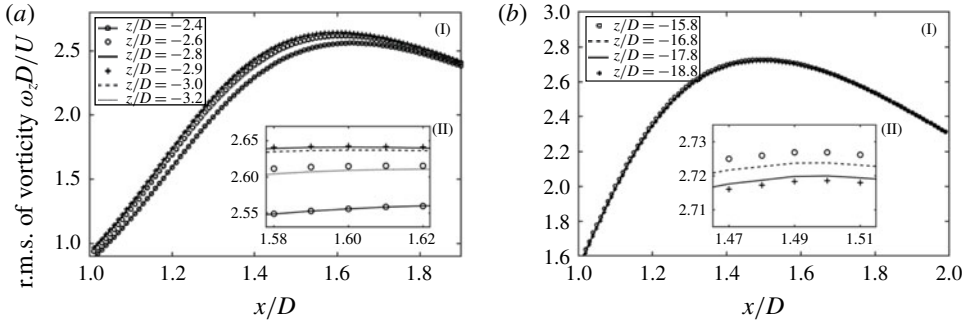


FIGURE 20. (a) (I) The distribution of r.m.s. of vorticity component $\omega_z D/U$ in a part of the N-cell region ($-3.2 < z/D < -2.4$). (II) A zoom-in view of the peak area of the curves in main panel (I). (b) (I) The distribution of r.m.s. of vorticity component $\omega_z D/U$ in a part of the L-cell region ($-18.8 < z/D < -15.8$). (II) A zoom-in view of the peak area of the curves in main panel (I).

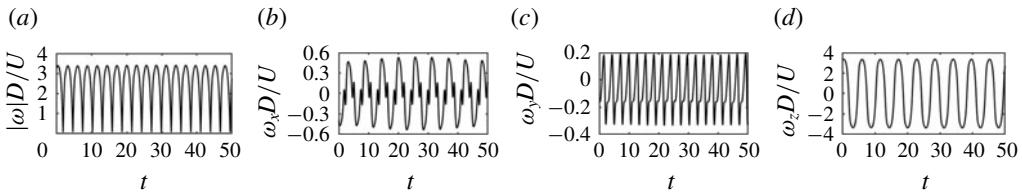


FIGURE 21. The time traces of magnitude of vorticity ($|\omega|D/U$) and its three components ($\omega_x D/U$, $\omega_y D/U$ and $\omega_z D/U$) in the L-cell region at the point $(x/D, y/D, z/D) = (1.5, 0, -15.8)$ are plotted in panels (a), (b), (c) and (d), respectively.

(figure 20a(II)). This means that the N-cell vortices can be treated as a regular shed spanwise vortex in the region $-3.2 \lesssim z/D \lesssim -2.6$. In the L-cell region, as illustrated in figure 20(b), the differences between the results of four sampling points are negligible. The zoom-in view (figure 20b(II)) shows that the largest difference in r.m.s. of ω_z is approximately $0.01U/D$, i.e. only 0.3% of the peak value. Generally, the regions $-3.2 \lesssim z/D \lesssim -2.6$ and $z/D \lesssim -15.8$ can be treated as the regular shedding region of N- and L-cell vortices, respectively.

As illustrated in § 3.2, far away from the step position, vortices shed regularly in the L-cell region. In figure 21, the vorticity magnitude $|\omega|$ and the three vorticity components (ω_x , ω_y and ω_z) are checked at point $(x/D, y/D, z/D) = (1.5, 0, -15.8)$. The time traces of all three vorticity components completely repeat themselves with the same period as the L-cell vortex. All vorticity components oscillate regularly enough to be used to monitor Φ of L-cell vortices. On the other hand, in the N-cell region, the vortex shedding is more complicated. In figure 22, at the position $(x/D, y/D, z/D) = (1.5, 0, -2.9)$, which is in the regular shedding region of N-cell vortices, the time traces of both ω_x and ω_y show substantial irregularities, which are possibly caused by the intensive downwash (Dunn & Tavoularis 2006) and the two pairs of streamwise vortices (Dunn & Tavoularis 2006; Morton *et al.* 2009), respectively. However, without disturbances, ω_z oscillates regularly in figure 22(d).

In general, ω_z of the N- and L-cell vortices oscillate regularly in parts of their shedding regions. It therefore becomes reasonable to select ω_z as the signal variable.

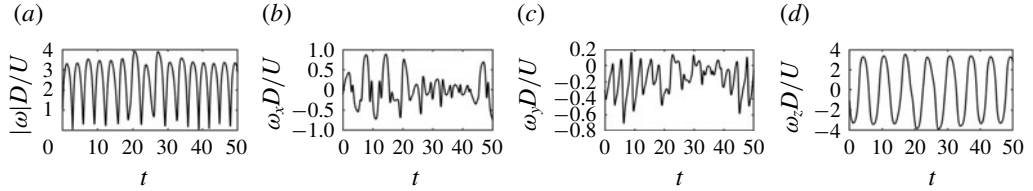


FIGURE 22. Same as in figure 21, but at a different position $(x/D, y/D, z/D) = (1.5, 0, -2.9)$, i.e. in the N-cell region.

A.2. The method for obtaining the phase (φ) and the shed position of vortices

Both the N- and L-cell vortices shed alternately from the two sides of the step cylinder. As mentioned at the beginning of appendix A and in supplementary file 4, in the present low-Reynolds-number case, the strength of a vortex and its induced vorticity at the centreline ($y/D = 0$) approximately reach their extreme values at the same time. Therefore, we can obtain φ and the shed position of vortices by monitoring the distributions of ω_z in the symmetry plane. (Note that the following analysis is based on data obtained from high-density ($0.01D$) sampling lines with sampling frequency $200U/D$. Considering that the shedding frequency of the N- and L-cell vortex is around $0.2U/D$, $200U/D$ is long enough to get accurate results.)

(i) Determination of φ and shed position of the vortex along a sampling line.

By checking the variation of ω_z along a sampling line in the symmetry plane ($y/D = 0$), the shed position and φ of each vortex can be obtained. In figure 23(a), as a vortex passes through a sampling line (from $(x/D, y/D, z/D) = (1, 0, -15.8)$ to $(2, 0, -15.8)$), the distributions of ω_z along this line are plotted in the period from $tU/D = 4.205$ to 6.205 with a time interval $0.1D/U$. In figure 23(a), the maximum of each curve is marked by a small red circle, whose position $(x/D, \omega_z D/U)$ represents the core line position and strength of the source vortex. A zoom-in plot of the red circle concentrated area (black rectangular area in panel (a)) is shown in figure 23(b), and the corresponding time trace of these red circles is plotted in figure 23(c). The number below each red circle represents its temporal order. One can see that, from the first to the tenth red circle, the corresponding ω_z gradually reaches its maximum at $x/D = 1.46$ (as shown in figure 23b) and at $tU/D = 5.265$ (as shown in figure 23c). This means that the source vortex contains maximum vorticity and separates from the shear layer at $x/D = 1.46$ when $tU/D = 5.265$. In other words, the shed position of this vortex is $x/D = 1.46$, and the corresponding φ at position $(x/D, y/D, z/D) = (1.46, 0, -15.8)$ is $5.265D/U$.

(ii) Obtaining φ of vortices at a fixed sampling point.

For a fixed sampling point in the symmetry plane ($y/D = 0$), ω_z will oscillate as vortices pass through the point. When the core lines of vortices pass the sampling point, ω_z reaches its extremum at this point. Figure 23(d) shows the oscillation of ω_z at position $(x/D, y/D, z/D) = (1.46, 0, -15.8)$, from which the abscissa of the peaks and troughs of this curve represents φ of vortices shed from the $-Y$ and $+Y$ sides of the step cylinder, respectively.

A.3. Monitoring both the N- and L-cell vortices at the same downstream position

In figure 24, the shed positions of the N- and L-cell vortices in the first $500D/U$ are examined. Figure 24(b) shows that, at two spanwise positions $z/D = -15.8$ and -17.8

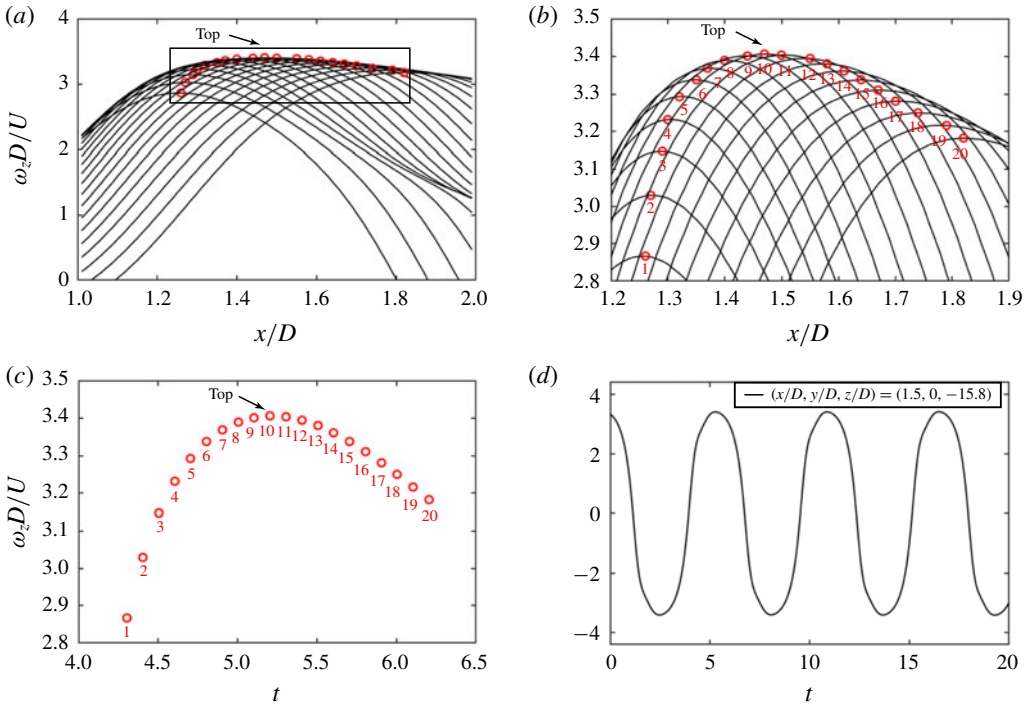


FIGURE 23. (a) From $tU/D = 4.205$ to 6.205 , distributions of vorticity $\omega_z U/D$ along a sampling line (from $(x/D, y/D, z/D) = (1, 0, -15.8)$ to $(2, 0, -15.8)$) are plotted with a time interval of $0.1D/U$. The maximum of each curve is marked by a small red circle. (b) A zoom-in plot of the rectangular area in panel (a), where the number below each red circle represents the time series of the corresponding curve. (c) Time trace of the maximum vorticity $\omega_z U/D$ (red circles in panel (a)). (d) Time trace of vorticity ω_z at sampling point $(x/D, y/D, z/D) = (1.5, 0, -15.8)$.

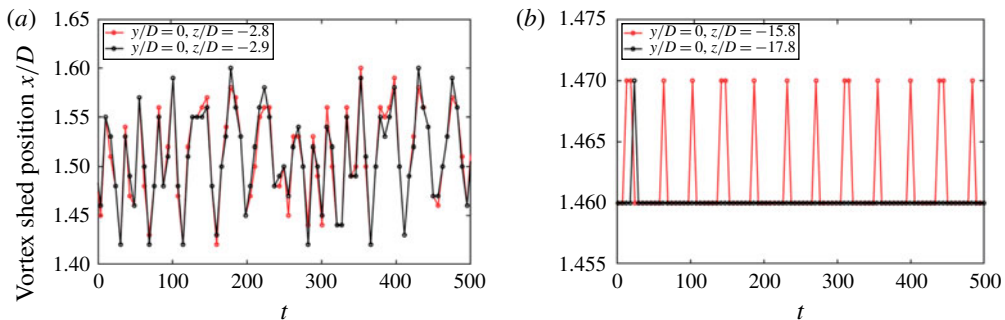


FIGURE 24. (a) Time traces of the shed positions of the N-cell vortices are calculated along two sampling lines (from $(x/D, y/D, z/D) = (1, 0, -2.8)$ to $(2, 0, -2.8)$ and from $(x/D, y/D, z/D) = (1, 0, -2.9)$ to $(2, 0, -2.9)$) and are plotted in red and black, respectively. Every small circle represents an N-cell vortex. (b) Time traces of the shed positions of the L-cell vortices are calculated along two sampling lines (from $(x/D, y/D, z/D) = (1, 0, -15.8)$ to $(2, 0, -15.8)$ and from $(x/D, y/D, z/D) = (1, 0, -17.8)$ to $(2, 0, -17.8)$) and are plotted in red and black, respectively. Every small circle represents an L-cell vortex.

(which are in the L-cell vortex's regular shedding region discussed in § A.1), most of the L-cell vortices shed at position $x/D = 1.46$. Only a few L-cell vortices shed at $x/D = 1.47$. Considering that $0.01D$ is a very small distance and equal to the spatial interval of the sampling points, $x/D = 1.46$ can be defined as the shed position of L-cell vortices. On the other hand, as illustrated in figure 24(a), the shed position of N-cell vortices severely fluctuates between $x/D = 1.4$ and 1.6 , which makes it hard to define a fixed shed position for all N-cell vortices. Luckily, as shown in table 4, at the key instant when the vortex dislocations occur, φ of the N-cell vortex is stable.

In table 4, φ of each vortex is calculated in two ways: (1) in the first column, φ is obtained along a sampling line (from $(x/D, y/D, z/D) = (1, 0, -2.9)$ to $(2, 0, -2.9)$) by using the method (i) described in § A.2; (2) in the second column, φ is obtained by using the method (ii) described in § A.2 at a fixed point $(x/D, y/D, z/D) = (1.5, 0, -2.9)$, in which $x/D = 1.5$ is the averaged shed position of the N-cell vortices. The differences between these two calculation methods are shown in the third column. The phases of the N-cell vortices that induced the vortex dislocations and formations of the NL-loop structures are highlighted in italics. At these key instants, the largest difference in φ is $0.015D/U$, which is small and equal to the finest grid size (all analysis is based on case 3 in table 1). Differences at the other points are even smaller than $0.1D/U$. The present paper focuses on the trend of Φ accumulation, rather than the exact value of Φ . We believe that these small differences have negligible influence on our discussions and conclusions.

For the L-cell vortices, at $x/D = 1.5$, they already shed from the shear layer and move regularly downstream. We admit that, from $x/D = 1.46$ (the shed position of the L-cell vortices) to 1.5 , the convective velocity contributes to the accumulation of Φ . Since these two points are only $0.04D$ apart in the x -direction, the contributions from the convective velocity will be limited. We believe that Φ calculated at $x/D = 1.5$ is still dominated by the different shedding frequencies between the N- and L-cell vortices. Therefore, the downstream position $x/D = 1.5$ is selected as the streamwise position of the sampling points for both N- and L-cell vortices. The Φ between the corresponding N- and L-cell vortices is calculated at this position, and defined as Φ_f .

A.4. The method to correct L-cell vortices from oblique shedding effects

Owing to the oblique shedding in the L-cell region shown in figure 1, φ of the L-cell vortices varies as the observation position moves in the spanwise direction. In order to get rid of this effect, φ of the L-cell vortex is divided into two parts:

$$\varphi_{LM} = \varphi_L + \varphi_\theta. \quad (\text{A } 2)$$

In (A 2), φ_{LM} is the phase of the L-cell vortex obtained at a specific sampling position, φ_θ is the component of φ_{LM} that can be affected by the oblique shedding and φ_L is the other component that is unaffected. In other words, when the sampling point moves in the spanwise direction within the L-cell region, φ_{LM} and φ_θ vary, but φ_L remains constant. As an example, we keep the monitoring position of the N-cell vortex at $(x/D, y/D, z/D) = (1.5, 0, -2.9)$, and capture φ of the L-cell vortices at two sampling points $(x/D, y/D, z/D) = (1.5, 0, -15.8)$ and $(1.5, 0, -17.8)$. By using equation (A 1), two time traces of Φ_f are calculated and shown in figure 25(a,b), in which the small circles represent Φ_f between an N-cell vortex and its corresponding L-cell vortex. One can see that the trend of the curves coincide in figure 25(a,b). When the sampling position of the L-cell vortex moves, the oblique shedding only

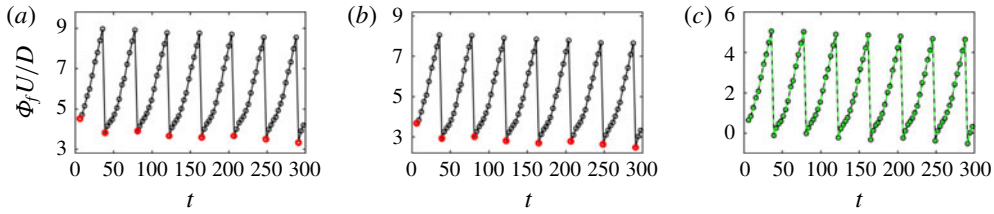


FIGURE 25. Time traces of Φ_f during the first long N-cell cycle are calculated at two groups of sampling points. (a) The calculations of Φ_f are based on φ of the N- and L-cell vortices which are calculated at $(x/D, y/D, z/D) = (1.5, 0, -2.9)$ and $(1.5, 0, -17.8)$, respectively. (b) The calculations of Φ_f are based on φ of the N- and L-cell vortices which are calculated at $(x/D, y/D, z/D) = (1.5, 0, -2.9)$ and $(1.5, 0, -15.8)$, respectively. (c) By using the regression method described in § A.4, the results in green and black in panel (c) have been obtained from panels (a) and (b), respectively. The circle represents Φ_f between an N-cell vortex and the corresponding L-cell vortex. In order to ease the observation, we reduce the size of the green circles.

φ obtained from a sampling line (D/U)	φ obtained at a fixed point (D/U)	Difference (D/U)
6.095	6.05	0.045
9.055	9.055	0
12.24	12.27	-0.03
15.625	15.585	0.04
18.78	18.73	0.05
22.12	22.2	-0.08
25.7	25.68	0.02
29	28.95	0.05
32.325	32.315	0.01
⋮	⋮	⋮
<i>74.365</i>	<i>74.355</i>	<i>0.01</i>
⋮	⋮	⋮
<i>116.28</i>	<i>116.29</i>	<i>-0.01</i>
⋮	⋮	⋮
<i>158.29</i>	<i>158.3</i>	<i>-0.01</i>
⋮	⋮	⋮
<i>200.3</i>	<i>200.29</i>	<i>0.01</i>
⋮	⋮	⋮
<i>242.23</i>	<i>242.215</i>	<i>0.015</i>

TABLE 4. Phase information φ of the N-cell vortices is obtained by two methods. In the first column, we use method (i) described in § A.2 to obtain φ along a sampling line (from $(x/D, y/D, z/D) = (1, 0, -2.9)$ to $(2, 0, -2.9)$). In the second column, we use method (ii) described in § A.2 to obtain φ at a fixed sampling point $(x/D, y/D, z/D) = (1.5, 0, -2.9)$. The differences between the first and second column are shown in the third column. The φ of the N-cell vortices that induce vortex dislocations are highlighted in italics.

causes a downward shift of the curves from figure 25(a) to (b). By subtracting the average value of all small red circles in each figure, we obtain the green curve (figure 25a) and the black curve (figure 25b), and we easily find that these two curves almost coincide. The average value of all the small red circles is φ_θ in (A 2). As long as the sampling position of the L-cell vortex is far from the step position, after subtracting φ_θ , figure 25(c) can always be obtained.

In the $D/d=2$ case, by using the method described in this appendix, we obtained φ of the N- and L-cell vortices at $(x/D, y/D, z/D) = (1.5, 0, -2.9)$ and $(1.5, 0, -15.8)$; therefore Φ_f is calculated on this basis. Following this method, Φ_f in the $D/d=2.4$ case can also be obtained. The detailed data of φ and Φ_f for both the $D/d=2$ and 2.4 cases are included in the supplementary files 1 and 2, respectively.

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