

# Regularized Nonlinear Moving Horizon Observer with Robustness to Delayed and Lost Data

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## Abstract

Moving horizon estimation provides a general method for state estimation with strong theoretical convergence properties under the critical assumption that global solutions are found to the associated nonlinear programming problem at each sampling instant. A particular benefit of the approach is due to the use of a moving window of data that is used to update the estimate at each sampling instant. This provides robustness to temporary data deficiencies such as lack of excitation and measurement noise, and the inherent robustness can be further enhanced by introducing regularization mechanisms. In this paper we study moving horizon estimation in cases when output measurements are lost or delayed, which is a common situation when digitally coded data are received over low quality communication channels or random access networks. Modifications to a basic moving horizon state estimation algorithm and conditions for exponential convergence of the estimation errors are given, and the method is illustrated by using a simulation example and experimental data from an offshore oil drilling operation.

## Index Terms

State Estimation; Parameter Estimation; Nonlinear Systems; Regularization; Wireless communication; Communication errors; Persistence of Excitation.

## I. INTRODUCTION

We consider the state estimation problem of nonlinear discrete-time systems, where a least-squares state estimation problem can be formulated by numerically minimizing a properly weighted least-squares criterion defined on a finite data history window, subject to the nonlinear model equations and possibly other constraints, [1]–[4]. This leads to a so-called nonlinear Moving Horizon State Estimator (NMHE). Compared to well-known sub-optimal nonlinear

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state estimators such as the Extended Kalman Filter (EKF), some empirical studies [5] show that the NMHE can perform better in terms of accuracy and robustness. In fact, while the EKF summarizes the past history in the current state estimate and its covariance estimate, an NMHE can make direct use of the past data history when updating the state estimate since the update is based on a window both current and historical measurement data in the least-squares numerical optimization criterion that can also account for state constraints. The NMHE's robust performance is a particular advantage since the EKF is based on various stochastic assumptions on noise and disturbances that are rarely met in practice, and in combination with nonlinearities, initialization errors and model uncertainty, which may lead to unacceptable performance of the EKF in some applications.

The analysis of convergence of NMHE typically makes assumptions of uniform observability, [1]–[4]. However, uniform observability is a restrictive assumption that is likely not to hold in certain interesting and important state estimation applications. This is in particular true for some combined state and parameter estimation problems, when the data may not be persistently exciting [6], [7], for systems that are detectable but not observable [6], or when data are missing due to digital data communication errors. In these cases the robustness and graceful degradation of the NMHE algorithm will strongly benefit from regularization mechanisms, as shown in [7]–[9] for cases when the system is detectable but the data are not persistently exciting. These papers provide results and guidelines about the choice of terms and weighting matrices in the moving horizon cost function in order to achieve regularization when data are not persistently exciting, based on monitoring of information contents using the singular value decomposition. This leads to different tuning criteria than e.g. [2] where similarities in formulation between the NMHE and EKF are exploited to propose the choice of weighting matrices.

The present paper continues the line of research presented in [7]–[10], and specifically considers situations when output data may be missing or delayed at some sampling instants. The objective of the paper is to suggest modifications in assumptions and MHE cost function formulation accompanied with a convergence analysis and guidelines for design and tuning to gracefully degrade performance when necessary in such cases. While the above mentioned references makes the assumption that the system is  $N$ -detectable and data are  $N$ -exciting in order to establish estimator convergence, in the present paper we generalize the assumption of data being  $N$ -exciting to data being  $N$ -informative. In simple terms,  $N$ -informative data are characterized by a sufficient number of measurements being available in an  $N$ -window with the input being  $N$ -exciting such that the state can be uniquely determined from the available measurements.

Missing or delayed data may result due to unreliable digital communication, either on noisy point-to-point links or

in communication networks that share a communication channel. In the latter case, corruption of data may typically be due to data collisions in a random access protocol, or interference on a wireless (radio) communication channel that may invalidate digital data in the absence of error-correcting coding and decoding. Such data corruption may lead to delayed data in the case when the communication protocol includes automatic re-transmission of lost data, or loss of data when no such quality-of-service mechanisms are utilized when erroneous data are rejected. Severe dropout rates or delays can result as a consequence of network congestion problems if, for example, re-transmissions due to dropouts are allowed to escalate. We can give three practical examples where very high dropout probabilities could happen for significant time periods:

- Wireless communication in industrial environments or mobile robotics, within a non-stationary environment characterized by moving metal, no line of sight, radio channel fading, external electromagnetic interference, and other factors [11]. Depending on the implemented protocols and communication technology, this may lead to severe data losses or delays for periods of time that may be beyond the window of an estimator. This may be a fairly frequent situation in some environments and can be captured by the Gilbert-Elliot channel model.
- Several industrial networks working at the controller level share critical real-time data at update rates down to 100 ms are based on UDP multicast over wired Ethernet. Several failure modes have been documented causing so-called network storm where retransmissions of packets across different network segment causes severe overloads of the network with severe data losses, e.g. [12]. Root causes could be configuration errors or component faults in network nodes that causes unwanted retransmission of data packets that eventually may overload the network and lead to congestion. Other forms of congestions in industrial automation networks may also lead to severe losses or delays.
- In underwater acoustic communication in networks of autonomous underwater vehicles the channel has highly time-varying properties and the environment can in some cases be very noising, leading to severe loss probabilities or latency [13].

With the increasing use of networks and wireless communication, with frequency spectrum being a limited resource, this is likely to be an increasing challenge in the future as cyber-physical systems are becoming reality to an increasing extent. Robust estimation with data dropout is an important challenge due to the increasing use of wireless sensor networks and networked control architectures.

Although various modifications of the Kalman-filter have been developed to handle missing data, e.g. [14]–[19], the purpose of the present paper is to investigate the use of robust (regularized) NMHE in order to harvest the

benefits of updating estimates based on a window of data. A few studies in this direction have been reported in the literature. The use of time-stamps on the measurements is proposed in [20] in order to effectively manage the moving horizon data buffer when there is asynchronous sampling and lost and delayed data that may arrive out of sequence. In [21], it is proposed a NMHE strategy that handles dropped measurement packets by choosing the window size different at each sample to ensure that a sufficient (constant) number of measurement packets are used in each state estimate update. A potential drawback of this approach is that it assumes that all sensors send their data in a common packet (i.e. either all measurements will be available in a given sample, or none). Moreover, the computational complexity may increase with the increasing window size due to lost packets, and it may be more challenging to implement in real time due to inherent variations in computational complexity. In the present paper, we therefore work with a fixed window size, and allow different data packets from individual sensors. It should also be mentioned that moving-horizon versions of the (linear) Kalman-filter have been proposed, [22], [23], which could be a useful starting point for modifications to accommodate delayed or lost data, and nonlinear models.

We consider moving horizon state and parameter estimation, which in its simplest form may be viewed as the inversion of a set of nonlinear algebraic equations for the unknown states and parameters [1]. Lost output data corresponds to less algebraic equations, or equivalently, more unknown variables (the unknown measurements) and may potentially lead to an originally well-posed inversion problem becoming ill-posed or ill-conditioned due to the lost data. We therefore utilize the regularized moving horizon estimator in order to provide diagnostic information and achieve graceful degradation of the estimator. In particular, diagnostic information from a singular value decomposition of the Hessian-like matrix will be provided by the estimator in order to determine which lost data items contributes most to the estimation uncertainty or error. This will be used in an adaptive weighting scheme in the MHE cost function in order to reduce the impact of noise on the estimates of un-excited state components.

There are potential industrial applications of state estimation in the presence of lost and delayed data is extensive. In this paper we study an application in oil well drilling, where digital communication is an essential technology in the automatic and remotely controlled drill floor machines and mud circulation system. The prevailing technologies include the use of UDP and TCP/IP protocols on Ethernet for the high-level top-side control network that links various Programmable Logic Controllers (PLCs) and information systems, together with reliable industrial fieldbus technology at lower level control, although there is considerable interest in the use of wireless sensor networks for monitoring, [24]. An important area of research and development is the use of downhole sensors, where digital communication to the top-side control and monitoring system is essential. Due to the harsh environment

the communication over several kilometers through the mud-filled rotating drilling string is highly challenging. Mud pulse telemetry, which modulates a digital signal as pressure pulses in the drilling fluid (mud), can achieve a few bits per second communication capacity from the drill bit to the top while drilling, and is the conventional technology, e.g. [25]–[27]. Wire pipe technology is emerging and promises kbit/s communication capacity, [28], [29] and offers considerable advantages over transmission of electromagnetic fields through the drill pipe [30]. A common challenge of all these approaches are communication reliability and corruption of data due to noise and external disturbances on the communication system, [31], [32]. The estimation of bottom hole pressure is important to implement pressure control strategies for managed pressure drilling, well control, and monitoring of influx of reservoir fluids that is essential for the safety and performance of the drilling operation, e.g. [33], [34]. The use of nonlinear MHE has been proposed for such applications, [35], without considering in detail the effects of missing and delayed data.

The main contributions of the paper are the nonlinear MHE problem is formulated in Section II for the case of lost and delayed data, the conditions for convergence of the state estimates in Section III, an adaptive weighting scheme introduced in Section IV in order to facilitate regularization and tuning of graceful degradation in cases the noisy data are not persistently exciting, and an experimental case study from oil well drilling found in Section VI.

## II. NONLINEAR MOVING HORIZON ESTIMATION PROBLEM WITH MISSING DATA

### A. Problem Formulation

Consider the following discrete-time nonlinear system:

$$x_{t+1} = f(x_t, u_t) \quad (1a)$$

$$y_t = h(x_t, u_t), \quad (1b)$$

where  $x_t \in \mathbb{X} \subset \mathbb{R}^{n_x}$ ,  $u_t \in \mathbb{U} \subset \mathbb{R}^{n_u}$  and  $y_t = (y_t^1, y_t^2, \dots, y_t^{n_y})^T \in \mathbb{R}^{n_y}$  are respectively the state, input and measurement vectors, and  $t$  is the discrete time index. The  $N + 1$  horizon measurements of outputs and inputs until time  $t$  are denoted as

$$Y_t^* = \begin{bmatrix} y_{t-N} \\ y_{t-N+1} \\ \vdots \\ y_t \end{bmatrix}, \quad U_t = \begin{bmatrix} u_{t-N} \\ u_{t-N+1} \\ \vdots \\ u_t \end{bmatrix}. \quad (2)$$

We consider the case when output data may be delayed or lost due to unreliable communication. This formulation handles both lost and delayed data, since delayed data can be inserted into the data buffer  $Y_t^*$  and the quality indicators of past data can be updated when delayed data arrive within the same sample as new data. For data  $y_{t-k}^j$  being unavailable at time  $t$  we use the convention that the quality indicator  $q_{t-k,t}^{y^j} = 0$  and the value  $y_{t-k}^j$  may be meaningless at time  $t$ , otherwise  $q_{t-k,t}^{y^j} = 1$ . The quality indicators are assumed to be available information to the moving horizon observer. This is a reasonable assumption, since it can be implemented based on standard protocols with error-detection codes such as checksums, and outage detection by time-stamps or sequence numbers.

To express  $Y_t^*$  as a function of  $x_{t-N}$  and  $U_t$ , note from (1b) that the following algebraic map is formulated [1]:

$$Y_t^* = H(x_{t-N}, U_t) = H_t(x_{t-N}) = \begin{bmatrix} h(x_{t-N}, u_{t-N}) \\ h(f(x_{t-N}, u_{t-N}), u_{t-N+1}) \\ \vdots \\ h(f(f(\cdots f(x_{t-N}, u_{t-N}), \dots), u_{t-1}), u_t) \end{bmatrix}. \quad (3)$$

When all the input and output data are available such that the  $N$ -information vector  $I_t^* = \text{col}(Y_t^*, U_t)$  is available at time  $t$ , the observer problem is to reconstruct  $x_{t-N}$  as a function of  $I_t^*$ . This is considered as an inverse problem, whose solution properties depend on the function  $H_t$ . If an inverse mapping of  $H_t$  exists, is unique, and continuous as a function of  $Y_t^*$  then this inverse problem is well-posed according to the definitions of Tikhonov and Arsenin [36], commonly formulated as a uniform observability property [1]–[4].

If the quality indicator  $q_{t-k,t}^{y^j} = 0$  then  $y_{t-k}^j$  shall be viewed as unknown, which means that the corresponding equation in (3) should be removed or given zero weight. We define  $Y_t = Q_t^Y Y_t^*$  and

$$Q_t^Y = \text{diag} \left( q_{t-N,t}^{y^1}, q_{t-N,t}^{y^2}, \dots, q_{t,t}^{y^{n_y-1}}, q_{t,t}^{y^{n_y}} \right).$$

such that the elements of  $Y_t$  are zero when the corresponding data is unavailable, and reformulate (3) to give zero weight on equations corresponding to missing data:

$$Y_t = Q_t^Y H(x_{t-N}, U_t), \quad (4)$$

In addition the problem may also be ill-posed or ill-conditioned due to lack of persistence of excitation as considered in [7]. In order to take into account such data deficiencies, we consider at time  $t$  the following moving horizon observer formulation that minimizes

$$J(\hat{x}_{t-N,t}; \bar{x}_{t-N,t}) = \|Y_t - Q_t^Y H_t(\hat{x}_{t-N,t})\|_{R_t}^2 + \|\bar{Y}_t - D_t^Y H_t(\hat{x}_{t-N,t})\|_{S_t}^2 + \|\bar{x}_{t-N,t} - \hat{x}_{t-N,t}\|_{W_t}^2 \quad (5)$$

with respect to  $\hat{x}_{t-N,t}$  and subject to

$$\hat{x}_{t-N,t} \in \mathbb{X} \quad (6)$$

where  $R_t, W_t > 0$  and  $S_t \geq 0$  are symmetric time-varying weight matrices and  $D_t^Y = I - Q_t^Y$ . The weighted Euclidean norm is defined as  $\|x\|_P = \sqrt{x^T P x}$  for vectors  $x$  and some symmetric matrix  $P > 0$ . Let  $J_t^o = \min_{\hat{x}_{t-N,t}} J(\hat{x}_{t-N,t}; \bar{x}_{t-N,t})$ , and  $\hat{x}_{t-N,t}^o$  be the associated optimal estimate. It is assumed that the a priori estimator is determined as

$$\bar{x}_{t-N,t} = f(\hat{x}_{t-N-1,t-1}^o, u_{t-N-1}), \quad (7)$$

and the a priori estimated output is defined as

$$\bar{Y}_t = D_t^Y H_t(\bar{x}_{t-N,t}). \quad (8)$$

It is remarked that the optimization variable  $\hat{x}_{t-N,t}$  is the state at the beginning of the horizon. Due to knowledge of the mapping  $H_t(\cdot)$ , this uniquely defines the state estimates at the entire horizon, including the current state estimate  $\hat{x}_{t,t}$  that is usually the main target of estimation. It is further remarked that the formulation can be extended with process noise (as in [2], [4]) or a Kalman-filter corrected predictor for pre-filtering of the a priori estimate (as in [37], [38]) in order to reduce the estimator's sensitivity to model errors and disturbances. For simplicity, we leave out this extension in the present paper.

The cost function (5) consists of three terms. The first term weights the errors between the measured and predicted outputs on the horizon in a least squares sense. The third term penalizes the difference between the state estimate at the beginning of the horizon and the one-step-ahead predicted (a priori) state estimate using the open loop model and the previous optimal state estimate, [4]. As discussed in [7], this term has a regularizing and low-pass filtering effect on the state estimate at it allows the estimate to degrade to an open loop model estimate when the first term is not sensitive to some combinations of estimated states. In particular, for detectable systems where a sub-system is not observable, the third term ensures that the unobservable states are updated according to the stable sub-system's open loop model. Moreover, when data are not persistently exciting such that the first term is not sensitive to the state estimate, the weighting of the third term means that un-excited states are estimated in an open loop fashion. The second term is less conventional, and introduced in order to put some weight on open loop estimates in cases when output measurements are not available. This term allows errors in the data to be weighted against errors in the model. As will be shown in Section III, convergence can be established also when this term has zero weight

( $S_t = 0$ ) such that this term should be considered optional although it might be useful to improve practical estimator accuracy in the presence of noise, model errors and missing data.

### III. CONVERGENCE

Before we state the sufficient conditions for convergence of the state estimate  $\hat{x}_{t-N,t}$  that minimizes the MHE cost function, we need to introduce some concepts and definitions. Following [1], the system (1) is *N-observable* if there exists a *K-function*  $\varphi$  such that for all  $x_1, x_2 \in \mathbb{X}$  there exists a feasible  $U_t \in \mathbb{U}^{N+1}$  such that

$$\varphi(\|x_1 - x_2\|^2) \leq \|H(x_1, U_t) - H(x_2, U_t)\|^2.$$

The input  $U_t$  and the output  $Y_t^*$  with the measurement quality  $Q_t^Y$  is said to be *N-informative* for the *N-observable* system (1) at time  $t$  if there exists a *K-function*  $\varphi_t$  that for all  $x_1, x_2 \in \mathbb{X}$  satisfies

$$\varphi_t(\|x_1 - x_2\|^2) \leq \|Q_t^Y H(x_1, U_t) - Q_t^Y H(x_2, U_t)\|^2.$$

Systems and data satisfying these properties at all time instants have properties similar to uniformly observable systems and allow convergence results to be derived. On the other hand, when a system is not *N-observable*, it is not possible to reconstruct exactly all the state components from the *N-information* vector due to lack of information. However, in some cases one may be able to reconstruct exactly at least some components, based on the *N-information* vector, and the remaining components can be reconstructed asymptotically. This corresponds to the concept of detectability, where we suppose there exists a coordinate transform  $T : \mathbb{X} \rightarrow \mathbb{D} \subseteq \mathbb{R}^{n_x}$ ,  $d = \text{col}(\xi, z) = T(x)$  such that the following dynamics are equivalent to (1),

$$\xi_{t+1} = F_1(\xi_t, z_t, u_t) \tag{9a}$$

$$z_{t+1} = F_2(z_t, u_t) \tag{9b}$$

$$y_t = g(z_t, u_t), \tag{9c}$$

The vector  $\xi_t \in \mathbb{R}^{n_\xi}$  contains un-observable state variables, and  $z_t \in \mathbb{R}^{n_z}$  contains observable state variables. Similar to  $H(\cdot)$ , the following algebraic map can be formulated [1]:

$$Y_t^* = G(z_{t-N}, U_t) = G_t(z_{t-N}) = \begin{bmatrix} g(z_{t-N}, u_{t-N}) \\ g(F_2(z_{t-N}, u_{t-N}), u_{t-N+1}) \\ \vdots \\ g(F_2(F_2(\cdots F_2(z_{t-N}, u_{t-N}), \dots), u_{t-1}), u_t) \end{bmatrix}, \tag{10}$$



and  $Y_t = Q_t^Y G(z_{t-N}, U_t)$ . Before we extend the definition of  $N$ -informativeness to  $N$ -detectable systems, we introduce the concept of incremental input-to-state stability ( $\delta ISS$ ) for the unobservable sub-system (9a) as in [10]. In order to be able to show exponential convergence of the estimates of the un-observable states, they must, by assumption, converge exponentially in an open-loop fashion when then observable state estimates converge exponentially. Although similar assumptions could be made (such as contraction or global exponential stability of the un-perturbed un-observable sub-system) they would lead to very similar results, and we chose the present formulation in order to use a similar analysis method as in [9], [10].

A continuous function  $V(\xi_t^1, \xi_t^2, P_\xi) = \|\xi_t^1 - \xi_t^2\|_{P_\xi}^2$  with  $P_\xi = P_\xi^T > 0$  is called a quadratic  $\delta ISS$ -Lyapunov function for the system  $\xi_{t+1} = F_1(\xi_t, z_t, u_t)$  if the following holds:

- $V(0, 0, P) = 0$ .
- There exist a symmetric  $Q_\xi > 0$  and symmetric  $\Sigma_u > 0, \Sigma_z > 0$ , such that for any  $\xi_t^1, \xi_t^2$  and any couple of input signals  $(u_t^1, u_t^2), (z_t^1, z_t^2)$ ,

$$V(\xi_{t+1}^1, \xi_{t+1}^2, P_\xi) - V(\xi_t^1, \xi_t^2, P_\xi) \leq -V(\xi_t^1, \xi_t^2, Q_\xi) + V(u_t^1, u_t^2, \Sigma_u) + V(z_t^1, z_t^2, \Sigma_z). \quad (11)$$

The input  $U_t$  and the output  $Y_t^*$  with the measurement quality  $Q_t^Y$  is said to be  $N$ -informative for the  $N$ -detectable system (1) at time  $t$  if

- (1) there exists a coordinate transform  $T : \mathbb{X} \rightarrow \mathbb{D}$  that brings the system in the form (9);
- (2) the input  $U_t$  and output  $Y_t^*$  with the measurement quality  $Q_t^Y$  is  $N$ -informative for the  $N$ -observable sub-system (9b)-(9c) at time  $t$ .
- (3) the sub-system (9a) has a quadratic  $\delta ISS$ -Lyapunov function (11).

As shown by the following result, for arbitrary choices of  $S_t \geq 0$  and  $W_t > 0$  there exists a sufficiently large  $R_t > 0$  such that the observer estimation error  $e_{t-N} = x_{t-N} - \hat{x}_{t-N,t}^o$  converges exponentially to zero, under some conditions.

*Theorem 1:* Suppose the following assumptions hold

- (A1) The functions  $f$  and  $h$  are twice differentiable, and the functions  $F_1, F_2$  and  $g$  are twice differentiable.
- (A2)  $T(x)$  is continuously differentiable and bounded away from singularity for all  $x \in \mathbb{X}$  such that  $T^{-1}(x)$  is well defined.
- (A3) The input  $U_t$  and output  $Y_t^*$  with the measurement quality  $Q_t^Y$  are  $N$ -informative for all  $t \geq 0$  for the  $N$ -detectable system (1).

(A4) The signals  $u_t$ ,  $y_t$  and  $x_t$  are bounded.

(A5) The set  $\mathbb{X}$  is closed, convex, and controlled invariant, *i.e.*  $f(x_t, u_t) \in \mathbb{X}$  for all  $x_t \in \mathbb{X}$  and the control  $u_t \in \mathbb{U}$  for all  $t \geq 0$ .

(A6) For any  $\text{col}(\xi_1, z_1) \in \mathbb{D}$  and  $\text{col}(\xi_2, z_2) \in \mathbb{D}$ , then  $\text{col}(\xi_1, z_2) \in \mathbb{D}$ ,  $\text{col}(\xi_2, z_1) \in \mathbb{D}$ .

Then for any  $S_t \geq 0$  and  $W_t > 0$  there exists a sufficiently large weight matrix  $R_t > 0$  such that for any initial a priori estimate  $\bar{x}_{0,N} \in \mathbb{X}$  the observer error converges exponentially to zero.

*Proof:* Given in the appendix. ■

We remark that the closed set  $\mathbb{X}$  is chosen by the user primarily in order to represent physical constraints on the state estimates, although its choice may be limited due to validity of the model or assumptions that must hold on this set  $\mathbb{X}$ . With the choice  $\mathbb{X} = \mathbb{R}^n$  we get a global exponential convergence result. In other cases, the region of attraction of the estimate will not be global, but limited by the set  $\mathbb{X}$ .

The key assumption is (A3) which requires that the system is  $N$ -detectable and the data are  $N$ -informative, which means that there is a sufficient number of exciting measurements are available. This means that the NMHE is inherently robust to delayed and lost data, provided that the amount of missing data is not too large compared to the window size  $N$ . In [21], it was proposed to handle lost data by online adaptation of the window size  $N$  in order to guarantee that the window of information is  $N$ -informative at each time step. While increasing the window size  $N$  will generally improve robustness, it may still not be desirable to do so. The two main reasons are increased computational complexity of the online nonlinear program, and increased degree of filtering of the estimate that may be undesired if operating in a non-stationary or highly time-varying environment that requires that the state estimator adapts quickly to rapidly changing parameters.

In this paper, we take into account that violation of the assumption of  $N$ -informative data may be expected, and the robustness of the NMHE algorithm to such data deficiency can be further enhanced using an adaptive weight selection algorithm as described in Section IV.

#### IV. ADAPTIVE WEIGHTING AND FURTHER ROBUSTNESS

This section provides some further regularization mechanisms and tuning guidelines to ensure robustness and graceful degradation when significant amounts of measurements are delayed or lost. First, we provide a characterization of the requirements on the weight matrix  $R_t$  based on Theorem 1 for the case when the assumptions are fulfilled.

*Proposition 1:* Define the following matrixes

$$\Gamma_{t-1} = \Gamma_{t-1}(x_{t-N-1}, \hat{x}_{t-N-1,t-1}^o) = \int_0^1 \frac{\partial}{\partial x} T((1-s)x_{t-N-1} + s\hat{x}_{t-N-1,t-1}^o) ds,$$

$$\Lambda_t = \Gamma_{t-1}^{-1T} \Theta_t^T (\Delta_t^T S_t \Delta_t + W_t) \Theta_t \Gamma_{t-1}^{-1},$$

$$\Psi_t = \Psi_t(x_{t-N}, \hat{x}_{t-N,t}^o) = Q_t^Y \int_0^1 \frac{\partial}{\partial x} H((1-s)x_{t-N} + s\hat{x}_{t-N,t}^o, U_t) ds.$$

where  $\Delta_t$  and  $\Theta_t$  are defined in Lemma 2 in the Appendix. For a suitable scalar  $\alpha > 0$ , matrix  $\Xi = \Xi^T > 0$ , and matrix  $P_2 = P_2^T > 0$  for all  $t \geq 0$ , if the weight matrix  $R_t$  is chosen such that the following matrix inequalities holds, where  $\eta = [0_{n_z \times n_\xi}, I_{n_z}]$ ,

$$\eta \Gamma_t^{-1T} \Psi_t^T R_t \Psi_t \Gamma_t^{-1} \eta^T \geq P_2, \quad (12a)$$

$$\begin{bmatrix} \alpha Q_\xi & 0 \\ 0 & P_2 - \alpha \Sigma_z \end{bmatrix} > \Xi + \Lambda_t, \quad (12b)$$

then the observer error is exponentially stable.

*Proof:* See Appendix. ■

Fulfillment of eq. (12a) at all time instants  $t$  requires that  $\Psi_t$  has full rank, which is guaranteed by data being  $N$ -informative. Eq. (12a) ensures that the chosen Lyapunov function decreases at each time instant. This is a sufficient condition that may not be necessary, and it may be sufficient that the Lyapunov function "decreases in average" as commonly exploited when using the concept of persistence of excitation. Intuitively, it is therefore reasonable to believe that some stability and convergence properties can still be achieved if this assumption is mildly violated, assuming that there are "enough measurements on average". Due to the second and third terms in the cost function, the estimator functionality degrades to an open loop observer in such cases, with selectivity such that the available measurements are still fully utilized in situations with partial measurements being available (like one of two outputs available). As discussed in [7], these regularization mechanisms may be sufficient in cases when the system is open loop asymptotically stable. However, when the system is marginally stable (e.g. by joint identification of parameters  $\theta$  with a state augmentation of the model with  $\dot{\theta} = 0$ ), or unstable, the open loop integration of the model in the estimator may lead to drifting estimates. As described in [39]–[42], the use of directional updating based on a decomposition of the information matrix can be used to prevent updating of combinations of state variables for which no information exists in the data. Effectively, this prevents drifting estimates due to noise and model errors that would otherwise be the dominant driving force of the estimate updates. Following [7] we

implement an adaptive (directional) weighting algorithm using the singular value decomposition. We define the data quality-weighted Jacobian-like matrix

$$\Psi_t = \Psi_t(\hat{x}_{t-N,t}^o, \hat{x}_{t-N,t}^o) \approx Q_t^Y \frac{\partial}{\partial x} H(\hat{x}_{t-N,t}^o, U_t). \quad (13)$$

Note that in the nonlinear MHE formulation, the matrix  $\Psi_t^T R_t \Psi_t$  plays a similar role as a weighted information matrix, and for small errors  $\|e_{t-N}\|$ , the approximation accuracy may be expected to be good.

Consider a singular value decomposition (SVD) [43]

$$\Psi_t = \tilde{U}_t \tilde{S}_t \tilde{V}_t^T. \quad (14)$$

The singular values are the diagonal elements of the matrix  $\tilde{S}_t$ . Any singular value that is zero (or close to zero) indicates a state component is either not observable or that the data are not sufficiently informative (or only weakly informative). Moreover, the corresponding row of the  $\tilde{V}_t$  matrix will indicate which components cannot be estimated. The Jacobian has the structural property that its rank will be no larger than  $\dim(z) = n_z$ , due to certain components being unobservable. Whether the data are  $N$ -informative may therefore be monitored through the robust computation of the rank of the Jacobian matrix using the SVD. One may selectively and gracefully degrade the performance of the observer to an open loop observer for those state components for which the data are not  $N$ -informative, while the other state components are updated using the data. To pursue this objective, we propose to choose  $R_t$  such that,

$$R_t = \bar{R}_t^T \bar{R}_t, \quad \text{with} \quad \bar{R}_t = \sqrt{\beta} \tilde{V}_t \tilde{S}_{\rho,t}^+ \tilde{U}_t^T \quad (15)$$

where  $\beta > 0$  is a scalar, and the thresholded pseudo-inverse  $\tilde{S}_{\rho,t}^+ = \text{diag}(0, \dots, 0, 1/\sigma_{t,1}, \dots, 1/\sigma_{t,\ell})$  where  $\sigma_{t,1}, \dots, \sigma_{t,\ell}$  are the singular values larger than some threshold  $\rho > 0$ , and the zeros correspond to small singular values whose inverse is set to zero [43]. Then we have

$$\Psi_t^T R_t \Psi_t = \beta D, \quad (16)$$

where  $D = \text{diag}(0, \dots, 0, 1, \dots, 1)$ . For  $N$ -informative input and  $\rho > 0$  sufficiently small, [7], such choice of  $R_t$  also satisfies that  $\Phi_t^T R_t \Phi_t = \beta I > 0$  which clearly satisfies (12a) for sufficiently large  $\beta$ . The problem becomes to find a suitable  $\beta$  such that (12) holds. Since ineq. (12b) may give a conservative bound  $P_2$  and the matrix  $\Gamma_t$  may be hard to compute, a qualitative guideline is to choose  $\beta > 0$  sufficiently large. A large  $\beta$  contributes to fast speed of convergence, while robustness to measurement noise must be taken into consideration and will be a primary reason why  $\beta$  should not be chosen too large.

Scaling of the model equations and variables is instrumental for the approach since the thresholded singular value decomposition is used to determine directions in the parameter space that should be updated based on data, and those that are not to be updated due to lack of information. In order to allow a direct comparison of the (scalar) singular values, all variables need to be scaled appropriately. Numerical robustness and simplification of the tuning are other good reasons for scaling. Determining the scaling factors is usually done in two steps. First, rough scaling in order to account for different physical units, e.g. scale all to a range 0-100. Second, some fine tuning of the scaling in order to maximize the performance of the observer. This usually requires an iterative procedure with some trial and error having in mind the importance of the individual variables in a given application.

For inputs that are not  $N$ -informative, the parameter  $\rho > 0$  may be tuned in order to enhance robustness of the algorithm such that  $R_t$  gives zero weight on state combinations for which there is insufficient information. The qualitative guideline is that increased  $\rho$  will require a higher degree of information in order to update estimates and thereby improve robustness to noise, missing data and model uncertainties at the cost of convergence speed. The choice of  $\rho$  may require extensive simulation and experimental testing since the primary objective of the thresholded SVD is to avoid undesired parameter estimator drift due to model errors under conditions characterized by lack of excitation or too little available data. It may also require re-tuning of the weights in  $W_t$  and some re-scaling of variables in order to tune the responses of the individual parameter estimates.

The 2nd term in the NMHE criterion, weighted with  $S_t$ , is introduced to allow simulated output data to be used as a substitute when real measurements are not available. The elements of  $S_t$  are tuning parameters that should increase with the confidence in the model, increase with measurement noise levels, but should usually be less than  $R_t$  since real measurements should be trusted more than simulated measurements.

Clearly, the choice of window size  $N$  is important for the performance of the algorithm. There are several effects involved. First, an increased window size  $N$  will lead to a high degree of low-pass filtering in the MHE. This has the benefits that effects of uncertainties such as noise, missing data and model errors are reduced, while the main drawbacks are reduced speed of convergence and increased computational load. Moreover, for a given application there is a minimum  $N \leq n$  that is necessary in order to achieve  $N$ -observability of the system. It should be remarked that increasing  $N$  is not the only option for increasing the degree of low-pass filtering within the MHE, as increasing the weights in  $W_t$  will also have this effect.

We mention that the diagnostic information resulting from the singular value decomposition could potentially be used to prioritize re-transmission requests for critical data while less important data need not be requested to

be re-transmitted. This contributes to the overall objective of greedy use of communication capacity in order to improve overall communication performance in terms of latency, power consumption, and data integrity.

## V. SUMMARY OF ALGORITHM

In summary, the estimation algorithm consists of the following steps

- 1) Initialization:  $N, W_t, S_t, \bar{x}_{0,N}, \mathbb{X}, \beta, \rho$
- 2) Acquire new data, and stack into the moving window vectors  $U_t$  and  $Y_t^*$  and associated quality indicators  $Q_t^Y$  and  $D_t^Y = I - Q_t^Y$ .
- 3) Generate  $Y_t$  according to (4) and  $\bar{Y}_t$  according to (8).
- 4) Compute the approximation of  $\Psi_t$  according to (13) using numerical finite difference approximations or analytical expressions.
- 5) Compute the SVD of  $\Psi_t$ , cf. (14) and [43].
- 6) Compute  $R_t$  according to (15).
- 7) Solve the nonlinear programming problem with objective function (5) and constraints (6) using a numerical solvers (such as NPSOL that was used in the examples) for the updated state estimate  $\hat{x}_{t-N,t}$ .
- 8) Update the a priori estimate according to (7), and return to step 2 for the next update.

## VI. EXAMPLES

A simulation example is first used to illustrate the main ideas, while the performance of the approach is evaluated using experimental data from an offshore oil well drilling operation in the second example. In the examples we use the NPSOL sequential quadratic programming algorithm to solve the nonlinear MHE problems. Matlab is used for simulation and other computations, with the TOMLAB interface to NPSOL.

### A. Example 1 - mixed state and parameter estimation

Consider the following system

$$\dot{x}_1 = -4x_1 + x_2 \tag{17a}$$

$$\dot{x}_2 = -x_2 + x_3 u \tag{17b}$$

$$\dot{x}_3 = 0 \tag{17c}$$

$$y = x_2 + v. \tag{17d}$$

It is clear that  $x_1$  is not observable, but corresponds to a  $\delta$ ISS system, while  $x_2$  and  $x_3$  are observable state variables. It is also clear that our ability to exactly compute  $x_3$  from measured input and output data will depend on the excitation  $u$ , while  $x_2$  is uniformly observable. One may think of  $x_3$  as a parameter representing an unknown gain on the input, where the third state equation is an augmentation for the purpose of estimating this parameter. The same observability and detectability properties hold for the discretized system with sampling interval  $t_f = 0.1$ s. It is easy to see that the sub-system (17a) has a quadratic  $\delta$ ISS-Lyapunov function.

In the example, the input  $u$  is discrete-time white noise, which is highly exciting. Independent uniformly distributed measurement noise  $v \in [-0.05, 0.05]$  is added to the output. Different scenarios are generated by simulating different percentages of lost output measurements. A window size  $N = 8$  was chosen. This window is larger than the theoretical minimum, which was found to improve the robust performance of the method. The criterion weight parameters are set to  $S_t = 0.1I$  and  $W_t = 0.7I$ , and use the adaptive weighting law (15) to define  $R_t$  using  $\beta = 10$ . This tuning was made as a trade-off between fast response and sensitivity to noise. The threshold  $\delta = 0.01$  was tuned to avoid drifting estimates during periods with insufficient measurements.

We evaluate the NMHE performance using the root mean square error

$$RMSE = \left( \frac{1}{M} \sum_{t=0}^M \|e_t\|^2 \right)^{1/2},$$

where  $e_t$  is the estimation error at time  $t$ , and  $M = 100$  is the length of the simulation run. The simulation results with different measurement loss probabilities, and the average of  $RMSE$  of state estimates, are shown in Table I for 20 different initial states. Table II shows the results obtained by the method in [19], where the Extended Kalman Filter (EKF) is implemented with mechanisms to handle intermittent observations. For the EKF, it is assumed that the disturbance standard deviation is 0.0167 and the same initial estimates were used in the EKF and NMHE. From Table I and Table II, it can be concluded that the accuracy of the proposed NMHE method is better than the implemented EKF.

Figure 1 shows the estimates of these two methods with the same initial state estimate when the probability of missing data is 80%. From Figure 1, it can be observed that  $x_3$  estimated by the EKF is updated only when new measurements become available, which leads to a somewhat slow response. On the other hand,  $x_3$  estimated by the proposed NMHE is updated at each time step due to the window of data, which results in improved accuracy compared to the implemented EKF. It takes on average around 50 ms to compute the state estimate with the NMHE method at each step, while the computation time of the EKF is around 5 ms. Although these computations are

made in Matlab on a standard PC without any attempt to optimize the implementation for computational efficiency, we believe their ratio is a fairly valid indicator of their computational performance ratio.

The results shows that performance degrades gracefully, with fairly small reduction in estimation accuracy up to about 30 % loss probability. Even at 80 % loss the estimator gives robust estimates with performance degradation of a factor less than 5.

Loss Probs (%)	0	2	5	10	20	30	50	70	80
RMSE of $x_1$	0.0605	0.0605	0.0604	0.0604	0.0603	0.0603	0.0601	0.0618	0.0715
RMSE of $x_2$	0.0097	0.0098	0.0118	0.0155	0.0216	0.0285	0.0326	0.0364	0.0375
RMSE of $x_3$	0.0149	0.0153	0.0158	0.0176	0.0203	0.0238	0.0517	0.0653	0.0746

TABLE I

EXAMPLE 1: THE ESTIMATION ERRORS OF THE PROPOSED MHE.

Loss Probs (%)	0	2	5	10	20	30	50	70	80
RMSE of $x_1$	0.0702	0.0704	0.0704	0.0705	0.0701	0.0701	0.0709	0.0716	0.0721
RMSE of $x_2$	0.0226	0.0247	0.0284	0.0359	0.0416	0.0459	0.0511	0.0571	0.0588
RMSE of $x_3$	0.0728	0.0863	0.1236	0.1316	0.1320	0.1474	0.1645	0.2026	0.2080

TABLE II

EXAMPLE 1: THE ESTIMATION ERRORS OF THE EKF.

### B. Example 2 - Estimation of Bottom Hole Pressure during Oil Well Drilling

In this example, we here implement the proposed approach to estimate the bottom hole pressure (BHP) during a Managed Pressure Drilling (MPD) operation. MPD is a drilling process used to precisely control an annular pressure profile throughout the well bore, cf. Figure 2. The drilling fluid (commonly called mud) is pumped down the rotating drillpipe. At the drill bit at the bottom of the hole the fluid is allowed to flow through the drill bit as it rotates to make the hole, and circulate back to the top side through the annulus. The purpose of this flow is twofold. First, it removes cuttings from the drilling at the bottom hole, and second, it provides a pressure in the well that acts as a barrier against uncontrolled inflow of hydrocarbons that might occur if an oil or gas reservoir is penetrated. The pressure should be controlled accurately within the range between the pore pressure of the reservoir and the fracture pressure, beyond which the drilling fluid may cause damage to the well bore, using the choke or



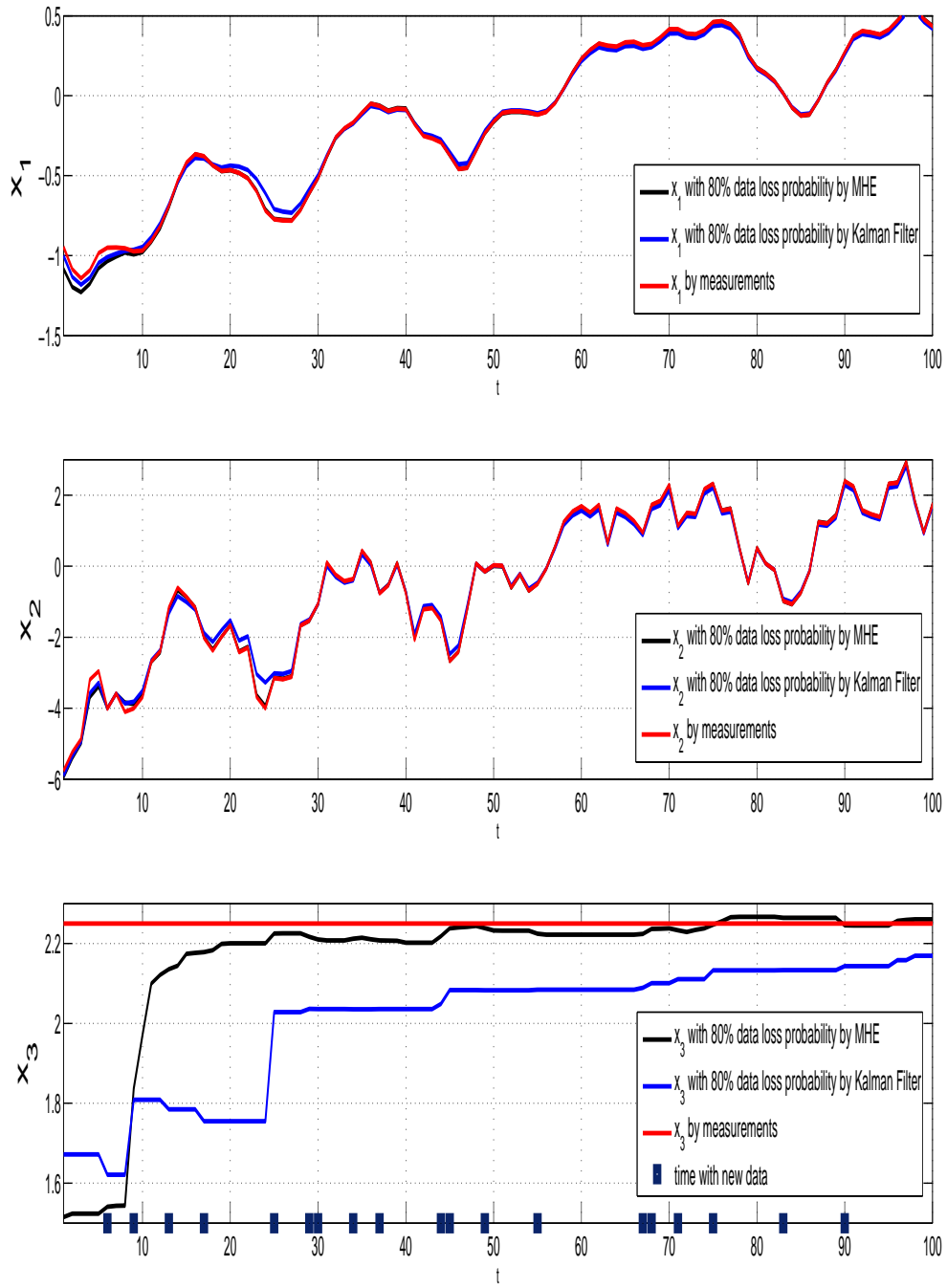


Fig. 1. Example 1: Estimates with loss probability being 80%.

back-pressure pump. The circulation of the drilling fluid also involves some top-side processing in order to remove foreign elements from the fluid before it is circulated.

To model the MPD drilling system for use in the estimator, we use a simplified model developed in [44]. The parameters used in the example are given in Table III.

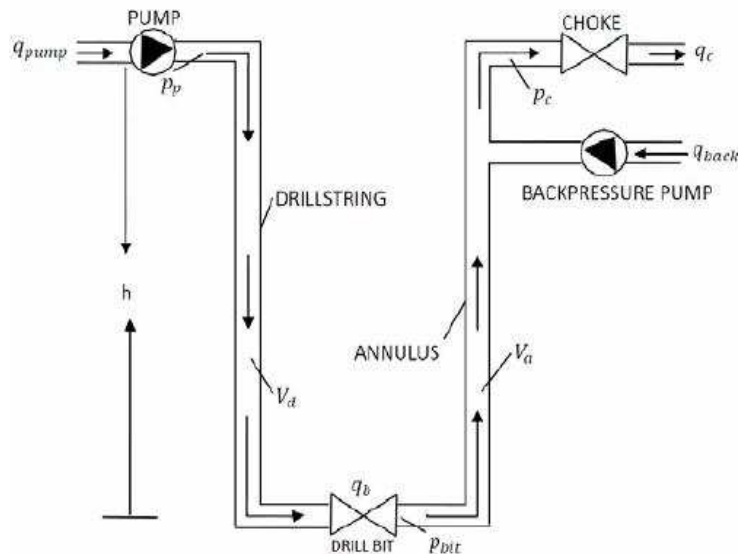


Fig. 2. A simplified drawing of the MPD drilling system.

The MPD system can be described as

$$\dot{p}_c = \frac{\beta_a}{V_a}(q_b - q_c + q_{back} + \dot{V}_a), \quad (18a)$$

$$\dot{p}_p = \frac{\beta_d}{V_d}(q_{pump} - q_b), \quad (18b)$$

$$\dot{q}_b = \frac{1}{M}(p_p - p_c - \lambda_1 q_{pump}^2 - \lambda_2 (q_c - q_{back})^2 + (\rho_d - \rho_a)gh), \quad (18c)$$

with the parameters  $M = M_a + M_d$  with  $M_a = \rho_a \int_0^{\ell_a} \frac{1}{A_a(x)} dx$  and  $M_d = \rho_d \int_0^{\ell_d} \frac{1}{A_d(x)} dx$ . The pressure of the bottom hole,  $p_{bit}$  (also called bottom hole pressure - BHP), depends on the choke pressure, pump pressure, frictional loss pressure and hydrostatic pressure, which is given as

$$p_{bit} = \frac{M_a}{M} p_p + \frac{M_d}{M} p_c + \frac{M_d}{M} \lambda_2 (q_c - q_{back})^2 - \frac{M_a}{M} \lambda_1 q_{pump}^2 + \left( \frac{M_d}{M} \rho_a + \frac{M_a}{M} \rho_d \right) gh. \quad (19)$$

In this example, it is assumed that the parameters  $\lambda_1, \lambda_2$  are unknown. With this parametrization one has to expect

Parameters	Description	Unit
$V_a$	Annulus volume	$m^3$
$V_d$	Drill string volume	$m^3$
$\beta_a$	Bulk modulus of fluid in annulus	bar
$\beta_d$	Bulk modulus of fluid in drill string	bar
$p_c$	Choke pressure	bar
$p_p$	Pump pressure	bar
$q_b$	Flow rate of the bit	$m^3/s$
$q_c$	Flow rate of the choke	$m^3/s$
$q_{back}$	Flow rate of the backpressure pump	$m^3/s$
$q_{pump}$	Flow rate of the pump	$m^3/s$
$\lambda_1$	Friction parameter of drill string	$bars^2/m^6$
$\lambda_2$	Friction parameter of annulus	$bars^2/m^6$
$\rho_a$	Density mud in annulus	$kg/m^3$
$\rho_d$	Density mud in drill string	$kg/m^3$
$g$	Acceleration of gravity	$m/s^2$
$h$	Vertical depth of the bit	$m$
$\ell_a$	Length of annulus	$m$
$\ell_d$	Length of drill string	$m$
$A_a$	Cross sectional area of annulus	$m^2$
$A_d$	Cross sectional area of drill string	$m^2$
$p_{bit}$	Bottom hole pressure	bar

TABLE III

MODEL VARIABLES.

that the model is over-parameterized such that the persistence of excitation condition (and uniform observability) will not hold. This challenging parametrization is chosen in order to illustrate the power of the proposed method, and in particular that the algorithm will accurately detect the information content of the available data at any time and adapt the weights accordingly when using  $R_t$  defined by (15). Therefore, the proposed NMHE algorithm is applied to the combined state and parameter estimation problem by considering the parameters  $\lambda_1, \lambda_2$  as augmented states,  $\dot{\lambda}_1 = 0$ , and  $\dot{\lambda}_2 = 0$ . The constraints on the states and estimations are given as

$$p_c \geq 0, p_p \geq 0, q_b \geq 0, \lambda_1 \geq 0, \lambda_2 \geq 0, p_{bit} \geq 0. \quad (20)$$

Some parameters such as  $q_{pump}, q_c, q_{back}, \rho_a, \rho_d, h, \ell_a, \ell_d, p_c$  and  $p_p$  can be measured by sensors while drilling. These

are available at  $t_f = 1$  s sampling rate from the top-side instrumentation and drilling mud logging system. Then the corresponding states, inputs and outputs and time-varying disturbances are given as

$$x = \begin{bmatrix} p_c \\ p_p \\ q_b \\ \lambda_1 \\ \lambda_2 \end{bmatrix}, \quad u = \begin{bmatrix} h \\ \rho_a \\ \rho_d \\ q_{pump} \\ q_c \\ q_{back} \end{bmatrix}, \quad y = \begin{bmatrix} p_c \\ p_p \end{bmatrix}, \quad w = \dot{V}_a, \quad (21)$$

where  $\dot{V}_a = A\dot{h}$  is a known input.

The available data consists of an experimental time series from an MPD drilling operation in the North Sea. The input signals are shown in Figure 3. Some of the measurements are noisy and also contain outright errors in some places. There are several uncertainties in drilling operation due to missing and inaccurate configuration data (inaccurate well profile plan compared with that actual achieved). Normally 5 bar difference between true BHP and estimated BHP is to be expected in many cases.

The window size is chosen as  $N = 10$ . We choose the tuning parameters of the cost function as  $S_t = 0.01I$  and  $W_t = 0.3I$ , and utilize the SVD-based adaptive weighting law with tuning parameters  $\beta = 0.1$  and  $\rho = 0.001$  to define  $R_t$ . The state variables are scaled with factors 0.1 for  $p_c$ , 0.1 for  $p_p$ , 1 for  $q_b$ , and 0.001 for both  $\lambda_1$  and  $\lambda_2$ . These tuning parameters were found after some trial and error in order to achieve a satisfactory combination of fast estimation and high robustness to uncertainties such as noise and data losses. Our experience is that the performance is not very sensitive to the choice of tuning parameters.

In the base case all data points are available, while different data sets with different loss probabilities were generated by randomly and independently picking out a certain percentage of the data points. Table IV shows the different measurement loss probabilities and RMSE between measurements and the estimations during  $t_{total} = 1650$ s. Table V shows the accuracy of the implemented EKF, [19], indicating that better accuracy in estimating the BHP is achieved with the NMHE method. The average computation time is around 400 ms at each step for the NMHE method, while it takes 30 ms for EKF. Although these computations are made in Matlab on a standard PC without any attempt to optimize the implementation for computational efficiency, we believe their ratio is a fairly valid indicator of their computational performance ratio. Comparison of the accuracy between estimates and experimental data with data loss probabilities in the range of 0-70 % are shown in Figures 4 - 8.

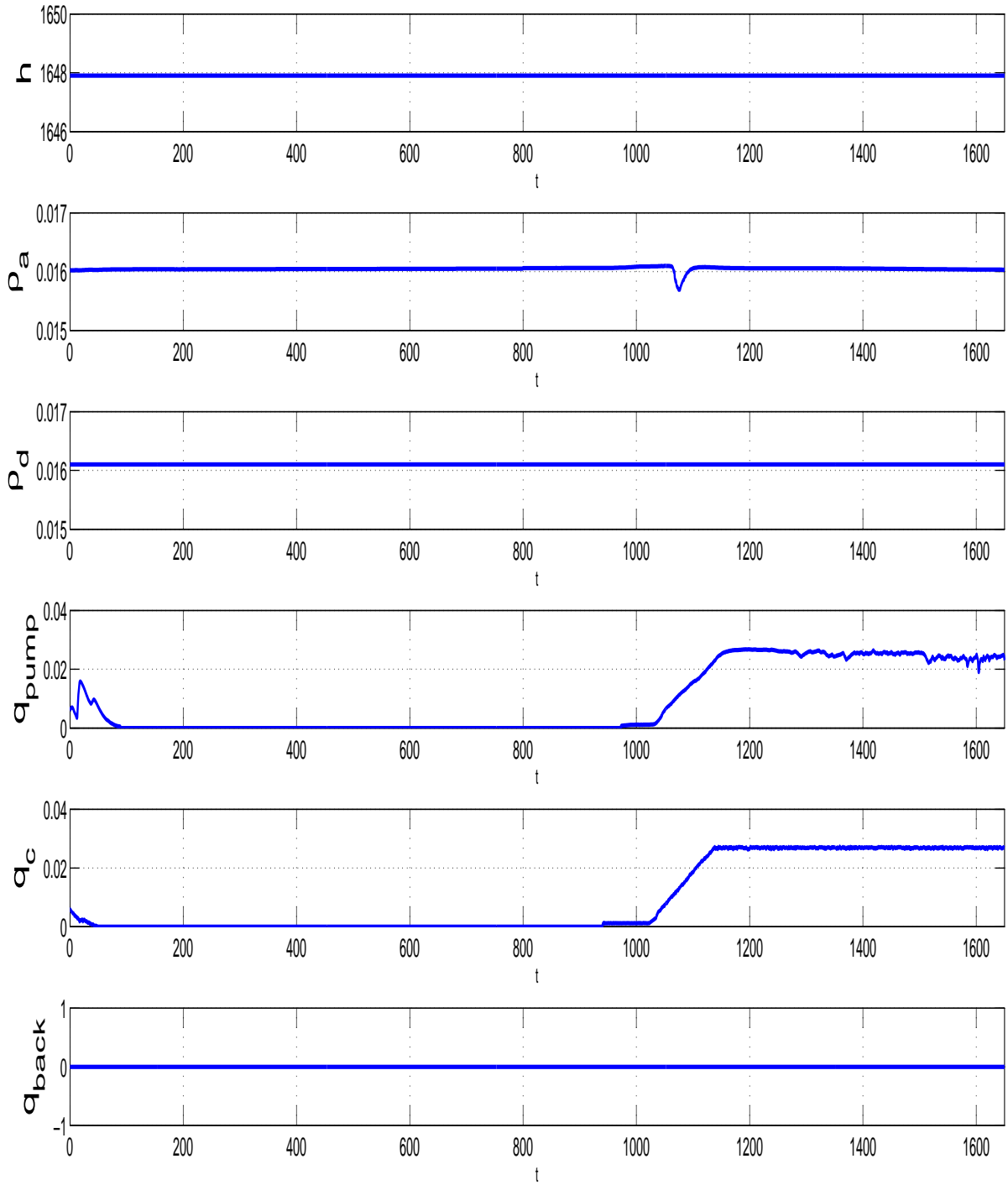


Fig. 3. Example 2: Input measurements.

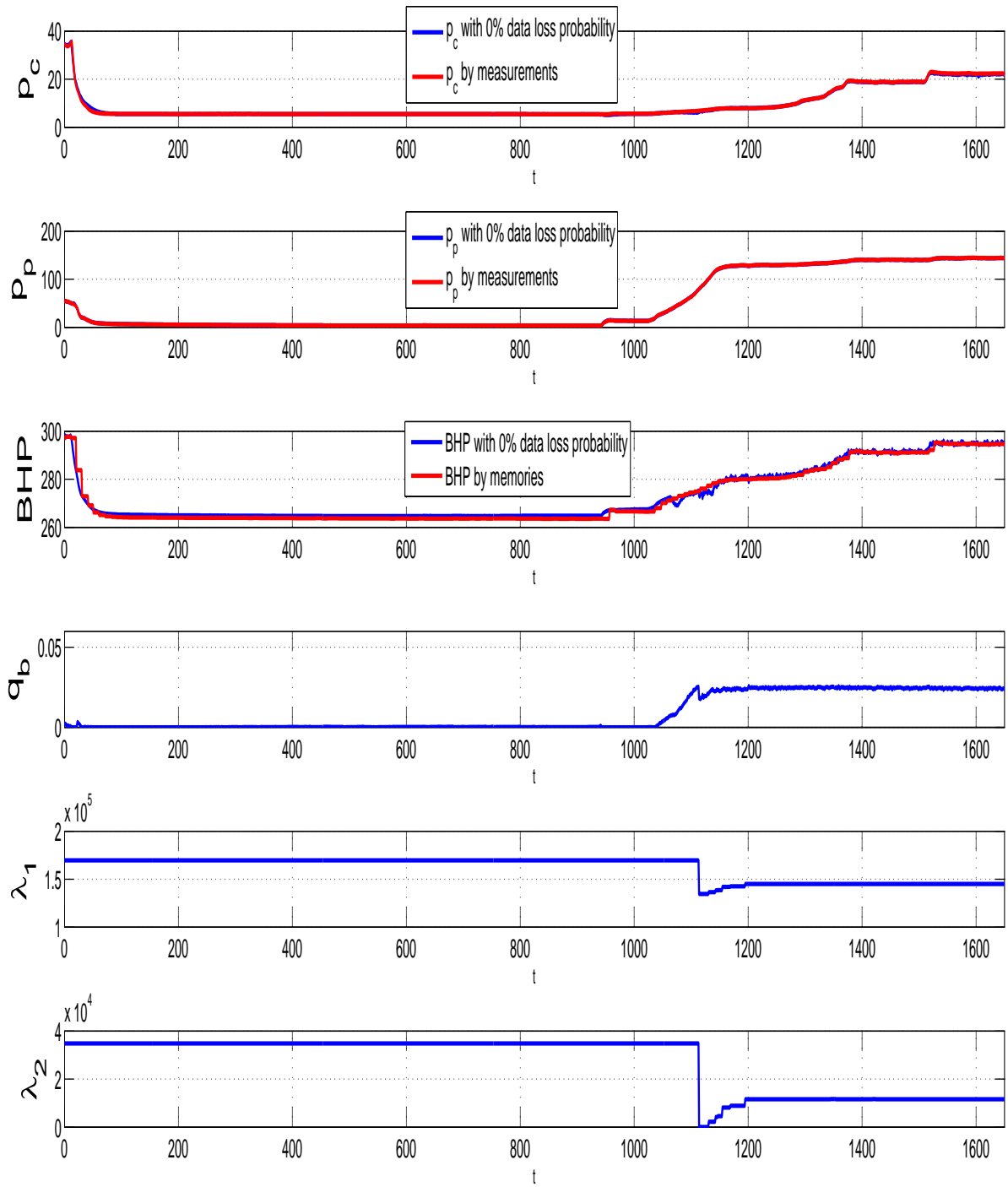


Fig. 4. Example 2: Loss probability being 0%.

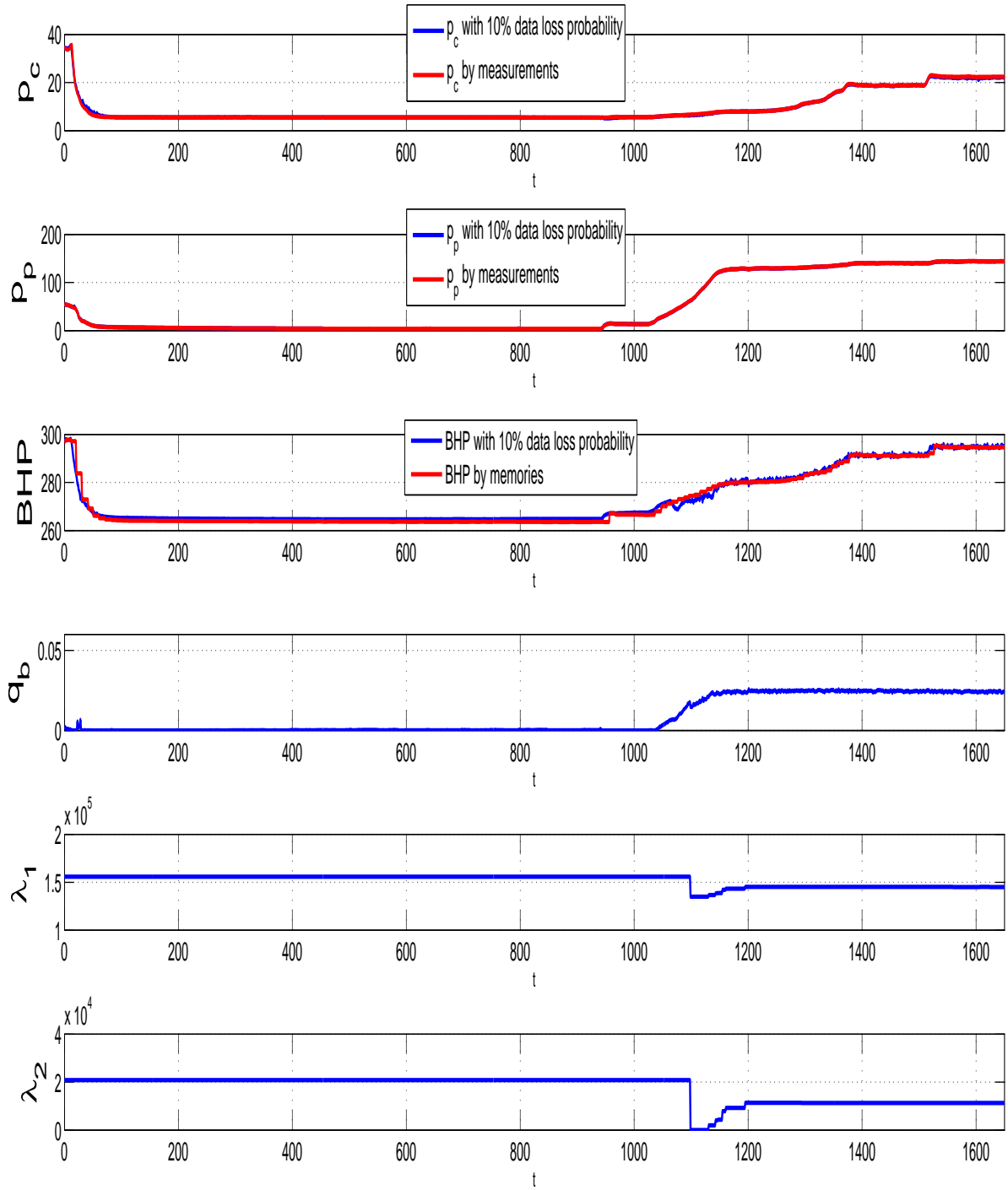


Fig. 5. Example 2: Loss probability being 10%.

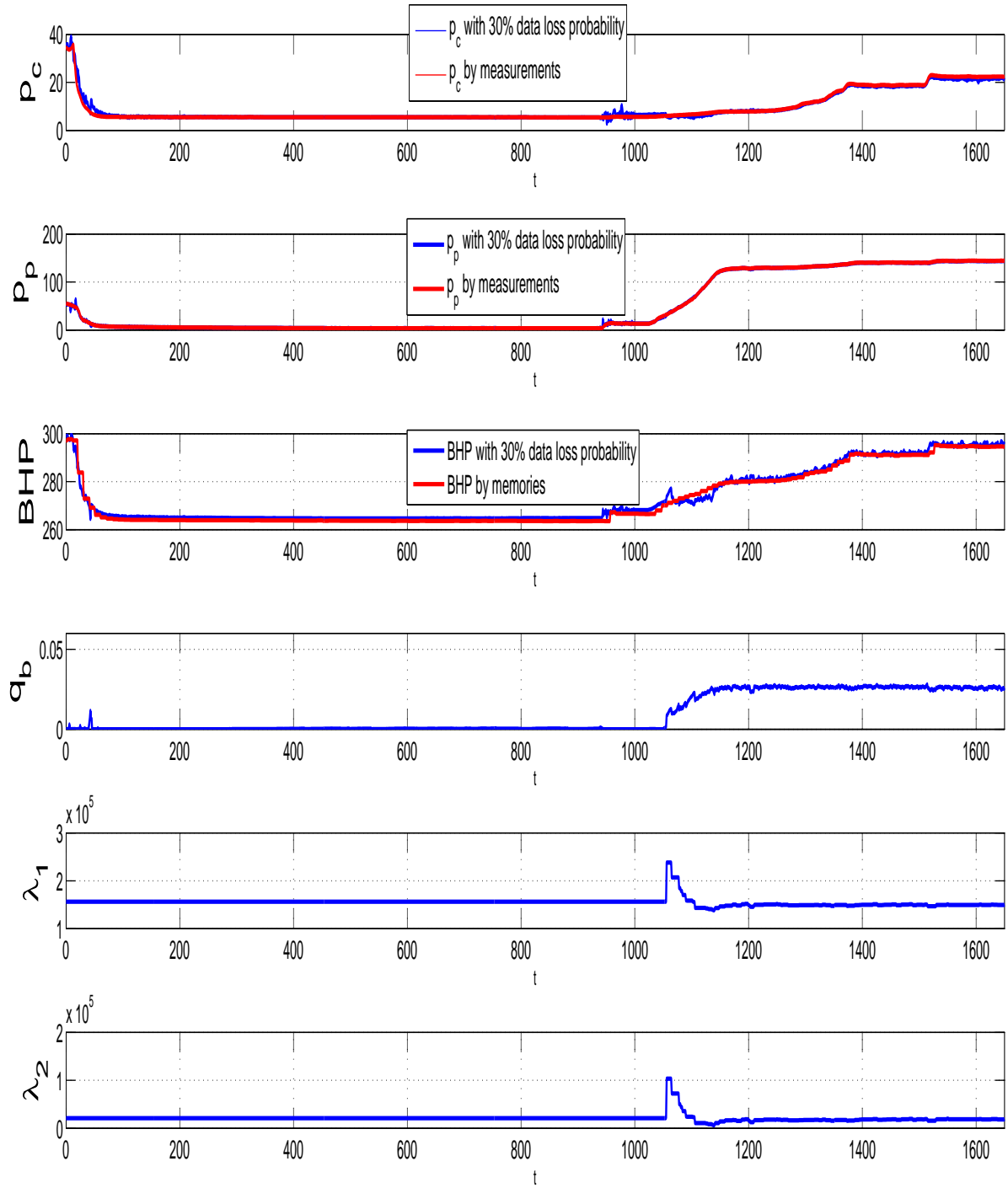


Fig. 6. Example 2: Loss probability being 30%.



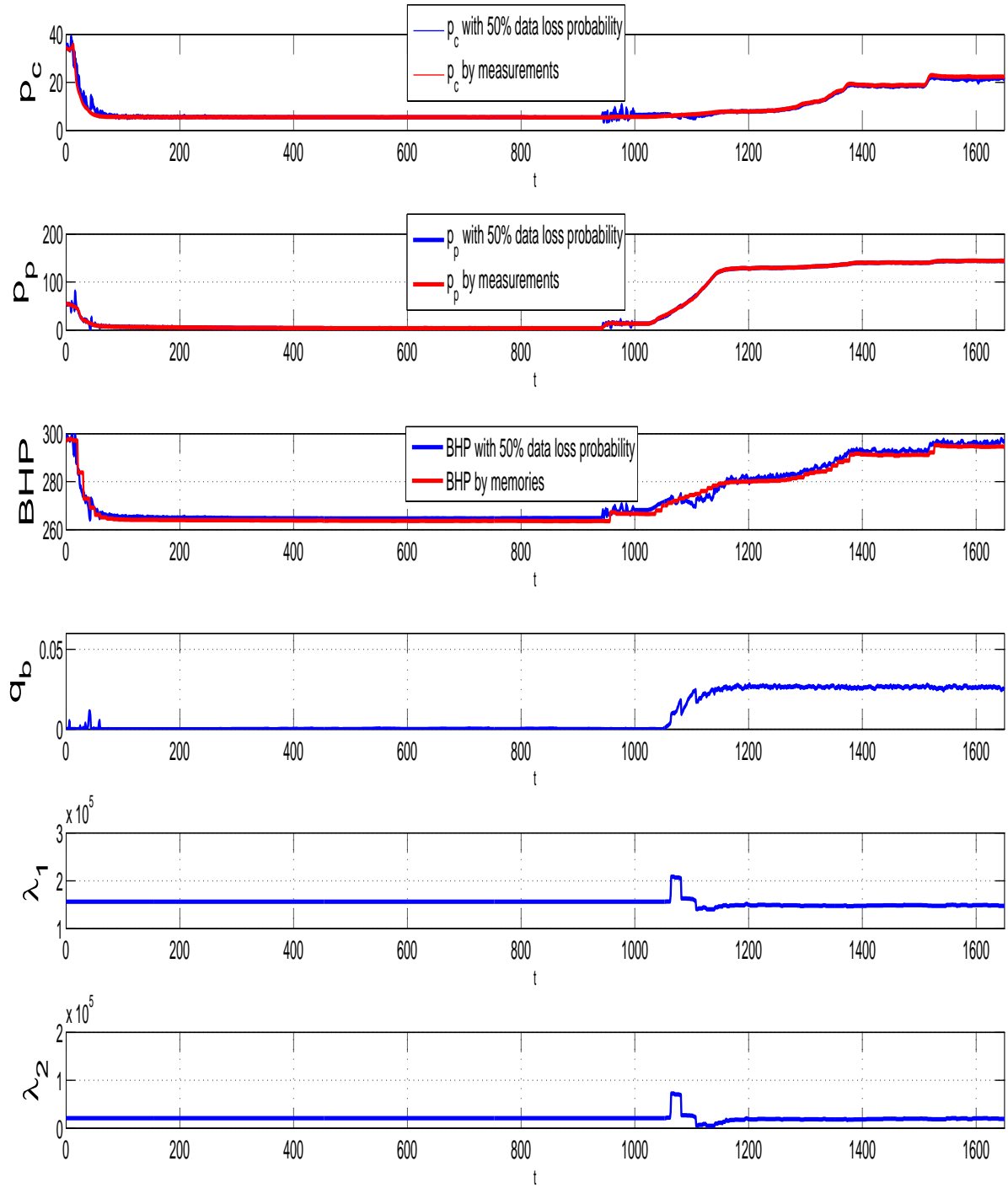


Fig. 7. Example 2: Loss probability being 50%.

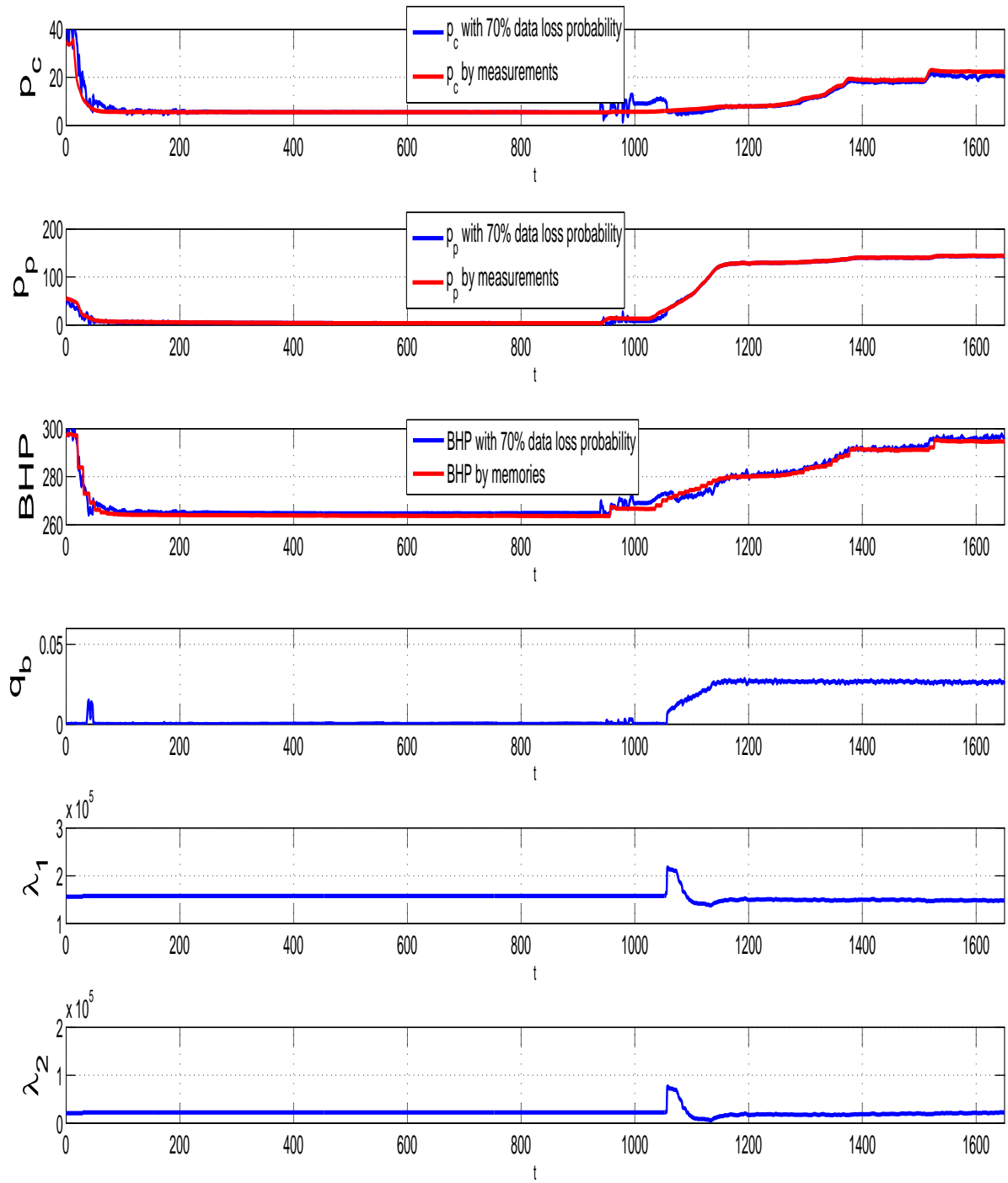


Fig. 8. Example 2: Loss probability being 70%.

Loss Probs (%)	0	2	10	30	50	70
RSME (bar) of $p_c$	0.1274	0.1297	0.1285	0.3870	0.3858	0.8559
RSME (bar) of $p_p$	0.2071	0.2179	0.2192	0.3386	0.4149	0.9396
RSME (bar) of $p_{bit}(BHP)$	0.9905	0.9923	1.0092	1.1889	1.4067	1.4824

TABLE IV

EXAMPLE 2: THE ESTIMATION ERROR OF THE PROPOSED MHE.

Loss Probs (%)	0	2	10	30	50	70
RSME (bar) of $p_c$	0.0847	0.0894	0.1136	0.1748	0.3471	0.8285
RSME (bar) of $p_p$	0.3592	0.3647	0.4082	0.4829	0.7403	1.3260
RSME (bar) of $p_{bit}(BHP)$	1.1963	1.2015	1.3137	1.4689	1.9167	2.1025

TABLE V

EXAMPLE 2: THE ESTIMATION ERROR OF THE EKF.

## VII. CONCLUSIONS

The use of nonlinear moving horizon estimation are studied for applications where output data may be lost or delayed due to unreliable digital communication. The contribution of the paper are nonlinear MHE formulations and weight selection methods that ensures robustness modifications using regularization. The regularizing mechanisms are stabilizing terms in the cost function that ensures graceful degradation to an open loop observer, and a SVD-based weight selection method that avoids drift of estimates when data are not informative and the dynamic model of the plant does not have strong enough internal open loop stability. Simulation and experimental results from an oil well drilling application shows that the performance of the nonlinear MHE degrades gracefully even when output measurements are lost with a probability above 50 %.

## APPENDIX

*Lemma 1:* Define the matrix

$$\Omega_t = \Omega_t(z_{t-N}, \hat{z}_{t-N,t}^o) = Q_t^Y \int_0^1 \frac{\partial}{\partial z} G((1-s)z_{t-N} + s\hat{z}_{t-N,t}^o, U_t) ds.$$

Then  $\Omega_t^T R_t \Omega_t > 0$  for all  $t$  and

$$J_t^o \geq \|z_{t-N} - \hat{z}_{t-N,t}^o\|_{\Omega_t^T R_t \Omega_t}^2. \quad (22)$$

*Proof:* Using the fact that the system (1a)-(1b) can be transformed using  $T$ , there exist  $d_{t-N} = T(x_{t-N})$ ,  $\hat{d}_{t-N,t}^o = T(\hat{x}_{t-N,t}^o)$  and  $\bar{d}_{t-N,t} = T(\bar{x}_{t-N,t})$  such that in the new coordinates, the system is in the form of (9a)-(9c).

Note that the first term in the right-hand side of expression (5) in the new coordinations can be rewritten as

$$\|Y_t - Q_t^Y H(\hat{x}_{t-N,t}^o, U_t)\|_{R_t}^2 = \|Q_t^Y G(z_{t-N}, U_t) - Q_t^Y G(\hat{z}_{t-N,t}^o, U_t)\|_{R_t}^2.$$

From Proposition 2.4.7 in [45],

$$Q_t^Y G(z_{t-N}, U_t) - Q_t^Y G(\hat{z}_{t-N,t}^o, U_t) = \Omega_t(z_{t-N} - \hat{z}_{t-N,t}^o).$$

and we have

$$\|Q_t^Y G(z_{t-N}, U_t) - Q_t^Y G(\hat{z}_{t-N,t}^o, U_t)\|_{R_t}^2 = \|z_{t-N} - \hat{z}_{t-N,t}^o\|_{\Omega_t^T R_t \Omega_t}^2.$$

Taking zero as the lower bound on the rest terms of (5), we get (22). Since the data are  $N$ -informative, the matrix  $\Omega_t$  has full rank and  $\Omega_t^T R_t \Omega_t > 0$  for all  $t$ . ■

*Lemma 2:* Define the matrices

$$\begin{aligned} \Delta_t &= \Delta_t(\bar{x}_{t-N,t}, x_{t-N}) = D_t^Y \int_0^1 \frac{\partial}{\partial x} H((1-s)\bar{x}_{t-N,t} + s x_{t-N}, U_t) ds, \\ \Theta_t &= \Theta_t(\hat{x}_{t-N-1,t-1}^o, x_{t-N-1}) = \int_0^1 \frac{\partial}{\partial x} f((1-s)\hat{x}_{t-N-1,t-1}^o + s x_{t-N-1}, u_{t-N-1}) ds. \end{aligned}$$

Then

$$J_t^o \leq \|x_{t-N-1} - \hat{x}_{t-N-1,t-1}^o\|_{\Theta_t^T (\Delta_t^T S_t \Delta_t + W_t) \Theta_t}^2. \quad (23)$$

*Proof:* We know that  $x_{t-N} \in \mathbb{X}$  is a feasible solution at time  $t$ . From the optimality of  $\hat{x}_{t-N,t}^o$ , we have  $J_t^o \leq J(x_{t-N}; \bar{x}_{t-N,t})$ . Then considering the cost function  $J(x_{t-N}; \bar{x}_{t-N,t})$ , we have  $\|Y_t - Q_t^Y H(x_{t-N}, U_t)\|_{R_t}^2 = 0$ . Like the proof of Lemma 1, the second term in the right-hand side of expression (5) can be rewritten as

$$\|\bar{Y}_t - D_t^Y H(x_{t-N}, U_t)\|_{S_t}^2 = \|D_t^Y H(\bar{x}_{t-N,t}, U_t) - D_t^Y H(x_{t-N}, U_t)\|_{S_t}^2 = \|\bar{x}_{t-N,t} - x_{t-N}\|_{\Delta_t^T S_t \Delta_t}.$$

Similarly,

$$\bar{x}_{t-N,t} - x_{t-N} = \Theta_t(\hat{x}_{t-N-1,t-1}^o - x_{t-N-1}).$$

Then, the terms of the right-hand side of expression (5) can be written as (23). ■

### Proof of Theorem 1:

Consider a Lyapunov function  $V(s_t) = \|s_t^1\|_{P_1}^2 + \|s_t^2\|_{P_2}^2$ , where  $s_t = \text{col}(s_t^1, s_t^2)$ ,  $P_1 = \alpha P_\xi$ ,  $\alpha > 0$  and  $P_2 = P_2^T > 0$  for all  $t \geq 0$ . Then it is easy to show that  $V(s_t) > 0$  and  $V(0) = 0$  for all  $t \geq 0$ . Let  $s_t^1 = \xi_{t-N} - \hat{\xi}_{t-N,t}^o$ ,  $s_t^2 = z_{t-N} - \hat{z}_{t-N,t}^o$ . In

the following  $V(s_{t-N}) - V(s_{t-N-1}) < 0, \forall s_{t-N} \neq 0$  for some  $W_t, S_t$  and  $R_t$  is shown. Since  $\mathbb{X}$  is controlled invariant, then  $\bar{x}_{t-N,t} \in \mathbb{X}$  is a feasible solution. From (A6), we know that  $\text{col}(\bar{\xi}_{t-N,t}, \hat{z}_{t-N,t}^o)$  is also a feasible solution. Considering the cost function of the MHE problem, it is clear that  $\text{col}(\bar{\xi}_{t-N,t}, \hat{z}_{t-N,t}^o)$  is also an optimal solution, since the first term does not depend on the unobservable states and the second term is zero, *i.e.*  $\hat{\xi}_{t-N,t}^o = \bar{\xi}_{t-N,t}$ . Since (A3) holds, we know that

$$\begin{aligned} \|s_t^1\|_{P_1}^2 - \|s_{t-1}^1\|_{P_1}^2 &= \|\xi_{t-N} - \bar{\xi}_{t-N,t}\|_{P_1}^2 - \|s_{t-1}^1\|_{P_1}^2 \\ &\leq -\|s_{t-1}^1\|_{\alpha Q_\xi}^2 + \|s_{t-1}^2\|_{\alpha \Sigma_z}^2 + \|u_{t-N-1} - u_{t-N-1}\|_{\alpha \Sigma_u}^2 \\ &= s_{t-1}^T \begin{bmatrix} -\alpha Q_\xi & 0 \\ 0 & \alpha \Sigma_z \end{bmatrix} s_{t-1} \end{aligned}$$

Since  $\Omega_t$  has full rank (Lemma 1) and there always exists a large  $R_t > 0$  such that  $0 < P_2 \leq \Omega_t^T R_t \Omega_t$ . From lemma 1 and 2, we know that

$$\|s_t^2\|_{P_2}^2 \leq \|s_t^2\|_{\Omega_t^T R_t \Omega_t}^2 \leq \|e_{t-1}\|_{\Theta_t^T (\Delta_t^T S_t \Delta_t + W_t) \Theta_t}^2.$$

From Proposition 2.4.7 in [45],  $s_{t-1} = \Gamma_{t-1} e_{t-1}$ , and we have  $\|s_t^2\|_{P_2}^2 \leq \|s_{t-1}\|_{\Lambda_t}^2 = s_{t-1}^T \Lambda_t s_{t-1}$ . Then,

$$\begin{aligned} V(s_t) - V(s_{t-1}) &\leq s_{t-1}^T \begin{bmatrix} -\alpha Q_\xi & 0 \\ 0 & \alpha \Sigma_z \end{bmatrix} s_{t-1} + s_{t-1}^T \Lambda_t s_{t-1} - \|s_{t-1}^2\|_{P_2}^2 \\ &= s_{t-1}^T \begin{bmatrix} -\alpha Q_\xi & 0 \\ 0 & \alpha \Sigma_z - P_2 \end{bmatrix} s_{t-1} + s_{t-1}^T \Lambda_t s_{t-1}. \end{aligned}$$

Since  $\|\Delta_t\|, \|\Theta_t\|, \|\Gamma_t\|$  are bounded, there always exist a sufficiently large weight matrix  $R_t$  and a suitable  $\alpha$  such that for all  $t \geq 0$ ,  $\alpha > 0$ ,  $S_t > 0$ ,  $W_t > 0$ , and

$$\Omega_t^T R_t \Omega_t \geq P_2, \quad (24a)$$

$$\begin{bmatrix} \alpha Q_\xi & 0 \\ 0 & P_2 - \alpha \Sigma_z \end{bmatrix} > \Xi + \Lambda_t, \quad (24b)$$

where  $\Xi = \Xi^T > 0$ . Then we have  $V(s_t) - V(s_{t-1}) \leq -\|s_{t-1}\|_{\Xi}^2$ , which implies that  $s_t$  is exponentially stable. Since (A2) holds, it is easy to obtain that the error dynamics is exponentially stable.

### Proof of Proposition 1:

Since (A1)-(A2) hold, from Proposition 2.4.7 in [45], we have

$$\begin{aligned} Y_t - Q_t^Y H(\hat{x}_{t-N,t}^o, U_t) &= \Psi_t(x_{t-N} - \hat{x}_{t-N,t}^o), \\ Y_t - Q_t^Y G(\hat{z}_{t-N,t}^o, U_t) &= \Omega_t(z_{t-N} - \hat{z}_{t-N,t}^o). \end{aligned}$$

Since  $Y_t - Q_t^Y H(\hat{x}_{t-N,t}^o, U_t) = Y_t - Q_t^Y G(\hat{z}_{t-N,t}^o, U_t)$ ,

$$\Psi_t(x_{t-N} - \hat{x}_{t-N,t}^o) = \Omega_t(z_{t-N} - \hat{z}_{t-N,t}^o) = \Omega_t \eta (d_{t-N} - \hat{d}_{t-N,t}^o) = \Omega_t \eta \Gamma_t (x_{t-N} - \hat{x}_{t-N,t}^o).$$

Then we have  $\Psi_t = \Omega_t \eta \Gamma_t \Rightarrow \Omega_t = \Psi_t \Gamma_t^{-1} \eta^T$ . Therefore, from the proof the Theorem 1, for some chosen  $S_t, W_t$ , the condition to find  $R_t$  becomes

$$\eta \Gamma_t^{-1 T} \Psi_t^T R_t \Psi_t \Gamma_t^{-1} \eta^T \geq P_2, \quad \begin{bmatrix} \alpha Q_\xi & 0 \\ 0 & P_2 - \alpha \Sigma_z \end{bmatrix} > \Xi + \Lambda_t, \quad \alpha > 0. \quad (25a)$$

### ACKNOWLEDGEMENTS

This work is supported by the Research Council of Norway through the Center for Drilling and Well for improved Recovery and the Center for Integrated Operations in the Petroleum Industry.

### REFERENCES

- [1] P. E. Moraal and J. W. Grizzle. Observer design for nonlinear systems with discrete-time measurement. *IEEE Transactions Automatic Control*, 40:395–404, 1995.
- [2] C. V. Rao, J. B. Rawlings, and D. Q. Mayne. Constrained state estimation for nonlinear discrete-time systems: Stability and moving horizon approximation. *IEEE Transactions Automatic Control*, 48:246–258, 2003.
- [3] A. Alessandri, M. Baglietto, T. Parisini, and R. Zoppoli. A neural state estimator with bounded errors for nonlinear systems. *IEEE Transactions on Automatic Control*, 44:2028 – 2042, 1999.
- [4] A. Alessandri, M. Baglietto, and G. Battistelli. Moving-horizon state estimation for nonlinear discrete-time systems: New stability results and approximation schemes. *Automatica*, 44:1753–1765, 2008.
- [5] E. L. Haseltine and J. B. Rawlings. Critical evaluation of extended Kalman filtering and moving-horizon estimation. *Ind. Eng. Chem. Res*, 44:2451–2460, 2005.
- [6] P. E. Moraal and J. W. Grizzle. Asymptotic observers for detectable and poorly observable systems. In *IEEE Conf. Decision and Control, New Orleans*, pages 109–114, 1995.
- [7] D. Sui and T. A. Johansen. Moving horizon observer with regularization for detectable systems without persistence of excitation. *Int. J. Control*, 84:1041–1054, 2011.
- [8] D. Sui and T. A. Johansen. Regularized nonlinear moving horizon observer for detectable systems. In *IFAC NOLCOS, Bologna, Italy*, 2010.

- [9] D. Sui and T. A. Johansen. Exponential stability of regularized moving horizon observer for  $n$ -detectable nonlinear systems. In *Proc. 9th IEEE International Conference on Control and Automation (ICCA11), Santiago, Chile*, pages 806–811, 2011.
- [10] D. Sui and T. A. Johansen. On the exponential stability of moving horizon observer for globally  $N$ -detectable nonlinear systems. *Asian J. Control*, 12, 2012.
- [11] D. E. Quevedo, A. Ahlén, and K. H. Johansson. Stability of state estimation over sensor networks with markovian fading channels. In *Proc. IFAC World Congress, Milano*, 2011.
- [12] H. Foss. Innovations in integrated control systems. In *Proc. MTS Dynamic Positioning Conference, Houston*, 2006.
- [13] A. Caiti, V. Calabro, and A. Munafo. Auv team cooperation: emerging behaviours and networking modalities. In *IFAC Conference on Manoeuvring and Control of Marine Craft, Arenzano, Italy*, 2012.
- [14] N. Nahi. Optimal recursive estimation with uncertain observation. *IEEE Trans. Information Theory*, 15:457–462, 1969.
- [15] M. Hadidi and S. Schwartz. Linear recursive state estimators under uncertainty observations. *IEEE Trans. Information Theory*, 24:944–948, 1979.
- [16] A. S. Matveev and A. V. Savkin. The problem of state estimation via asynchronous communication channels with irregular transmission times. *IEEE Trans. Automatic Control*, 48:670–676, 2003.
- [17] B. Sinopoli, L. Schenato, M. Franceschetti, K. Poolla, M. I. Jordan, and S. S. Sastry. Kalman filtering with intermittent observations. *IEEE Trans. Automatic Control*, 49:1453–1464, 2004.
- [18] S. C. Smith and P. Seiler. Estimation with lossy measurements: Jump estimators for jump systems. *IEEE Trans. Automatic Control*, 48:2163–2170, 2003.
- [19] S. Kluge, K. Reif, and M. Brokate. Stochastic stability of the extended kalman filter with intermittent observations. *IEEE Trans. Automatic Control*, 55:514 – 518, 2010.
- [20] P. Philipp and B. Lohmann. Moving horizon estimation for nonlinear networked control systems with unsynchronized timescales. In *Preprints 18th IFAC World Congress, Milano*, pages 12457–12464, 2011.
- [21] Z. Jin, C.-K. Ko, and R. M. Murray. Estimation for nonlinear dynamics systems over packet-dropping networks. In *Proc. American Control Conference, New York, NY*, pages 5037–5042, 2007.
- [22] J. do Val and E. Costa. Stability of receding horizon Kalman filter in state estimation of linear time-varying systems. In *Proceedings of the 39th IEEE Conference on Decision and Control*, 2000.
- [23] B. K. Kwon, S. Han, H. Lee, and W. H. Kwon. A receding horizon Kalman filter with the estimated initial state on the horizon. In *International Conference on Control, Automation and Systems*, pages 1686 –1690, 2007.
- [24] M. R. Akhondi, A. Talevski, S. Carlsen, and S. Petersen. Applications of wireless sensor networks in the oil, gas and resource industries. In *IEEE Int. Conf. Advanced Information Networking and Applications*, pages 941–948, 2010.
- [25] P. Tubel, C. Bergeron, and S. Bell. Mud pulse telemetry system for down hole measurement-while-drilling. In *Proc. IEEE Instrumentation and Measurement Technology Conf*, pages 219–223, 1992.
- [26] Z. Jianhui, W. Liyan, L. Fan, and L. Yanlei. An effective approach for the noise removal of mud pulse telemetry system. In *The 8th Int. Conf. Electronic Measurement and Instrumentation*, pages 971–974, 2007.
- [27] R. W. Tennent and W. J. Fitzgerald. Passband complex fractionally-spaced equalization of MSK signals over the mud pulse telemetry channel. In *Prof. IEEE 1st Workshop on Signal Processing Advances in Wireless Communication*, 1997.

- [28] H. Wolter et al. The first offshore use of an ultrahigh-speed drillstring telemetry network involving a full LWD logging suite and rotary-steerable drilling system. In *Proc. SPE Annual Tech. Conf. and Exhibition, Anaheim*, page SPE 110939, 2007.
- [29] S. Hovda, H. Wolter, G.-O. Kaasa, and T. S. Ølberg. Potential of ultra high-speed drill string telemetry in future improvements of the drilling process control. In *Proc. IADC/SPE Asia Pacific Drilling Tech. Conf. Exhib., Jakarta*, page IADC/SPE 115196, 2008.
- [30] K. Xuanchao and C. Guojian. The research of information and power transmission property for intelligent drillstring. In *Proc. 2nd Int. Conf. Information Technology and Computer Science, Kiev*, pages 174–177, 2010.
- [31] F. Iversen et al. Offshore drilling field test of a new system for model integrated closed-loop drilling control. In *Proc. IADC/SPE Drilling Conference, Orlando*, pages 518–520, 2009.
- [32] J. Thorogood, W. Aldred, F. Florence, and F. Iversen. Drilling automation: Technologies, terminology and parallels with other industries. In *Proc. SPE/IADC Drilling Conf. Exhib., Amsterdam*, page SPE/IADC 119884, 2009.
- [33] J. Zhou, Ø. N. Stamnes, O. M. Aamo, and G.-O. Kaasa. Switched control for pressure regulation and kick attenuation in a managed pressure drilling system. *IEEE Trans. Control Systems Technology*, 19:337–350, 2011.
- [34] J. E. Gravdal, R. J. Lorentzen, and R. W. Time. Wire drill pipe telemetry enables real-time evaluation of kick during managed pressure drilling. In *Proc. SPE Asia Pacific Oil and Gas Conf. Exhib, Brisbane*, page SPE 132989, 2010.
- [35] M. Paasche, T. A. Johansen, and L. S. Imsland. Estimation of bottomhole pressure during oil well drilling using regularized adaptive nonlinear moving horizon observer. In *IFAC World Congress, Milano, Italy*, 2011.
- [36] A. N. Tikhonov and V. Y. Arsenin. *Solutions of Ill-posed Problems*. Wiley, 1977.
- [37] T. Poloni, B. Rohal-Ilkiv, and T. A. Johansen. Damped one-mode vibration model state and parameter estimation via pre-filtered moving horizon observer. In *5th IFAC Symposium on Mechatronic Systems, Boston*, 2010.
- [38] D. Sui, T. A. Johansen, and L. Feng. Linear moving horizon estimation with pre-estimating observer. *IEEE Trans. Automatic Control*, 55:2363 – 2368, 2010.
- [39] R. Kulhavy. Restricted exponential forgetting in real-time identification. *Automatica*, 23:589–600, 1987.
- [40] S. Bittanti, P. Bolzern, and M. Campi. Convergence and exponential convergence of identification algorithms with directional forgetting factor. *Automatica*, 26:929–932, 1990.
- [41] L. Y. Cao and H. M. Schwartz. A directional forgetting algorithm based on the decomposition of the information matrix. In *Proceedings of the 7th Mediterranean Conference on Control and Automation, Haifa, Israel*, 1999.
- [42] M. Hovd and R. R. Bitmead. Directional leakage and parameter drift. *Int. J. Adaptive. Control and Signal Processing*, 20:27–39, 2007.
- [43] G. H. Golub and C. F. van Loan. *Matrix computations*. Oxford University Press, 1983.
- [44] Ø. N. Stamnes. *Observer for bottomhole pressure during drilling*. Master Thesis, NTNU, 2007.
- [45] R. Abraham, J. E. Marsden, and T. Ratiu. *Manifolds, Tensor Analysis, and Applications*. Springer-Verlag New York, 1983.