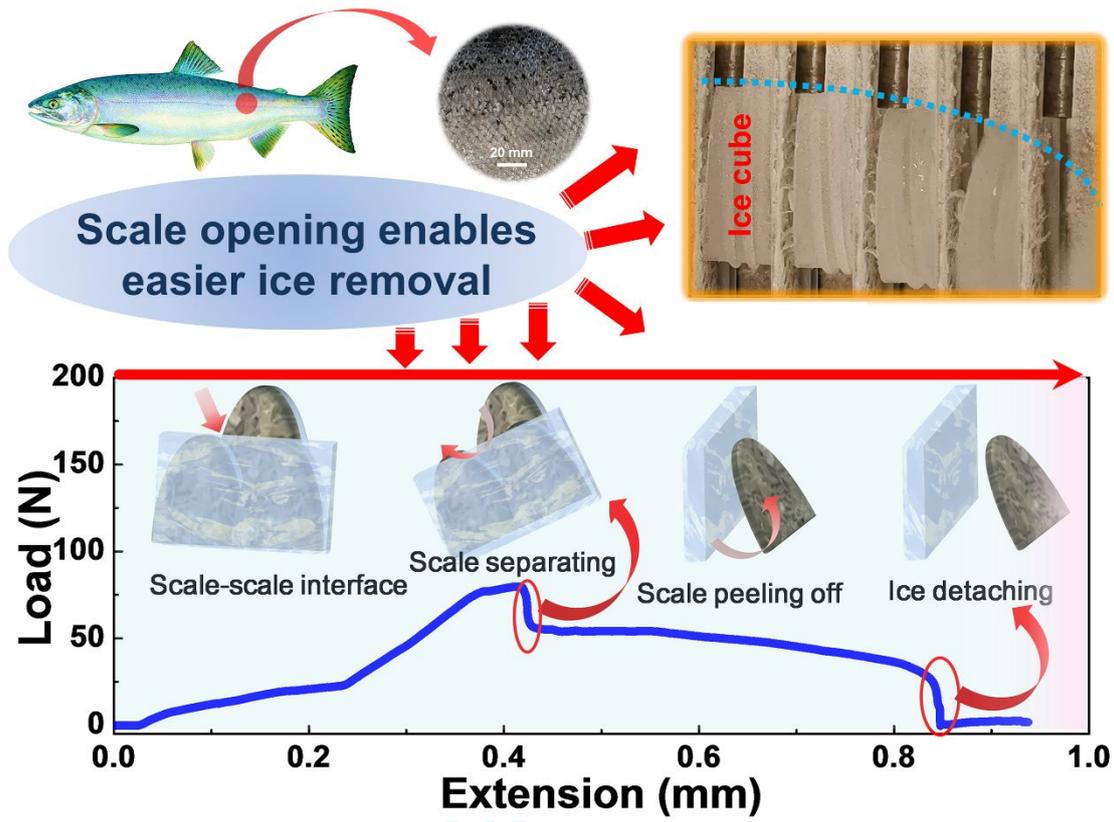


Unravelling the mystery of fish scales in lowering ice adhesion

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Unravelling the mystery of fish scales in lowering ice adhesion

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Abstract

The influence of static surface properties, such as free energy, toughness, and elasticity, on icephobicity has been extensively researched and documented in existing literature.

However, there remains a limited understanding of the role played by surface dynamic characteristics in facilitating ice removal. This study investigates the ice adhesion strength of authentic Arctic salmon (*Salmon salar*) skin, revealing intriguing anisotropic ice adhesion behavior. Results indicate a significant decrease in ice adhesion strength (141 ± 47 kPa) when sheared against the growth orientation of fish scales compared to shearing along this orientation (353 ± 95 kPa). The distinctive structural evolution of fish scales during shearing can lead to a sequential rupture process, thereby diminishing ice adhesion. Additionally, the study highlights the significance of the opening and peeling capacity of fish scales in controlling ice detachment, defined as the ability of unit scales to separate from their underlying structures and adhesives under applied force. Enhancing this capacity could further

24 reduce ice adhesion strength (66 ± 15 kPa), facilitating effortless ice detachment on fish
25 scales. The mechanical robustness of fish scales offers new possibilities for designing
26 hard and durable anti-icing surfaces.

27 **Keywords:** fish scale, ice adhesion, dynamic behaviors, sequential rupture, anti-icing.

29 Introduction

30 Icing is a phenomenon commonly observed in nature (1). Excessive ice accumulation
31 on infrastructure, transport facilities, and renewable energy production equipment has
32 resulted in numerous safety and economic problems (2–6). Passive anti-icing surfaces
33 that enable easy ice removal without active chemical/energy input have received
34 worldwide attention as a mitigation method (7–9). Anti-icing surfaces are typically
35 designed to repel water, delay ice nucleation, reduce frost formation and coverage, and
36 lower ice adhesion (7–12). However, if surfaces are exposed to air for a prolonged
37 period of time at low temperatures, ice will eventually form in areas where water cannot
38 be drained, such as on standstill wind turbine blades. Lowering ice adhesion and
39 removing ice automatically under wind and gravitational force has become a desirable
40 strategy (13–18).

41 Cutting-edge icephobic surfaces with minimal ice adhesion primarily rely on
42 manipulating static surface parameters. Ice adhesion strength (τ_{ice}) on solid surfaces is
43 commonly described using a semi-empirical equation: $\tau_{ice} = \sqrt{E^* G / \pi a \Lambda}$, where E^*
44 represents the surface's elastic modulus, G denotes surface free energy, a signifies the
45 length of interface cracks, and Λ is a non-dimensional constant (19, 20). Adjusting

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4 46 static surface parameters, such as surface free energy and elastic modulus, can
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6 47 effectively reduce surface ice adhesion (7, 9, 21, 22). Silicone elastomers, characterized
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9 48 by low surface energy and elastic modulus, are frequently employed as icephobic
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12 49 surfaces (9, 14, 15, 23, 24). Interfacial toughness is another parameter utilized to modify
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15 50 surface ice adhesion (13, 25, 26). Surfaces with low interfacial toughness require nearly
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17 51 the same mechanical force for ice removal on surfaces larger than a certain size (13,
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19 52 27). While static strategies have shown remarkable icephobicity on soft gels and
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22 53 rubbers, designing anti-icing surfaces for hard materials remains challenging. A
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25 54 prevalent approach to reducing ice adhesion on hard surfaces is employing a
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27 55 superhydrophobic structure with low E^* and large a . However, the practical
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30 56 applications of superhydrophobic surfaces are hindered by their poor durability in
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33 57 icing/de-icing cycles. Achieving durable low ice adhesion on high modulus surfaces
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35 58 remains a significant challenge.

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38 59 State-of-the-art icephobic surfaces with low ice adhesion are primarily designed by
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41 60 manipulating static surface parameters. To describe ice adhesion strength (τ_{ice}) on solid
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43 61 surfaces, a semi-empirical equation, $\tau_{ice} = \sqrt{E^* G / \pi a \Lambda}$, is commonly used. E^*
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45 62 represents the elastic modulus of the surface, G represents the surface free energy, a
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48 63 represents the length of interface cracks, and Λ is a non-dimensional constant (19, 20).
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51 64 According to this theory, adjusting static surface parameters such as surface free energy
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54 65 and surface elastic modulus can decrease surface ice adhesion (7, 9, 21, 22). For
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56 66 example, silicone elastomers with low surface energy and elastic modulus are a
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59 67 common type of icephobic surface (9, 14, 15, 23, 24). Another parameter, interfacial
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4 68 toughness, has also been used to modify surface ice adhesion (13, 25, 26). The surfaces
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6 69 with low interfacial toughness allow for the use of nearly the same mechanical force to
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9 70 remove ice on surfaces larger than a certain size (13, 27). While static strategies have
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11 71 achieved excellent icephobicity on soft gels and rubbers, designing anti-icing surfaces
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14 72 on hard materials remains a challenge. A common approach to reducing ice adhesion
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17 73 on hard surfaces is to use a superhydrophobic structure with low E^* and large a .
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19 74 However, the practical applications of superhydrophobic surfaces are limited due to
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21 75 their poor durability in icing/de-icing cycles. Achieving durable low ice adhesion on
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24 76 high modulus surfaces remains a significant challenge.

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27 77 Recent studies have highlighted the potential of leveraging dynamic properties in
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29 78 both artificial and bioinspired surfaces to enhance the design of ice-repellent surfaces
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31 79 (8, 16, 18, 24, 28). The modulation of surface properties in response to temperature,
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34 80 light, and mechanical stimuli can be harnessed to create surfaces with exceptionally
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37 81 low ice adhesion strength (29–31). Golovin et al. conducted a notable study
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39 82 demonstrating that the dynamic buckling behavior of metallic surfaces can significantly
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42 83 mitigate ice adhesion (32). Thus, utilizing the dynamic nature of surface properties
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45 84 presents a promising strategy for reducing ice adhesion on hard surfaces with improved
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48 85 mechanical robustness.

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50 86 Fish scales, renowned for their distinctive wettability, have spurred the development
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52 87 of subaquatic, low-adhesion superoleophobic surfaces (33, 34). Yet, our understanding
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55 88 of ice adhesion on fish scales remains limited (35). In our prior research employing
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58 89 atomistic modeling, fish scale-like structures revealed a distinctive sequential rupture
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4 90 mechanism that mitigates ice adhesion. Norwegian salmon, an anadromous species
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6 91 abundant in Norway's seas and rivers, ranks among the world's most consumed fish.
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9 92 While anti-icing characteristics are irrelevant to salmon, unraveling how fish scales
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11 93 reduce ice adhesion could foster innovative anti-icing strategies, particularly in Arctic
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13 94 regions. This study delved into the de-icing dynamics of authentic salmon skin, altering
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15 95 de-icing directions relative to scale orientation to gauge varied ice adhesion strengths.
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17 96 Findings underscore the correlation between ice adhesion strength and the mode of
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19 97 rupture at ice-surface contact points. Detailed observation of ice removal from fish
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21 98 scales elucidated the underlying mechanisms, highlighting the pivotal role of scales'
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23 99 opening and peeling in mitigating adhesion during de-icing. Modulating surface
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25 100 structure parameters to enhance scales' opening or peeling capability holds promise for
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27 101 reducing ice adhesion. Therefore, fish scales inspire a new principle for fabricating
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29 102 robust surfaces with low ice adhesion.

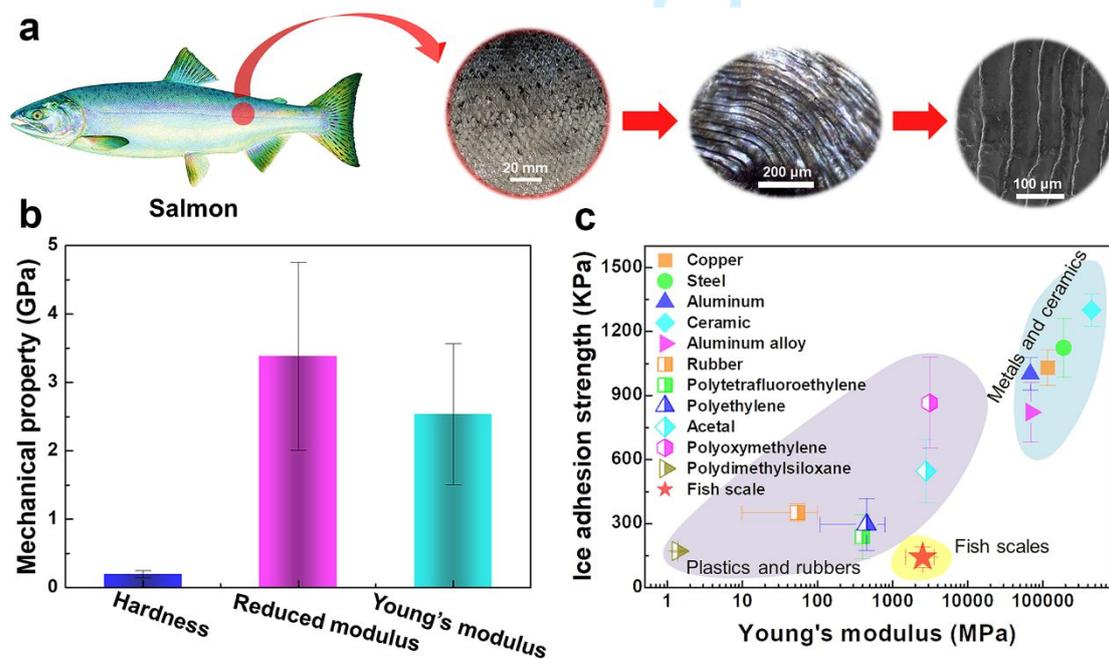
103 **Results and discussions**

104 This work investigates the adhesion of ice on authentic salmon skin. Figure 1a
105 illustrates the structures of fish scales on Atlantic salmon skin, characterized by their
106 specific orientation. Surface analysis indicates that fish scales exhibit a rough texture
107 composed of ribbing micropatterns. Previous research has highlighted the remarkable
108 underwater superoleophobic properties of fish scales, attributed to their
109 superhydrophilicity and micropatterned structure (33, 34). These properties prevent oil
110 and fouling contamination, facilitating exceptional self-cleaning abilities (33).
111 Additionally, fish scales exhibit intriguing mechanical characteristics, such as

flexibility, high strength, resistance to penetration, and lightweight nature [36].

However, the potential anti-icing properties of fish scales remain unexplored.

Mechanical testing of fish scales depicted in Figure 1b was conducted using cylindrical flat punch nanoindentation (see Supplementary Section 1) (37). Fish scales demonstrate greater durability compared to elastomers. According to the adhesion equation $\tau_{ice} = \sqrt{E^* G/\pi a \Lambda}$, materials with low surface energy and elastic modulus, such as plastics and rubbers, typically exhibit lower ice adhesion than metals and ceramics (Figure 1c). Consequently, state-of-the-art anti-icing surfaces primarily utilize soft polymers (8, 9). Nonetheless, enhancing the mechanical and chemical durability of soft materials poses a significant challenge in achieving prolonged icephobicity (8, 9). Despite its high elastic modulus, ice adhesion strength on fish scales is significantly lower than on many plastics and rubbers. Further exploration of the role of fish scales in mitigating ice adhesion holds promise for developing robust and enduring anti-icing surfaces.

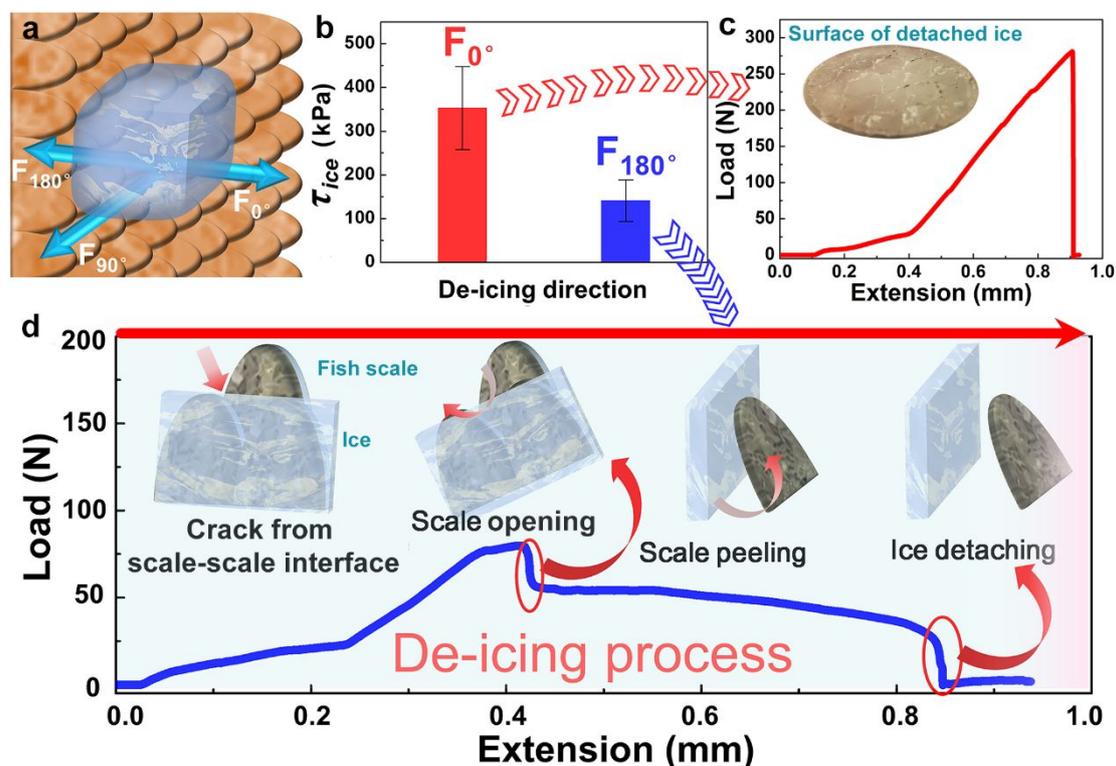


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4 126 **Figure 1. Properties of a real salmon scale.** (a) The appearance of fish scales, observed using a
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6 127 camera, an optical microscope and a scanning electron microscope (SEM). (b) Nanoindentation is
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9 128 used to determine the mechanical characteristics of fish scales. (c) The ice adhesion strength on
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12 129 various surfaces and is comparable to the ice adhesion strength on fish scales. The ice adhesion
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14 130 strength on copper, steel, aluminum, ceramic, aluminum alloy, and rubber is obtained from Ref. 38
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17 131 (38). The ice adhesion strength of polytetrafluoroethylene, polyethylene, acetal, and
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20 132 polyoxymethylene is obtained from Ref. 39 (39). The Young's modulus of the various materials is
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22 133 obtained from Ref. 39 (39). Ref. 40 (40) reports on the ice adhesion strength of
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25 134 polydimethylsiloxane as well as the Young's modulus. The ice adhesion strength on the fish scale
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27 135 is determined by de-icing against the scale growth orientation.
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30 136 The ice adhesion strength on fish scales exhibits anisotropy, depending on the direction
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32 137 of the applied shearing force (Fig. 2a). A comparative analysis was conducted to assess
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35 138 the ice adhesion strength on fish scales during de-icing along (F_{0°) and against (F_{180°)
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38 139 the scale growth orientation (Fig. 2b). The measured ice adhesion by F_{180° is 141 ± 47
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40 140 kPa, representing a reduction of up to 60% compared to F_{0° (353 ± 95 kPa).
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43 141 Examination of the load-extension curves for both de-icing directions allows for the
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46 142 discussion of the underlying mechanism. Figure 2c illustrates a typical load-extension
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49 143 curve when applying a shearing force along the scale growth orientation, reaching
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52 144 maximum load and swiftly decreasing to zero (20). The robust mechanical interlocking
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55 145 between ice and rough fish scales necessitates significant force for ice removal. Upon
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58 146 detachment of the ice cube from fish scales (Fig. 2c), the surface appears rough,
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60 147 indicating strong interlocking during ice formation. Conversely, applying a shearing

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4 148 force against the scale growth orientation results in a distinctive curve, where the load
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6 149 gradually evolves before decreasing to zero (Fig. 2d). Our prior research, employing
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9 150 atomistic modeling and molecular dynamics simulation, identified two distinct fracture
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11 151 modes responsible for this phenomenon (35). Ice removal along the scale orientation
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14 152 leads to simultaneous rupture of the entire scale-ice interface, termed concurrent rupture
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17 153 mode. Conversely, de-icing against the scale orientation follows a sequential rupture
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20 154 mode, where the interface breaks incrementally. It has been suggested that the
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22 155 sequential rupture mode can result in elongated energy depth and, consequently, a
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24 156 significantly lower rupture force compared to the concurrent rupture mode (35).
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27 157 However, experimental clarification and understanding of these differences are lacking.
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30 158 This study demonstrates the reduced ice adhesion on fish scales through de-icing
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33 159 against the scale growth orientation, validating the role of sequential rupture in
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35 160 diminishing ice adhesion strength.
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38 161 Figure 2d illustrates the dynamic fracture occurring during de-icing against the
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41 162 orientation of scale growth. This process comprises three stages: scale opening, scale
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43 163 peeling, and ice detachment. Initially, the force increases until the scale-scale interfaces
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46 164 fracture, initiating scale opening. Upon reaching maximum load, the interactions
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49 165 between scales are disrupted. Consequently, the force required to displace the ice
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52 166 decreases slightly, although the ice remains adhered to the surface. The process of
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54 167 rupturing fish scales is governed by peeling them from the ice due to their flexibility.
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56 168 Peeling the scales necessitates a smaller shearing force compared to fracturing the
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169 scale-scale interfaces. The load gradually diminishes during scale peeling and
 170 diminishes to zero as the ice detaches.



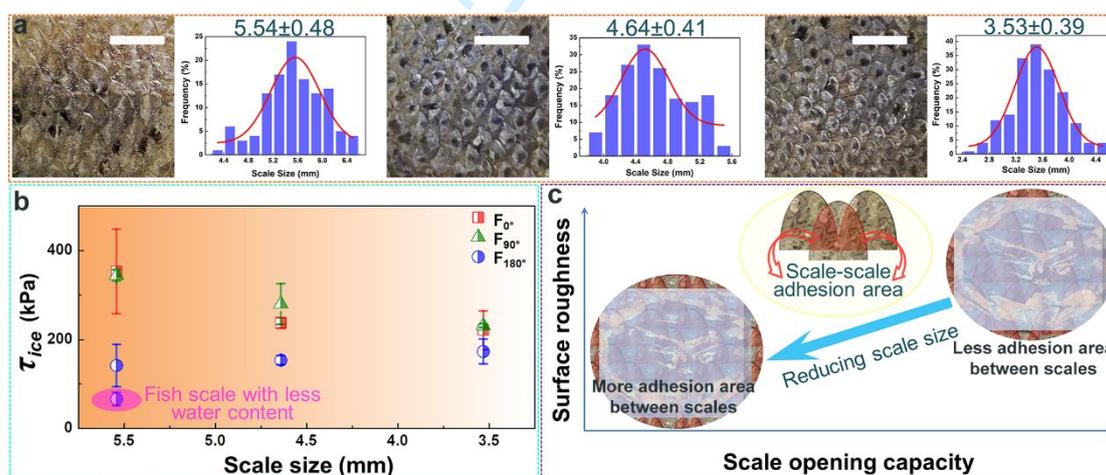
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172 **Figure 2. Ice adhesion behaviors on salmon scales.** (a) A schematic graphic depicts the direction
 173 of the shearing force used during the de-icing operation. F_{0° , F_{90° , and F_{180° are the de-icing forces
 174 along, vertical to, and against the direction of fish scale growth, respectively. (b) Ice adhesion
 175 strength on fish scales through de-icing along and against the direction of fish scale expansion. (c)
 176 The load-displacement curve for de-icing along the direction of fish scale growth. (d) The load-
 177 displacement curve and dynamic evolution of scales and ice during de-icing are plotted against the
 178 direction of fish scale growth.

179 Based on the preceding discussion, it becomes apparent that the opening of fish scales
 180 during the de-icing process is paramount for achieving minimal ice adhesion. To
 181 elucidate the impact of opening capacity, inversely linked to scale-scale adhesion, on
 182 reducing ice adhesion, we conducted an analysis of fish scales with varying sizes, as

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4 183 delineated in Supplementary Section 2. Figure 3a illustrates three distinct types of fish
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6 184 scales, each measuring 5.54 mm, 4.64 mm, and 3.53 mm, sourced from the skin of
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9 185 Atlantic salmon. Ice adhesion strength post-de-icing in the F_{0° , F_{90° , and F_{180° directions
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12 186 is detailed in Figure 3b. Notably, discernible trends emerge in de-icing with F_{0° and F_{90°
13
14 187 in contrast to de-icing along the F_{180° direction. Ice adhesion diminishes as the scale
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17 188 size decreases during de-icing with F_{0° and F_{90° . However, de-icing against the direction
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20 189 of scale growth results in increased ice adhesion strength as the scale size decreases.
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22 190 This variation arises from different fracture modes influencing ice adhesion across scale
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24 191 sizes. Reducing the scale size diminishes surface roughness, thereby mitigating
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27 192 mechanical interlocking between ice and the surface. Consequently, during de-icing at
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30 193 F_{0° and F_{90° without dynamic surface changes or with slight surface opening, ice
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33 194 adhesion strength is lower on surfaces with smaller scales. However, reducing the scale
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35 195 size enhances the threshold of scale opening.
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37 196 As illustrated in Fig. 3c, a simplified model depicting the adhesion between scales is
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40 197 presented. Each fish scale overlaps with two others beneath it. In freezing conditions,
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43 198 water between the scales freezes, binding them together. To diminish ice adhesion and
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46 199 facilitate scale opening, it's vital to induce a fracture where the scales adhere.
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48 200 Consequently, ice adhesion strength is inversely proportional to the scale's opening
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51 201 capacity. Reducing the scale size enlarges the adhesion area between the scale and the
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54 202 ice cube, diminishing the scale's opening capacity and necessitating greater forces.
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56 203 When de-icing along the F_{180° direction, decreasing the scale size diminishes the scale's
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59 204 opening capacity, resulting in stronger ice adhesion. With a scale size of 3.53 mm, ice
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205 adhesion on fish scales during de-icing at F_{0° and F_{90° mirrors that at F_{180° , indicating
 206 negligible differences in scale opening capacity for this size. An alternative method to
 207 modulate the scale's opening capacity is by adjusting the water content. After a year in
 208 the freezer, the scales maintained their shape with reduced water content due to ice
 209 sublimation. Lower water content weakens scale-scale interactions after freezing,
 210 enhancing the scale's opening capacity. This facilitates easier separation between scales.
 211 The results in Fig. 3b demonstrate that ice adhesion strength on fish scales with reduced
 212 water content during de-icing along F_{180° is only 66 ± 15 kPa, falling within the range
 213 of icephobic surfaces. Enhancing the opening capacity of fish scale-like structures can
 214 effectively mitigate surface icephobicity.



215
 216 **Figure 3. Ice adhesion behaviors on fish scales with different sizes.** (a) Fish scales of various
 217 sizes are used to measure ice adhesion strength. Each variety of fish skin had at least 100 scales
 218 measured to determine its size. The photos' scale bars are 10 mm. (b) The ice adhesion strength
 219 through de-icing in F_{0° , F_{90° , and F_{180° directions on surfaces of different scale sizes. (c) A schematic
 220 figure depicts the effect of scale size on surface roughness and scale opening capacity.

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4 221 After the fish scales have opened, ice fracture is governed by the peeling process.
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6 222 Supplementary Movies S1 and S4 provide detailed documentation of de-icing against
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9 223 the fish scale growth orientation and the peeling process. As illustrated in Fig. 4a, fish
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12 224 scales exhibit various bending patterns during de-icing. Importantly, the scales revert
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14 225 to their original states immediately after ice detachment. Designing scales with
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16 226 mechanical robustness can confer durable icephobicity through fish scale-like
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19 227 structures. These scales can retain their shape and functionality during icing and de-
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22 228 icing cycles on actual fish skin. Nonetheless, weak connections between the scales and
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25 229 skin pose a problem, as the scales are prone to being dislodged from the fish skin when
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28 230 removing ice. Enhancing the interaction between scales and substrate is a critical
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30 231 endeavor for the future design of fish scale-inspired anti-icing surfaces

32 232 Peeling an elastic film from a rigid substrate can generally be described by Eq. 1 (41)

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34
35 233
$$\left(\frac{F}{b}\right)^2 \frac{1}{2Ed} + \left(\frac{F}{b}\right)(1 - \cos\theta) - R = 0 \quad (1)$$

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38 234 The formula for calculating the applied peeling force (F) encompasses several
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40 235 parameters, including the width of the adhesive (b), adhesive thickness (d), Young's
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43 236 modulus of the film (E), peeling angle (θ), and adhesive energy (R). A schematic
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46 237 diagram illustrating these parameters is available in Supplementary Section 4. During
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48 238 fish scale de-icing, the scales are treated as elastic films, and the ice as a rigid substrate.
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51 239 The angle $\theta (= 180^\circ - \beta)$ can be determined as depicted in Figure 4b-d. Although scales
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54 240 exhibit various bending behaviors, β values consistently decrease from approximately
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56 241 135° to 30° . Consequently, the θ in the scale peeling process increases from about 45°
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59 242 to 150° . Meanwhile, the force required for ice removal gradually decreases until
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4 243 detachment. It's worth noting that the scales' bending response affects angle α , not angle
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6 244 β at detachment (Fig. 4b-d). Scale peeling capacity depends on intrinsic parameters
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9 245 such as R, E, d, and b of fish scales. De-icing forces on scales with reduced water
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11 246 content (Supplementary Fig. S6) show significantly lower peeling forces due to reduced
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14 247 R compared to those in Fig. 2d. Future research focusing on modulating R, E, d, or b
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17 248 and understanding their relationships with scale peeling capacity could facilitate easier
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19 249 ice removal from fish scale-like surfaces.

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22 250 The connection between scales and skin must be considered, as it can impact the de-
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24 251 icing process. A soft, mechanically friction-free connection between scales and skin
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27 252 can facilitate crack formation at scale-scale interfaces compared to a hard connection.
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30 253 Additionally, a soft connection can benefit scale opening, emphasizing the importance
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32 254 of using soft salmon skin to reduce ice adhesion on scales. Based on the preceding
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35 255 discussions, it's evident that the sequential rupture mode in de-icing against fish scale
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38 256 growth orientation can lead to exceptionally low ice adhesion. The critical parameters
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40 257 controlling ice removal are scale opening capacity and scale peeling capacity.
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43 258 Enhancing these parameters can facilitate easy ice detachment. Fish scale-inspired
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46 259 surfaces with improved scale opening and peeling capacity hold promise for future anti-
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48 260 icing applications.

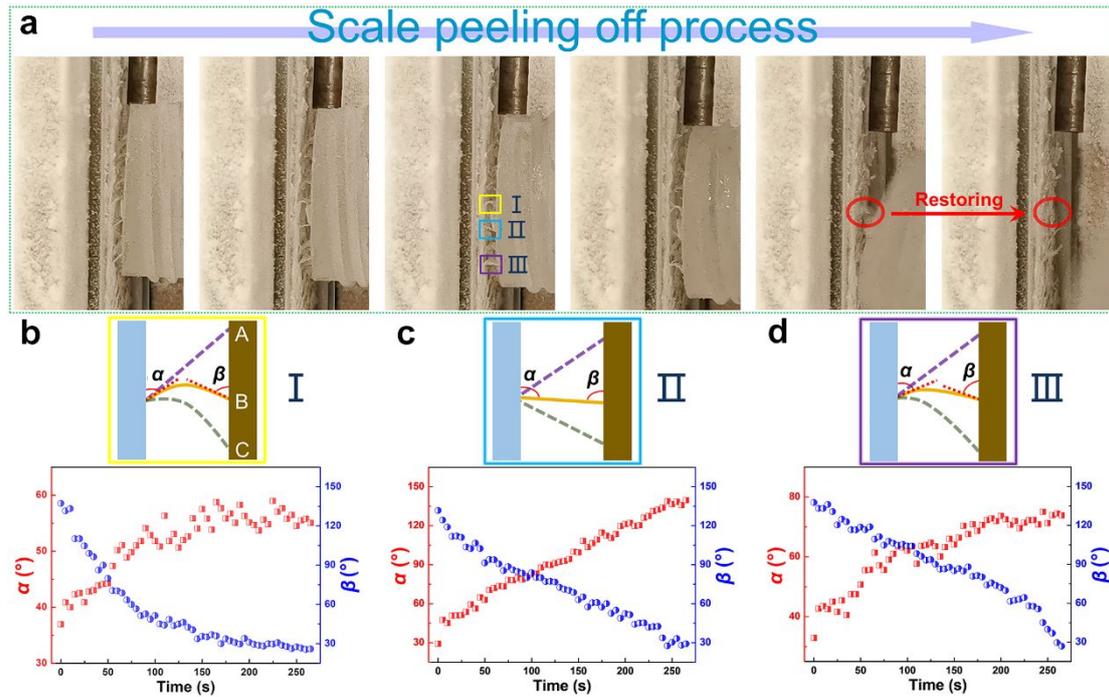


Figure 4. Fish scale peeling behaviors in de-icing. (a) The photographs depict the fish scales peeling off process as captured by a camera. The angles of the fish scale to the skin and ice change during the de-icing process. Figures (b), (c), and (d) show the angle evolutions of three typical scales (I, II, and III) over de-icing time.

Conclusions

This work investigates anisotropic ice adhesion behaviors by examining the ice adhesion strength on Arctic salmon skin. Shearing against the fish scale's growth direction yields a 60% reduction in ice adhesion strength (141 ± 47 kPa) compared to shearing along the growth orientation (353 ± 95 kPa). This diminished adhesion is attributed to the dynamic response of fish scales when sheared against their growth orientation. The de-icing process follows a sequential rupture mode, with fish scales opening first and then gradually peeling off. The scale opening and peeling capacity are identified as critical parameters controlling ice detachment. Enhancing these parameters can lead to further reductions in ice adhesion strength (66 ± 15 kPa). Despite

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4 276 bending during de-icing, fish scales regain their initial shape post-ice removal.
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6 277 Additionally, the high Young's modulus and mechanical/chemical robustness of fish
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9 278 scales contribute to their effectiveness as durable anti-icing surfaces. Thus, the
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12 279 mechanism by which fish scales mitigate ice adhesion presents opportunities for
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14 280 designing effective icephobic surfaces. Developing structures inspired by fish scales
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17 281 and dynamic response surfaces holds promise for future anti-icing research.

282 **Materials and methods**

283 **Materials**

284 For the tests, a piece of fish skin from an Arctic Salmon purchased from Ravnkloa
285 Fish & Shellfish AS in Trondheim, Norway, was used. The fish skin is cut into small
286 pieces measuring 50 mm × 50 mm and adhered to a glass substrate (60 mm × 60 mm)
287 for ice adhesion testing. Prior to adhesion, the underside of the skin is dried with wipers
288 several times. The fish skin is then firmly attached to the glass using Lynlim (Scotch,
289 3M Norge AS). Different parts of the fish skin produce scales of varying sizes. For
290 instance, the skin near the fishtail has smaller scales than the skin near the fishhead.
291 The fabricated samples were stored in a freezer at -18°C for subsequent ice adhesion
292 tests.

293 **Characterizations**

294 The morphology of fish scales was characterized using a combination of a camera, DIC
295 microscope (Zeiss AxioScope A1 for reflected light, BF-DIC/POL, Carl Zeiss), and a
296 field-emission scanning electron microscope (FEI APREO SEM). Direct observation
297 of the scales was conducted without any additional treatment using the camera and
298 optical microscope. Prior to SEM analysis, the scales underwent drying in an oven at

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4 299 60°C for 24 hours, followed by coating with 10 nm platinum/palladium layers using a
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7 300 sputter coater (208 HR B, Cressington). Ice adhesion strength was assessed utilizing a
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9 301 universal mechanical tester (Instron Model 5944) equipped with a custom cooling
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11 302 system and chamber, as detailed in previous studies. A polypropylene centrifuge tube,
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14 303 with a wall thickness of 1 mm and an inner diameter of 28 mm, was placed on the fish
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17 304 scales. Subsequently, 6 mL of deionized water was added to the mold, and the samples
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19 305 were stored in a freezer at -18°C for 3 hours to ensure complete ice formation. To
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22 306 prevent water leakage onto the fish scales, a weight of 200 g was applied to ensure tight
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25 307 contact between the mold and scales, sealing the contacted area with babassu oil. Before
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27 308 testing, the samples were transferred from the freezer to the cooling chamber of the
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30 309 testing machine and stabilized at -18°C for 15 minutes. During the adhesion test, a force
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32 310 probe propelled the adhered samples at a velocity of 0.01 mm⁻¹, with the probe
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35 311 positioned within close proximity to the tested coating surface (less than 1 mm) to
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38 312 minimize torque on the ice cylinder. Five samples were prepared for each adhesion test
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41 313 type to determine the average adhesion strength. Although salmon is commonly
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43 314 available, tests were conducted using a single large salmon to maintain consistency.
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46 315 Five repeated tests were performed on intact surface samples for each adhesion
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48 316 measurement type to mitigate sampling differences and uncertainties. Supplementary
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50
51 317 Movie S1 depicts the de-icing process against the growth direction of fish scales,
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53 318 showcasing their dynamic surface properties and effectiveness in ice removal.

319 **Competing Interests**

320 The authors declare no conflicts of interest.

321 **Data availability Statement**

322 The data supporting the findings of this investigation are accessible from the
323 corresponding author upon reasonable request.

324 **Acknowledgments**

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327 project Towards Design of Super-Low Ice Adhesion Surfaces (SLICE, 250990), and
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