

Article

Enhancing Photovoltaic Efficiency with the Optimized Steepest Gradient Method and Serial Multi-Cellular Converters

Arezki Fekik ^{1,2}, Ahmad Taher Azar ^{3,4,5,*}, Ibrahim A. Hameed ^{6,*}, Mohamed Lamine Hamida ², Karima Amara ², Hakim Denoun ² and Nashwa Ahmad Kamal ⁷

- ¹ Department of Electrical Engineering, University Akli Mohand Oulhadj-Bouria, Rue Drissi Yahia Bouira, Bouïra 10000, Algeria; arezkitdk@yahoo.fr or a.fekik@univ-bouira.dz
- ² Electrical Engineering Advanced Technology Laboratory (LATAGE), Tizi Ouzou 15000, Algeria; ml_hamida@yahoo.com (M.L.H.); amarakarima140@yahoo.fr (K.A.); akim_danoun2002dz@yahoo.fr (H.D.)
- ³ Automated Systems & Soft Computing Lab (ASSCL), Prince Sultan University, Riyadh 11586, Saudi Arabia
- ⁴ College of Computer & Information Sciences, Prince Sultan University, Riyadh 11586, Saudi Arabia
- ⁵ Faculty of Computers and Artificial Intelligence, Benha University, Benha 13518, Egypt
- ⁶ Department of ICT and Natural Sciences, Norwegian University of Science and Technology, Larsgårdsvengen, 2, 6009 Ålesund, Norway
- ⁷ Faculty of Engineering, Cairo University, Giza 12613, Egypt; nashwa.ahmad.kamal@gmail.com
- * Correspondence: aazar@psu.edu.sa or ahmad.azar@fci.bu.edu.eg or ahmad_t_azar@ieee.org (A.T.A.); ibib@ntnu.no (I.A.H.)

Abstract: Many methods have been developed to aid in achieving the maximum power point (MPP) generated by PV fields in order to improve photovoltaic (PV) production. The optimized steepest gradient technique (OSGM), which is used to extract the maximum power produced by a PV field coupled to a multicell series converter, is one such promising methodology. The OSGM uses the power function's first and second derivatives to find the optimal voltage (V_{pv}) and converge to the voltage (V_{ref}) that secures the MPP. The mathematical model was developed in Matlab/Simulink, and the MPPT algorithm's performance was evaluated in terms of reaction time, oscillations, overshoots, and stability. The OSGM has a faster response time, fewer oscillations around the MPP, and minimal energy loss. Furthermore, the numerical calculation of the gradient and Hessian of the power function enables accurate modeling, improving the system's precision. These findings imply that the OSGM strategy may be a more efficient way of obtaining MPP for PV fields. Future research can look into the suitability of this method for different types of PV systems, as well as ways to improve the algorithm's performance for specific applications.

Keywords: photovoltaic (PV); maximum power point (MPP); optimized steepest gradient method (OSGM); multicellular converter; response time



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1. Introduction

Over three-quarters of the world's energy consumption is derived from fossil fuels. However, these energy sources—gas, oil, and coal, which will run out in the coming decades—are now known to cause air pollution and an increase in the greenhouse effect, resulting in global warming. Organizations are pushing for the development of greener energy sources in response to rising global demand. Alternative energy sources for power include solar, wind, and hydroelectric sources. Furthermore, distribution networks cannot serve the entire global population; whether in the mountains or on an island, in the least populated areas or in the middle of the desert, difficult-to-access or very isolated sites cannot always be connected to the grid due to technical constraints or a lack of economic viability. Renewable energy sources, which may be scaled for residential use, are ideal for providing power in remote or micro-grid locations. They are frequently paired with batteries, which store excess energy output or compensate for transient power shortages during peak consumption periods. The worldwide need for energy is continuously expanding,

and as traditional energy sources, such as gas, oil, and coal, deplete, the need for cleaner and renewable energy sources will grow [1–3]. Solar energy is one of the most effective and least polluting renewable energy sources available. PV systems, which convert solar energy into electrical energy, are extensively employed in a variety of applications, ranging from modest household systems to large-scale power plants [4–8]. However, the non-linearity of the photovoltaic generator results in a low energy conversion rate, which is a major disadvantage of the PV system. To address this issue, researchers are working on maximum power point tracking (MPPT) algorithms that aid in maintaining maximum power output despite fluctuations in sunshine and temperature. MPPT algorithms are critical for increasing the amount of energy generated by solar systems [9–15]. MPPT algorithms are classified into two types: dependent and independent. Dependent algorithms make use of parameter databases to maximize the power of the photovoltaic system [16]. These methods make use of intelligent controllers, such as artificial neural networks (ANNs) [17], adaptive neuro-fuzzy inference systems (ANFISs) [18,19], and fuzzy logic controllers (FLCs). FLC is the easiest to construct among these controllers, but it has several drawbacks, such as rule definition, algorithm complexity, and reaction time to reach the maximum power point [20–23]. On the other hand, independent MPPT algorithms do not require knowledge of the PV system model and can be implemented without any prior knowledge of the system. These algorithms are based on mathematical models and are often classified as perturb and observe (P&O), incremental conductance (INC), or hill climbing (HC) methods. These algorithms use the voltage and current measurements to estimate the PV system's maximum power point.

Recent energy research intends to build better MPPT algorithms to improve the performance of solar systems [24–26]. These algorithms provide faster reaction, fewer oscillations around the maximum power point, and reduced energy loss. The development of these algorithms is critical in order to fulfill the rising demand for energy while lowering prices and creating a sustainable environment. MPPT (maximum power point tracking) is a technique for optimizing the power output of a photovoltaic (PV) system under different conditions by continually adjusting the operating point of the PV panels to the maximum power point (MPP). This allows the system to harvest the greatest amount of electricity from the solar panels, enhancing the system's total efficiency. MPPT algorithms are divided into two types: open-loop and closed-loop approaches. Open-loop approaches, such as the perturb and observe (P&O) method, are based on the observation of the solar panel's output current and voltage and alter the operating point correspondingly. Closed-loop approaches, such as the incremental conductance (IC) method, employ a feedback loop to change the operating point continuously until the maximum power point is attained [23,27,28]. The study in [29] compares several MPPT approaches, such as perturb and observe, incremental conductance, and fractional open circuit voltage. The authors rate each technique's performance based on parameters such as convergence time, steady-state oscillation, and tracking efficiency. Ref. [30] presents a thorough examination of two common MPPT strategies, perturb and observe and incremental conductance, covering their fundamental concepts, benefits, and drawbacks. The authors also address current advancements and changes to these strategies. The authors in [31] provide a detailed discussion of several MPPT strategies, including old methods, such as perturb and observe, incremental conductance, and hill climbing, as well as modern techniques like artificial neural networks and fuzzy logic. Each approach is evaluated by the authors based on variables such as convergence speed, steady-state oscillation, and efficacy in dealing with partial shading. The work in [32] reviews many MPPT strategies for PV systems, such as perturb and observe, incremental conductance, and other advanced techniques, such as model reference adaptive control and sliding mode control. Each approach is evaluated by the authors based on variables such as convergence speed, steady-state oscillation, and efficacy in dealing with partial shading. In [33], the authors offered an MPPT technique based on an artificial neural network (ANN) for solar applications. The suggested technique estimates the ideal duty cycle that maximizes PV output power using

a neural network model. A dataset of PV power and voltage values recorded under various climatic circumstances is used to train the ANN model.

The study [34] describes an MPPT control technique for solar systems based on an adaptive neuro-fuzzy inference system (ANFIS). The ANFIS model is trained to predict the ideal voltage for maximizing PV output power. To increase the performance of the ANFIS controller, the suggested technique additionally employs an updated antlion optimizer (ALO) algorithm. In the study [35], an enhanced maximum power point tracking (EMPTT) method for solar systems is proposed. To estimate the best voltage that maximizes PV output power, the suggested technique employs an artificial bee colony (ABC) optimization algorithm. To increase the performance of the EMPTT controller, the ABC algorithm is integrated with a neural network. The hybrid fuzzy logic and artificial neural network based maximum power point tracking for photovoltaic systems is proposed in [36] to predict the ideal duty cycle that maximizes the PV output power. To increase the performance of the MPPT controller, the fuzzy logic controller is paired with an ANN. The study [37] offers a novel MPPT approach for solar power systems based on the cuckoo search algorithm (CSA) and ANFIS in the study. The suggested technique estimates the best voltage that maximizes the PV output power using the CSA algorithm. To increase the performance of the MPPT controller, the CSA algorithm is integrated with an ANFIS model.

This paper describes how to use the optimized steepest gradient technique (OSGM) in conjunction with a multicellular series converter to maximize the power output of a photovoltaic (PV) field. The OSGM is an independent approach for tracking the maximum power point (MPP) that allows for precise and efficient PV system operation. Unlike other MPPT methods that utilize a constant or variable step to update the voltage or duty cycle, the OSGM uses an optimized step value based on the power function's second-order approximation with regard to the voltage V_{pv} to update the voltage value to achieve the reference voltage (V_{ref}). The suggested OSGM technique is evaluated using MATLAB/SIMULINK simulation under varied solar radiation conditions. The findings reveal that the OSGM algorithm is more effective and precise than other approaches for obtaining MPP. The reaction time is faster, and there are fewer oscillations around the MPP, which result in less energy waste. Furthermore, the numerical calculation of the gradient and Hessian of the power function allows for accurate modeling, which improves system precision.

The MPPT approach is critical for sustaining maximum power production regardless of changes in sunshine and temperature. The OSGM approach provides a viable alternative for improving the energy quality delivered by solar fields. This strategy is especially appropriate for isolated or micro-grid places when distribution networks are unable to offer energy to the full world population, owing to technical constraints or a lack of economic feasibility.

The following is the paper's structure: Section 1 discusses the related work. Section 2 shows the proposed system's presentation and modeling. Section 3 discusses the proposed MPPT algorithm (OSGM), and Section 4 offers the research work's conclusion.

2. Presentation and Modeling of the Proposed System

As shown in Figure 1, the proposed system comprises a SHELL SP75 PV generator coupled to a DC load via a multicellular series converter made up of three cells. This converter increases the quality of energy sent to the load, whereas a boost converter extracts the highest power. A multicellular inverter is required between the boost converter and the load for AC loads, resulting in a two-stage power conversion process. If the energy generated by the solar system exceeds the demand of the load, the extra energy is sent back into the electrical network and consumed by grid users.

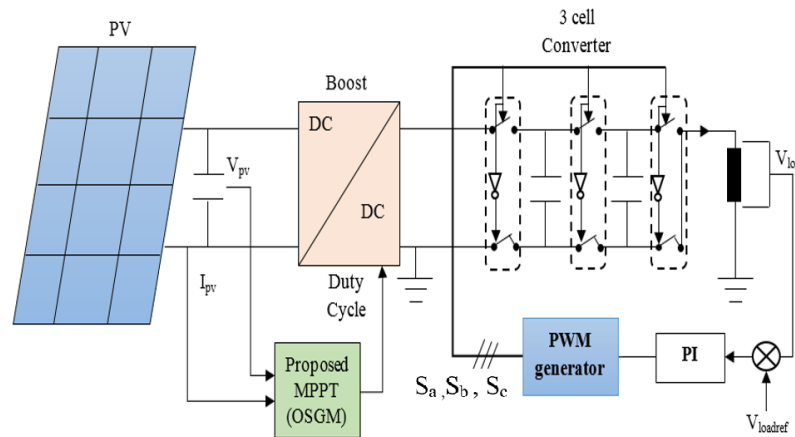


Figure 1. The proposed structure.

2.1. Mathematical Model of the Photovoltaic System

The single-diode photovoltaic cell model was used for this study because it is a widely used and simple model that accurately reflects the behavior of a solar cell under varied operational conditions. The following equations reflect the conventional I-V characteristic of a solar array:

$$V = V_{oc} + I_{sc} * R_s - I * R_{sh} \tag{1}$$

$$I = I_{ph} - I_0 * (e^{(V+I*R_{sh})/(n*V_t)}) \tag{2}$$

The widely used and basic single-diode model of the solar cell was used for this study because it properly captures the cell’s behavior under varied operating situations. The conventional I-V characteristic equation of a solar array includes the following variables: V for the terminal voltage of the cell, I for the current through the cell, V_{oc} for the open circuit voltage, I_{sc} for the short circuit current, R_s for the series resistance, R_{sh} for the shunt resistance, I_{ph} for the photocurrent, I_0 for the reverse saturation current, n for the ideality factor, and V_t for the thermal voltage. By utilizing this model, important parameters (as shown in Table 1) affecting the photovoltaic cell’s performance, such as temperature, radiation, load resistance, and internal resistance of the cell, can be represented. This model can provide predictions of the solar cell’s performance under different conditions and can optimize the system performance by adjusting various parameters.

Table 1. The main parameters of PV.

Module Parameters	Values
Power at MPP: P_{max}	$P_{max} = 75 \text{ W}$
Open circuit voltage: V_{oc}	$V_{oc} = 21.7 \text{ V}$
Short current circuit: I_{sc}	$I_{sc} = 4.8 \text{ A}$
Voltage at MPP: V_{mpp}	$V_{mpp} = 17 \text{ V}$
Current at MPP: I_{mpp}	$I_{mpp} = 4.4 \text{ A}$

2.2. Mathematical Model of Boost Converter

The boost converter shown in Figure 2 is a popular form of converter made up of two energy storage components, the inductor L and the capacitor C. The inductor stores energy in a magnetic field during switch closure, and when the switch opens, it distributes energy to the load. The capacitor contributes to smoothing the output voltage and reducing ripple. The switch state changes between on and off states in response to the control signal u . The on state is in the time interval of $t \in [0, DT]$, while the off state is in $t \in [DT, (1 - D)T]$, where D is the duty cycle. The duty cycle represents the ratio of time that the switch is closed to the entire switching period [38].

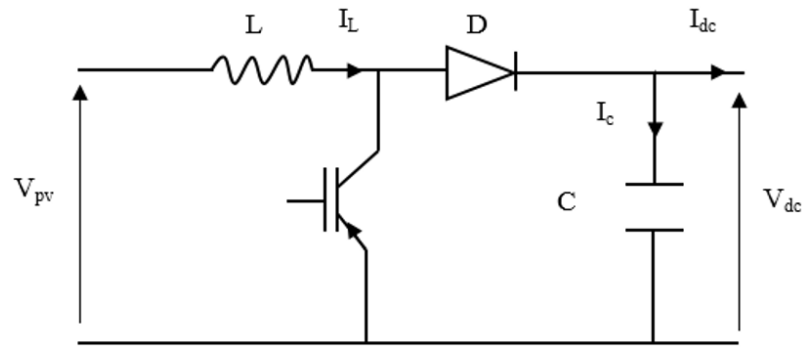


Figure 2. Boost structure.

- Switch On ($u = 1$)

$$V_{pv} = L \frac{dI_L}{dt} \tag{3}$$

$$0 = C \frac{dV_{dc}}{dt} + I_{dc} \tag{4}$$

- Switch Off ($u = 0$)

$$V_{pv} = L \frac{dI_L}{dt} + V_{dc} \tag{5}$$

$$I_L = C \frac{dV_{dc}}{dt} + I_{dc} \tag{6}$$

The two above-mentioned models of the converter, the continuous conduction mode (CCM) and the discontinuous conduction mode (DCM), can be gathered and represented in a single set of equations that describes the behavior of the converter under different operating conditions:

$$V_{pv} = L \frac{dI_L}{dt} + (1 - u) * V_{dc} \tag{7}$$

$$I_L * (1 - u) = C \frac{dV_{dc}}{dt} + I_{dc} \tag{8}$$

By substituting variable u with its average value D (duty cycle) over a period $T = 1/f$, where D is defined as the ratio of the time the switch is on (T_{ON}) to the total period (T), we can obtain the average model of the converter:

$$V_{pvm} = \frac{1}{L} \frac{dI_{Lm}}{dt} + (1 - D) * V_{dcm} \tag{9}$$

$$I_{Lm} * (1 - D) = \frac{1}{C} \frac{dV_{dcm}}{dt} + I_{dcm} \tag{10}$$

The relationship between the average input voltage (V_{pvm}) and the average output voltage (V_{dcm}) is represented by the average inductor current (I_{Lm}) and the average output current (I_{dcm}). This relationship is important in understanding the performance of the system and making adjustments to optimize it. It can also be used to predict the behavior of the system under different conditions and to design new systems with improved performance:

$$V_{dcm} = \frac{1}{1 - D} V_{pvm} \tag{11}$$

2.3. Multi-Cell Converter

The multicellular converter array is made up of a number of separate capacitor cells, each with two complementary switches [39]. Accurate voltage specifications for each cell's terminals are necessary to ensure appropriate functioning. The eight alternative modes of operation for a three-cell converter are depicted in Figure 3. It is critical to

recognize that the multicellular converter array is used in a variety of electronic systems, including inverters, voltage converters, and energy storage devices. It transforms voltage or current energy sources into usable types of energy for powering electrical equipment. The use of complementary switches for each cell increases the conversion efficiency while decreasing energy loss. Furthermore, precise voltage specifications for each cell’s terminals are required to ensure system stability and reliability.

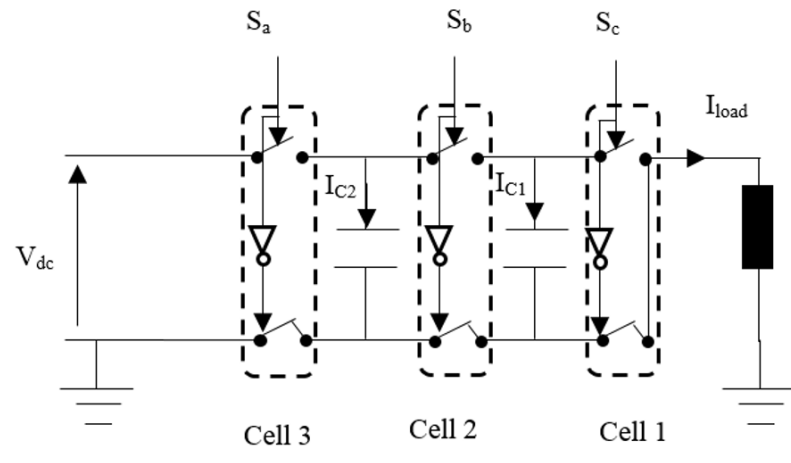


Figure 3. Three-cell converter.

The equation for the three-cell converter system is as follows:

$$I_{Ck} = (S_{k+1} - S - k) * I_{load} \tag{12}$$

$$I_{Ck} = C_k \frac{dV_{Ck}}{dt} \tag{13}$$

by combining the two previous equations, we will have:

$$dV_{Ck} = \frac{S_{k+1} - S_k}{C_k} * I_{load} \tag{14}$$

The voltage equations for the two floating capacitors in the converter are represented by the following differential equations:

$$\begin{cases} \frac{dV_{C1}}{dt} = \frac{S_2 - S_1}{C_1} * I_{load} \\ \frac{dV_{C2}}{dt} = \frac{S_3 - S_2}{C_2} * I_{load} \end{cases} \tag{15}$$

Based on the mesh theorem, the voltage V_{load} is determined by the sum of the voltages at the interrupt terminals:

$$V_{load} = \sum_{k=0}^p (V_{Ck} - V_{Ck-1}) * S_k \tag{16}$$

With $V_{C0} = 0$ V and $V_{Cp} = E$ (in this case, $V_{Cp} = V_{bus}$), V_{bus} is the output voltage of the boost converter powered by the solar field. The load current is represented by

$$\frac{dI_{load}}{dt} = \frac{V_{out}}{L} - \frac{R}{L} I_C \tag{17}$$

The variation of the load current is given by the following relationship:

$$\frac{dI_{load}}{dt} = -\frac{R}{L} I_C - \frac{S_2 - S_1}{L} V_{C1} - \frac{S_3 - S_2}{L} V_{C2} + \frac{E}{L} S_3 \tag{18}$$

The switches are controlled by pulses that are generated by the intersection between a modulating carrier signal and a triangular waveform as illustrated in Figure 4. The duty cycle is determined by the output voltage regulation algorithm of the serial multicellular converter.

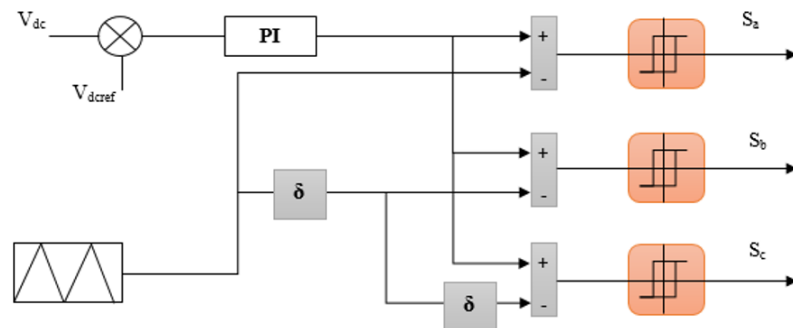


Figure 4. PWM with PI Control.

The triangular signals are defined by the following equations:

$$\left\{ \begin{array}{l} f_1(u) = \frac{\arcsin(\sin(2\pi f_p * t - \phi)) + \pi/2}{\pi} \\ f_2(u) = \frac{\arcsin(\sin(2\pi f_p * t - \phi) - \sigma) + \pi/2}{\pi} \\ \vdots \\ f_p(u) = \frac{\arcsin(\sin(2\pi f_p * t - \phi) - (p-1)\sigma) + \pi/2}{\pi} \end{array} \right. \quad (19)$$

The output signal’s harmonics would be reduced by a phase shift of $2\pi/p$.

3. MPPT-Optimized Steepest Gradient Method

The proposed MPPT method involves utilizing the first- and second-order Taylor approximations to optimize the cost function $F(X_k)$ in each iteration k . The first-order Taylor approximation is used to determine the gradient direction, while the second-order Taylor approximation determines the optimal step size in the gradient direction [40]. In each iteration k , the cost function is assessed, and the function’s gradient is computed. The gradient directs towards the steepest descent, and it is used to update the parameter vector X_k . The updated parameter vector X_k is then utilized to assess the cost function $F(X_k)$ in the next iteration. This process is repeated until the cost function reaches its minimum or maximum value, depending on the case.

In summary, the suggested MPPT method is an effective and efficient methodology for optimizing the power output of a solar panel by shifting the operating point to the maximum power point. The approach includes modifying the operating point iteratively using first- and second-order Taylor approximations until the maximum power point is reached.

The first-order approximation of the function $F(X_k)$ in the proximity of X_k is

$$F(X_k) + \Delta F(X_k) = F(X_k + \sigma_k) \quad (20)$$

$$F(X_{k+1}) = F(X_k) + g^T(X_k)\sigma_k = F(X_k) + \sigma_k F(X_k) \quad (21)$$

with

$$g_k = g(X_k) = \nabla F(X_k) \quad (22)$$

$$X_k \in R^{nx1}, g(X_k) \in R^{nx1}, \sigma_k \in R^{nx1} \quad (23)$$

Then, the variation of the cost function ($\Delta F(X_k)$) is defined as the sum of the products of the gradients of the variables of the cost function by the corresponding normal vectors (g_i) and the unit variation vectors (σ_i) that define the search direction. The final formula given by Equation (24) is then obtained by calculating the dot product between the gradient vector of the cost function (g_k) and the corresponding unit variation vector (σ_k) multiplied by the cosine of the angle between these two vectors (θ_k):

$$\Delta F(X_k) = \sum_{i=0}^n g_i \sigma_i = \|g_k\| \|\sigma_k\| \cos \theta_k \tag{24}$$

To maximize $F(X_k)$, the greatest increase in $F(X_k)$ is achieved when

$$\theta_k = 0 \longrightarrow \sigma_k = g_k \tag{25}$$

where σ_k is the steepest descent direction.

In numerical computation, the solution does not always converge to X^* (the optimal value of X_k). A tuning parameter α (a positive value) is required to ensure that the algorithm converges to the X^* solution. When maximizing $F(X_k)$, this is the case:

$$X_{k+1} = X_k + \alpha g_k, \alpha > 0 \tag{26}$$

Choosing the optimal α can be determined by using the second-order approximation of $F(X_{k+1})$:

$$F(X_{k+1}) \approx F(X_k) + \alpha g_k^T g_k + \frac{1}{2} \alpha^2 g_k^T H_k g_k \tag{27}$$

where

$$H_k = \nabla^2 F(X_k) \tag{28}$$

If the Hessian of $F(X_k)$ is available, the α^* that minimizes $F(X_k)$ can be calculated analytically by using the second-order approximation of $F(X_{k+1})$. By evaluating the Hessian at the current iterate, it can be used to approximate the local behavior of the function in the vicinity of X_k . This approximation can be used to determine the step size α that will minimize $F(X_{k+1})$ and, therefore, converge to the optimal solution X^* :

$$\frac{dF(X_k + \alpha g_k)}{d\alpha} = g_k^T g_k + \alpha g_k^T H_k g_k \tag{29}$$

$$\frac{dF(X_k + \alpha g_k)}{d\alpha} = 0 \longrightarrow \alpha^x = -\frac{g_k^T g_k}{g_k^T H_k g_k} \tag{30}$$

Then,

$$X_{k+1} = X_k - \frac{g_k^T g_k}{g_k^T H_k X_k g_k} g_k \tag{31}$$

In this particular case, the parameter X_k , represented as V_{pvk} (voltage), is a scalar value (a single parameter). The power function, represented as $P_{pvk} = F(V_{refk})$, is a concave function that has a maximum value at the maximum power point (MPP). The first and second derivatives of this power function, represented as g_k and H_k , respectively, can be calculated using the expression of P_{pvk} in terms of current and voltage values. These derivatives are essential in determining the optimal value of V_{pvk} through the use of numerical optimization techniques, such as the Newton–Raphson method.

To better understand the proposed method, here are the steps of the complete mathematical modeling for the MPPT-optimized steepest gradient method control technique:

1. Solar panel model:

The solar panel model can be represented by the following equivalent circuit equation:

$$I_{pvk} = I_{ph} - I_0 * (e^{(V_{pvk} + I_{pvk} * R) / (\alpha * V_t)} - 1) \tag{32}$$

where I_{pvk} is the output current of the solar panel at point k ; I_{ph} is the current photo-generated by the solar panel; I_0 is the reverse saturation current of the diode; V_{pvk} is the solar panel output voltage at point k ; R is the load resistor connected to the solar panel; a is the voltage temperature coefficient; and V_t is the thermal voltage.

The output power of the solar panel can be calculated as follows:

$$P_{pvk} = V_{pvk} * I_{pvk} \tag{33}$$

2. Calculation of the power function: The power function can be represented by the following expression:

$$P_{pvk} = F(V_{refk}) = V_{refk} I_{ph} - \frac{I_0 \alpha V_t^2}{R} e^{\left(\frac{V_{refk}}{\alpha V_t} - 1\right)} \tag{34}$$

where V_{refk} is the solar panel reference voltage at point k .

3. Calculation of the first and second derivatives of the power function: The first derivative of the power function with respect to the reference voltage can be calculated as follows:

$$g_k = \frac{dF(V_{refk})}{d(V_{refk})} = I_{ph} - \frac{2I_0 \alpha V_t}{R} e^{\left(\frac{V_{refk}}{\alpha V_t} - 1\right)} e^{\frac{V_{refk}}{\alpha V_t}} \tag{35}$$

The second derivative of the power function with respect to the reference voltage can be calculated as follows:

$$H_k = \frac{d^2F(V_{refk})}{d(V_{refk}^2)} = -\frac{2I_0 \alpha V_t}{R} \left[\frac{e^{\frac{V_{refk}}{\alpha V_t}}}{\alpha V_t} + e^{\left(\frac{V_{refk}}{\alpha V_t} - 1\right)} e^{\frac{V_{refk}}{\alpha V_t}} \right] \tag{36}$$

The algorithm of the MPPT-optimized steepest gradient method technique can be described as follows:

- Initialize the reference voltage V_{refk} to a known value;
- Calculate the quantities of the algorithm.

4. Results and Discussion

The simulation procedure entails modeling the system with MATLAB software tools and performing simulations to evaluate the performance of the suggested control mechanism and structure. The MPPT OSGM, an optimization technique used to maximize the power output of a photovoltaic (PV) system, is the focus of the first half of the simulation. Three tests are carried out to validate the efficiency and effectiveness of the proposed control technique and structure.

The global system parameters are summarized in Table 2 as follows.

Table 2. System parameters.

Parameters	Values (Unit)
Boost Capacitor	2200 μ F
Floating Capacitor (multicell converter)	33 μ F
Inductance (Multicell converter)	15 mH
Inductance boost	100 mH
DC Voltage reference (Multicell converter)	145 V
Commutation frequency	1.5 KHz
PI Gains (Multi cell voltage regulation)	$K_p = 40$; & $K_i = 0.001$

4.1. Test 1

One of the tests conducted is Test 1, where the system is subjected to constant lighting conditions of $G = 1000 \text{ W/m}^2$.

Apart from the previously mentioned results, it is worth noting that the OSGM technique also achieved a higher efficiency rate when compared to the *P&O* method. The higher output power and fewer oscillations produced with the OSGM technique demonstrate this. Furthermore, the OSGM method is well known for its robustness and adaptability to changing environmental conditions, which is an important factor to consider when choosing an MPPT algorithm for a solar power system. Overall, the simulation results presented in Figure 5 provide clear evidence of the advantages of utilizing the OSGM method over the *P&O* method in terms of performance and efficiency.

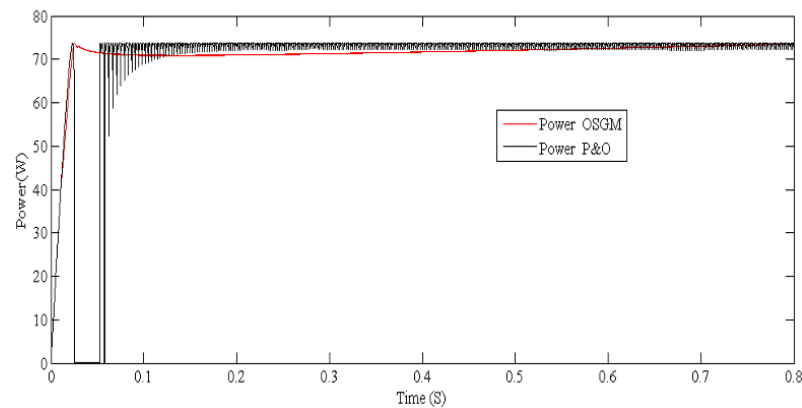


Figure 5. PV output power.

The OSGM approach not only improves response time and signal quality, but it also improves the system's overall efficiency and stability. It tracks the maximum power point precisely and quickly, resulting in increased power production from the solar system. Reduced chattering ensures system stability and reduces the risk of system failure. Furthermore, the OSGM method is a more robust choice for MPPT control in solar systems due to its adaptability to changing environmental conditions and a wider range of operating conditions. The results presented in Figure 6 confirm the superiority of the OSGM method over the traditional *P&O* control method.

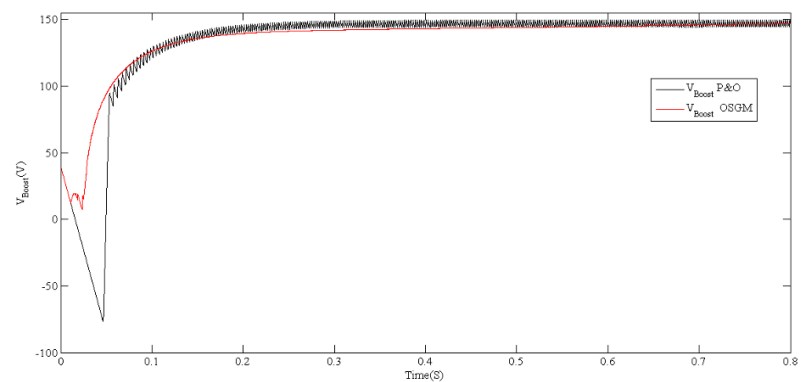


Figure 6. Output boost voltage.

The OSGM control approach, in addition to its capacity to eliminate disturbances, provides a more steady and constant charging current, which is critical for assuring the appropriate working and lifetime of the battery or load being charged. This is owing to its capacity to identify the maximum power point precisely and promptly, resulting in a higher power output from the solar system and effective charging of the load. Furthermore, the OSGM method is a more robust choice for MPPT control in solar systems due to its adaptability to changing environmental conditions and ability to handle a wider range of operating conditions. Overall, the results presented in Figure 7 further highlight the benefits of using the OSGM method over the traditional *P&O* technique for charging applications.

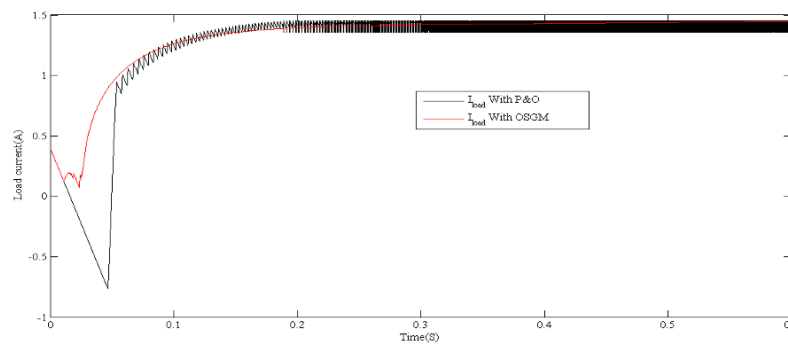


Figure 7. Current load.

It is important to note that the OSGM-MPPT method also exhibits better steady-state performance as evidenced by the smaller V_{c1} and V_{c2} voltage oscillations when compared to the $P&O$ method. This is a significant advantage, as it reduces the risk of converter failures and increases the overall lifespan of the system. Overall, the findings in Figure 8 underscore the superiority of the OSGM-MPPT method over the $P&O$ method in terms of performance and efficiency in solar systems.

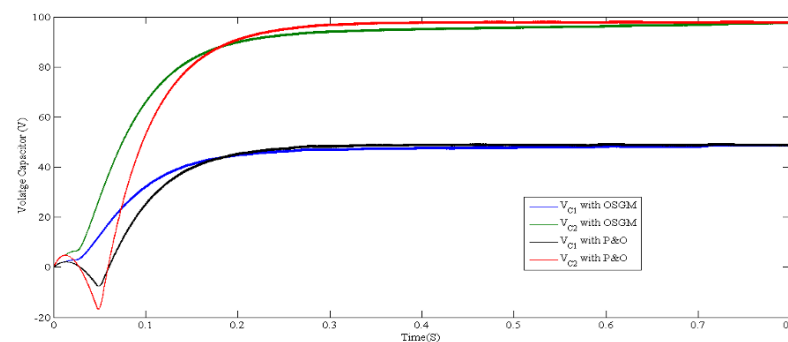


Figure 8. Floating voltage.

4.2. Test 2

The second test evaluates the OSGM method's adaptability and effectiveness in MPPT control for solar systems by changing the lighting conditions from 600 W/m^2 to 1000 W/m^2 .

The simulation results in Figure 9 illustrate the superiority of the OSGM algorithm over the conventional $P&O$ MPPT control method in terms of power value and stability during a test where the irradiance is varied from 600 W/m^2 to $G = 1000 \text{ W/m}^2$. The output power tracked by the OSGM algorithm reaches the highest value with minimal oscillations, highlighting its capability to optimize power output in a photovoltaic system. These results are consistent with the anticipated outcomes and demonstrate the effectiveness of the proposed OSGM algorithm.

The results of the simulation in Figure 10 are clear in their demonstration of the superiority of the OSGM method over the $P&O$ method when there is a change in the irradiance from 600 W/m^2 to $G = 1000 \text{ W/m}^2$. The figure highlights the better energy quality and stability of the output voltage produced by the proposed boost method as compared to that of the $P&O$ control.

The OSGM control method also provides a more stable charging current during a change in irradiance from 600 W/m^2 to $G = 1000 \text{ W/m}^2$ as shown in Figure 11. This is important for ensuring the proper functioning and longevity of the battery or load being charged.

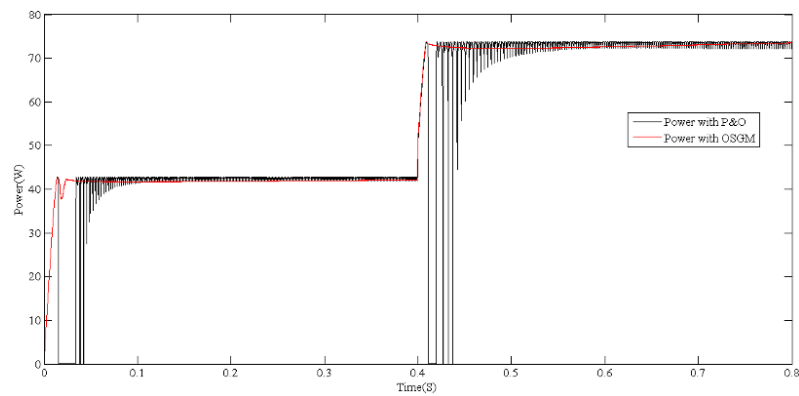


Figure 9. PV power output.

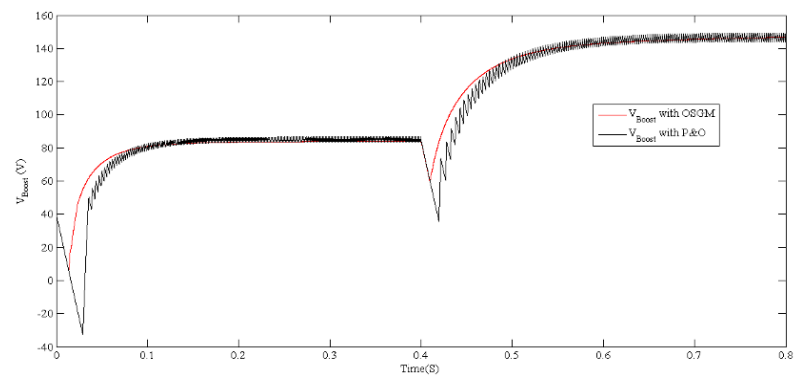


Figure 10. Output boost voltage.

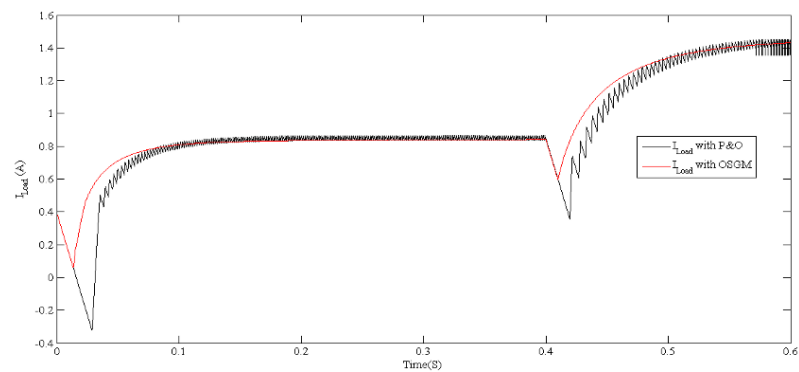


Figure 11. Current load.

Figure 12 illustrates that the OSGM-MPPT method has superior performance compared to the P&O method, with smaller V_{c1} and V_{c2} voltage oscillations, even under changing irradiance conditions.

4.3. Test 3

Two tests for variable climatic conditions were added to assess the robustness of the proposed structure. The variations were made on the TFT site in Illizi in Algeria as part of the national research project “Design of a Cathodic Protection System with Photovoltaic Panels”. In the first case, the temperature is set at a value of 298 K, while the illumination is varied according to Figure 13.

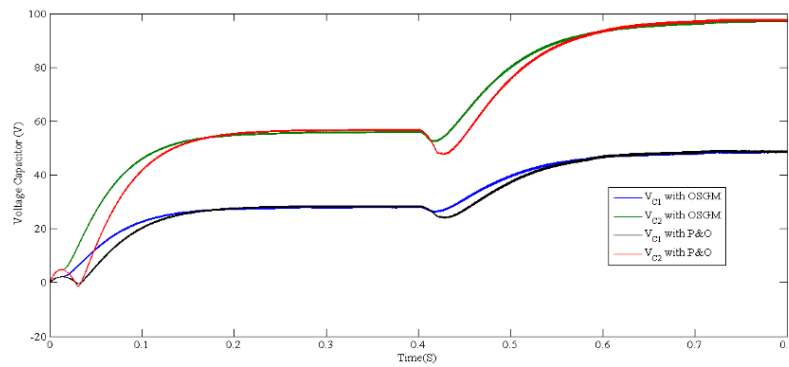


Figure 12. Floating voltage.

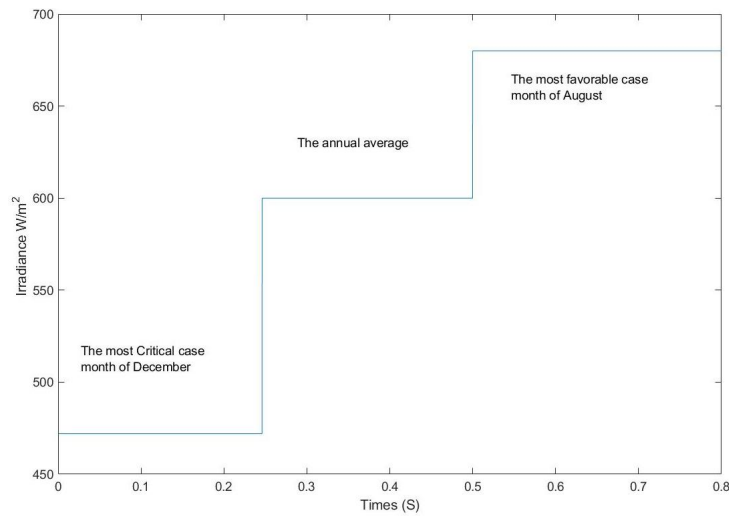


Figure 13. Illumination variation.

Three cases of illumination variation are shown in Figure 13, including the most critical case “month of December”, the annual average of illumination in the TFT zone in Illizi, Algeria, and the last most favorable case.

The power and stability during the test where the site’s actual irradiance was used are illustrated by the simulation results in Figure 14. The proposed structure achieved the highest output power with minimal oscillations, demonstrating its ability to optimize the output power in a photovoltaic system and reduce loss due to switching effects.

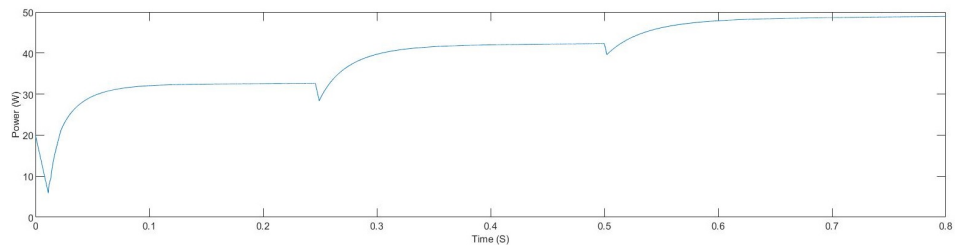


Figure 14. Power with illumination variation.

The results of the simulation of Figure 15 are clear in their demonstration during a change of illumination in the real case. The figure highlights the better power quality and the stability of the output voltage produced by the proposed boosting method.

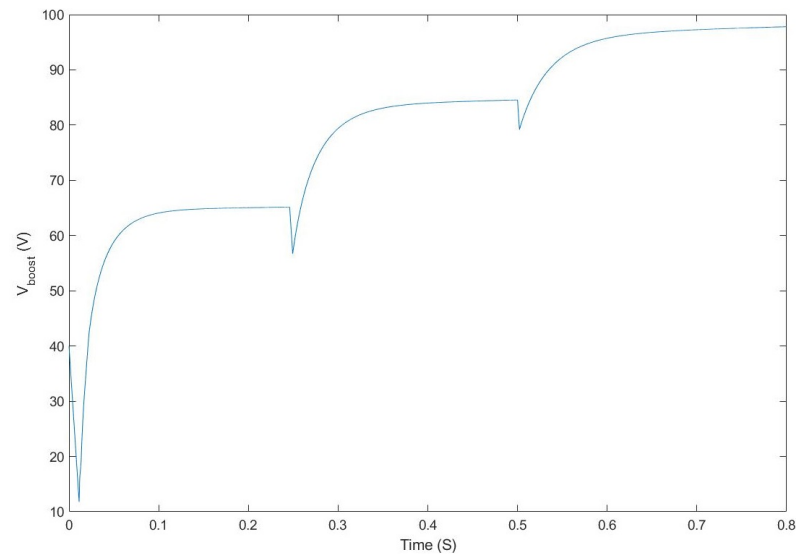


Figure 15. Output voltage with illumination variation.

Better transient performance of the structure is demonstrated by the smaller V_{c1} and V_{c2} voltage oscillations, even during changes in illuminance as shown in Figure 16. This is a notable advantage, as it lowers the likelihood of converter failures and extends the overall lifespan of the system.

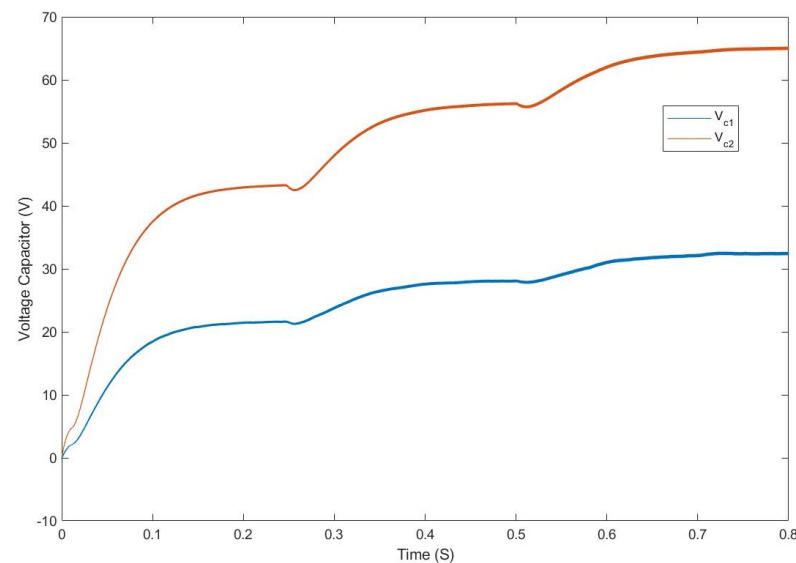


Figure 16. Voltage capacitors with illumination variation.

In the second case, the illumination is fixed at a value of 1000 W/m^2 , while the temperature is varied according to Figure 17.

Three cases of temperature variation are shown in Figure 17, including the most critical case “month of August”, the annual average of illumination in the TFT zone in Illizi, Algeria, and the last most favorable case.

Figures 18–20 show the results of the proposed system during temperature variations in the Saharan environment: the output power, the boost voltage, and the floating capacitors’ voltages, respectively.

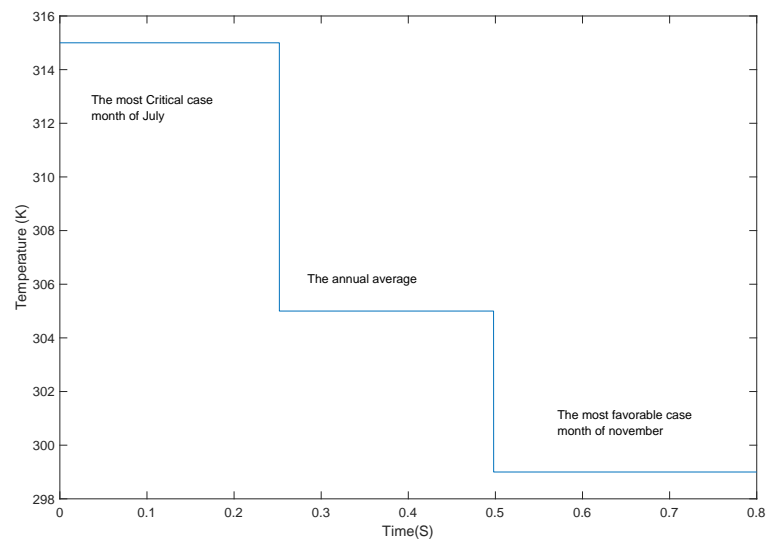


Figure 17. Temperature variation.

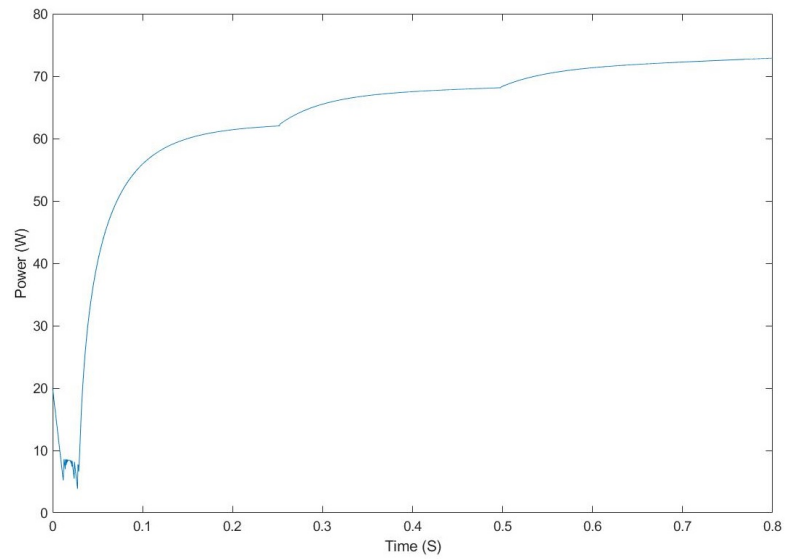


Figure 18. Power with temperature variation.

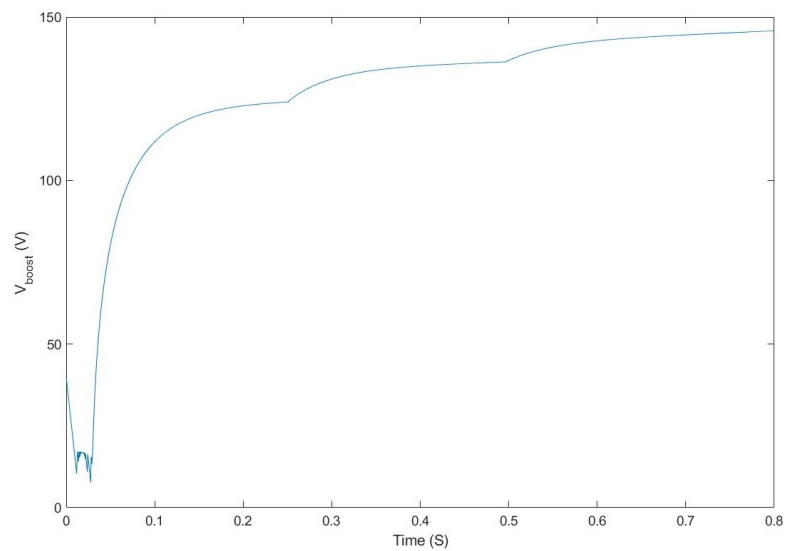


Figure 19. Output voltage with temperature variation.

The MPPT (maximum power point tracking) control is crucial for optimizing the energy production of solar panels. It regulates the voltage and current output of the panel to maximize the supplied electrical power. However, the temperature of the photovoltaic panel can influence the performance of the MPPT control.

Indeed, an increase in the panel temperature leads to a decrease in the output voltage, which can impact energy production. This is explained by the effect of temperature on the electrical characteristics of solar cells.

However, the proposed structure for the MPPT control seems to be effective, as it does not generate energy losses due to switching, even during temperature variations. Thus, the cathodic protection system applied in Saharan areas can operate at lower temperatures without any negative effects on the performance of the MPPT control.

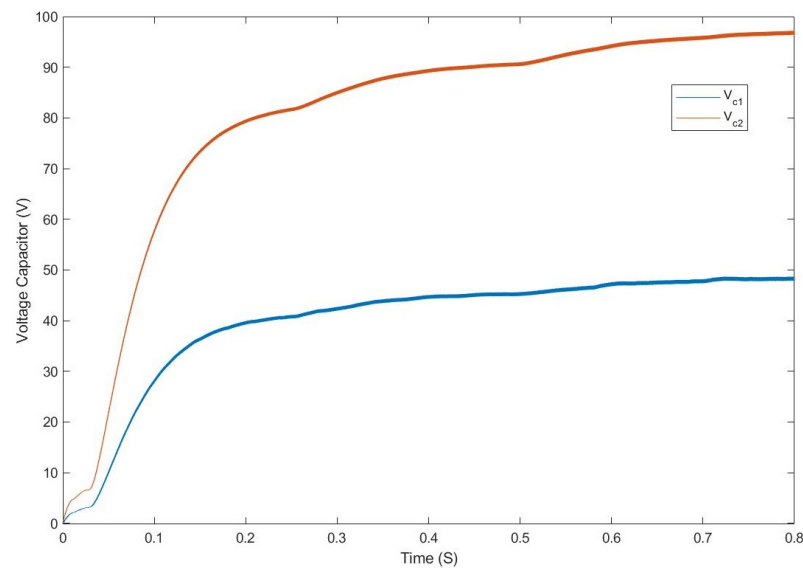


Figure 20. Floating voltage with temperature variation.

4.4. Comparative Study

The study conducted a comparative analysis of two techniques proposed by [41,42], with respect to the technique investigated in this work. The comparison criteria included P_{mpp} (watts), current (A), V_{mpp} (volts), time response (seconds), and the larger oscillations. The results of the comparison are presented in Table 3. The suggested approach outperformed the other two strategies in terms of response time and oscillations around the highest power point, according to the data. This performance enhancement enables the series multicellular converter to have a more steady voltage with less disturbance. These findings imply that the suggested approach is a superior choice for systems requiring higher levels of stability and efficiency. Further research can be conducted to investigate the technique’s applicability in other systems and to optimize its performance in specific applications.

Table 3. Comparative study.

MPPT Techniques	P_{mpp} (Watts)	Current (A)	V_{mpp} (Volts)	Time Response (Seconds)	The Larger of Oscillations	References
P&O	72.80	4.67	15.60	0.40 (Slow)	Very large	[42]
ANFIS	74.45	4.43	16.78	0.05 (Fast)	Small	[41]
Proposed Method	74.75	4.42	16.88	0.025 (very Fast)	Small	—

5. Conclusions

The results of the simulation studies clearly demonstrate the superiority of the OSGM-MPPT method over the conventional *P&O* method. The OSGM method provides higher output power, more stability, better efficiency, and improved steady-state performance compared to the *P&O* method. It is also more resilient and flexible to changing climatic circumstances, which is critical for maintaining the solar system's correct operation. These advantages make the OSGM-MPPT approach a viable option for MPPT control in solar energy systems. Future research might concentrate on increasing the performance of the OSGM-MPPT approach by the incorporation of additional algorithms and control strategies. Furthermore, implementing the OSGM-MPPT method in real-world solar systems and evaluating its performance under different environmental conditions would provide valuable insights for further improving the method. Simulation study, experimental analysis, and investigating the application of the OSGM-MPPT method in other renewable energy systems, such as wind or hydro-power systems, may open up new avenues for improving the efficiency and performance of these systems, which are considered future directions.

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