



– a Matlab Toolbox for Analysis of Random Waves and Loads

Tutorial for WAFO version 2017

by the WAFO group

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LUND UNIVERSITY

FACULTY OF ENGINEERING
CENTRE FOR MATHEMATICAL SCIENCES
MATHEMATICAL STATISTICS

Mathematical Statistics
Lund University
Box 118
SE-221 00 Lund
Sweden
<http://www.maths.lth.se/>

IN THE HOPE THAT IT IS USEFUL

Foreword

Foreword to 2017 edition

This WAFO tutorial 2017 has been successfully tested with MATLAB 2017a on WINDOWS 10.

The tutorial for WAFO 2.5 appeared 2011, with routines tested on MATLAB 2010b. Since then, many users have commented on the toolbox, suggesting clarifications and corrections to the routines and to the tutorial text. We are grateful for all suggestions, which have helped to keep the WAFO project alive.

Major updates and additions have also been made during the years, many of them caused by new MATLAB versions. The new graphics system introduced with MATLAB 2014b motivated updates to all plotting routines. Syntax changes and warnings for deprecated functions have required other updates.

Several additions have also been made. In 2016, a new module, handling non-linear Lagrange waves, was introduced. A special tutorial for the Lagrange routines is included in the module `lagrange`; [30]. Two sets of file- and string-utility routines were also added 2016.

During 2015 the WAFO-project moved from <http://code.google.com/p/wafo/> to <https://github.com/wafo-project/>, where it can now be found under the generic name WAFO – no version number needed.

In order to facilitate the use of WAFO outside the MATLAB environment, most of the WAFO routines have been checked for use with OCTAVE. On `github` one can also find a start of a PYTHON-version, called `pywafo`.

Recurring changes in the MATLAB language may continue to cause the command window flood with warnings for deprecated functions. The routines in this version of WAFO have been updated to work well with MATLAB 2017a. We will continue to update the toolbox in the future, keeping compatibility with older versions.

Foreword to 2011 edition

This is a tutorial for how to use the MATLAB toolbox WAFO for analysis and simulation of random waves and random fatigue. The toolbox consists of a number of

MATLAB m-files together with executable routines from FORTRAN or C++ source, and it requires only a standard MATLAB setup, with no additional toolboxes.

A main and unique feature of WAFO is the module of routines for computation of the exact statistical distributions of wave and cycle characteristics in a Gaussian wave or load process. The routines are described in a series of examples on wave data from sea surface measurements and other load sequences. There are also sections for fatigue analysis and for general extreme value analysis. Although the main applications at hand are from marine and reliability engineering, the routines are useful for many other applications of Gaussian and related stochastic processes.

The routines are based on algorithms for extreme value and crossing analysis, developed over many years by the authors as well as many results available in the literature. References are given to the source of the algorithms whenever it is possible. These references are given in the MATLAB-code for all the routines and they are also listed in the Bibliography section of this tutorial. If the references are not used explicitly in the tutorial; it means that it is referred to in one of the MATLAB m-files.

Besides the dedicated wave and fatigue analysis routines the toolbox contains many statistical simulation and estimation routines for general use, and it can therefore be used as a toolbox for statistical work. These routines are listed, but not explicitly explained in this tutorial.

The present toolbox represents a considerable development of two earlier toolboxes, the FAT and WAT toolboxes, for fatigue and wave analysis, respectively. These toolboxes were both Version 1; therefore WAFO has been named Version 2. The routines in the tutorial are tested on WAFO-version 2.5, which was made available in beta-version in January 2009 and in a stable version in February 2011.

The persons that take actively part in creating this tutorial are (in alphabetical order): *Per Andreas Brodtkorb*¹, *Pär Johannesson*², *Georg Lindgren*³, *Igor Rychlik*⁴.

Many other people have contributed to our understanding of the problems dealt with in this text, first of all Professor Ross Leadbetter at the University of North Carolina at Chapel Hill and Professor Krzysztof Podgórski, Mathematical Statistics, Lund University. We would also like to particularly thank Michel Olagnon and Marc Provosto, at Institut Français de Recherches pour l'Exploitation de la Mer (IFREMER), Brest, who have contributed with many enlightening and fruitful discussions.

Other persons who have put a great deal of effort into WAFO and its predecessors FAT and WAT are Mats Frendahl, Sylvie van Iseghem, Finn Lindgren, Ulla Machado, Jesper Ryén, Eva Sjö, Martin Sköld, Sofia Åberg.

This tutorial was first made available for the beta version of WAFO Version 2.5 in November 2009. In the present version some misprints have been corrected and some more examples added. All examples in the tutorial have been run with success on MATLAB up to 2010b.

¹Norwegian Defense Research Establishment, Horten, Norway.

²SP Technical Research Institute, Borås, Sweden.

³Centre for Mathematical Sciences, Lund University, Sweden.

⁴Mathematical Sciences, Chalmers, Göteborg, Sweden.

Technical information

- WAFO was released in a stable version in February 2011. The most recent stable updated and expanded version of WAFO can be downloaded from <https://github.com/wafo-project/>
Older versions can also be downloaded from the WAFO homepage [91] <http://www.maths.lth.se/matstat/wafo/>
- To get access to the WAFO toolbox, unzip the downloaded file, identify the `wafo` package and save it in a folder of your choice. Take a look at the routines `install.m`, `startup.m`, `initwafo.m` in the `WAFO` and `WAFO/docs` folders to learn how MATLAB can find WAFO.
- To let MATLAB start WAFO automatically, edit `startup.m` and save it in the starting folder for MATLAB.
- To start WAFO manually in MATLAB, add the `WAFO` folder manually to the MATLAB-path and run `initwafo`.
- In this tutorial, the word `WAFO`, when used in path specifications, means the full name of the WAFO main catalogue, for instance `C:/wafo/`
- The MATLAB code used for the examples in this tutorial can be found in the WAFO catalogue `WAFO/papers/tutorcom/`
The total time to run the examples in fast mode is less than fifteen minutes on a PC from 2017, running Windows 10 pro with Intel(R) Core(TM) i7-7700 CPU, 3.6 GHz, 32 GB RAM. All details on execution times given in this tutorial relates to that configuration.
- WAFO is built of modules of platform independent MATLAB m-files and a set of executable files from C++ and Fortran source files. These executables are platform and MATLAB-version dependent, and they have been tested with recent MATLAB and WINDOWS installations.
- If you have many MATLAB-toolboxes installed, name-conflicts may occur. Solution: arrange the MATLAB-path with `WAFO` first.
- For help on the toolbox, write `help wafo`.
- Comments and suggestions are solicited — send to `wafo@maths.lth.se`

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Nomenclature

Roman letters

A_c, A_t	Zero-crossing wave crest height and trough excursion.
a_i	Lower integration limit.
b_i	Upper integration limit.
c_0	Truncation parameter of truncated Weibull distribution.
$C[X, Y]$	Covariance between random variables X and Y .
$D(\omega, \theta),$ $D(\theta)$	Directional spreading function.
$dd_{crit} d_{crit} z_{crit}$	Critical distances used for removing outliers and spurious points.
$E[X]$	Expectation of random variable X .
$E(\omega_i, \omega_j)$	Quadratic transfer function.
f	Wave frequency [Hz].
f_p	Spectral peak frequency.
$F_X(\cdot), f_X(\cdot)$	Cumulative distribution function and probability density function of variable X .
$G(\cdot), g(\cdot)$	The transformation and its inverse.
g	Acceleration of gravity.
H, h	Dimensional and dimensionless wave height.
H_{m0}, H_s	Significant wave height, $4\sqrt{m_0}$.
H_c	Critical wave height.
H_d, H_u	Zero-downcrossing and -upcrossing wave height.
h	Water depth.
h_{\max}	Maximum interval width for Simpson method.
H_{rms}	Root mean square value for wave height defined as $H_{m0}/\sqrt{2}$.
$K_d(\cdot)$	Kernel function.
k	Wave number [rad/m] or index.
L_p	Average wave length.
L_{\max}	Maximum lag beyond which the autocovariance is set to zero.
M, M_k	Local maximum.
M_k^{tc}	Crest maximum for wave no. k .

m, m_k	Local minimum.
m_k^{RFC}	Rainflow minimum no. k .
m_k^{tc}	Trough minimum for wave no. k .
m_n	n'th spectral moment, $\int_0^\infty \omega^n S_{\eta\eta}^+(\omega) d\omega$.
N	Number of variables or waves.
N_{c1c2}	Number of times to apply regression equation.
NIT	Order in the integration of wave characteristic distributions.
n_i, n	Sample size.
$P(A)$	Probability of event A .
$O(\cdot)$	Order of magnitude.
Q_p	Peakedness factor.
$R_\eta(\tau)$	Auto covariance function of $\eta(t)$.
S_p	Average wave steepness.
S_s	Significant wave steepness.
$S_{\eta\eta}^+(f), S_{\eta\eta}^+(\omega)$	One sided spectral density of the surface elevation η .
$S(\omega, \theta)$	Directional wave spectrum.
s	Normalized crest front steepness.
s_c	Critical crest front steepness.
s_{cf}	Crest front steepness.
s_N	Return level for return period N .
s_{rms}	Root mean square value for crest front steepness, i.e., $5/4 H_{m0}/T_{m02}^2$.
T_c, T_{cf}, T_{cr}	Crest, crest front, and crest rear period.
$T_{m(-1)0}$	Energy period.
T_{m01}	Mean wave period.
T_{m02}	Mean zero-crossing wave period calculated as $2\pi\sqrt{m_0/m_2}$.
T_{m24}	Mean wave period between maxima calculated as $2\pi\sqrt{m_2/m_4}$.
T_{Md}	Wave period between maximum and downcrossing.
T_{Mm}	Wave period between maximum and minimum.
T_p	Spectral peak period.
T_z	Mean zero-crossing wave period estimated directly from time series.
T	Wave period.
U_{10}	10 min average of windspeed 10[m] above the watersurface.
U_i	Uniformly distributed number between zero and one.
V, v	Dimensional and dimensionless velocity.
$V[X]$	Variance of random variable X .
V_{cf}, V_{cr}	Crest front and crest rear velocity.
V_{rms}	Root mean square value for velocity defined as $2H_{m0}/T_{m02}$.
W_{age}	Wave age.
$W(x, t)$	Random Gassian field.
$X(t)$	Time series.
X_i, Y_i, Z_i	Random variables.
x_c, y_c, z_c	Truncation parameters.

Greek letters

α	Rayleigh scale parameter or JONSWAP normalization constant.
α	Irregularity factor; spectral width measure.
$\alpha(h), \beta(h)$	Weibull or Gamma parameters for scale and shape.
α_i	Product correlation coefficient.
Δ	Forward difference operator.
$\delta_{i 1}$	Residual process.
ϵ_2	Narrowness parameter defined as $\sqrt{m_0 m_2 / m_1^2 - 1}$.
ϵ_4	Broadness factor defined as $\sqrt{1 - m_2^2 / (m_0 m_4)}$.
ϵ	Requested error tolerance for integration.
ϵ_c	Requested error tolerance for Cholesky factorization.
$\eta(\cdot)$	Surface elevation.
Γ	Gamma function.
γ	JONSWAP peakedness factor or Weibull location parameter.
λ_i	Eigenvalues or shape parameter of Ochi-Hubble spectrum.
$\mu_X(v)$	Crossing intensity of level v for time series $X(t)$.
$\mu_X^+(v)$	Upcrossing intensity of level v for time series $X(t)$.
$\Phi(\cdot), \phi(\cdot)$	CDF and PDF of a standard normal variable.
Θ_n	Phase function.
ρ_3, ρ_4	Normalized cumulants, i.e., skewness and excess, respectively.
ρ_{ij}	Correlation between random variables X_i and X_j .
Σ	Covariance matrix.
σ_X^2	Variance of random variable X .
τ	Shift variable of time.
τ_i	Parameters defining the eigenvalues of Σ .
ω	Wave angular frequency [rad/s].
ω_p	Wave angular peak frequency [rad/s].

Abbreviations

AMISE	Asymptotic mean integrated square error.
CDF	Cumulative distribution function.
FFT	Fast Fourier Transform.
GEV	Generalized extreme value.
GPD	Generalized Pareto distribution.
HF	High frequency.
ISSC	International ship structures congress.
ITTC	International towing tank conference.
IQR	Interquartile range.
KDE	Kernel density estimate.
LS	Linear simulation.
MC	Markov chain.
MCTP	Markov chain of turning points.
ML	Maximum likelihood.
NLS	Non-linear simulation.
MISE	Mean integrated square error.
MWL	Mean water line.
PDF	Probability density function.
PSD	Power spectral density.
QTF	Quadratic transfer function.
SCIS	Sequential conditioned importance sampling.
TLP	Tension-leg platform.
TP	Turning points.
WAFO	Wave analysis for fatigue and oceanography.

CHAPTER 1

Introduction to WAFO

1.1 What is WAFO?

WAFO (Wave Analysis for Fatigue and Oceanography) is a toolbox of Matlab routines for statistical analysis and simulation of *random waves* and *random loads*. Using WAFO you can, for example, calculate theoretical distributions of wave characteristics from observed or theoretical power spectra of the sea or find the theoretical density of rainflow cycles from parameters of random loads. These are just two examples of the variety of problems you can analyze using this toolbox.

There are three major audiences to which this toolbox can have a great deal of appeal. First, *ocean engineers* will find a comprehensive set of computational tools for statistical analysis of random waves and ship's responses to them. Second, the toolbox contains a number of procedures of prime importance for *mechanical engineers* working on *random loads* or *damage and fatigue analysis*. Finally, any *researcher* who is interested in *statistical analysis of random processes* will find an extensive and up-to-date set of computational and graphical tools, including simulation from spectrum of Gaussian and non-Gaussian processes and fields.

In a random wave model, like that for Gaussian or transformed Gaussian waves, the distribution of wave characteristics such as wave period and crest-trough wave height can be calculated with high accuracy for almost any spectral type. WAFO is a third-generation package of MATLAB routines for handling statistical modelling, calculation and analysis of random waves and wave characteristics and their statistical distributions. The package also contains routines for cycle counting and computation in random load models, in particular the rainflow counting procedure often used in fatigue life prediction.

Random wave distributions are notoriously difficult to obtain in explicit form from a random wave model. However, numerical algorithms, based on the so-called regression approximation and on contemporary methods to compute very high-dimensional normal integrals, work very well and are simple to use with context

specific interface, included in WAFO. These methods to calculate wave distributions are the only known methods that give correct answers valid for general spectra. The theoretical background is reviewed in [46] and computational aspects and algorithms in [75] and [16, 63].

The algorithms are based on a specification of the random waves by means of their (uni-directional or directional) spectrum, and on the underlying assumption of linear wave theory and Gaussian distribution. For non-Gaussian waves, WAFO offers three alternatives. The first is simple though often sufficient, is to use a transformation of sea elevation data to obtain a desired (horizontal) asymmetric marginal distribution. The two others include second order wave theory, and a Lagrange horizontal transformation of the wave field, respectively.

A first complete toolbox appeared 1993, called the Fatigue Analysis Toolbox (FAT), [21]. It was followed by the Wave Analysis Toolbox (WAT¹) in 1995, written by Rychlik and Lindgren, [76], being extended with routines for probabilistic modelling problems in oceanography. In WAFO, presented 2000, [11], a considerable improvement in computational speed and accuracy was achieved. Many new routines were introduced, for example routines for spatial waves with time dynamics, thus extending the analysis to random fields. Algorithms for rainflow analysis of switching Markov chains as well as for decomposition of the rainflow matrix were included. Many of the new tools were the result of new research, e.g. [73, 64, 63, 33, 14].

WAFO version 2.5 appeared in beta-version January 2009, and in stable version February 2011, adding a great number of general statistical routines, making the toolbox useful also for statistical analysis in many other areas than marine and mechanical engineering; see `help statistics`. In 2016, routines for simulation and analysis of non-Gaussian Lagrange waves were added. The present version of the toolbox simply called WAFO with year 2017 to indicate tested MATLAB version.

From version 2.5, WAFO has a modular structure, so users can easily add their own algorithms for special purposes. The modules of the toolbox handle

- wave/load data analysis and estimation,
- spectral distributions,
- transformation to Gaussian marginals and calculation of exact distributions,
- simple parametric approximations to wave characteristic distributions,
- simulation of Gaussian and Markovian wave/load time series,
- simulation of Lagrange wave fields and second order models,
- extreme value and other statistical analysis,
- cycle counting,
- rainflow cycle analysis and calculation,
- fatigue life calculation,
- smoothing and visualization,
- general statistical analysis and computation.

¹<http://www.maths.lth.se/matstat/staff/georg/watinfo.html>

In the following section, we discuss in more detail the idea of the modular structure. That section is followed by an overview of the organization of WAFO, presenting some of the capabilities of the toolbox. Finally, we give a number of examples to demonstrate the use of some of the tools in WAFO for analysis and modelling.

1.2 Philosophy – some features of WAFO

A common problem with research involving complex scientific (numerical) computations is that when researchers try to advance and leverage their colleagues work, they often spend a considerable amount of time just reproducing it.

Often after few months since the completion of their own work, authors are not capable of reproducing it without a great deal of agony, due to various circumstances such as the loss of the original input data or/and parameter values etc. Thus many scientific articles are reproducible in principle, but not in practice.

To deal with this and to organize computational scientific research and hence to conveniently transfer our technology, we impose a simple filing discipline on the authors contributing to the WAFO-toolbox. (A positive side effect of this discipline is a reduced amount of errors which are prone to occur in computational science.)

This philosophy was inspired by the article by Matthias Schwab et al “Making scientific computations reproducible”, [79]. The idea is to develop reproducible knowledge about the results of the computational experiments (research) done and to make it available to other researchers for their inspection, modification, re-use and criticism.

As a consequence, WAFO is freely available through the Internet². Other researchers can obtain the MATLAB code that generated figures in articles and reproduce them. They can if they wish modify the calculations by editing the underlying code, input arguments and parameter values. They can use the algorithms on other data sets or they can try their own methods on the same data sets and compare the methods in a fast and easy fashion.

This is the reason of existence for the `WAFO/papers` directory, which contains sub-directories including scripts for recreating figures in published articles and technical reports. Each article has its own subdirectory. The directories contain demonstration scripts to generate individual figures and (possibly) specialized tools/functions not available in the official release of WAFO for generating these figures.

Just like the `WAFO/papers` directory, the `WAFO/wdemos` directory also contains different subdirectories with scripts producing figures. The only difference is that these do not reproduce figures from published articles but merely test and demonstrate various methodologies, highlight some features of WAFO, and release code that approximately reproduces figures in other articles. The important thing for both directories is not the printed figures, but the underlying algorithm and code. In addition, the `papers` and `wdemos` scripts constitute an excellent starting point for the novel user to learn about WAFO.

²<https://github.com/wafo-project>

The documentation directory `WAFO/docs` contains documentation available for the toolbox, mostly as PDF-files. Also each function is well documented containing a help header describing how the function works with a detailed list of input and output arguments with examples of how to use the function.

The Matlab code to each function file also contains references to related functions and reference to published articles from which the user can obtain further information if such exist.

One important element in the toolbox is the use of *structure arrays*, introduced in MATLAB, Version 5, by which several types of data can be stored as one object. This significantly simplifies the passing of input and output arguments of functions and also makes the MATLAB workspace much tidier when working with the new toolbox compared to the old ones. Three general data structures or object classes are implemented and extensively used: spectrum structure, covariance structure, and probability density function (hereafter denoted pdf) structure. Other structures are used, e.g. to set parameters for numerical computation and simulation

The most complete implementation of the WAFO toolbox is the one for Windows 10, working together with MATLAB. A reduced set can be used with Linux platform together with OCTAVE.

All the files in the package are located in subdirectories under the main directory. The following directories are related to what has been discussed above. In the next section, we describe in more details the directories (or modules) which contain routines for application.

`WAFO` is the main directory containing different directories for the WAFO software, datasets and documentation.

`WAFO/docs` contains the documentation for the toolbox.

`WAFO/papers` is a subdirectory including scripts for reproducing figures in various articles and technical reports. The scripts `tutorcom` for the examples in this tutorial are found here.

`WAFO/wdemos` contains different demonstrations that illustrate and highlight certain aspects of WAFO.

`WAFO/data` contains datasets used in the demo and paper scripts.

`WAFO/source` contains `mex` and FORTRAN source files.

`WAFO/exec/...` contains FORTRAN compiled executables for different platforms and MATLAB versions.

1.3 Organization of WAFO

In this section, we make a brief presentation of each module. We want to emphasize that all routines in WAFO work together – the division into sub-toolboxes is only to make it easier for the user to find the routines for the actual problem.

Data analysis

Routines in the category `onedim` treat data in the form of time series. As examples of routines, we find procedures for extraction of so-called turning points, from which troughs and crests may be obtained, as well as procedures for estimation of auto-covariance function and one-sided spectral density. One routine extracts wave heights and steepnesses. Numerous plotting routines are included.

Routines in the category `multidim` treat multidimensional problems in space and time. One routine estimates a directional spectrum from a series of wave field measurements, and other routines handle problems with directional spreading and wave measurements.

Spectrum

Computation of spectral moments and covariance functions, given a spectrum, is a necessary step for calculation of exact probability distributions of wave characteristics. The spectrum structure mentioned in the previous section allows this calculation to be performed for directional spectra as well as encountered spectra. We present routines for calculations of commonly used frequency spectra $S(\omega)$, e.g. JONSWAP and Torsethaugen. The spectra can be expressed in frequency as well as wave number. Libraries of spreading functions $D(\theta)$, in some cases allowed to be also frequency dependent, cf. [34], are included.

Gaussian and related processes – exact results

A unique feature of the WAFO toolbox is its capacity to deliver the exact statistical distribution of wave characteristics of linear, Gaussian waves, given a spectrum; for example

- pdf for apparent wavelength and period,
- joint pdf for wavelength (period) and amplitude,
- joint pdf of half wavelengths.

Routines for transformed Gaussian processes, cf. [73], are included. Contrary to what is often stated in the technical literature, these routines are very efficient and accurate and they can be used for engineering purposes; cf. [53, Sec. 4.4.1].

Simulation of random processes and fields

Efficient simulation of a Gaussian or transformed Gaussian process $X(t)$ and its derivative $X'(t)$, given the spectral density or the auto-correlation function, can be performed. For fast and exact simulation, some routines use a technique with circulant embedding of the covariance matrix, [20]. More traditional spectral simulation methods (FFT) are also used. Space-time simulation of non-linear wave fields can be made to generate front/back and crest/trough asymmetric 3D waves, including second order Stokes waves and Lagrange waves with directional spreading.

Simulation of discrete Markov chains, Markov chains of turning points, switching Markov chains and Hidden Markov Models, etc, is possible. Other routines generate time-varying random (Gaussian or transformed Gaussian) wave fields with directional spectrum.

Parametric wave models

In WAFO, we have implemented certain models for distributions of wave characteristics found in the literature. For example, one finds

- approximations of the density of crest period and amplitude, (T_c, A_c) , in a stationary Gaussian transformed process proposed in [18], and [49],
- a model for the cdf/pdf of breaking limited wave heights proposed in [84],
- a model for the cdf/pdf of large wave heights in [85].

These are parametric models, where the calculations need as input the spectral moments, as opposed to the algorithms in the exact Gaussian module, where the whole spectrum is required.

Discretization and cycle counting

After extraction of the so-called sequence of turning points (the sequence of local maxima and minima) from data, cycle counts can be obtained, e.g. max-to-min cycles, trough-to-crest cycles, rainflow cycles. For descriptive statistics, the counting distribution and the rainflow matrix are important; these can be obtained. Given a cycle matrix, one can obtain histograms for amplitude and range, respectively.

Markov models

If the sequence of turning points forms a Markov chain it is called an MC of turning points (MCTP). The Markov matrix is the expected histogram matrix of min-to-max and max-to-min cycles. Given a rainflow matrix of an MCTP, one can find its Markov matrix, and vice versa. In WAFO, algorithms are implemented to calculate the rainflow matrix for an MC and an MCTP; cf. [22].

In some applications, one wants to model data, whose properties change according to an underlying, often unobserved process, called the regime process. The state of the regime process controls which parameters to use and when to switch the parameter values. If the regime process is modelled by a Markov chain we have a Hidden Markov Model (HMM), and this is the fundamental basis for the set of routines presented. For an application with such switching Markov models for fatigue problems, see [32, 33].

Fatigue and Damage

In WAFO, routines for calculation of the accumulated damage according to the Palmgren-Miner rule have been implemented. It is possible to compute the total

damage from a cycle count as well as from a cycle matrix. The relation between load energy spectrum and fatigue can be analysed by using the spectrum for a transformed Gaussian load process to first calculate a cycle matrix and then the total damage. See `help fatigue` for a list of fatigue routines available in the different WAFO directories.

Extreme value distributions

Certain probability distributions are extensively used in ocean engineering, e.g. Rayleigh, Gumbel, Weibull. The generalized extreme-value distributions (GEV) and generalized Pareto distributions (GPD) are also important. For these and other popular distributions, used in reliability and life-span models, it is possible to estimate parameters, generate random variables, evaluate pdf and cumulative distribution function, and plot in various probability papers.

Kernel-density-estimation tools

The routines in this category complement the ones found in 'Data analysis' and, obviously, the routines in 'Statistical tools and extreme value distributions'. They are, however, also applicable to multi-dimensional data, and hence very useful for smoothing purposes when comparing (theoretical) joint distributions of wave characteristics to data; cf. [80] and [92].

WAFO as a statistics toolbox

Besides the special statistical routines for extreme value analysis and kernel smoothing, WAFO contains statistical routines for handling univariate and multi-variate distribution functions, simulation, moments, likelihood estimation, regression and factor analysis, hypothesis testing and confidence intervals, bootstrap and jackknife estimation, and design of experiment.

Miscellaneous routines

We find here various plot routines, algorithms for numerical integration, and functions for documentation of WAFO with modules. Note, that the figures in this tutorial have been edited with respect to font size, and some other properties.

1.4 Some applications of WAFO

In this section we demonstrate some of the capabilities of WAFO. For further examples and knowledge about the algorithms used in the routines, we refer to the tutorial and the documentation in the routines. The necessary MATLAB code for generation of the figures in this tutorial is found in the directory `WAFO/papers/tutorcom/`. The commands for this chapter are collected in `Chapter1.m` and run with MATLAB 9.1 in 5 seconds on a 3.6 GHz 64 bit PC with Windows 10.

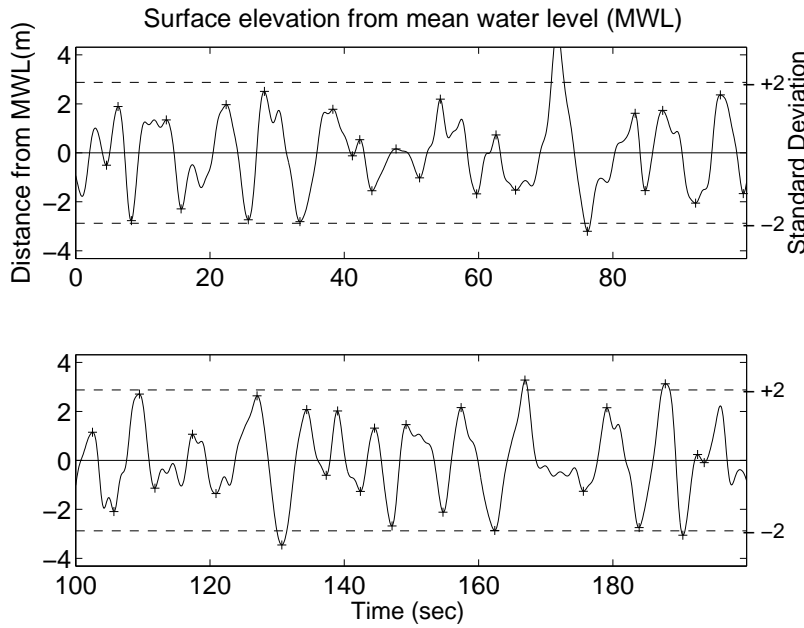


Figure 1.1: A simulation from $S(\omega)$, a Torsethaugen spectrum with $H_{m0} = 6$ [m], $T_p = 8$ [s]. Total number of points = 2000, $\Delta t = 0.1$ [s].

We start by defining a frequency spectrum, $S(\omega)$, which will be used in many of the examples; we choose a Torsethaugen spectrum with the parameters $H_{m0} = 6$ [m], $T_p = 8$ [s], describing significant wave height and primary peak period, respectively. The energy is divided between two peaks, corresponding to contributions from wind and swell; [88]. WAFO allows spectra to be defined simply by their parameters H_{m0} and T_p . The list in Section 1.5 helps to keep track of the different theoretical and empirical spectra we use in this tutorial.

1.4.1 Simulation from spectrum, estimation of spectrum

In Figure 1.1, plotted using `waveplot`, we have simulated a sample path from $S(\omega)$. The user specifies the number of wanted points in the simulation. The following code in MATLAB generates 200 seconds of data sampled with 10 Hz from the discussed spectrum. More on simulation can be found in Section 2.3.

```
Hm0 = 6; Tp = 8; plotflag = 1; clf
ST = torsethaugen([], [Hm0 Tp], plotflag);
dt = 0.1; N = 2000;
xs = spec2sdat(ST, N, dt); clf
waveplot(xs, '-')
```

In a common situation, data is given in form of a time series, for which one wants to estimate the related spectrum. We will now simulate 20 minutes of the signal sampled with 4 Hz, find an estimate $S_{\text{est}}(\omega)$ and compare the result to the original Torsethaugen spectrum $S(\omega)$. The following code was used to generate Figure 1.2, where the original and estimated spectra are displayed. The maximum lag size of the Parzen window function used (here 400) can be chosen by the user or automatically by WAFO.

```

plotflag = 1; Fs = 4; clf
dt = 1/Fs; N = fix(20*60*Fs);
xs = spec2sdat(ST,N,dt);
STest = dat2spec(xs,400)
plotspec(ST,plotflag), hold on
plotspec(STest,plotflag,'--')
axis([0 3 0 5]), hold off

```

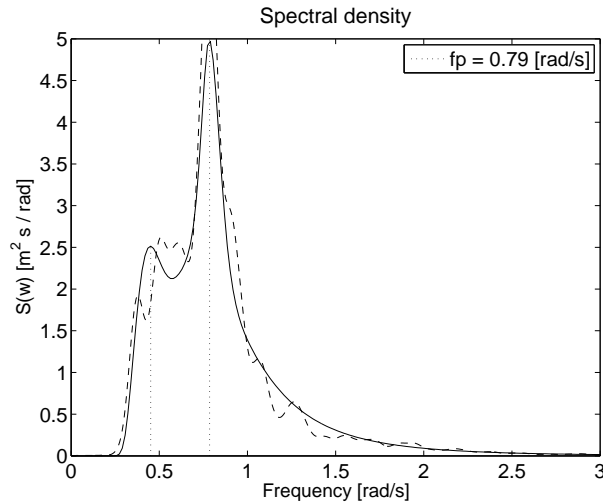


Figure 1.2: Solid: Thorsethaugen spectrum **ST**. Dashed: spectrum **STest** estimated from data (20 minutes). Maximum lag size of Parzen window = 400.

1.4.2 Probability distributions of wave characteristics

WAFO gives the possibility to compute exact probability distributions for a number of wave characteristics, given a spectral density. A wave characteristic as, for example, wave period, can be defined in several ways, see Table 3.1, page 67, in Chapter 3, and WAFO allows the user to choose between a number of definitions: trough-to-crest, down-to-up crossing, up-to-up crossing, etc. In Chapter 3 we analyse wave characteristics from observed data, and present some commonly used approximative distributions. Chapter 4 describes how to use WAFO to compute the exact theoretical distributions for all these wave characteristics in a Gaussian or transformed Gaussian model.

In the numerical example, we consider the trough period, i.e. the down-to-up crossing definition. The wave periods can be extracted from the realization in Figure 1.1, and are shown as a histogram in Figure 1.3. This histogram may be compared to the theoretical density, calculated from the original spectrum $S(\omega)$, and from the estimated spectrum $S_{\text{est}}(\omega)$; see Figure 1.3. Recall that, for this spectrum, $T_p = 8$ [s]. The figure shows the density for the half period; the results are in good agreement with that from the original spectrum. The following code lines are used to produce the presented figure. The different steps are: first extract half periods from the data by means of the routine `dat2wa` and store in the variable `T`, then use `spec2tpdf` to

calculate the theoretical distribution. The parameter NIT determines the accuracy of the calculation.

```
NIT = 3; paramt = [0 10 51]; clf
dtyex = spec2tpdf(ST,[],'Tt',paramt,0,NIT);
dtyest = spec2tpdf(STest,[],'Tt',paramt,0,NIT);
[T, index] = dat2wa(xs,0,'d2u');
histgrm(T,25,1,1), hold on
pdfplot(dtyex), pdfplot(dtyest,'-.')
axis([0 10 0 0.35]), hold off
```

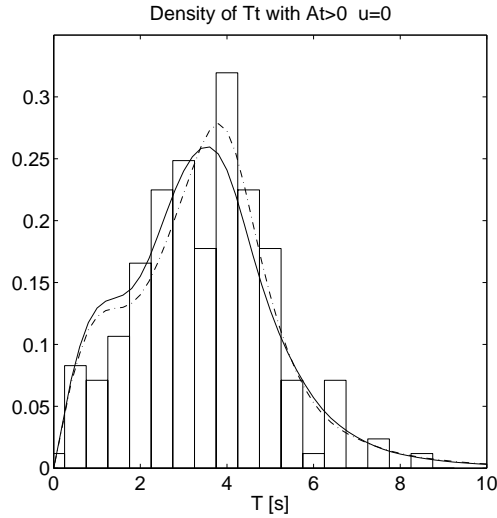


Figure 1.3: Pdf for wave trough period for Torsethaugen spectrum **ST** (solid line) and estimated spectrum **STest** (dash-dotted line). The histogram shows the wave periods extracted from the simulated data in Figure 1.1.

1.4.3 Directional spectra

In WAFO one finds means for evaluation and visualization of directional spectra to model sea states with waves coming from many different directions, that is

$$S(\omega, \theta) = S(\omega) D(\theta, \omega),$$

where $S(\omega)$ is a frequency spectrum and $D(\theta, \omega)$ is a spreading function. A number of common spreading functions can be chosen by the user.

One way of visualizing $S(\omega, \theta)$ is a polar plot. In Figure 1.4 we show the resulting directional spectrum (solid line) for the Torsethaugen spectrum used above. The spreading function is of the *cos-2s* type, that is (in the frequency independent case),

$$D(\theta) = \frac{\Gamma(s+1)}{2\sqrt{\pi}\Gamma(s+1/2)} \cos^{2s} \left(\frac{\theta}{2} \right)$$

with $s=15$. Note that the two peaks can be distinguished. The dash dotted line is the corresponding result when the spreading function is frequency dependent, cf. [34].

Remark 1.1. “Wave direction” is the direction from which waves are coming. In WAFO we adhere to the mathematical convention to count direction counter-clockwise from the positive x -axis. Thus, waves with direction 0° are coming from the East and waves with direction 90° are coming from the North, just the opposite to ocean standard. \square

Here are a few lines of code, which produce the graph of these directional spectra with frequency independent and frequency dependent spreading. The main directions are 90° and 0° , respectively.

```
plotflag = 1; clf
Nt = 101; % number of angles
th0 = pi/2; % primary direction of waves
Sp = 15; % spreading parameter
D1 = spreading(Nt,'cos',th0,Sp,[],0); %frequency independent
D12 = spreading(Nt,'cos',0,Sp,ST.w,1); %frequency dependent
STD1 = mkdspec(ST,D1); STD12 = mkdspec(ST,D12);
plotspec(STD1,plotflag), hold on
plotspec(STD12,plotflag,'-.'), hold off
```

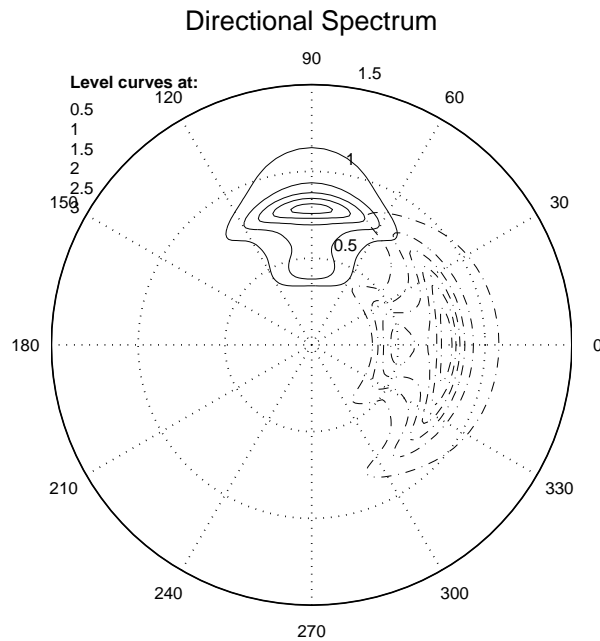


Figure 1.4: Directional spectrum. The frequency spectrum is a Torsethaugen spectrum and the spreading function is of $\cos\text{-}2s$ type with $s = 15$. Solid line: directional spectrum with frequency independent spreading. Dash dotted line: directional spectrum, using frequency dependent spreading function.

We finish the section with 20 seconds of simulated sea surfaces on 512[m] by 1024[m] for a sea with directional spectra `STD1` and `STD12`. The routine `spec2field` is used for simulation and the parameters for the simulation in space and time are defined by the options function `simoptset`.

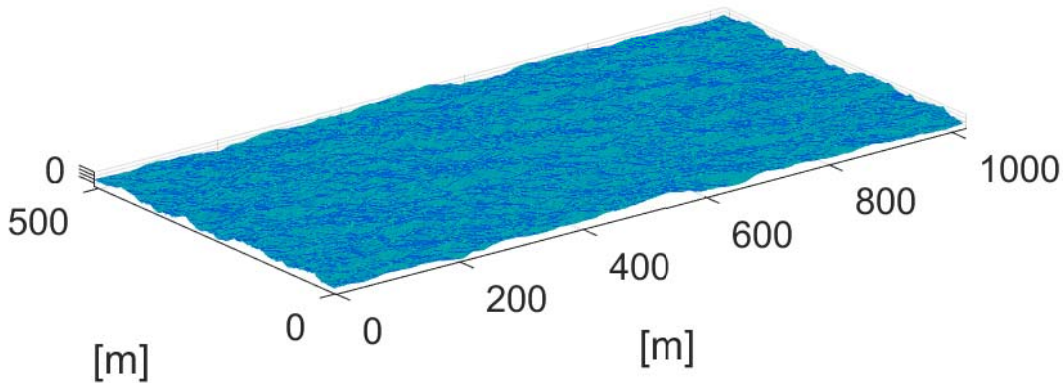


Figure 1.5: Gaussian sea surface, 512 [m] by 1024 [m], with directional spectrum SD1, spreading independent of frequency, waves from North.

```
rng('default'); clf
opt = simoptset('Nt',20,'dt',1,'Nu',1024,'du',1,'Nv',512,'dv',1)
W1 = spec2field(STD1,opt);
W12 = spec2field(STD12,opt)

W12 = struct with fields:
Z: [512 x 1024 x 20 double]
y: [1024 x 1 double]
x: [512 x 1 double]
t: [20 x 1 double]
```

The generated space-time fields can be presented and optionally saved as a movie by the routine `seamovie`. Specifying a file name saves the movie in avi-format, as for `Movie12`.

```
figure(1); clf
Movie1 = seamovie(W1,1);
figure(2); clf
Movie12 = seamovie(W12,1,'GaussianSea12.avi')
```

The last frame of the movies are shown in Figures 1.5-1.6 and one can see that waves are coming from different directions. However, frequency dependent spreading leads to a more irregular surface, so the orientation of waves is less transparent. From the figures it is not easy to deduce that both sea surfaces have the same period distribution, but it is more obvious that the wavelength distributions are different.

1.4.4 Fatigue, load cycles, and Markov models

In fatigue applications the exact sample path is not important, but only the peaks and troughs of the load, called the turning points (TP). From these one can extract load cycles, from which damage calculations and fatigue life predictions can be performed. In WAFO there are numerous routines for evaluating fatigue measured loads, as well as making theoretical calculations of distributions that are important for fatigue evaluation. A powerful

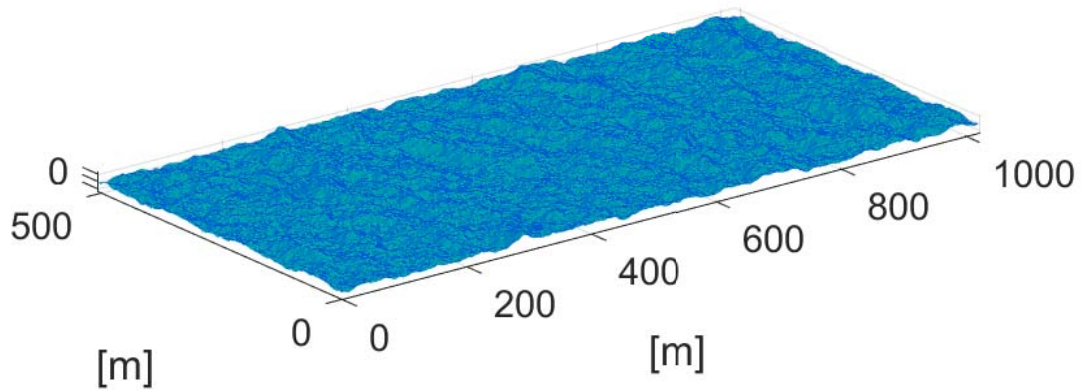


Figure 1.6: Gaussian sea surface, 512 [m] by 1024 [m], with directional spectrum SD12, frequency dependent spreading, waves from East.

technique when analysing loads is to use Markov models as approximations, especially to model the sequence of turning points by a Markov chain. For such models there exist many explicit results. Here, we will use this Markov approximation for computing the intensity of rainflow cycles and trough-to-crest cycles for the Gaussian model with spectrum from Figure 1.2.

For fatigue analysis the rainflow cycle, defined in Figure 5.1 in Chapter 5, is often used. The Markov model is defined by the min-to-max pdf, which is obtained from the power spectral density by using approximations in Slepian model processes, see e.g. [46] and references therein. Chapter 4 describes how WAFO routines can be used to find the min-to-max distribution for Gaussian loads. For the Markov model, there is an explicit solution for the intensity of rainflow cycles, see [22]. By using the routines in WAFO the intensity of rainflow cycles can be found using Markov approximation; see Figure 1.7, where also the rainflow cycles found in the simulated load signal are shown. The figure has been plotted using the following commands:

```
paramu = [-6 6 61];
frfc = spec2cmat(ST,[],'rfc',[],paramu);
pdfplot(frfc); hold on
tp = dat2tp(xs);      rfc = tp2rfc(tp);
plot(rfc(:,2),rfc(:,1),'.'); hold off
```

The WAFO toolbox also contains routines for computing the intensity of rainflow cycles in more complex load processes, for example for a switching Markov chain of turning points, TP. Details on fatigue load analysis are given in Chapter 5.

1.4.5 Statistical extreme value analysis

The WAFO-toolbox contains almost 600 routines for general statistical analysis, description, plotting, and simulation. In Chapter 6 we describe some routines which are particularly important for wave and fatigue analysis, related to statistics of extremes. These are based on the generalized extreme value (GEV) and generalized Pareto distribution (GPD), combined with the peaks over threshold (POT) method. As an example we show an analysis of wave elevation data from the Poseidon platform in the Japan Sea. Data

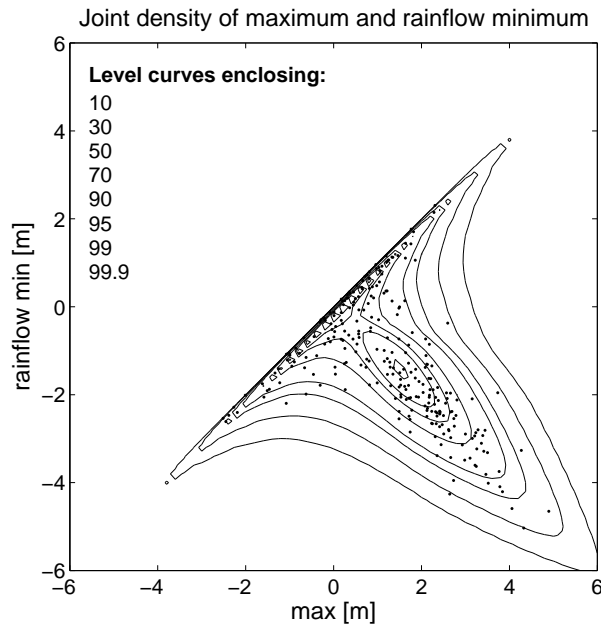


Figure 1.7: Intensity of rainflow cycles computed from the power spectrum through Markov approximation, compared with cycles found in the simulation.

from about 23 hours of registration are stored in the data set `yura87`, taken with a 1 Hz sampling rate. We first load and plot, in Figure 1.8, part of the data and calculate the maximum over 5 minute periods.

```
xn = load('yura87.dat'); subplot(211);
plot(xn(1:30:end,1)/3600,xn(1:30:end,2),'.')
title('Water level'), ylabel('m')
yura = xn(1:85500,2);
yura = reshape(yura,300,285);
maxyura = max(yura); subplot(212)
plot(xn(300:300:85500,1)/3600,maxyura,'.')
xlabel('Time (h)'), ylabel('m')
title('Maximum 5 min water level')
```

It is clear from the figures that there is a trend in the data, with decreasing spreading with time. In Chapter 5 we will deal with that problem; here we make a crude extreme value analysis, by fitting a GEV distribution to the sequence of 5 minute maxima, simply by issuing the commands

```
phat = fitgev(maxyura,'plotflag',1);
```

Figure 1.9 shows cumulative distribution and density of the fitted GEV distribution together with diagnostic plots of empirical and model quantiles. The non-stationarity gives a very bad fit in the upper tail of the distribution. The fitted GEV has shape parameter 0.1, with a 95% confidence interval (0.01,0.18).

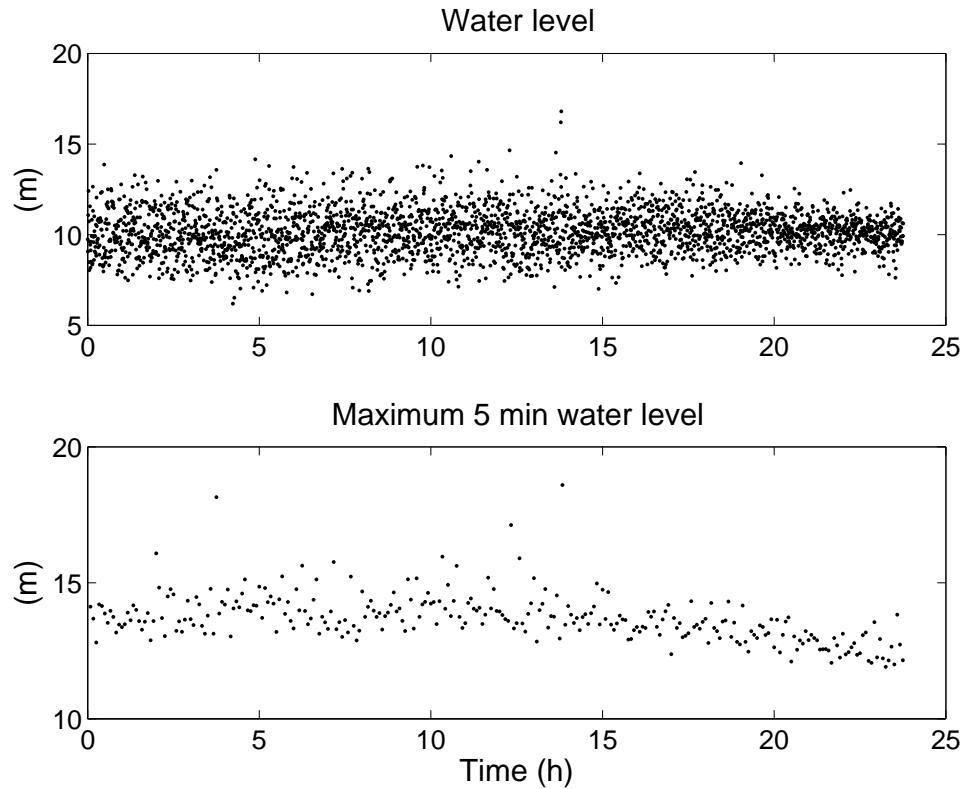


Figure 1.8: Water level variation in the Japan Sea from the data set `yura87` and maxima over 5 minute periods.

1.5 Spectra used in the tutorial

In this tutorial we illustrate the routines on many different wave and load spectra. Some are empirical, estimated from wave data, others are theoretical spectra suggested in the literature as suitable for special wave conditions. The following list and name convention should help the reader to keep track of the different types through the many examples in the next chapters. The notation `SXest` will occasionally be used for estimated spectra.

1.5.1 SG, Empirical spectrum from waves in `gfaksr89.dat`

Bi-modal spectrum `SG` estimated at the Gullfaks C platform at 2.5 [Hz], 39 000 data points. This spectrum is used in Examples 10–12.

1.5.2 SJ, Theoretical JONSWAP spectrum

Theoretical uni-modal JONSWAP spectrum `SJ` designed for North Sea waves. This spectrum is used in Examples 2, 5, and 6.

1.5.3 SS, Empirical spectrum from waves in `sea.dat`

Bi-modal spectrum `SS`, estimated from shallow water wave data, sample rate 4 [Hz], 9 524 data points. This spectrum is used in Examples 1, 3, 7, 9.

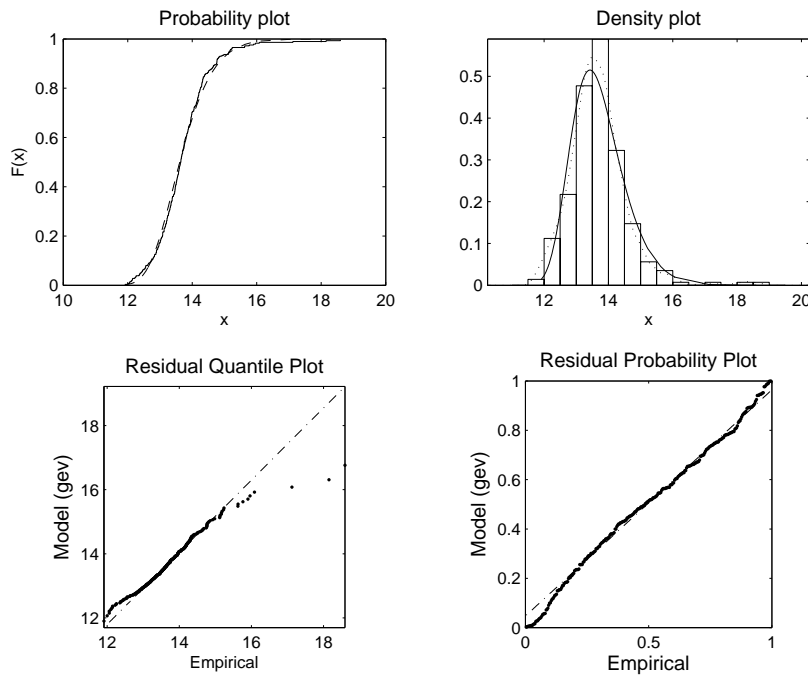


Figure 1.9: Diagnostic plots of GEV extreme value analysis of yura87.

1.5.4 ST, Theoretical TORSETHAUGEN spectrum

Theoretical bi-modal TORSETHAUGEN spectrum ST designed for mixed sea with wind waves and swell. This spectrum is used in Example 8.

1.6 Datastructures

help datastructures

DATASTRUCTURES of spectrum (S), covariance function (cvf) and probability density (pdf) in WAFO

To represent spectra, covariance functions and probability density functions in WAFO, the MATLAB datatype 'structured array' is used. Here follows a list of the fields in the struct representing S, cvf and pdf, respectively.

Spectrum structure

~~~~~

Requisite fields:

- .type String: 'freq', 'dir', 'k2d', 'k1d', 'encdir', 'enc'.
- .S Spectrum values (size=[nf 1] or [np nf]).
- .w OR .f OR .k Frequency/wave number lag, length nf.
- .tr Transformation function (default [] (none)).
- .h Water depth (default inf).
- .norm Normalization flag, Logical 1 if S is normalized, 0 if not.
- .note Memorandum string.
- .date Date and time of creation or change.

Type-specific fields:

- .k2 Second dim. wave number lag, if .type='k2d', 'rotk2d', length np.
- .theta Angular lags, if .type='dir', 'rotdir' or 'encdir', length np.
- .v Ship speed, if .type = 'enc' or 'encdir'.
- .phi angle of rotation of the coordinate system (counter-clockwise) e.g. azimuth of a ship.

See also createspec, plotspec

Covariance function (cvf) structure

~~~~~

- .R Covariance function values, size [ny nx nt], all singleton dim. removed.
- .x Lag of first space dimension, length nx.
- .y Lag of second space dimension, length ny.
- .t Time lag, length nt.
- .h Water depth.
- .tr Transformation function.
- .type 'enc', 'rot' or 'none'.
- .v Ship speed, if .type='enc'.
- .phi Rotation of coordinate system, e.g. direction of ship.

```
.norm Normalization flag, Logical 1 if autocorrelation,
      0 if covariance.
.Rx ... .Rtttt Obvious derivatives of .R.
.note Memorandum string.
.date Date and time of creation or change.
```

See also `createcov`, `spec2cov`, `cov2spec`, `covplot`

Probability density function (pdf) structure

~~~~~

Describing a density of n variables:

```
.f      Probability density function values,
      (n-dimensional matrix).
.x      Cell array of vectors defining grid for variables,
      (n cells).
.labx   Cell array of label strings for the variables,
      (n cells).
.title  Title string.
.note   Memorandum string.
```

See also `createpdf`, `pdfplot`



## CHAPTER 2

# Random waves and loads

---

In this chapter we present some tools for analysis of random functions with respect to their correlation, spectral, and distributional properties. We first give a brief introduction to the theory of Gaussian processes and then we present programs in WAFO, which can be used to analyse random functions. For deeper insight in the theory we refer to [40, 45].

The presentation will be organized in three examples: Example 1 is devoted to estimation of different parameters in the model, Example 2 deals with spectral densities and Example 3 presents the use of WAFO to simulate samples of a Gaussian process. The commands, collected in `Chapter2.m`, run in less than 5 seconds on a 3.60 GHz 64 bit PC with Windows 10; add another two minutes for the display of simulated wave fields.

### 2.1 Introduction and preliminary analysis

The functions we shall analyse can be measured stresses or strains, which we call loads, or other measurements, where waves on the sea surface is one of the most important examples. We assume that the measured data are given in one of the following forms:

1. In the time domain, as measurements of a response function denoted by  $x(t)$ ,  $0 \leq t \leq T$ , where  $t$  is time and  $T$  is the duration of the measurements. The  $x(t)$ -function is usually sampled with a fixed sampling frequency and a given resolution, i.e. the values of  $x(t)$  are also discretised. The effects of sampling can not always be neglected in estimation of parameters or distributions. We assume that measured functions are saved as a two column ASCII or `mat` file.

Some general properties of measured functions can be summarized by using a few simple characteristics. Those are the *mean*  $m$ , defined as the average of all values, the *standard deviation*  $\sigma$ , and the *variance*  $\sigma^2$ , which measure the variability around the mean in linear and quadratic scale. These quantities are estimated by

$$m = 1/T \int_0^T x(t) dt, \quad (2.1)$$

$$\sigma^2 = 1/T \int_0^T (x(t) - m)^2 dt, \quad (2.2)$$

for a continuous recording or by corresponding sums for a sampled series.

2. In the frequency domain, as a power spectrum, which is an important mode in systems analysis. This means that the signal is represented by a Fourier series,

$$x(t) \approx m + \sum_{i=1}^N a_i \cos(\omega_i t) + b_i \sin(\omega_i t), \quad (2.3)$$

where  $\omega_i = i \cdot 2\pi/T$  are angular frequencies,  $m$  is the mean of the signal and  $a_i, b_i$  are Fourier coefficients.

3. Another important way to represent a load sequence is by means of the *crossing spectrum* or *crossing intensity*,  $\mu(u)$  = the intensity of upcrossings = average number of upcrossings per time unit, of a level  $u$  by  $x(t)$  as a function of  $u$ , see further in Section 2.2.3. The *mean frequency*  $f_0$  is usually defined as the number of times  $x(t)$  crosses upwards (upcrosses) the mean level  $m$  normalized by the length of the observation interval  $T$ , i.e.  $f_0 = \mu(m)$ . An alternative definition,<sup>1</sup> which we prefer to use is that  $f_0 = \max \mu(u)$ , i.e. it is equal to the maximum of  $\mu(u)$ . The *irregularity factor*  $\alpha$  is defined as the mean frequency  $f_0$  divided by the intensity of local maxima (“intensity of cycles”, i.e. the average number of local maxima per time unit) in  $x(t)$ . Note, a small  $\alpha$  means an irregular process,  $0 < \alpha \leq 1$ .

**Example 1. (Sea data)** In this example we use a series with wave data `sea.dat` with time argument in the first column and function values in the second column. The data used in the examples are wave measurements at shallow water location, sampled with a sampling frequency of 4 Hz, and the units of measurement are seconds and meters, respectively. The file `sea.dat` is loaded into MATLAB and after the mean value has been subtracted the data are saved in the two column matrix `xx`.

```
xx = load('sea.dat');
me = mean(xx(:,2))
sa = std(xx(:,2))
xx(:,2) = xx(:,2) - me;
lc = dat2lc(xx);
plotflag = 2;
lcplot(lc,plotflag,0,sa)
```

Here `me` and `sa` are the mean and standard deviation of the signal, respectively. The variable `lc` is a two column matrix with levels in the first column and the number of upcrossing of the level in the second. In Figure 2.1 the number of upcrossings of `xx` is plotted and compared with an estimation based on the assumption that `xx` is a realization of a Gaussian sea.

Next, we compute the mean frequency as the average number of upcrossings per time unit of the mean level ( $= 0$ ); this may require interpolation in the crossing intensity curve, as follows.

---

<sup>1</sup>Still another definition, to be used in Chapter 5, is that  $f_0$  is the average number of completed load cycles per time unit.

```

T = max(xx(:,1))-min(xx(:,1))
f0 = interp1(lc(:,1),lc(:,2),0)/T
    % zero up-crossing frequency

```

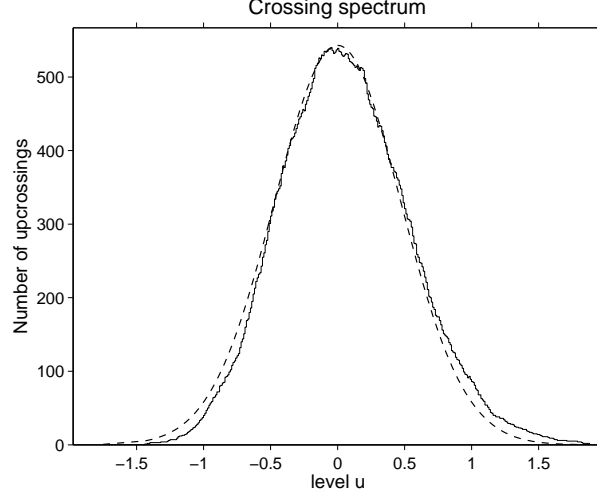


Figure 2.1: The observed crossings intensity compared with the theoretically expected for Gaussian signals, see (2.8).

The process of fatigue damage accumulation depends only on the values and the order of the local extremes in the load. The sequence of local extremes is called the *sequence of turning points*. It is a two column matrix with time for the extremes in the first column and the values of the extremes in the second.

```

tp = dat2tp(xx);
fm = length(tp)/(2*T)           % frequency of maxima
alfa = f0/fm

```

Here `alfa` is the irregularity factor. Note that `length(tp)` is equal to the number of local maxima and minima and hence we have a factor 2 in the expression for `fm`.  $\square$

We finish this section with some remarks about the quality of the measured data. Especially sea surface measurements can be of poor quality. It is always good practice to visually examine the data before the analysis to get an impression of the quality, non-linearities and narrow-bandedness of the data.

**Example 1. (contd.)** First we shall plot the data `xx` and zoom in on a specific region. A part of the sea data is presented in Figure 2.2 obtained by the following commands.

```

waveplot(xx,tp,'k-', '*',1,1)
axis([0 2 -inf inf])

```

However, if the amount of data is too large for visual examination, or if one wants a more objective measure of the quality of the data, one could use the following empirical criteria:

- $x'(t) < 5$  [m/s], since the raising speed of Gaussian waves rarely exceeds 5 [m/s],
- $x''(t) < 9.81/2$ , [m/s<sup>2</sup>] which is the limiting maximum acceleration of Stokes waves,

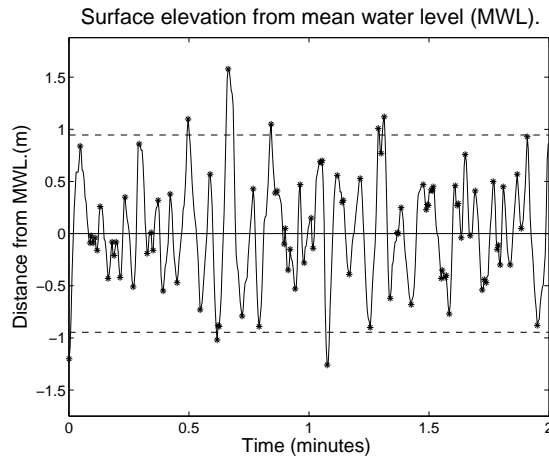


Figure 2.2: A part of the sea data with turning points marked as stars.

- if the signal is constant in some intervals, then this will add high frequencies to the estimated spectral density; constant data may occur if the measuring device is blocked during some period of time.

To find possible spurious points of the dataset use the following commands.

```
dt = diff(xx(1:2,1));
dcrit = 5*dt;
ddcrit = 9.81/2*dt*dt;
zcrit = 0;
[inds indg] = findoutliers(xx,zcrit,dcrit,ddcrit);
```

The program will give the following list when used on the sea data.

```
Found 0 missing points
Found 0 spurious positive jumps of Dx
Found 0 spurious negative jumps of Dx
Found 37 spurious positive jumps of D^2x
Found 200 spurious negative jumps of D^2x
Found 244 consecutive equal values
Found the total of 1152 spurious points
```

The values for `zcrit`, `dcrit` and `ddcrit` can be chosen more carefully. One must be careful using the criteria for extreme value analysis, because it might remove extreme waves that belong to the data and are not spurious. However, small changes of the constants are usually not so crucial. As seen from the transcripts from the program a total of 1152 points are found to be spurious which is approximately 12 % of the data. Based on this one may classify the datasets into good, reasonable, poor, and useless. Obviously, uncritical use of data may lead to unsatisfactory results. We return to this problem when discussing methods to reconstruct the data. □

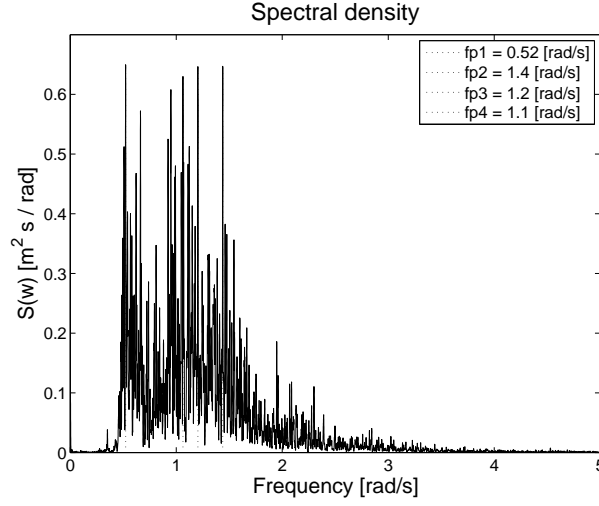


Figure 2.3: The observed, unsmoothed, spectrum in the data set `sea.dat`.

## 2.2 Frequency modelling of load histories

### 2.2.1 Power spectrum, periodogram

The most important characteristic of signals of the form (2.3) in frequency domain is their power spectrum

$$\hat{s}_i = (a_i^2 + b_i^2)/(2\Delta\omega),$$

where  $\Delta\omega$  is the sampling interval in frequency domain, i.e.  $\omega_i = i \cdot \Delta\omega$ . The two-column matrix  $\hat{s}(\omega_i) = (\omega_i, \hat{s}_i)$  will be called the *power spectrum* of  $x(t)$ . The alternative term *periodogram* was introduced as early as 1898 by A. Schuster, [78].

The sequence  $\theta_i$  such that  $\cos \theta_i = a_i/\sqrt{2 \hat{s}_i \Delta\omega}$  and  $\sin \theta_i = -b_i/\sqrt{2 \hat{s}_i \Delta\omega}$ , is called a sequence of phases and the Fourier series can be written as follows:

$$x(t) \approx m + \sum_{i=1}^N \sqrt{2 \hat{s}_i \Delta\omega} \cos(\omega_i t + \theta_i).$$

If the sampled signal contains exactly  $2N + 1$  points, then  $x(t)$  is equal to its Fourier series at the sampled points. In the special case when  $N = 2^k$ , the so-called FFT (Fast Fourier Transform) can be used to compute the Fourier coefficients (and the spectrum) from the measured signal and in reverse the signal from the Fourier coefficients.

The Fourier coefficient to the zero frequency is just the mean of the signal, while the variance is given by  $\sigma^2 = \Delta\omega \sum \hat{s}(\omega_i) \approx \int_0^\infty \hat{s}(\omega) d\omega$ . The last integral is called the zero-order spectral moment  $m_0$ . Similarly, higher-order spectral moments are defined by

$$m_n = \int_0^\infty \omega^n \hat{s}(\omega) d\omega.$$

**Example 1. (contd.)** We now calculate the spectrum  $\hat{s}(\omega)$  for the sea data signal `xx`.

```
Lmax = 9500;
SS = dat2spec(xx,Lmax);
plotspec(SS); axis([0 5 0 0.7])
```

The produced plot, not reproduced in this tutorial, shows the spectrum  $\hat{s}(\omega)$  in blue surrounded by 95% confidence limits, in red. These limits can be removed by the command

```
SS = rmfield(SS,'CI')
plotspec(SS); axis([0 5 0 0.7])
```

giving Figure 2.3 where we can see that the spectrum is extremely irregular with sharp peaks at many distinct frequencies. In fact, if we had analysed another section of the sea data we had found a similar general pattern, but the sharp peaks had been found at some other frequencies. It must be understood, that the observed irregularities are random and vary between measurements of the sea even under almost identical conditions. This will be further discussed in the following section, where we introduce smoothing techniques to get a stable spectrum that represents the “average randomness” of the sea state.

Next, the spectral moments will be computed.

```
[mom text] = spec2mom(SS,4)
[sa sqrt(mom(1))]
```

The vector `mom` now contains spectral moments  $m_0, m_2, m_4$ , which are the variances of the signal and its first and second derivative. We can speculate that the variance of the derivatives is too high because of spurious points. For example, if there are several points with the same value, the Gibb’s phenomenon leads to high frequencies in the spectrum.  $\square$

## 2.2.2 Gaussian processes in spectral domain

In the previous section we studied the properties of one specific signal in frequency domain. Assume now that we get a new series of measurements of a signal, which we are willing to consider as equivalent to the first one. However, the two series are seldom identical and differ in some respect that it is natural to regard as purely random. Obviously it will have a different spectrum  $\hat{s}(\omega)$  and the phases will be changed.

A useful mathematical model for such a situation is the random function (stochastic process) model which will be denoted by  $X(t)$ . Then  $x(t)$  is seen as particular randomly chosen function. The simplest model for a stationary signal with a fixed spectrum  $\hat{s}(\omega)$  is

$$X(t) = m + \sum_{i=1}^N \sqrt{\hat{s}_i \Delta\omega} \sqrt{2} \cos(\omega_i t + \Theta_i), \quad (2.4)$$

where the phases  $\Theta_i$  are random variables, independent and uniformly distributed between 0 and  $2\pi$ . However, this is not a very realistic model either, since in practice one often observes a variability in the spectrum amplitudes  $\hat{s}(\omega)$  between measured functions. Hence,  $\hat{s}_i$  should also be modelled to include a certain randomness.

The best way to accomplish this realistic variability is to assume that there exists a deterministic function  $S(\omega)$  such that the *average value* of  $\hat{s}(\omega_i)\Delta\omega$  over many observed series can be approximated by  $S(\omega_i)\Delta\omega$ . In fact, in many cases one can model the variability of  $\hat{s}_i$  as

$$\hat{s}_i = R_i^2 \cdot S(\omega_i)/2,$$

where  $R_i$  are independent random factors, all with a Rayleigh distribution, with probability density function  $f_R(r) = r \exp(-r^2/2), r > 0$ . (Observe that the average value of  $R_i^2$  is 2.)

This gives the following random function as a model for the series,

$$X(t) = m + \sum_{i=1}^N \sqrt{S(\omega_i) \Delta\omega} R_i \cos(\omega_i t + \Theta_i). \quad (2.5)$$

The process  $X(t)$  has many useful properties that can be used for analysis. In particular, for any fixed  $t$ ,  $X(t)$  is normally (Gaussian) distributed. Then, the probability of any event defined for  $X(t)$  can, in principle, be computed when the mean  $m$  and the spectral density  $S$  are known.

In sea modelling, the components in the sum defining  $X(t)$  can be interpreted as individual waves. The assumption that  $R_i$  and  $\Theta_i$  are independent random variables implies that the individual waves are independent stationary Gaussian processes<sup>2</sup> with mean zero and covariance function given by

$$r_i(\tau) = \Delta\omega S(\omega_i) \cos(\omega_i \tau).$$

Consequently, the covariance between  $X(t)$  and  $X(t + \tau)$  is given by

$$r_X(\tau) = E[(X(t) - m)(X(t + \tau) - m)] = \Delta\omega \sum_{i=1}^N S(\omega_i) \cos(\omega_i \tau).$$

A process like (2.5), which is the sum of discrete terms, is said to have discrete spectrum. Its total energy is concentrated to a set of distinct frequencies.

More generally, for a stationary stochastic process with spectral density  $S(\omega)$ , the covariance function  $r(\tau)$  of the process is defined by its spectral density function  $S(\omega)$ , also called power spectrum,

$$r(\tau) = C[X(t), X(t + \tau)] = \int_0^\infty \cos(\omega\tau) S(\omega) d\omega. \quad (2.6)$$

Since  $V[X(t)] = r_X(0) = \int_0^\infty S(\omega) d\omega$ , the spectral density represents a continuous distribution of the wave energy over a continuum of frequencies. The spectrum is continuous.

The covariance function and the spectral density form a *Fourier transform pair*. The spectral density can be computed from the covariance function by the Fourier inversion formula, which for continuous-time signals reads,

$$S(\omega) = \frac{2}{\pi} \int_0^\infty \cos(\omega\tau) r(\tau) d\tau. \quad (2.7)$$

The Gaussian process model is particularly useful in connection with linear filters. If  $Y(t)$  is the output of a linear filter with the Gaussian process  $X(t)$  as input, then  $Y(t)$  is also normally distributed. Further, the spectrum of  $Y(t)$  is related to that of  $X(t)$  in a simple way. If the filter has *transfer function*  $H(\omega)$ , also called *frequency function*, then the spectrum of  $Y(t)$ , denoted by  $S_Y$ , is given by

$$S_Y(\omega) = |H(\omega)|^2 S_X(\omega).$$

For example, the derivative  $X'(t)$  is a Gaussian process with mean zero and spectrum  $S_{X'}(\omega) = \omega^2 S_X(\omega)$ . The variance of the derivative is equal to the second spectral moment,

$$\sigma_{X'}^2 = \int S_{X'}(\omega) d\omega = \int \omega^2 S_X(\omega) d\omega = m_2.$$

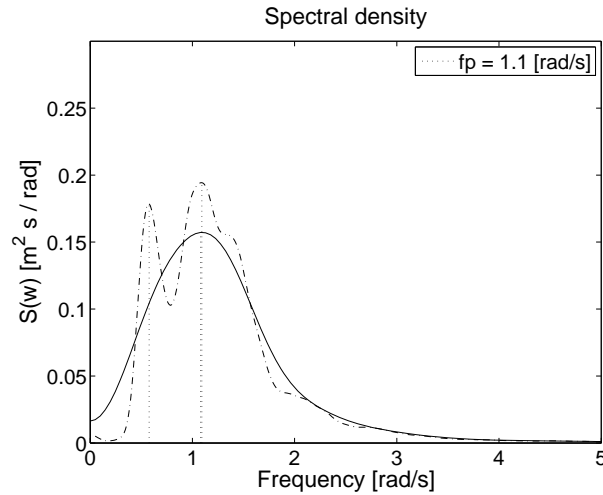


Figure 2.4: Estimated spectra SS1, SS2 for the data set `sea.dat` with varying degree of smoothing; dash-dotted: `Lmax1 = 200`, solid: `Lmax2 = 50`.

**Example 1. (contd.)** In order to estimate the spectrum of a Gaussian process one needs several realizations of the process. Then, one spectrum estimate can be made for each realization, which are then averaged. However, in many cases only one realization of the process is available. In such a case one is often assuming that the spectrum is a smooth function of  $\omega$  and one can use this information to improve the estimate. In practice, it means that one has to use some smoothing techniques. For the `sea.dat` we shall estimate the spectrum by means of the WAFO function `dat2spec` with a second parameter defining the degree of smoothing.

```
Lmax1 = 200;
Lmax2 = 50;
SS1 = dat2spec(xx,Lmax1);
SS2 = dat2spec(xx,Lmax2);
plotspec(SS1,[],'-.'), hold on
plotspec(SS2), hold off
```

In Figure 2.4 we see that with decreasing second input the spectrum estimate becomes smoother, and that in the end it becomes unimodal.

An obvious question after this exercise is the following: Which of the two estimates in Figure 2.4 is more correct, in the sense that it best reflects important wave characteristics? Since the correlation structure is a very important characteristic, we check which spectrum can best reproduce the covariance function of the data `xx`.

The following code in WAFO will compute the covariance for the bimodal spectral density S1 and compare it with the estimated covariance in the signal `xx`.

```
Lmax = 80;
R1 = spec2cov(SS1,1);
Rest = dat2cov(xx,Lmax);
covplot(R1,Lmax,[],'.'), hold on
covplot(Rest), hold off
```

---

<sup>2</sup>A Gaussian stochastic process  $X(t)$  is any process such that all linear combinations  $\sum a_k X(t_k)$  have a Gaussian distribution; also derivatives  $X'(t)$  and integrals  $\int_a^b X(t) dt$  are Gaussian.



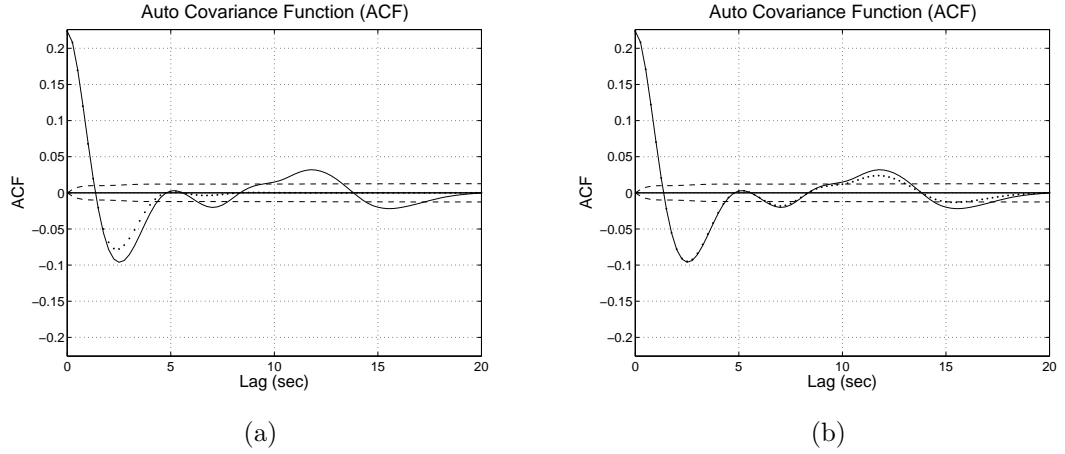


Figure 2.5: The covariance function estimated in the data set `sea.dat`, solid line, compared to the theoretically computed covariance functions for the spectral densities `SS2` in (a) and `SS1` in (b).

With the unimodal spectrum `SS2` instead of `SS1` we also compute the covariance function `R2 = spec2cov(SS2,1)` and plot it together with `Rest`.

We can see in Figure 2.5(a) that the covariance function corresponding to the spectral density `SS2` differs significantly from the one estimated directly from data. The covariance corresponding to `SS1` agrees much better with the estimated covariance function, as seen in Figure 2.5(b). Our conclusion is that the bimodal spectrum in Figure 2.4 is a better model for the data `sea.dat` than the unimodal one.  $\square$

Observe that the WAFO function `spec2cov` can be used to compute a covariance structure which can contain covariances both in time and in space as well as that of the derivatives. The input can be any spectrum structure, e.g. wavenumber spectrum, directional spectrum or encountered directional spectrum; type `help spec2cov` for detailed information.

### 2.2.3 Crossing intensity – Rice’s formula

The Gaussian process is a sum (or in fact an integral) of cosine terms with amplitudes defined by the spectrum, and the instantaneous value  $X(t)$  has a normal distribution with mean 0 and variance  $\sigma^2 = \int S(\omega) d\omega$ . The spectral density  $S(\omega)$  determines the relative importance of components with different frequencies.

In wave analysis and fatigue applications there is another quantity that plays a central role, namely the *upcrossing intensity*  $\mu(u)$ , which yields the average number, per time or space unit, of upcrossings of the level  $u$ . It contains important information on the fatigue properties of a load signal and also of the wave character of a random wave.<sup>3</sup>

For a Gaussian process the crossing intensity is given by the celebrated *Rice’s formula*,

$$\mu(u) = f_0 \exp \left\{ -\frac{(u - m)^2}{2\sigma^2} \right\}. \quad (2.8)$$

<sup>3</sup>The general expression for the upcrossing intensity for a stationary process is  $\mu(u) = \int_{z=0}^{\infty} z f_{X(0),X'(0)}(u, z) dz$ , where  $f_{X(0),X'(0)}(u, z)$  is a joint probability density function.

Using spectral moments we have that  $\sigma^2 = m_0$  while  $f_0 = \frac{1}{2\pi} \sqrt{\frac{m_2}{m_0}}$  is the mean frequency.

### 2.2.4 Transformed Gaussian models

The standard assumptions for a sea state under stationary conditions are that  $X(t)$  is a stationary and ergodic stochastic process with mean  $E[X(t)]$  assumed to be zero, and with a spectral density  $S(\omega)$ . The knowledge of which kind of spectral densities  $S(\omega)$  are suitable to describe different sea state data is well established from experimental studies.

Real data  $x(t)$  seldom perfectly support the Gaussian assumption for the process  $X(t)$ . But since the Gaussian case is well understood and there are approximative methods to obtain wave characteristics from the spectral density  $S(\omega)$  for Gaussian processes, one often looks for a model of the sea state in the class of Gaussian processes. Furthermore, in previous work, [73], we have found that for many sea wave data, even such that are clearly non-Gaussian, the wavelength and amplitude densities can be very accurately approximated using the Gaussian process model.

However, the Gaussian model can lead to less satisfactory results when it comes to the distribution of crest heights or joint densities of troughs and crests. In that case we found in [73] that a simple transformed Gaussian process used to model  $x(t)$  gave good approximations for those densities.

Consequently, in WAFO we shall model  $x(t)$  by a process  $X(t)$  which is a function of a single Gaussian process  $\tilde{X}(t)$ , i.e.

$$X(t) = G(\tilde{X}(t)), \quad (2.9)$$

where  $G(\cdot)$  is a continuously differentiable function with positive derivative. We shall denote the spectrum of  $X$  by  $S$ , and the spectrum of  $\tilde{X}(t)$  by  $\tilde{S}$ . The transformation  $G$  performs the appropriate non-linear translation and scaling so that  $\tilde{X}(t)$  is always normalized to have mean zero and variance one, i.e. the first spectral moment of  $\tilde{S}$  is one.

Note that once the distributions of crests, troughs, amplitudes or wavelengths in a Gaussian process  $\tilde{X}(t)$  are computed, then the corresponding wave distributions in  $X(t)$  are obtained by a simple variable transformation involving only the inverse of  $G$ , which we shall denote by  $g$ . Actually we shall use the function  $g$  to define the transformation instead of  $G$ , and use the relation  $\tilde{x}(t) = g(x(t))$  between the real sea data  $x(t)$  and the transformed data  $\tilde{x}(t)$ . If the model in Eq. (2.9) is correct, then  $\tilde{x}(t)$  should be a sample function of a process with Gaussian marginal distributions.

There are several different ways to proceed when selecting a transformation. The simplest alternative is to estimate the function  $g$  directly from data by some parametric or non-parametric techniques. A more physically motivated procedure is to use some of the parametric functions proposed in the literature, based on approximations of non-linear wave theory. The following options are programmed in the toolbox:

```
dat2tr      - non-parametric transformation g proposed by Rychlik,
hermitetr   - transformation g proposed by Winterstein,
ochitr      - transformation g proposed by Ochi et al.
```

The transformation proposed by Ochi et al., [58], is a monotonic exponential function, while Winterstein's model, [94], is a monotonic cubic Hermite polynomial. Both

transformations use higher moments of  $X(t)$  to compute  $g$ . Information about the moments of the process can be obtained by site specific data, laboratory measurements or from physical considerations. Rychlik's non-parametric method is based on the crossing intensity  $\mu(u)$ ; see [73]. Martinsen and Winterstein, [52], derived an expression for the skewness and kurtosis for narrow banded Stokes waves to the leading order and used these to define the transformation. The skewness and kurtosis (excess) of this model can also be estimated from data by the WAFO functions `skew` and `kurt`.

**Example 1. (contd.)** We begin with computations of skewness and kurtosis for the data set `xx`. The commands

```
rho3 = skew(xx(:,2))
rho4 = kurt(xx(:,2))
```

give the values `rho3 = 0.25` and `rho4 = 3.17`, respectively, compared to `rho3 = 0` and `rho4 = 3` for Gaussian waves. We can compute the same model for the spectrum  $\tilde{S}$  using the second order wave approximation proposed by Winterstein. His approximation gives suitable values for skewness and kurtosis

```
[sk, ku] = spec2skew(S1);
```

Here we shall use Winterstein's Hermite transformation and denote it by `gh`, and compare it with the linear transformation, denoted by `g`, that only has the effect to standardize the signal, assuming it is already Gaussian,

```
gh = hermitetr([], [sa sk ku me]);
g = gh; g(:,2)=g(:,1)/sa;
trplot(g)
```

These commands will result in two two-column matrices, `g`, `gh`, with equally spaced  $y$ -values in the first column and the values of  $g(y)$  in the second column.

Since we have data we may estimate the transformation directly by the method proposed by Rychlik et al., in [73]:

```
[glc test0 cmax irr gemp] = dat2tr(xx,[], 'plotflag',1);
hold on
plot(glc(:,1),glc(:,2), 'b-')
plot(gh(:,1),gh(:,2), 'b-.'), hold off
```

The same transformation can be obtained from data and the crossing intensity by use of the WAFO functions `dat2lc` followed by `lc2tr`.

In Figure 2.6 we compare the three transformations, the straight line is the Gaussian linear model, the dash dotted line is the Hermite transformation based on higher moments of the response computed from the spectrum and the solid line is the direct transformation estimated from crossing intensity. (The unsmoothed line shows the estimation of the direct transformation from unsmoothed crossing intensity). We can see that the transformation derived from crossings will give the highest crest heights. It can be proved that asymptotically the transformation based on crossings intensity gives the correct density of crest heights.

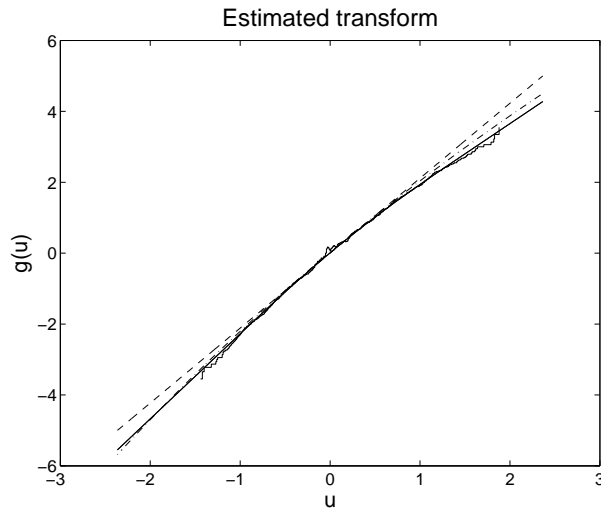


Figure 2.6: Comparisons of the three transformations  $g$ , straight line is the Gaussian model, dash dotted line the Hermite transformation  $gh$  and solid line the Rychlik method  $glc$ .

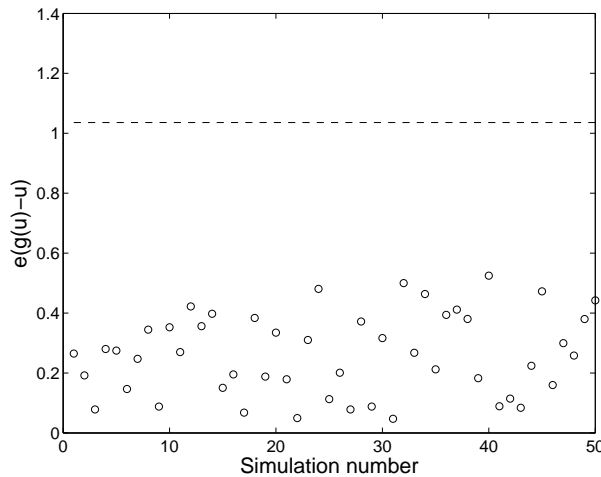
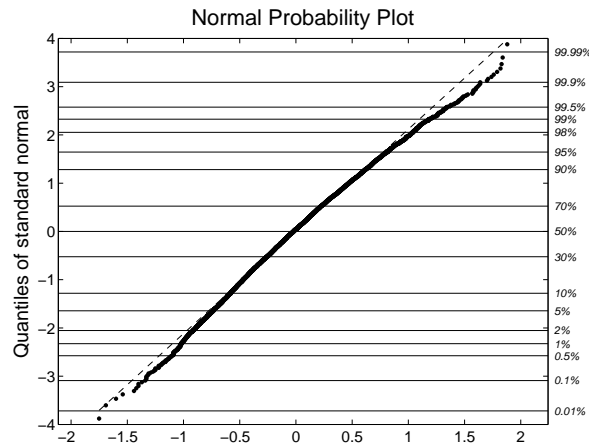


Figure 2.7: The simulated 50 values of the `test` variable for the Gaussian process with spectrum `S1` compared with the observed value (dashed line).

The transformations indicate that data `xx` has a light lower tail and heavy upper tail compared to a Gaussian model. This is also consistent with second order wave theory, where the crests are higher and the troughs shallower compared to Gaussian waves. Now the question is whether this difference is significant compared to the natural statistical variability due to finite length of the time series.

To determine the degree of departure from Gaussianity, we can compare an indicator of non-Gaussianity `test0` obtained from Monte Carlo simulation. The value of `test0` is a measure of how much the transformation  $g$  deviates from a straight line.

The significance test is done by simulating 50 independent samples of `test0` from a true Gaussian process with the same spectral density and length as the original data. This is accomplished by the WAFO program `testgaussian`. The output from the program is a plot of the ratio `test1` between the simulated (Gaussian) `test0`-values and the sample `test0`, that was calculated in the previous call to `dat2tr`:

Figure 2.8: The data `sea.dat` on normal probability plot.

```
N = length(xx);
test1 = testgaussian(S1,[N,50],test0);
```

The program gives a plot of simulated `test` values, see Figure 2.7. As we see from the figure none of the simulated values of `test1` is above 1.00. Thus the data significantly departs from a Gaussian distribution; see [73] for more detailed discussion of the testing procedure and the estimation of the transformation  $g$  from the crossing intensity.

We finish the tests for Gaussianity of the data by a more classical approach and simply plot the data on normal probability paper. Then  $N$  independent observations of identically distributed Gaussian variables form a straight line in a normalplot. Now, for a time series the data is clearly not independent. However, if the process is ergodic then the data forms a straight line as  $N$  tends to infinity.

The command

```
plotnorm(xx(:,2))
```

produces Figure 2.8. As we can see the normal probability plot is slightly curved indicating that the underlying distribution has a heavy upper tail and a light lower tail.  $\square$

### 2.2.5 Spectral densities of sea data

The knowledge of which kind of spectral density  $S(\omega)$  is suitable to describe sea state data is well established from experimental studies. One often uses some parametric form of spectral density functions, e.g. a JONSWAP-spectrum. This formula is programmed in a WAFO function `jonswap`, which evaluates the spectral density  $S(\omega)$  with specified wave characteristics. There are several other programmed spectral densities in WAFO to allow for bimodal and finite water depth spectra. The list includes the following spectra:

|                            |                                           |
|----------------------------|-------------------------------------------|
| <code>jonswap</code>       | - JONSWAP spectral density                |
| <code>wallop</code>        | - Wallop spectral density                 |
| <code>ochihubble</code>    | - Bimodal Ochi-Hubble spectral density    |
| <code>torsethaugen</code>  | - Bimodal (swell + wind) spectral density |
| <code>bretschneider</code> | - Bretschneider (Pierson-Moskowitz)       |

```

                                spectral density
mccormick    - McCormick spectral density
tmaspec      - JONSWAP spectral density
              for finite water depth

```

WAFO also contains some different spreading functions; use the help function on `spec` and `spreading` for more detailed information.

The spectrum of the sea can be given in many different formats, that are interconnected by the dispersion relation<sup>4</sup>. The spectrum can be given using frequencies, angular frequencies or wavenumbers, and it can also be directional.

A related spectrum is the encountered spectrum for a moving vessel. The transformations between the different types of spectra are defined by means of integrals and variable change defined by the dispersion relation and the Doppler shift of individual waves. The function `spec2spec` makes all these transformations easily accessible for the user. (Actually many programs perform the appropriate transformations internally whenever it is necessary and for example one can compute the density of wave-length, which is a quantity in space domain, from an input that is the directional frequency spectrum, which is related to the time domain.)

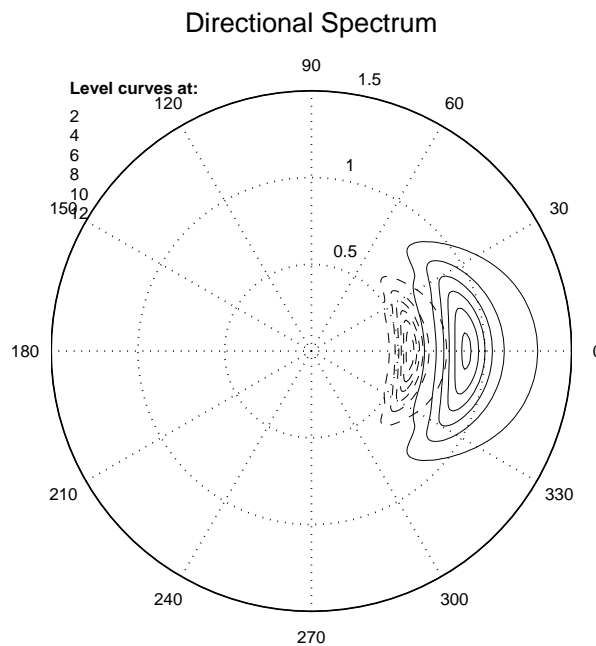


Figure 2.9: Directional spectrum `SJd` of JONSWAP sea (dashed line) compared with the encountered directional spectrum `SJe` for heading sea, speed 10 [m/s] (solid line).

**Example 2.** (*Different forms of spectra*) In this example we have chosen a JONSWAP spectrum with parameters defined by significant wave height  $H_{m0} = 7$  [m] and peak period  $T_p = 11$  [s]. This spectrum describes the measurements of sea level at a fixed point (buoy).

```

Hm0 = 7; Tp = 11;
SJ = jonswap([], [Hm0 Tp]);
SJ.note

```

<sup>4</sup>The dispersion relation between frequency  $\omega$  and wavenumber  $\kappa$  on finite water depth  $h$ , reads  $\omega^2 = g\kappa \tanh h\kappa$ , where  $g$  is the acceleration of gravity.

In order to include the space dimension, i.e. the direction in which the waves propagate, we compute a directional spectrum by adding spreading; see dashed curves in Figure 2.9.

```
D = spreading(101,'cos2s',0,[],SJ.w,1)
SJd = mkdspec(SJ,D) % Directional spectrum
```

Next, we consider a vessel moving with speed 10[m/s] against the waves. The sea measured from the vessel will have a different directional spectrum, called the encountered directional spectrum. The following code will compute the encountered directional spectrum and plot it on top of the original spectrum. The result is shown as the solid curves in Figure 2.9.

```
SJe = spec2spec(SJd,'encdir',0,10); % Encountered dir spectrum
plotspec(SJe), hold on
plotspec(SJd,1,'--'), hold off
```

Obviously, the periods of waves in the directional sea are defined by the JONSWAP spectrum (in a linear wave model spreading does not affect the sea level at a fixed point), but the encountered periods will be shorter with heading seas. This can be seen by comparing the original JONSWAP spectrum SJ with the following two point spectra.

```
SJd1 = spec2spec(SJd,'freq'); % Point spectrum from dir spectrum
SJd2 = spec2spec(SJe,'enc'); % Point encountered spectrum at ship
plotspec(SJ), hold on
plotspec(SJd1,1,'.'),
plotspec(SJd2), hold off
```

We can see in Figure 2.10(a) that the spectra SJ and SJd1 are identical (in numerical sense), while spectrum SJd2 contains more energy at higher frequencies.

A similar question is how much the wave length differs between a longcrested JONSWAP sea and a JONSWAP sea with spreading. The answer lies in the *wavenumber spectrum* that measures how the wave energy is distributed over different wavenumbers, i.e. radians (or cycles) per unit length along a specified direction, usually the main wave direction.

The wavenumber spectra along the main wave direction can be computed by the following code, the result of which is shown in Figure 2.10(b).

```
SJk = spec2spec(SJ,'k1d') % Unidirectional waves
SJkd = spec2spec(SJd,'k1d') % Waves with directional spreading
plotspec(SJk), hold on
plotspec(SJkd,1,'--'), hold off
```

We see how the spreading of energy away from the main direction makes observed waves longer. The total energy is of course the same but shifted to lower wavenumbers.

Finally, we shall show how the JONSWAP spectrum can be corrected for a finite depth, see [17] for a theoretical and empirical study. The WAFO function `phi1` computes the frequency dependent reduction of the spectrum for waters of finite depth, here 20 meters.

```
plotspec(SJ,1,'--'), hold on
SJ20 = SJ;
SJ20.S = SJ20.S.*phi1(SJ20.w,20); % Finite depth correction
SJ20.h = 20;
plotspec(SJ20), hold off
```

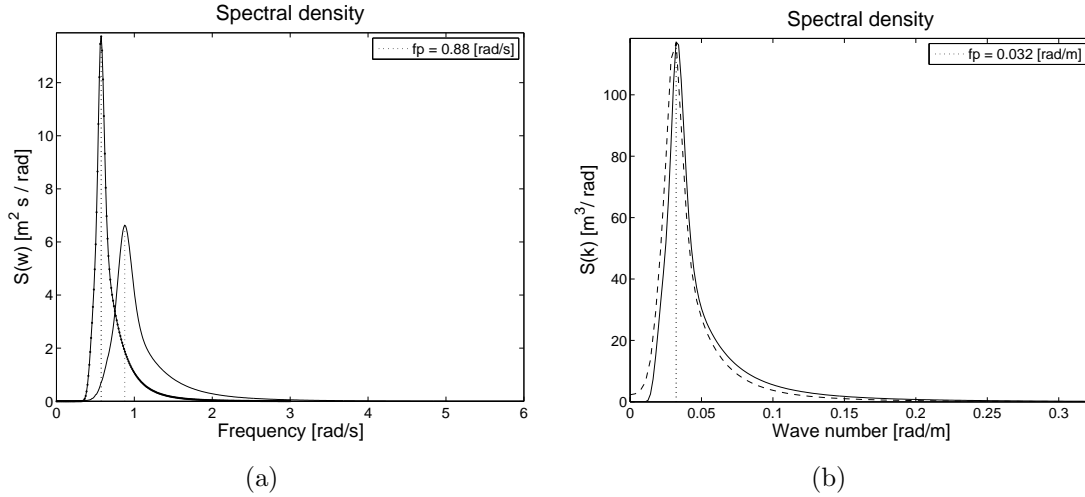


Figure 2.10: (a) Frequency JONSWAP spectrum SJ and point spectrum SJd1 compared with encountered point spectrum SJd2 for heading sea speed 10 [m/s] (solid line). (b) Wavenumber spectrum SJk for longcrested JONSWAP sea (solid line) compared with wavenumber spectrum SJkd for JONSWAP with spreading (dashed).

The resulting spectra are shown in Figure 2.11. □

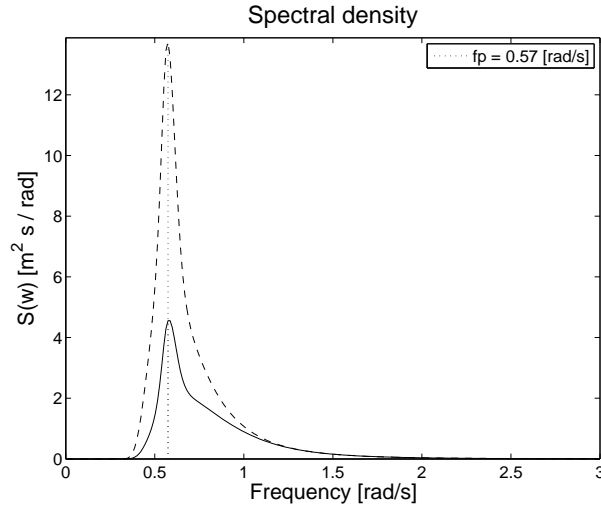


Figure 2.11: Standard JONSWAP spectrum SJ (dashed line) compared with the spectrum SJ20 on finite depth of 20 [m] (solid line)

## 2.3 Simulation of transformed Gaussian process

In this section we shall present some of the programs that can be used to simulate the transformed Gaussian model for sea  $X(t) = G(\tilde{X}(t))$ . In WAFO there are several other programs to simulate random functions or surfaces, both Gaussian and non-Gaussian; use `help simtools`. We give examples of some of these functions in Section 2.4.

The first important case is when we wish to reproduce random versions of the measured signal  $x(t)$ . Using `dat2tr` one first estimates the transformation  $g$ . Next, using a



function `dat2gaus` one can compute  $\tilde{x}(t) = g(x(t))$ , which we assume is a realization of a Gaussian process. From  $\tilde{x}$  we can then estimate the spectrum  $\tilde{S}(\omega)$  by means of the function `dat2spec`. The spectrum  $\tilde{S}(\omega)$  and the transformation  $g$  will uniquely define the transformed Gaussian model. A random function that models the measured signal can then be obtained using the simulation program `spec2sdat`, which includes the desired transformation. In the following example we shall illustrate this approach on the data set `sea.dat`.

Before we can start to simulate we need to put the transformation into the spectrum data structure, which is a MATLAB structure variable; see Section 1.6, page 17. Since WAFO is based on transformed Gaussian processes the entire process structure is defined by the spectrum and the transformation together. Therefore the transformation has been incorporated, as part of a model, into the spectrum structure, and is passed to other WAFO programs via the spectrum. If no transformation is given then the process is Gaussian.

Observe that the possibly nonzero mean `m` for the model is included in the transformation. The change of mean by for example 0.5 [m] is simply accomplished by modifying the transformation by the command `g(:,2) = g(:,2)+0.5`; Consequently the spectrum structure completely defines the model.

**IMPORTANT NOTE 1:** When the simulation routine `spec2sdat` is called with a spectrum argument that contains a scale changing transformation `spectrum.tr`, then it is assumed that the input spectrum is standardized with spectral moment  $m_0 = 1$ , i.e. unit variance. The correct standard deviation for the output should normally be obtained via the transformation `spectrum.tr`. If you happen to use a transformation *together with* an input spectrum that does not have unit variance, then you get the double scale effect, both from the transformation and via the standard deviation from the spectrum. It is only the routine `spec2sdat` that works in this way. All other routines, in particular those which calculate cycle distributions, perform an internal normalization of the spectrum before the calculation, and then transforms back to the original scale at the end.

**IMPORTANT NOTE 2:** When you run the simulation examples with different time horizon and time step you may experience a warning

'Spectrum matrix is very large'.

This is a warning from the WAFO routine `specinterp`, which is used internally to adapt the spectrum to the correct Nyquist frequency and frequency resolution. You can turn off the warning by commenting out three lines in `specinterp` in the `spec` module.

**Example 3.** (*Simulation of a random sea*) In Example 1 on page 21 we have shown that the data set `xx = sea.dat` contains a considerable amount of spurious points that we would like to omit or censor.

The program `reconstruct` replaces the spurious data by synthetic data. The new data points are obtained by simulation of a conditional Gaussian vector, based on the remaining data, taking the fitted transformed Gaussian process model into account; see [12, 14] for more details. The reconstruction is performed as

```
[y grec] = reconstruct(xx,inds);
```

where `y` is the reconstructed data and `grec` is the transformation estimated from the signal `y`. In Figure 2.12 we can see the transformation (solid line) compared with the empirical

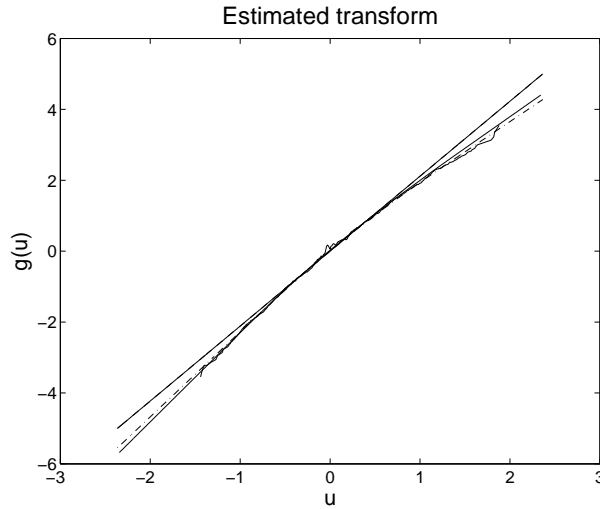


Figure 2.12: The transformation computed from the reconstructed signal  $y$  (solid line) compared with the transformation computed from the original signal  $xx$  (dashed dotted line).

smoothed transformation, `glc`, which is obtained from the original sequence  $xx$  without removing the spurious data (dash-dotted line). We can see that the new transformation has slightly smaller crests. Actually, it is almost identical with the transformation `gh` computed from the spectrum of the signal, however, it may be only a coincident (due to random fluctuations) and hence we do not draw any conclusions from this fact.

The value of the `test` variable for the transformation `grec` is 0.84 and, as expected, it is smaller than the value of `test0` = 1.00 computed for the transformation `glc`. However, it is still significantly larger than the values shown in Figure 2.7, i.e. the signal  $y$  is not a Gaussian signal.

We turn now to estimation of the spectrum in the model from the simulated data but first we transform data to obtain a sample  $\tilde{x}(t)$ :

```
L = 200
x = dat2gaus(y,grec); %Gaussian process from reconstructed data
SSx = dat2spec(x,L); %Spectrum from Gaussian reconstructed process
```

The important remark here is that the smoothing of the spectrum defined by the parameter `L`, see `help dat2spec`, removes almost all differences between the spectra in the three signals  $xx$ ,  $y$ , and  $x$ . (The spectrum `SSx` is normalized to have first spectral moment one and has to be scaled down to have the same energy as the spectrum `SS1` on page 26.)

Next, we shall simulate a random function equivalent to the reconstructed measurements  $y$ . The Nyquist frequency gives us the time sampling of the simulated signal,

```
dt = spec2dt(Sx)
```

and is equal to 0.25 seconds, since the data has been sampled with a sampling frequency of 4 Hz. We then simulate 2 minutes ( $2 \times 60 \times 4$  points) of the signal, to obtain a synthetic wave equivalent to the reconstructed non-Gaussian sea data.

```
Ny = fix(2*60/dt) % = two minutes
SSx.tr = grec;
```

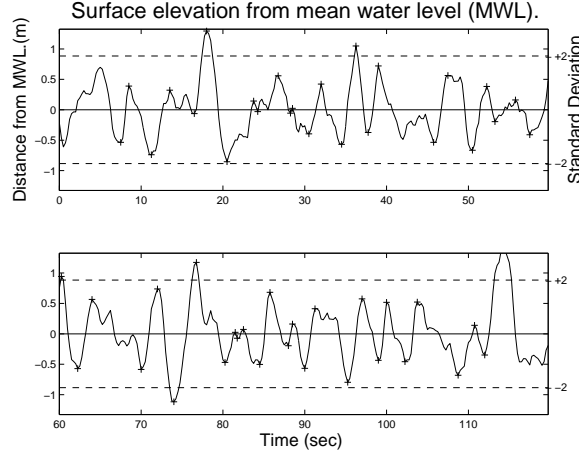


Figure 2.13: Two minutes of simulated sea data, equivalent to the reconstructed data.

```
ysim = spec2sdat(SSx,Ny);
waveplot(ysim,'-')
```

The result is shown in Figure 2.13. □

In the next example we consider a signal with a given theoretical spectrum. Here we have a problem whether the theoretical spectrum is valid for the transformed Gaussian model, i.e. it is a spectrum  $S(\omega)$  or is it the spectrum of the linear sea  $\tilde{S}$ . In the previous example the spectrum of the transformed process was almost identical with the normalized spectrum of the original signal. In [73] it was observed that for sea data the spectrum estimated from the original signal and that for the transformed one do not differ significantly. Although more experiments should be done in order to recommend using the same spectrum in the two cases, here, if we wish to work with non-Gaussian models with a specified transformation, we shall derive the  $\tilde{S}$  spectrum by dividing the theoretical spectrum by the square root of the first spectral moment of  $S$ .

**Example 3. (contd.)** Since the spectrum SS1 in Figure 2.4 is clearly two-peaked with peak frequency  $T_p = 1.1$  [Hz] we choose to use the Torsethaugen spectrum. (This spectrum is derived for a specific location and we should not expect that it will work well for our case.) The inputs to the programs are  $T_p$  and  $H_s$ , which we now compute.

```
Tp = 1.1;
H0 = 4*sqrt(spec2mom(S1,1))
ST = torsethaugen([0:0.01:5],[H0 2*pi/Tp]);
plotspec(SS1), hold on
plotspec(ST,[],'-')
```

In Figure 2.14, we can see that the Torsethaugen spectrum has too little energy on the swell peak. Despite this fact we shall use this spectrum in the rest of the example.

We shall now create the spectrum  $\tilde{S}(\omega)$  ( $=$  STnorm), i.e. the spectrum for the standardized Gaussian process  $\tilde{X}(t)$  with standard deviation equal to one.

```
STnorm = ST;
```

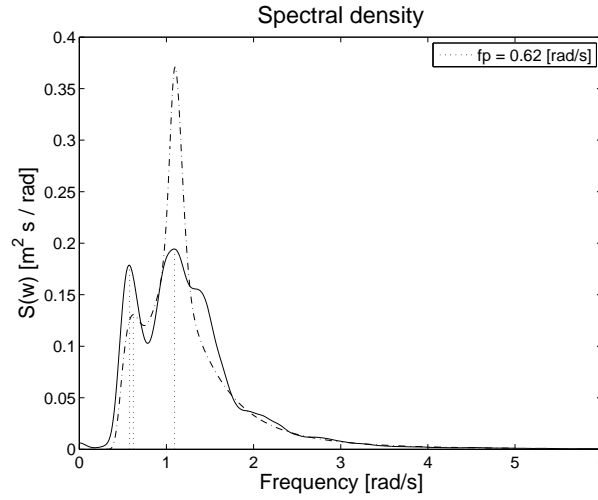


Figure 2.14: Comparison between the estimated spectrum  $SS1$  in the signal `sea.dat` (solid line) and the theoretical spectrum  $ST$  of the Torsethaugen type (dash-dotted line).

```
STnorm.S = STnorm.S/sa^2;
dt = spec2dt(STnorm)
```

The sampling interval  $dt = 0.63$  [s] ( $= \pi/5$ ), is a consequence of our choice of cut off frequency in the definition of the  $ST$  spectrum. This will however not affect our simulation, where any sampling interval  $dt$  can be used.

Next, we recompute the theoretical transformation `gh`.

```
[Sk Su] = spec2skew(ST);
sa = sqrt(spec2mom(ST,1));
gh = hermitetr([], [sa sk ku me]);
STnorm.tr = gh;
```

The transformation is actually almost identical to `gh` for the spectrum  $SS1$ , which can be seen in Figure 2.6, where it is compared to the Gaussian model `g`, given by a straight line. We can see from the diagram that the waves in a transformed Gaussian process  $X(t) = G(\tilde{X}(t))$ , will have an excess of high crests and shallow troughs compared to waves in the Gaussian process  $\tilde{X}(t)$ . The difference is largest for extreme waves with crests above 1.5 meters, where the excess is 10 cm, ca 7 %. Such waves, which have crests above three standard deviations, are quite rare and for moderate waves the difference is negligible.

In order to illustrate the difference in distribution for extreme waves we will simulate a sample of 4 minutes of  $X(t)$  with sampling frequency 2 Hz. The result is put into `ysim_t`. In order to obtain the corresponding sample path of the process  $\tilde{X}$  we use the transformation `gh`, stored in `STnorm.tr`, and put the result in `xsim_t`.

```
dt = 0.5;
ysim_t = spec2sdat(STnorm,240,dt);
xsim_t = dat2gaus(ysim_t,STnorm.tr);
```

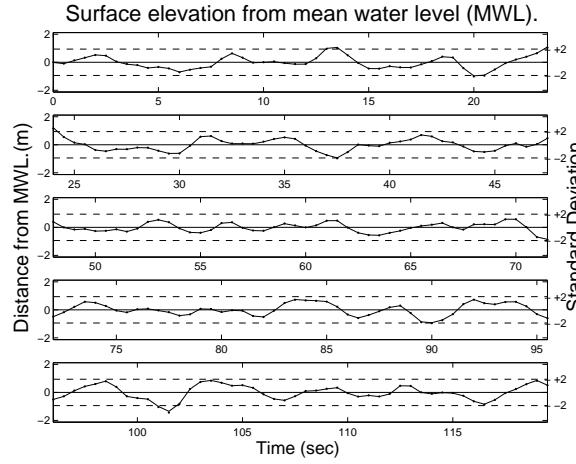


Figure 2.15: Simulated  $X(t) = G(\tilde{X}(t))$  (solid line) compared with  $\tilde{X}(t)$  (dots) scaled to have the same  $H_s$  as  $X(t)$  for a theoretical spectrum given by Torsethaugen spectrum **St**.

Since the process  $\tilde{X}(t)$  always has variance one, in order to compare the Gaussian and non-Gaussian models we scale `xsim_t` to have the same second spectral moment as `ysim_t`, which will be done by the following commands:

```
xsim_t(:,2) = sa*xsim_t(:,2);
waveplot(xsim_t,ysim_t,5,1,sa,4.5,'r.','b')
```

In Figure 2.15 we have waves that are not extremely high and hence the difference between the two models is hardly noticeable in this scale. Only in the second subplot we can see that Gaussian waves (dots) have troughs deeper and crests lower than the transformed Gaussian model (solid line). This also indicates that the amplitude estimated from the transformed Gaussian and Gaussian models are practically identical. Using the empirical transformation `glc` instead of the Hermite transformation `gh` would give errors of ca 11%, which for waves with higher significant wave height would give considerable underestimation of the crest height of more extreme waves. Even if the probability for observing an extreme wave during the period of 20 minutes is small, it is not negligible for safety analysis and therefore the choice of transformation is one of the most important questions in wave modelling.

Since the difference between Gaussian and non-Gaussian model is not so big we may ask whether 20 minutes of observation of a transformed Gaussian process presented in this example is long enough to reject the Gaussian model. Using the function `testgaussian` we can see that rejection of Gaussian model would occur very seldom. Observe that the `sea.dat` is 40 minutes long and that we clearly rejected the Gaussian model.  $\square$

## 2.4 More on simulation with WAFO

The WAFO toolbox contains additional routines for simulation of random loads and random waves. One important class used in fatigue analysis and in modelling the long term variability of sea state are the Markov models, in which the model parameters are allowed

to switch to new values according to a Markov chain. Another group of simulation routines generate non-linear waves and loads, like second order Stokes waves with interaction between frequency components in the Gaussian wave model, and Lagrange waves, with a horizontal deformation of space. This group includes a program to simulate the output of second order oscillators with nonlinear spring, when external force is white noise. The nonlinear oscillators can be used to model nonlinear responses of sea structures.

### 2.4.1 Markov models

The following routines from the `simtools` module can be used to generate realistic load sequencies for for reliability and fatigue analysis; see more in Chapter 5.

`lc2sdat` Simulates a load process with specified crossing spectrum and irregularity

`mcsim` Simulates a finite Markov chain from its probability transition matrix

`mctpsim` Simulates a Markov chain of turning points from transition matrix

`sarmasim` Simulates an ARMA time series with Markov switching parameters

`smcsim` Simulates a Markov chain with Markov switching regime

**Example 4. (Switching ARMA model)** In many applications, the standard stationary time series Auto-regressive/Moving average ARMA-model, [45, Ch. 7], can be made more realistic if the parameters are allowed to change with time, according to abrupt changes in environment conditions. Examples are found in econometrics [25], climate and environmental research [4], automotive safety [32], and many other areas. A special case are the *Hidden Markov models* where the changes occur according to an (unobserved) Markov chain

The WAFO routine `sarmasim` was developed by Johannesson [32] in order to find a good model for stress loads on a truck serving on an irregular scheme, loading and unloading gravel. The following example from `sarmasim` illustrates the principles on an ARMA(4,2)-process swithching by a Markov *regime process* between two states.

```
p1 = 0.005; p2=0.003; % Switching probabilities
P = [1-p1 p1; p2 1-p2]; % Markov transition matrix
C = [1.00 1.63 0.65; 1.00 0.05 -0.88]; % MA-parameters
A = [1.00 -0.55 0.07 -0.26 -0.02; ...
     1.00 -2.06 1.64 -0.98 0.41]; % AR-parameters
m = [46.6; 7.4]*1e-3; % Mean values for sub-processes
s2 = [0.5; 2.2]*1e-3; % Innovation variances
[x,z] = sarmasim(C,A,m,s2,P,2000); % Simulate 2000 steps
plothmm(x,z) % Plotting
% x = Switching ARMA, z = Markov regime process
```

Figure 2.16 shows the hidden Markov states and the, seemingly non-stationary, ARMA-process. In fact, the Markov chain is simulated from its stationary distribution and each ARMA-section starts with the stationary distribution for that particular ARMA-process, so the process is stationary!  $\square$

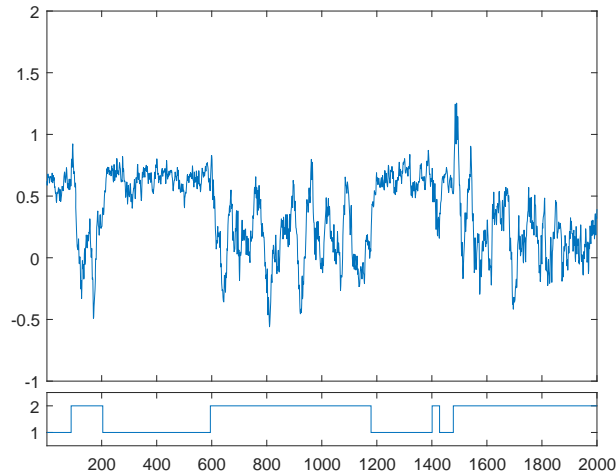


Figure 2.16: Switching ARMA-process with Markov regime process.

### 2.4.2 Space-time and non-linear waves and loads

The following routines in modules `simtools` and `lagrange` generate continuous time series and continuous space-time realizations.

`duffsim` Generates a sample path of a linear or non-linear random oscillator

`spec2wave` and `spec2field` Generate samples of space-time (transformed) 2D and 3D Gaussian waves

`seamovie` Makes a movie in time of 2D or 3D random waves and optionally exports movie in avi format

`seasim` Old routine that generates a space-time Gaussian process and movie with 1D or 2D space parameter

`spec2l1dat` and `spec2l1dat3D` Routines in module `lagrange` that generate front-back and crest-trough asymmetric modifications of Gaussian wave fields

`spec2nl1dat` Simulates a random 2nd order non-linear wave from a spectral density

**Example 5.** (*How to export a sea movie*) In Section 1.4.3 we gave an example of how to use `spec2field` to generate and plot a Gaussian sea surface with directional spreading. We now show how to use `seamovie` to generate and save a movie of the time evolution of the sea.

We define and plot the `demospec` spectrum, with frequency independent spreading

```
SD = demospec('dir')
plotspec(SD)
```

to get Figure 2.17 and the structure

```
SD =
  struct with fields:
    S: [101 x 257 double]
    w: [257 x 1 double]
```

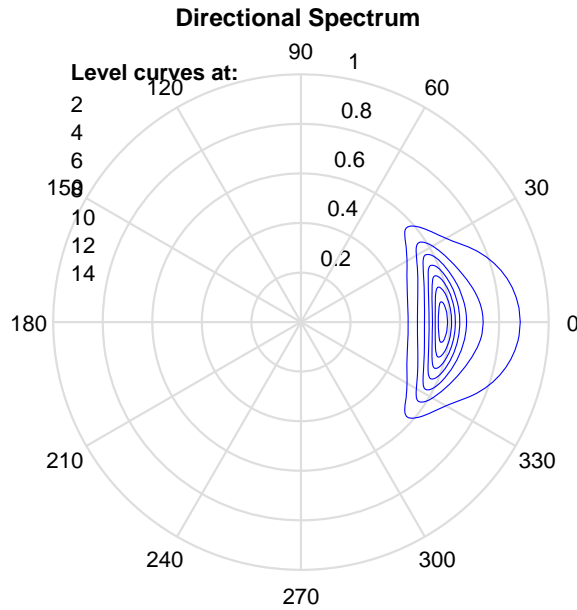


Figure 2.17: Directional spectrum demospec

```
theta: [101 x 1 double]
tr: []
h: Inf
type: 'dir'
phi: 0
norm: 0
note: 'Demospec: JONSWAP, Hm0 = 7, Tp = 11, gamma = 2.3853; Sprea...'
```

To generate two minutes of a wave field of size 500[m] by 250[m] we define parameters by the function `simoptset`, generate the field with `spec2field`, and make three different types of movies with `seamovie`.

```
opt = simoptset('Nt',600,'dt',0.2,'Nu',501,'du',1,'Nv',251,'dv',1)
rng('default')
W = spec2field(SD,opt); % structure with fields .Z, .x, .y, .t
figure(2); Mv2 = seamovie(W,2); pause
figure(3); Mv3 = seamovie(W,3); pause
figure(1); Mv1 = seamovie(W,1,'sea.avi')
```

The last movie command saves the movie as `sea.avi` in the working directory. If `sea.avi` already exists, the new movie file is given a random name.  $\square$

**Remark 2.2.** The wave fields generated by `spec2field` differ from animated wave fields used for example in feature films. They are intended to be used in applications where the fine structure, so important for the visual impression, can be neglected. Examples involve extreme value analysis, fatigue loads, and ship dynamics.  $\square$



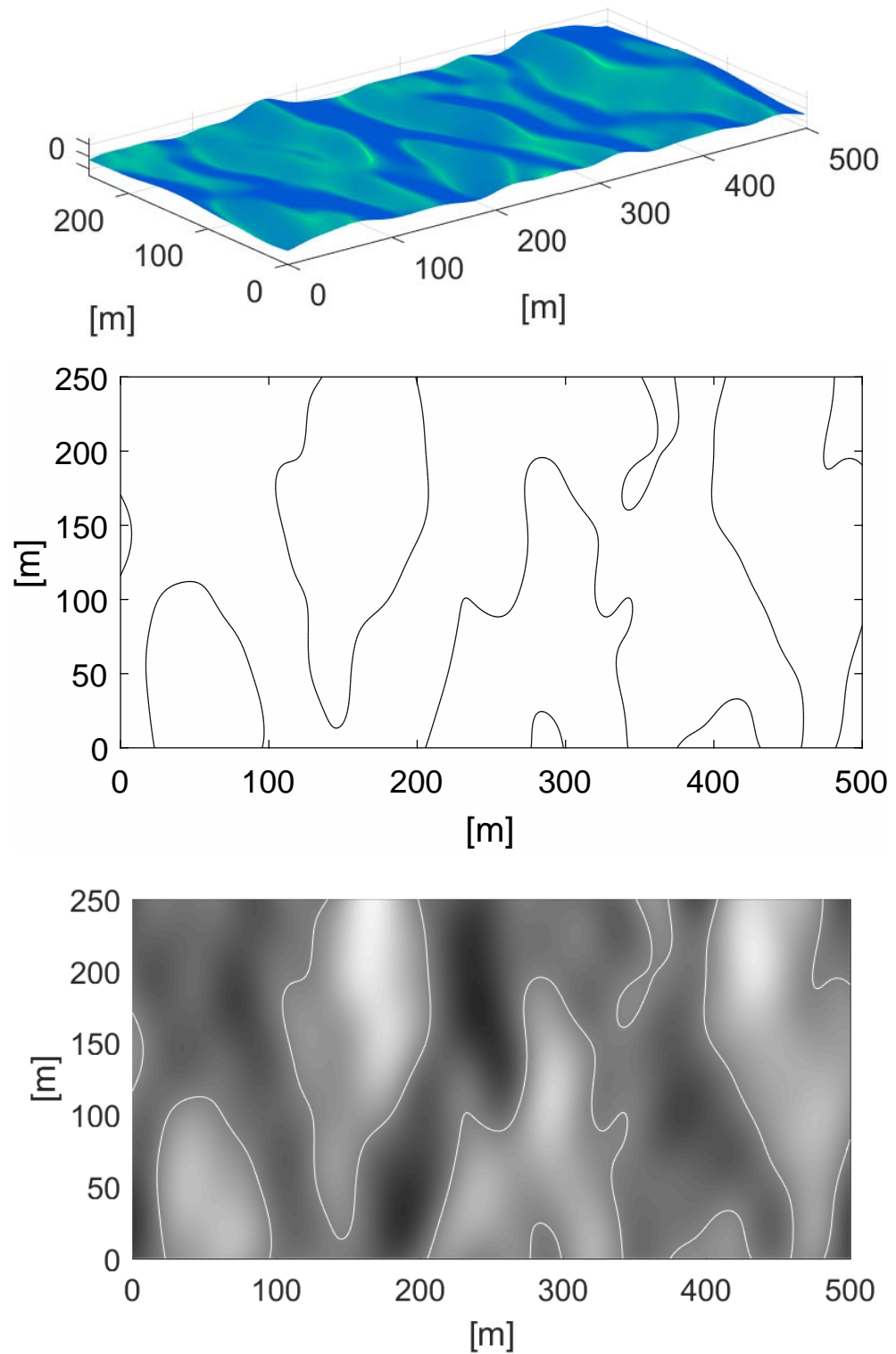


Figure 2.18: Three aspects of a simulated Gaussian wave field with directional spectrum `demospec('dir')`; last frames in `Mv1`, `Mv1`, and `Mv3`.

### 2.4.3 Structure of spectral simulation

The following table explains the sequencing of spectral simulation routines in modules `simtools` and `lagrange`. A (freq) or (dir) indicates the type of input spectrum.

| 1 <sup>st</sup> and 2 <sup>nd</sup> order Gaussian waves in module <code>simtools</code> |                                                        |                                                      |                                                       |                                                   |
|------------------------------------------------------------------------------------------|--------------------------------------------------------|------------------------------------------------------|-------------------------------------------------------|---------------------------------------------------|
| Routine                                                                                  | spec2sdat                                              | spec2wave                                            | spec2field                                            | spec2nlsdat                                       |
| Type                                                                                     | 1 <sup>st</sup> order Gaussian<br>time or space series | 1 <sup>st</sup> order Gaussian<br>2D space-time wave | 1 <sup>st</sup> order Gaussian<br>3D space-time field | 2 <sup>nd</sup> order Gauss-Euler<br>2D time wave |
| Output                                                                                   | ↓<br>[x,xder]                                          | ↓<br>W.Z, .x, .t                                     | ↓<br>W.Z, .x, .y, .t                                  | ↓<br>[xs2,xs1]                                    |
| Movie                                                                                    |                                                        | M = seamovie(W,type)                                 | M = seamovie(W,type)                                  |                                                   |

| 1 <sup>st</sup> and 2 <sup>nd</sup> order Lagrange waves in module <code>lagrange</code> |                                                            |                                                  |                                                            |                                                            |
|------------------------------------------------------------------------------------------|------------------------------------------------------------|--------------------------------------------------|------------------------------------------------------------|------------------------------------------------------------|
| Routine                                                                                  | spec2l1dat (freq)                                          | spec2l1series (dir)                              | spec2l1dat3D (dir)                                         | spec2l1dat3DM/P                                            |
| Type                                                                                     | 1 <sup>st</sup> order Lagrange 2D<br>space/time components | 1 <sup>st</sup> order Lagrange 2D<br>time series | 1 <sup>st</sup> order Lagrange 3D<br>space/time components | 2 <sup>nd</sup> order Lagrange 3D<br>space/time components |
| Output                                                                                   | ↓<br>[w,x]                                                 | ↓<br>L.Z, .t, .points                            | ↓<br>[w,x,y]                                               | ↓<br>[w,x,y,w2,x2,y2]                                      |
| Series/field                                                                             | ↓<br>L = ldat2lwav                                         | ↓<br>—                                           | ↓<br>L = ldat2lwav3D                                       | ↓<br>L = ldat2lwav3D                                       |
| Movie                                                                                    | M = seamovie(L,type)                                       | M = seamovie(L,type)                             | M = seamovie(L,type)                                       | M = seamovie(L,type)                                       |

## CHAPTER 3

# Empirical wave characteristics

---

One of the unique capabilities of WAFO is the treatment of the statistical properties of wave characteristic. This, and the next chapter, describe how to extract information on distributions of observables like wave period, wave length, crest height, etc, either directly from data, or from empirically fitted approximative models, or, in the next chapter, by means of exact statistical distributions, numerically computed from a spectral model.

We first define the different wave characteristics commonly used in oceanographic engineering and science, and present the WAFO routines for handling them. Then we compare the empirical findings with some approximative representations of the statistical distributions, based on empirical parameters from observed sea states. The code for the examples are found in the m-file `Chapter3.m`, and it takes a few seconds to run.

### 3.1 Introduction

#### 3.1.1 The Gaussian paradigm - linear wave theory

In the previous chapter we discussed modelling of random functions by means of Fourier methods. The signal was represented as a sum of independent random cosine functions with random amplitudes and phases. In linear wave theory those cosine functions are waves travelling in water. Waves with different frequencies have different speeds, defined by the dispersion relation. This property causes the characteristic irregularity of the sea surface. Even if it were possible to arrange a very particular combination of phases and amplitudes, so that the signal looks, for example, like a saw blade, it will, after a while, change shape totally. The phases will be almost independent and the sea would again look like a Gaussian random process. On the other hand an observer clearly can identify moving sea waves. The shape of those waves, which are often called the *apparent* waves, since theoretically, those are not mathematical waves, but are constantly changing up to the moment when they disappear.

The wave action on marine structures is often modelled using linear filters. Then the sea spectrum, together with the filter frequency function, gives a complete characterization of the response of the structure. However, often such models are too simplistic and non-linearities have to be considered to allow more complex responses. Then one may not

wish to perform a complicated numerical analysis to derive the complete response but is willing to accept the simplification that the response is proportional to the waves. One may also wish to identify some properties of waves that are dangerous in some way for the particular ocean operation. Also the apparent waves themselves can be the reason for non-linear response. For example, for waves with crests higher than some threshold, water may fill a structure and change its dynamical properties. The combined effect of apparent waves, often described by their height and wave period, is therefore important in ocean engineering. These aspects are discussed in more detail in the textbook [60].

The apparent waves will be described by some geometric properties, called wave characteristics, while frequencies of occurrences of waves with specified characteristics will be treated in the statistical sense and described by a probability distribution. Such distributions can then be used to estimate the frequency of occurrences of some events important in the design of floating marine systems, e.g. wave breaking, slamming, ringing, etc.

### 3.1.2 Wave characteristics in time and space

The wave surface is clearly a two-dimensional phenomenon that changes with time and its study naturally deals with moving two-dimensional objects (surfaces). Theoretical studies of random surfaces are the subject of ongoing research, for example, [6, 55], for general studies of Gaussian random surfaces, [2, 3, 7, 8, 65, 81, 82], for space-time related wave results, and [62] for wave geometry. Related results for Lagrange models are found in [1, 37, 38, 39, 42, 43].

At present, there are only few programs in WAFO that handle the space-time relations of waves, and hence in this tutorial we limit the presentation to simpler cases of waves in one-dimensional records.<sup>1</sup> By this we mean the apparent waves extracted from functions (measured signals) with one-dimensional parameter, either in time or in space. These functions can be extracted from a photograph of the sea surface as, for example, the *instantaneous profile* along a line in some fixed horizontal direction on the sea, or they can be obtained directly as a *record taken in time at a fixed position in space* as by means of a wave pole or distance meter. The *encountered sea*, another important one-dimensional record, can be collected by means of a ship-borne wave recorder moving across the random sea.

To analyze collected wave data we need natural and operational definitions of an individual wave, its period, height, steepness, and possibly some other meaningful characteristics. There are several possible definitions of apparent wave, and here we shall concentrate mostly on zero down-crossing waves. Namely, the *apparent individual wave* at a fixed time or position is defined as the part of the record that falls between two consecutive down-crossings of the zero seaway level (the latter often more descriptively referred to as the still water level). For individual waves one can consider various natural characteristics, among them *apparent periods* and *apparent heights (amplitudes)*. The pictorial definitions of these characteristics are given in Figure 3.1.

The definitions of the most common wave characteristics are given in Table 3.1. In the WAFO toolbox, the most important can be retrieved by the help commands for `wavedef`, `perioddef`, `ampdef`, and `crossdef`, producing the output in Section 3.4.

---

<sup>1</sup>The Lagrange module in WAFO contains special space-time routines for (Gaussian and) non-Gaussian waves; a tutorial is included in that module.

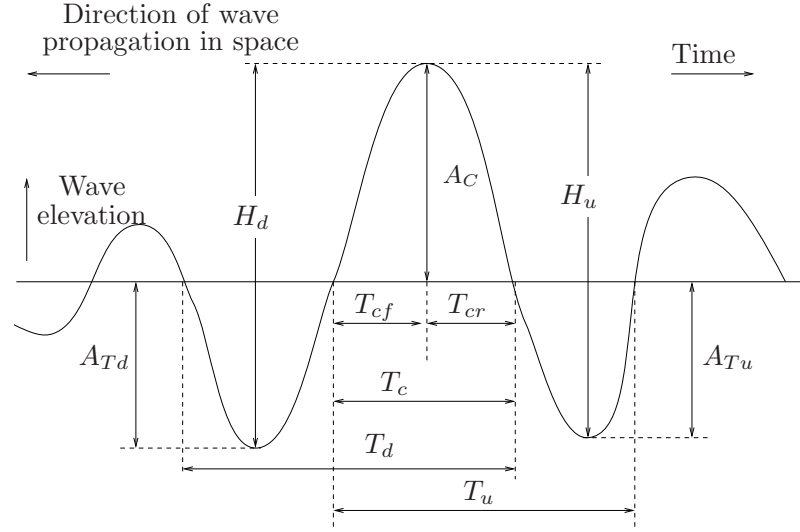


Figure 3.1: Definition of wave parameters. The notation for the parameters used in our examples are given in Table 3.1 at the end of this chapter.

Having precisely defined the characteristics of interest, one can extract their frequency (empirical) distributions from a typical sufficiently long record. For example, measurements of the apparent period and height of waves could be taken over a long observation interval to form an empirical two-dimensional distribution. This distribution will represent some aspects of a given sea surface. Clearly, because of the irregularity of the sea, empirical frequencies will vary from record to record. However if the sea is in “steady” condition, which corresponds mathematically to the assumption that the observed random field is stationary and ergodic, their variability will be insignificant for sufficiently large records. Such limiting distributions (limiting with respect to observation time, for records measured in time, increasing without bound) are termed the *long-run distributions*. Obviously, in a real sea we seldom have a so long period of “steady” conditions that the limiting distribution will be reached. On average, one may observe 400-500 waves per hour of measurements, while the stationary conditions may last from 20 minutes to only a few hours.

Despite of this, a fact that makes these long-run distributions particularly attractive is that they give probabilities of occurrence of waves that may not be observed in the short records but still are possible. Hence, one can estimate the intensity of occurrence of waves with special properties and then extrapolate beyond the observed types of waves. What we shall be concerned with next is how to compute such distributional properties.

In the following we shall consider three different ways to obtain the wave characteristic probability densities (or distributions):

- To fit an empirical distribution to observed (or simulated) data in some parametric family of densities, and then relate the estimated parameters to some observed wave climate described by means of significant wave height and wave period. Algorithms to extract waves, estimate the densities and compute some simple statistics will be presented here in Chapter 3
- To simplify the model for the sea surface to such a degree that explicit computation

of wave characteristic densities (in the simplified model) is possible. Some examples of proposed models from the literature will also be given in this chapter.

- To exactly compute the statistical distribution from the mathematical form of a random seaway. This requires computation of infinite dimensional integrals and expectations that have to be computed numerically. WAFO contains efficient numerical algorithms to compute these integrals, algorithms which do not require any particular form of the sea surface spectrum. The methods are illustrated in Chapter 4 on period, wavelength, and amplitude distributions, for many standard types of wave spectra.

## 3.2 Estimation of wave characteristics from data

In this section we shall extract the wave characteristics from a measured signal and then use non-parametric statistical methods to describe the data, i.e. empirical distributions, histograms, and kernel estimators. (In the last chapter of this tutorial we present some statistical tools to fit parametric models; for kernel estimators, see Appendix A.)

It is generally to be advised that, before analyzing sea wave characteristics, one should check the quality of the data by inspection and by the routine `findoutliers` used in Section 2.1. Then, one usually should remove any present trend from the data. Trends could be due to tides or atmospheric pressure variations that affect the mean level. Detrending can be done using the WAFO functions `detrend` or `detrendma`.

### 3.2.1 Wave period

**Example 1. (contd.)** We now continue the analysis of the shallow water waves in `sea.dat` that we started on page 20. We begin with extracting the apparent waves and record their period. The signal `sea.dat` is recorded at 4 Hz sampling frequency. One of the possible definitions of period is the time between the consecutive wave crests. For this particular variable it may be convenient to have a higher resolution than 4 Hz and hence we shall interpolate the signal to a denser grid. This will be obtained by giving an appropriate value to the variable `rate` which can be used as input to the WAFO routine `dat2wa`. The following code will return crest2crest wave periods  $T_{cc}$  in the variable `Tcrcr` and return the crest period  $T_c$  in `Tc`, i.e. the time from up-crossings to the following down-crossing.

```
xx = load('sea.dat');
xx(:,2) = detrend(xx(:,2));
rate = 8;
Tcrcr = dat2wa(xx,0,'c2c','tw',rate);
Tc = dat2wa(xx,0,'u2d','tw',rate);
```

Next we shall use a kernel density estimator (KDE) to estimate the probability density function (pdf) of the crest period and compare the resulting pdf with a histogram of the observed periods stored in `Tc`. In order to define a suitable scale for the density we first compute the mean and maximum of the observed crest periods.

```
mean(Tc)
```

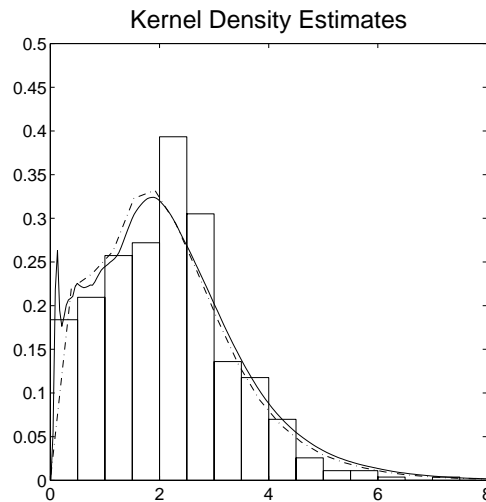


Figure 3.2: Kernel estimate of crest period density observed in `sea.dat`; solid line: full KDE, dash dotted line: binned KDE, compared with histogram of the data.

```
max(Tc)
t = linspace(0.01,8,200);
kopt = kdeoptset('L2',0);
ftc1 = kde(Tc,kopt,t);
pdfplot(ftc1), hold on
histgrm(Tc,[],[],1)
axis([0 8 0 0.5])
```

(The parameter `L2=0` is used internally in `kde`, and causes a logarithmic transformation of the data to ensure that the density is zero for negative values. Run `help kdeoptset` to see the definition.)

In Figure 3.2 we can see that many short waves have been recorded (due to relatively high sampling frequency). The kernel estimate will be compared with the theoretically computed density in Figure 4.6 in Chapter 4, page 80.  $\square$

**Remark 3.3.** Note that the program `kde` can be quite slow for large data sets. If a faster estimate of the density for the observations is preferred one can use `kdebin`, which is an approximation to the true kernel density estimator. An important input parameter in the program, that defines the degree of approximation, is `inc` which should be given a value between 100 and 500. (A value of `inc` below 50 gives fast execution times but can lead to inaccurate results.)

```
kopt.inc = 128;
ftc2 = kdebin(Tc,kopt); pdfplot(ftc2,'-.')
title('Kernel Density Estimates'), hold off
```

The result is in Figure 3.2  $\square$

### 3.2.2 Extreme waves – model check

We turn now to joint wave characteristics, e.g. the joint density of half period and crest height ( $T_c, A_c$ ), or waveheight and steepness ( $A_c, S$ ). The program `dat2steep` identifies apparent waves and for each wave gives several wave characteristics (use the help function on `dat2steep` for a list of computed variables). We begin by examining profiles of waves having some special property, e.g. with high crests, or that are extremely steep.

**Example 1. (contd.)** The following code finds a sequence of waves in `sea.dat` and extracts their characteristics:

```
method = 0; rate = 8;
[S, H, Ac, At, Tcf, Tcb, z_ind, yn] = ...
    dat2steep(xx,rate,method);
```

The first preliminary analysis of the data is to find the individual waves which are extreme by some specified criterion, e.g. the steepest or the highest waves, etc. To do such an analysis one can use the function `spwaveplot(xx,ind)`, which plots waves in `xx` that are selected by the index variable `ind`. For example, let us look at the highest and the steepest waves.

```
[Smax indS] = max(S)
[Amax indA] = max(Ac)
spwaveplot(yn,[indA indS], 'k.')
```

The two waves are shown in Figure 3.3(a). The shape of the biggest wave reminds of the so called "extreme" waves. In the following we shall examine whether this particular shape contradicts the assumption of a transformed Gaussian model for the sea.

This is done as follows. First we find the wave with the highest crest. Then we mark all positive values in that wave as missing. Next we reconstruct the signal, assuming the Gaussian model is valid, and compare the profile of the reconstructed wave with the actual measurements. Confidence bands for the reconstruction will also be plotted. In the previous chapter we have already used the program `reconstruct`, and here we shall need some additional output from that function, to be used to compute and plot the confidence bands.

```
inds1 = (5965:5974)'; Nsim = 10;
[y1, grec1, g2, test, tobs, mu1o, mu1oStd] = ...
    reconstruct(xx,inds1,Nsim);
spwaveplot(y1,indA-10), hold on
plot(xx(inds1,1),xx(inds1,2),'+')
lamb = 2.;
muLstd = tranproc(mu1o-lamb*mu1oStd,fliplr(grec1));
muUstd = tranproc(mu1o+lamb*mu1oStd,fliplr(grec1));
plot (y1(inds1,1), [muLstd muUstd], 'b-')
axis([1482 1498 -1 3]), hold off
```

(Note that we have used the function `tranproc` instead of `gaus2dat`, since the last function requires a two column matrix. Furthermore we have to use the index `indA-10` to identify



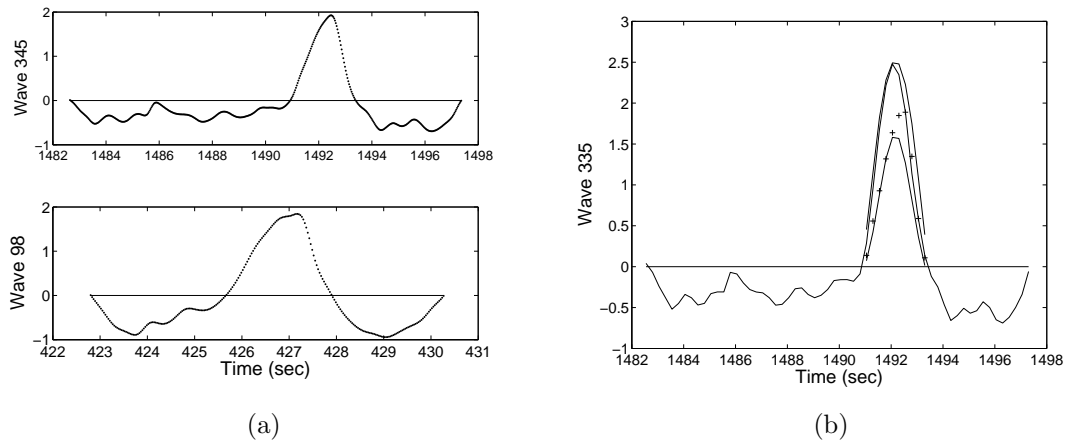


Figure 3.3: (a): Two waves, the highest and the steepest, observed in `sea.dat`. (b): Crosses are observations removed from the highest wave. The reconstructed wave, using transformed Gaussian model, is given by the middle solid line. Upper and lower curves give the confidence band defined as the conditional mean of the process plus minus two conditional standard deviations.

the highest wave in `y1`. This is caused by the fact that the interpolated signal `yn` has a few additional small waves that are not in `xx`.)

In Figure 3.3(b) the crosses are the removed values from the wave. The reconstructed wave, plotted by a solid line, is close to the measured. (Observe that this is a simulated wave, using the transformed Gaussian model, and hence each time we execute the command the shape will change.) The confidence bands gives limits containing 95% of the simulated values, pointwise. From the figure we can deduce that the highest wave could have been even higher and that the height is determined by the particularly high values of the derivatives at the zero crossings which define the wave. The observed wave looks more asymmetric in time than the reconstructed one. Such asymmetry is unusual for the transformed Gaussian waves but not impossible. By executing the following commands we can see that actually the observed wave is close to the expected in a transformed Gaussian model.

```
plot(xx(inds1,1),xx(inds1,2),'+'), hold on
mu = tranproc(mu1o,flipplr(grec1));
plot(y1(inds1,1), mu), hold off
```

We shall not investigate this question further in this tutorial. □

### 3.2.3 Crest height

We turn now to the kernel estimators of the crest height density. It is well known that for Gaussian sea the tail of the density is well approximated by the Rayleigh distribution. Wand and Jones (1995, Chap. 2.9) show that Gaussian distribution is one of the easiest distributions to obtain a good Kernel Density Estimate from. It is more difficult to find good estimates for distributions with skewness, kurtosis, and multi-modality. Here, one can get help by transforming data. This can be done choosing different values of input `L2` into the program `kde`.

**Example 1. (contd.)** We shall continue with the analysis of the crest height distribution. By letting  $L2 = 0.6$  we see that the normalplot of the transformed data is approximately linear. (Note: One should try out several different values for  $L2$ . It is also always good practise to try out several different values of the smoothing parameter; see the help text of `kde` and `kdebin` for further explanation.)

```
L2 = 0.6;
plotnorm(Ac.^L2)
fac = kde(Ac,{'L2',L2},linspace(0.01,3,200));
pdfplot(fac)
simpson(fac.x{1},fac.f)
```

The integral of the estimated density `fac` is 0.9675 but it should be one. Therefore, when we use the estimated density to compute different probabilities concerning the crest height the uncertainty of the computed probability is at least 0.03. We suspect that this is due to the estimated density being non-zero for negative values. In order to check this we compute the cumulative distribution using the formula,

$$P(Ac \leq h) = 1 - \int_h^{+\infty} f_{Ac}(x) dx,$$

where  $f_{Ac}(x)$  is the estimated probability density of  $Ac$ . For the pdf saved in `fac` the following code gives an estimate of the cumulative distribution function (cdf) for crest height and compares it with the empirical distribution computed from data by means of function `edf` or `plotedf`.

```
Fac = flipud(cumtrapz(fac.x{1},flipud(fac.f)));
Fac = [fac.x{1} 1-Fac];
Femp = plotedf(Ac,Fac);
axis([0 2 0 1]), hold off
```

Since a kernel density estimator KDE in essence is a smoothed histogram it is not very well suited for extrapolation of the density to the region where no data are available, e.g. for high crests. In such a case a parametric model should be used. In WAFO there is a function `trraylpdf` that combines the non-parametric approach of KDE with a Rayleigh density. Simply, if the Rayleigh variable can be used to describe the crests of Gaussian waves then a transformed Rayleigh variable should be used for the crests of the transformed Gaussian waves. The method has several nice properties and will be described more in Section 3.3.3. Here we just use it in order to compare with the non-parametric KDE method.

```
facr = trraylpdf(fac.x{1},'Ac',grec1);
Facr = cumtrapz(facr.x{1},facr.f); hold on
plot(facr.x{1},Facr,'.')
axis([1.25 2.25 0.95 1]), hold off
```

Figure 3.4(a) shows that our hypothesis that the pdf `fac` is slightly too low for small crests seems to be correct. Next from Figure 3.4(b) we can see that also the tail is reasonably well modelled even if it is lighter than, i.e. gives smaller probabilities of high waves than, the one derived from the transformed Gaussian model.  $\square$

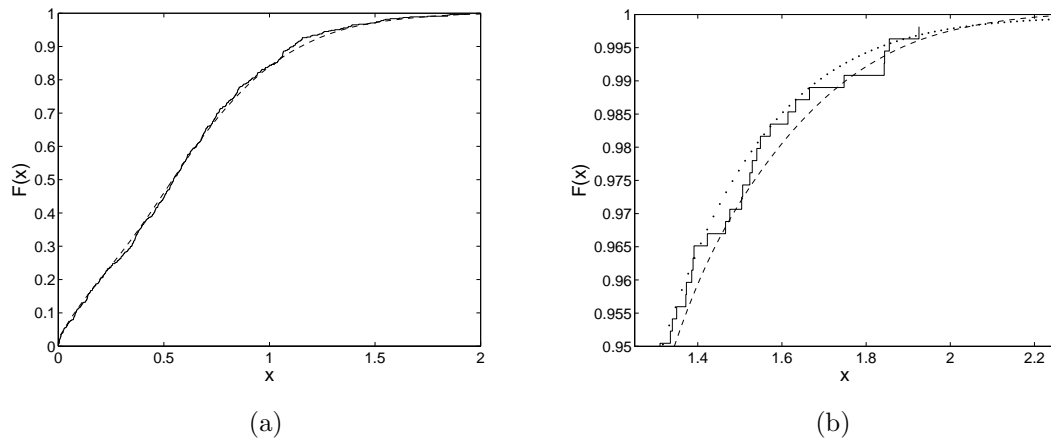


Figure 3.4: (a) Comparison of the empirical distribution of the crest height with the cumulative distribution computed from the KDE estimator. (b) Zooming in on the tails of distributions in (a) together with the tail of the transformed Rayleigh approximation (dots) to the crest height distribution.

### 3.2.4 Joint crest period and crest height distribution

We shall use the kernel density estimator to find a good estimator of the central part of the joint density of crest period and crest height. Usually, kernel density estimators give poor estimates of the tail of the distribution, unless large amounts of data is available. However, a KDE gives qualitatively good estimates in regions with sufficient data, i.e. in the main part of the distribution. This is good for visualization (`pdfplot`) and detecting modes, symmetries (anti-symmetry) of distributions.

**Example 1. (contd.)** The following command examines and plots the joint distribution of crest period  $T_c = T_{cf} + T_{cb}$  and crest height  $A_c$  in `sea.dat`.

```
kopt2 = kdeoptset('L2',0.5,'inc',256);
Tc = Tcf+Tcb;
fTcAc = kdbin([Tc Ac],kopt2);
fTcAc.labx={'Tc [s]' 'Ac [m]'} % make labels for the plot
pdfplot(fTcAc), hold on
plot(Tc,Ac,'k.'), hold off
```

In Figure 3.5 are plotted 544 pairs of crest period and height. We can see that the kernel estimate describes the distribution of data quite well. It is also obvious that it can not be used to extrapolate outside the observation range. In the following chapter we shall compute the theoretical joint density of crest period and height from the transformed Gaussian model and compare with the KDE estimate.  $\square$

## 3.3 Explicit results - parametric wave models

In this section we shall consider the Gaussian sea with well-defined spectrum. We assume that the reference level is zero. We will present some explicit results that are known and studied in the literature about wave characteristics. Some of them are exact, others are derived by simplification of the random functions describing the sea surface.

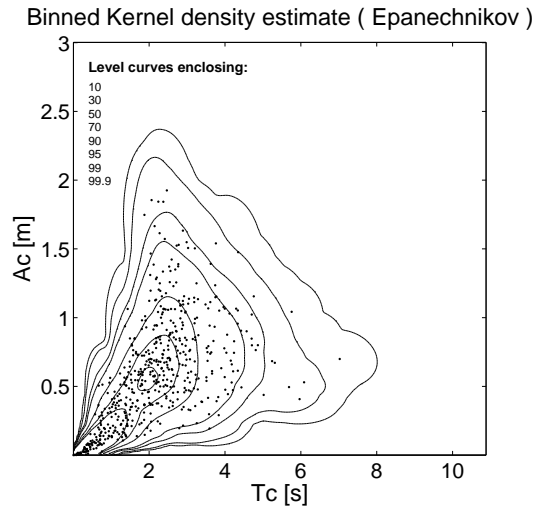


Figure 3.5: Kernel estimate of joint density of crest period  $T_c$  and crest height  $A_c$  in `sea.dat` compared with the observed data (dots). The contour lines are drawn in such a way that they contain specified (estimated) proportions of data.

### 3.3.1 The average wave

For Gaussian waves the spectrum and the spectral moments contain exact information about the average behaviour of many wave characteristics. The WAFO routines `spec2char` and `spec2bw` compute a long list of wave characteristic parameters.

**Example 6.** (*Simple wave characteristics obtained from spectral density*) We start by defining a JONSWAP spectrum, describing a sea state with  $T_p = 10$  [s],  $H_{m_0} = 5$  [m]. Type `spec2mom` to see what spectral moments are computed.

```
SJ = jonswap([], [5 10]);
[m mt] = spec2mom(SJ, 4, [], 0);
```

The most basic information about waves is contained in the spectral moments. The variable `mt` now contains information about what kind of moments have been computed, in this case spectral moments up to order four ( $m_0, \dots, m_4$ ). Next, the irregularity factor  $\alpha$ , significant wave height, zero crossing wave period, and peak period can be computed.

```
spec2bw(SJ)
[ch Sa2] = spec2char(SJ, [1 3])
```

The interesting feature of the program `spec2char` is that it also computes an estimate of the variance of the characteristics, given the length of observations (assuming the Gaussian sea); see [35], [90], and [98] for more detailed discussion. For example, for the JONSWAP Gaussian sea, the standard deviation of significant wave height estimated from 20 minutes of observations is approximately 0.25 meter.  $\square$

### 3.3.2 Explicit approximations of wave distributions

In the module `wavemodels`, we have implemented some of the approximative models that have been suggested in the literature. To get an overview of the routines in the module, use the `help` function on `wavemodels`.

We will investigate two suggested approximations for the joint pdf of  $(T_c, A_c)$ ; for the nomenclature, see the routines `perioddef` and `ampdef` in the module `docs`. Both functions need spectral moments as inputs. One should bear in mind that the models only depend on a few spectral moments and not on the full wave spectrum.

#### Model by Longuet-Higgins

Longuet-Higgins, [48, 49], derived his approximative distribution by considering the joint distribution of the envelope amplitude and the time derivative of the envelope phase. The model is valid for narrow-band processes. It seems to give relatively accurate results for big waves, e.g. for waves with significant amplitudes.

The Longuet-Higgins density depends, besides the significant wave height  $H_s$  and peak period  $T_p$ , on the spectral width parameter  $\nu = \frac{m_0 m_2}{m_1^2} - 1$ , which can be calculated by the command `spec2bw(S, 'eps2')`, (for a narrow-band process,  $\nu \approx 0$ ). The explicit density is given by

$$f_{T_c, A_c}^{\text{LH}}(t, x) = c_{\text{LH}} \left(\frac{x}{t}\right)^2 \exp \left\{ -\frac{x^2}{8} [1 + \nu^{-2}(1 - t^{-1})^2] \right\},$$

where

$$c_{\text{LH}} = \frac{1}{8} (2\pi)^{-1/2} \nu^{-1} [1 + (1 + \nu^2)^{-1/2}]^{-1}.$$

The density is calculated by the function `lh83pdf`.

**Example 6. (contd.)** For the Longuet-Higgins approximation of the  $T_c, A_c$  distribution for JONSWAP waves we use the spectral moments just calculated.

```
t = linspace(0,15,100);
h = linspace(0,6,100);
flh = lh83pdf(t,h,[m(1),m(2),m(3)]);
```

In WAFO we have modified the Longuet-Higgins density to be applicable also for transformed Gaussian models. Following the examples from the previous chapter we compute the transformation proposed by Winterstein and combine it with the Longuet-Higgins model.

```
[sk, ku] = spec2skew(SJ);
sa = sqrt(m(1));
gh = hermitetr([], [sa sk ku 0]);
flhg = lh83pdf(t,h,[m(1),m(2),m(3)],gh);
```

In Figure 3.6 the densities `flh` and `flhg` are compared. The contour lines are drawn in such a way that they contain predefined proportions of the total probability mass inside the contours. We can see that including some nonlinear effects gives somewhat higher waves for the JONSWAP spectrum.  $\square$

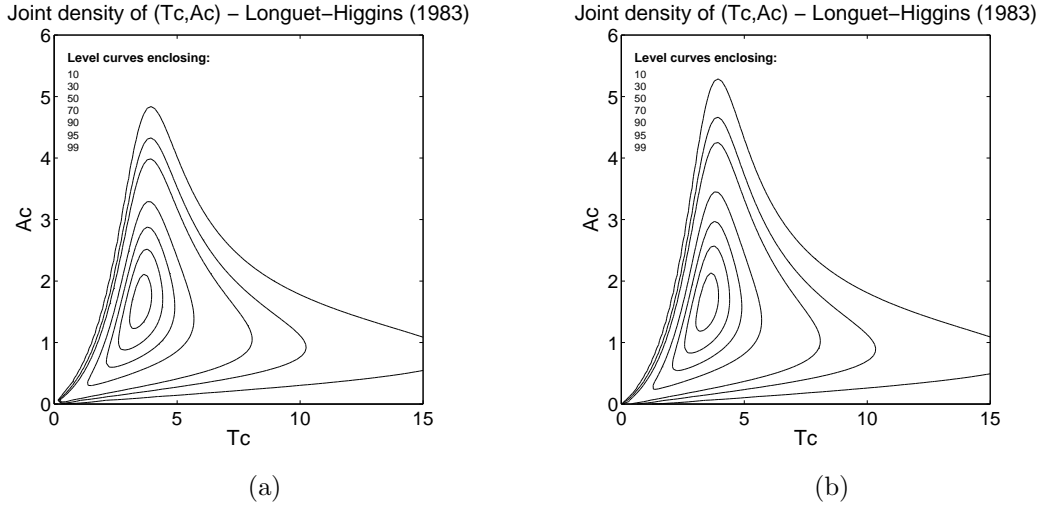


Figure 3.6: Longuet-Higgins model for joint pdf of crest period  $T_c$  and crest height  $A_c$ . Spectrum: JONSWAP with  $T_p = 10$  [s],  $H_{m0} = 5$  [m]. (a) linear Gaussian sea, (b) transformed Gaussian sea.

### Model by Cavanié et al.

Another explicit density for the crest height was proposed by Cavanié et al., [18]. Here any positive local maximum is considered as a crest of a wave, and then the second derivative (curvature) at the local maximum defines the wave period as if the entire wave was a cosine function with the same height and the same crest curvature.

The model uses the parameter  $\nu$  and a higher order bandwidth parameter<sup>2</sup>  $\epsilon$ , defined by

$$\epsilon = \sqrt{1 - \frac{m_2^2}{m_0 m_4}};$$

where, for a narrow-band process,  $\epsilon \approx 0$ . The Cavanié distribution is given by

$$f_{T_c, A_c}^{CA}(t, x) = c_{CA} \frac{x^2}{t^5} \exp \left\{ -\frac{x^2}{8\epsilon^2 t^4} \left[ \left( t^2 - \left( \frac{1 - \epsilon^2}{1 + \nu^2} \right) \right)^2 + \beta^2 \left( \frac{1 - \epsilon^2}{1 + \nu^2} \right) \right] \right\},$$

where

$$\begin{aligned} c_{CA} &= \frac{1}{4}(1 - \epsilon^2)(2\pi)^{-1/2}\epsilon^{-1}\alpha_2^{-1}(1 + \nu^2)^{-2}, \\ \alpha_2 &= \frac{1}{2}[1 + (1 - \epsilon^2)^{1/2}], \\ \beta &= \epsilon^2/(1 - \epsilon^2). \end{aligned}$$

The density is computed by

```
t = linspace(0,10,100);
h = linspace(0,7,100);
fcav = cav76pdf(t,h,[m(1) m(2) m(3) m(5)],[]);
```

and a contour plot of the pdf is obtained by `pdfplot(fcav)`; see Figure 3.7.

<sup>2</sup>The value of  $\epsilon$  may be calculated by `spec2bw(S, 'eps4')`

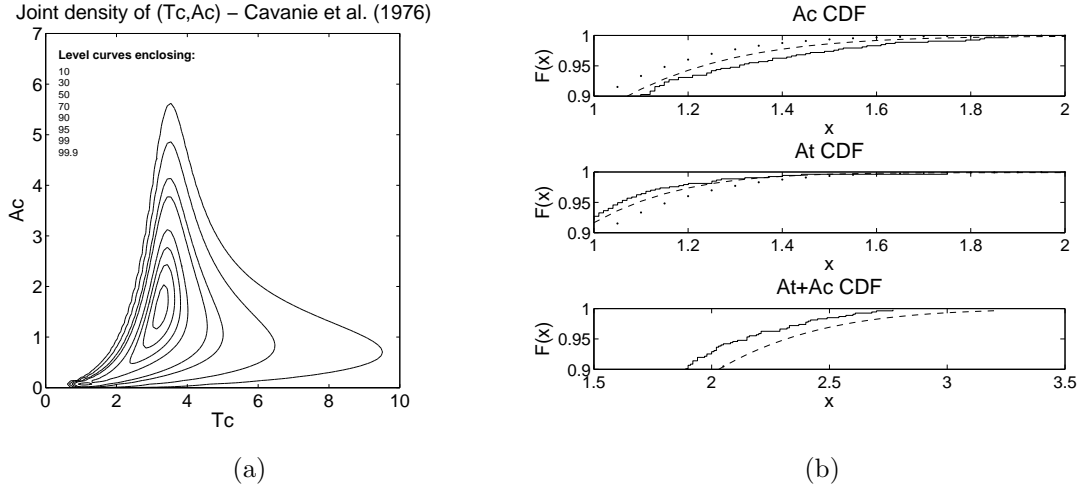


Figure 3.7: (a) Contour lines of the joint density of crest period and crest height proposed by Cavanié et al, for Gaussian sea with JONSWAP spectrum ( $T_p = 10$  [s],  $H_{m0} = 5$  [m]). (b) The tail of the empirical distribution of crest height (top), trough depth (middle) and amplitude (bottom) compared with Rayleigh approximation (dots) and transformed Rayleigh model with Hermite transformation.

### 3.3.3 Rayleigh approximation for wave crest height

There are several densities proposed in the literature to approximate the height of a wave crest or its amplitude. Some of them are programmed in WAFO; execute `help wavemodels` for a list. For Gaussian sea the most simple and most frequently used model is the Rayleigh density. The standardized Rayleigh variable  $R$  has probability density  $f(r) = r \exp(-r^2/2)$ ,  $x > 0$ . It is well known that for Gaussian sea the Rayleigh approximation works very well for high waves, and actually it is a conservative approximation since we have

$$P(A_c > h) \leq P(R > 4h/H_s) = e^{-8h^2/H_s^2},$$

see [74]. In that paper it is also shown that for any sea wave model with crossing intensity  $\mu(u)$ , one has  $P(A_c > h) \leq \mu(u)/\mu(0)$ . The approximation becomes more accurate as the level  $h$  increases.

The crossing intensity  $\mu(u)$  is given by Rice's formula, Rice (1944), and it can be computed when the joint density of sea level  $X(t)$  and its derivative  $X'(t)$  is known, see Section 2.2.3,

$$\mu(u) = \int_0^\infty z f_{X(t), X'(t)}(u, z) dz.$$

For a Gaussian sea it can be computed explicitly,

$$\mu(u) = \frac{1}{T_z} e^{-8u^2/H_s^2}.$$

For non-linear wave models with random Stokes waves the crossing intensity has to be computed using numerical integration; see the work by Machado and Rychlik, [51].

Knowing the crossing intensity  $\mu(u)$  one can compute the transformation  $g$ , by using the routine `lc2tr`, such that the transformed Gaussian model has crossing intensity equal to  $\mu(u)$ . Consequently, we have that  $P(A_c > h) \leq P(R > g(h)) = 1 - P(G(R) \leq h)$ . The

function `trraylpdf` computes the pdf of  $G(R)$ . (Obviously the function works for any transformation  $g$ .)

In previous examples we used the estimated crossing intensity to compute the transformation and then approximated the crest height density using the transformed Rayleigh variable. The accuracy of the approximation for the high crests in the data set `xx = sea.dat` was checked, see Figure 3.4(b). A more extensive study of the applicability of this approximation is done in [74].

**Example 7.** (*Rayleigh approximation of crest height from spectral density*) In this example we shall use a transformed Rayleigh approximation for crest height derived from a sea spectrum. In order to check the accuracy of the approximations we shall use the estimated spectrum from the record `sea.dat`.

```
xx = load('sea.dat');
x = xx;
x(:,2) = detrend(x(:,2));
SS = dat2spec2(x);
[sk, ku, me, si] = spec2skew(SS);
gh = hermitetr([], [si sk ku me]);
Hs = 4*si;
r = (0:0.05:1.1*Hs)';
fac_h = trraylpdf(r, 'Ac', gh);
fat_h = trraylpdf(r, 'At', gh);
h = (0:0.05:1.7*Hs)';
facat_h = trraylpdf(h, 'AcAt', gh);
pdfplot(fac_h), hold on
pdfplot(fat_h), hold off
```

Next, we shall compare the derived approximation with the observed crest heights in `x`. As before, we could use the function `dat2steep` to find the crests. Here, for illustration only, we shall use `dat2tc` to find the crest heights `Ac` and trough depth `At`.

```
TC = dat2tc(xx, me);
tc = tp2mm(TC);
Ac = tc(:,2); At = -tc(:,1);
AcAt = Ac+At;
```

Finally, the following commands will give the cumulative distributions for the computed densities.

```
Fac_h = [fac_h.x{1} cumtrapz(fac_h.x{1}, fac_h.f)];
subplot(3,1,1)
Fac = plottedf(Ac, Fac_h); hold on
plot(r, 1-exp(-8*r.^2/Hs^2), '.')
axis([1. 2. 0.9 1])
Fat_h = [fat_h.x{1} cumtrapz(fat_h.x{1}, fat_h.f)];
subplot(3,1,2)
Fat = plottedf(At, Fat_h); hold on
```



```

plot(r,1-exp(-8*r.^2/Hs^2),'.')
axis([1. 2. 0.9 1])
Facat_h = [facat_h.x{1} cumtrapz(facat_h.x{1},facat_h.f)];
subplot(3,1,3)
Facat = plottedf(AcAt,Facat_h); hold on
r2 = (0:05:2.1*Hs)';
plot(r2,1-exp(-2*r2.^2/Hs^2),'.')
axis([1.5 3.5 0.9 1]), hold off

```

In Figure 3.7(b) we can see some differences between the observed crest and trough distributions and those obtained from the transformation `gh`. However, it still gives a much better approximation than the standard Rayleigh approximation (dots). As it was shown before, using the transformation computed from the crossing intensity, the transformed Rayleigh approach is giving a perfect fit. Finally, one can see that the Rayleigh and transformed Rayleigh variables give too conservative approximations to the distribution of wave amplitude.  $\square$

## 3.4 WAFO wave characteristics

### 3.4.1 spec2char

help spec2char

SPEC2CHAR Evaluates spectral characteristics and their variance

CALL: [ch r chtext] = spec2char(S,fact,T)

ch = vector of spectral characteristics  
 r = vector of the corresponding variances given T  
 chtext = a cellvector of strings describing the elements of ch  
 S = spectral struct with angular frequency  
 fact = vector with factor integers, see below.  
       (default [1])  
 T = recording time (sec) (default 1200 sec = 20 min)

If input spectrum is of wave number type, output are factors for corresponding 'k1D', else output are factors for 'freq'.

Input vector 'factors' correspondence:

|    |       |                                                                      |                                          |
|----|-------|----------------------------------------------------------------------|------------------------------------------|
| 1  | Hm0   | = $4 \cdot \sqrt{m_0}$                                               | Significant wave height                  |
| 2  | Tm01  | = $2 \cdot \pi \cdot m_0 / m_1$                                      | Mean wave period                         |
| 3  | Tm02  | = $2 \cdot \pi \cdot \sqrt{m_0 / m_2}$                               | Mean zero-crossing period                |
| 4  | Tm24  | = $2 \cdot \pi \cdot \sqrt{m_2 / m_4}$                               | Mean period between maxima               |
| 5  | Tm_10 | = $2 \cdot \pi \cdot m_{-1} / m_0$                                   | Energy period                            |
| 6  | Tp    | = $2 \cdot \pi / \{w \mid \max(S(w))\}$                              | Peak period                              |
| 7  | Ss    | = $2 \cdot \pi \cdot Hm0 / (g \cdot Tm02^2)$                         | Significant wave steepness               |
| 8  | Sp    | = $2 \cdot \pi \cdot Hm0 / (g \cdot Tp^2)$                           | Average wave steepness                   |
| 9  | Ka    | = $\text{abs}(\text{int } S(w) \exp(i \cdot w \cdot Tm02) dw) / m_0$ | Groupiness parameter                     |
| 10 | Rs    | = se help spec2char                                                  | Quality control parameter                |
| 11 | Tp    | = $2 \cdot \pi \cdot \text{int } S(w)^4 dw$                          | Peak Period                              |
|    |       | -----                                                                | (more robust estimate)                   |
|    |       | $\text{int } w \cdot S(w)^4 dw$                                      |                                          |
| 12 | alpha | = $m_2 / \sqrt{m_0 \cdot m_4}$                                       | Irregularity factor                      |
| 13 | eps2  | = $\sqrt{m_0 \cdot m_2 / m_1^2 - 1}$                                 | Narrowness factor                        |
| 14 | eps4  | = $\sqrt{1 - m_2^2 / (m_0 \cdot m_4)}$                               | = $\sqrt{1 - \alpha^2}$ Broadness factor |
| 15 | Qp    | = $(2 / m_0^2) \text{int}_0^\infty w \cdot S(w)^2 dw$                | Peakedness factor                        |

Order of output is same as order in 'factors'

The variances are computed with a Taylor expansion technique and is currently only available for factors 1,2 and 3.

### 3.4.2 spec2bw

help spec2bw

SPEC2BW Evaluates some spectral bandwidth and irregularity factors

CALL: `bw = spec2bw(S,factors)`

`bw` = vector of factors

`S` = spectrum struct

`factors` = vector with integers, see below. (default [1])

If input spectrum is of wave-number type, output are factors for corresponding 'k1D', else output are factors for 'freq'.

Input vector 'factors' correspondence:

- |   |                                                                     |                       |
|---|---------------------------------------------------------------------|-----------------------|
| 1 | $\alpha = m_2 / \sqrt{m_0 * m_4}$                                   | (irregularity factor) |
| 2 | $\epsilon_2 = \sqrt{m_0 * m_2 / m_1^2 - 1}$                         | (narrowness factor)   |
| 3 | $\epsilon_4 = \sqrt{1 - m_2^2 / (m_0 * m_4)} = \sqrt{1 - \alpha^2}$ | (broadness factor)    |
| 4 | $Q_p = (2 / m_0^2) \int_0^\infty f * S(f)^2 df$                     | (peakedness factor)   |

Order of output is the same as order in 'factors'

Example:

`S=demospec;`

`bw=spec2bw(S,[1 2 3 4]);`

### 3.4.3 wavedef

help wavedef

WAVEDEF wave definitions and nomenclature

Definition of trough and crest:

~~~~~

A trough (t) is defined as the global minimum between a level v down-crossing (d) and the next up-crossing (u) and a crest (c) is defined as the global maximum between a level v up-crossing and the following down-crossing.

Definition of down- and up-crossing waves:

~~~~~

A level v-down-crossing wave (dw) is a wave from a down-crossing to the following down-crossing. Similarly a level v-up-crossing wave (uw) is a wave from an up-crossing to the next up-crossing.

Definition of trough and crest waves:

~~~~~

A trough to trough wave (tw) is a wave from a trough (t) to the following trough. The crest to crest wave (cw) is defined similarly.

Definition of min2min and Max2Max wave:

~~~~~

A min2min wave (mw) is defined starting from a minimum (m) and ending in the following minimum. A Max2Max wave (Mw) is a wave from a maximum (M) to the next maximum (all waves optionally rainflow filtered).

```

      <----- Direction of wave propagation
      <-----Mw-----> <----mw----->
      M          : : c          :
      / \        M : / \_      :      c_          c
      F  \       / \m/      \   :      /: \        /:\   level v
-----d-----u-----d-----u-----d-----u-----d-----
      \      /:          \ : /: : : \_    _/ : : \_    L
      \_    / :          \_t_/ : : : \_t_/ : : \m/
      \t/  <-----uw-----> : <----dw----->
      :          :          :          :
      <-----tw----->      <----cw----->

```

(F= first value and L=last value).

See also: tpdef, crossdef, dat2tc, dat2wa, dat2crossind

### 3.4.4 perioddef

help perioddef

PERIODDEF wave periods (lengths) definitions and  
nomenclature

Definition of wave periods (lengths):

```

-----
<----- Direction of wave propagation

                <-----Tu----->
                :                   :
                <---Tc----->      :
                :                   : <-----Tcc----->
M              :       c       :   :                   :
/ \            : M   / \_ :   : c_                   c
F \           : / \m/   \:   : / \                   / \ level v
-----d-----u-----d-----u-----d-----u-----d-----
      \       /                \   /      : \_   _/:      : \_   L
      \_     /                \t_/      : \t_/ :      : \m/
      \t/                :                :      :      :
      :<-----Ttt----->:                <---Tt---> :
                                :<-----Td----->:

Tu  = Wave up-crossing period
Td  = Wave down-crossing period
Tc  = Crest period, i.e., period between up-crossing and
      the next down-crossing
Tt  = Trough period, i.e., period between down-crossing and
      the next up-crossing
Ttt = Trough2trough period
Tcc = Crest2crest period

```

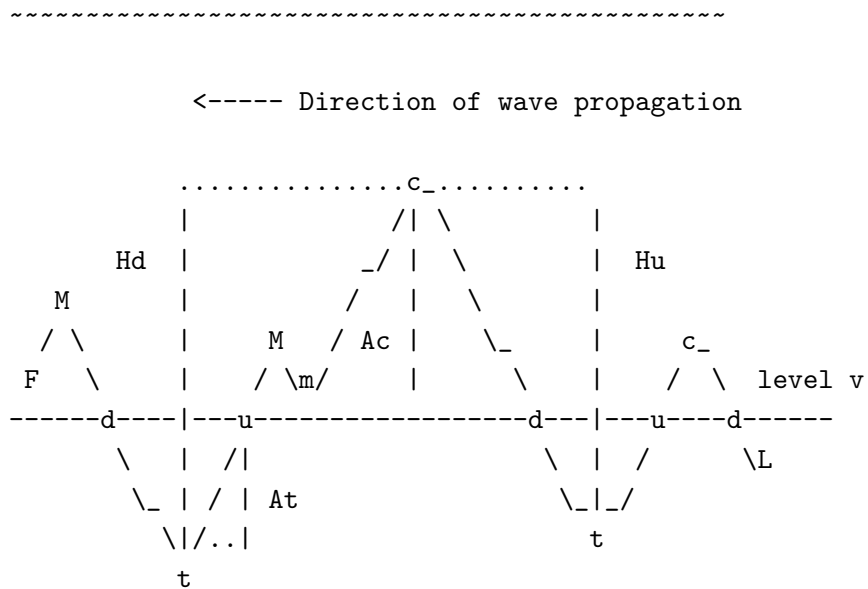


### 3.4.5 ampdef

help ampdef

AMPDEF wave heights and amplitude definitions and  
nomenclature

Definition of wave amplitude and wave heights:



Ac = crest amplitude  
At = trough amplitude  
Hd = wave height as defined for down-crossing waves  
Hu = wave height as defined for up-crossing waves

See also: wavedef, ampdef, crossdef, tpdef

### 3.4.6 crossdef

help crossdef

CROSSDEF level v crossing definitions and nomenclature

Definition of level v crossing:

~~~~~

Let the letters 'm', 'M', 'F', 'L', 'd' and 'u' in the figure below denote local minimum, maximum, first value, last value, down- and up-crossing, respectively. The remaining sampled values are indicated with a '.'. Values that are identical with v, but do not cross the level is indicated with the letter 'o'.

We have a level up-crossing at index, k, if

$$x(k) < v \text{ and } v < x(k+1)$$

or if

$$x(k) == v \text{ and } v < x(k+1) \text{ and } x(r) < v \text{ for some } d_i < r \leq k-1$$

where d_i is the index to the previous down-crossing.

Similarly there is a level down-crossing at index, k, if

$$x(k) > v \text{ and } v > x(k+1)$$

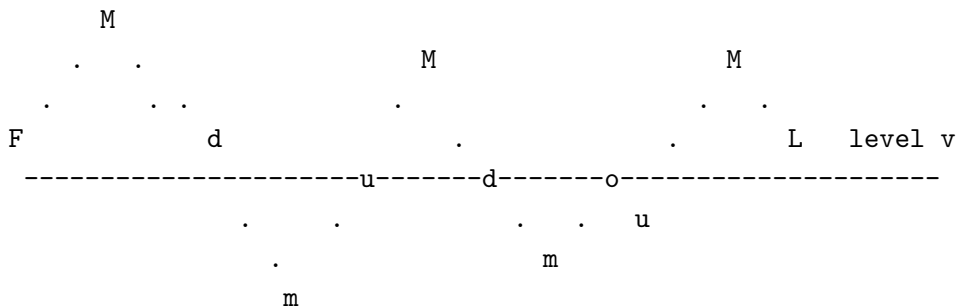
or if

$$x(k) == v \text{ and } v > x(k+1) \text{ and } x(r) > v \text{ for some } u_i < r \leq k-1$$

where u_i is the index to the previous up-crossing.

The first (F) value is a up-crossing if $x(1) = v$ and $x(2) > v$.

Similarly, it is a down-crossing if $x(1) = v$ and $x(2) < v$.



See also: perioddef, wavedef, tpdef, findcross, dat2tp

upcrossing wave		wave between two successive mean level upcrossings
downcrossing wave		wave between two successive mean level downcrossings
wave crest		the maximum value between a mean level upcrossing and the next downcrossing = the highest point of a wave
wave trough		the minimum value between a mean level downcrossing and the next upcrossing = the lowest point of a wave
crest front wave period	T_{cf}	time span from upcrossing to wave crest
crest back (rear) wave period .	$T_{cb}(T_{cr})$	time from wave crest to downcrossing
crest period	T_c	time from mean level up- to downcrossing
trough period	T_t	time from mean level down- to upcrossing
upcrossing period	T_u	time between mean level upcrossings
downcrossing period	T_d	time between mean level downcrossings
crest-to-crest wave period	T_{cc}	time between successive wave crests
crest amplitude	A_c	crest height above mean level
trough depth	A_t	through depth below mean level ($A_t > 0$)
upcrossing wave amplitude ...	H_u	crest-to-trough vertical distance
downcrossing wave amplitude .	H_d	trough-to-crest vertical distance
wave steepness	S	Generic symbol for wave steepness Symbol also used for spectral density
min-to-max period		time from local minimum to next local maximum
min-to-max amplitude		height between local minimum and the next local maximum
max-to-min period/amplitude		similar to min-to-max definitions

Table 3.1: Wave characteristic definitions

CHAPTER 4

Exact wave characteristics

The wave characteristic distributions in Chapter 3 have been empirical, either constructed directly from data, or from a specific model fitted by means of data, via a few spectral moments. In this chapter we will use the Gaussian paradigm, described in Section 3.1.1, to produce exact, up to numeric accuracy, wave characteristic distributions directly from an assumed spectral density, without any further assumptions than Gaussianity and a following transformation. This is a unique facility in WAFO, not available in any other wave analysis software. The routines are collected in the module `trgauss` and they are listed in Section 4.4.

The functions are the results of long time research at Lund University, see [63] and [44], where a review of the historical development and the mathematical tools behind the algorithms are given.

The MATLAB code for the examples in this chapter are found in `Chapter4.m` and is takes 10 minutes to run on a 3.6 GHz 64-bit i7 7700, in fast mode and 40 minutes in slow mode.

4.1 Exact wave distributions routines

By means of a number of examples, we shall demonstrate the most important functions for computation of exact wave probability distributions. The variables are the crest and wave periods, T_c , $T_u = T_c + T_t$, the corresponding crest length and wave length variables, L_c , $L_u = L_c + L_t$, and crest height and trough depth A_c , A_t , and we compute both marginal densities and joint densities for combination of variables. The same functions compute densities for trough period, length, and depth, as for the corresponding crest variables. The common form of the routines is `spec2yyxxx`.

In WAFO there are also functions computing exact densities for other wave characteristics, which will not be presented here. The WAFO routines are collected in the module `trgauss`. Use the help function on `trgauss` to see the list of all the routines.

4.2 Marginal distributions of wave characteristics

In this section we analysis the marginal distributions of crest and wave period/length variables, and how they depend on the crest height. We also discuss the numerical accuracy of the WAFO routines, and how to obtain a reasonable compromise between accuracy and computational speed. More example on this matter will follow in subsequent sections. We start will some introductory examples.

4.2.1 Crest period, crest length and crest height

One of the most useful functions in WAFO is the routine `spec2tpdf`, which computes the density function for crest and trough period, as well as for the corresponding length variables in space. The function also computes the density of waves with crest above a specified height `h`. This is a useful option allowing computation of the probability that a crest is higher than a specified threshold. It can also be used to provide information about the distribution of the period (length) of such high waves.

The function `spec2tpdf` performs all necessary transformations, scalings, etc, making it very flexible. It handles different spectra as inputs. Which kind of density is computed (output) is defined by the variable `def` that takes values `'Tc'` for crest period, `'Lc'` for crest length, `'Tt'` for trough period, and `'Lt'` for trough length. The transformation is only affecting the value of the still water level `u` and the threshold `h`. The function `spec2tpdf` allows any value for the still water level; if `u` it is not equal to the most frequently crossed level then the densities of `Tc` and `Tt` are not identical.

Example 8. (*Torsethaugen waves*) We start by defining the same directional frequency spectrum, $S(\omega)$, as we used in Chapter 1. We choose a directional Torsethaugen spectrum with parameters $H_{m0} = 6$ [m], $T_p = 8$ [s], describing significant wave height and primary peak period, respectively; see Figure 1.2 on page 9.

```
ST = torsethaugen([], [6 8], 1);
D1 = spreading(101, 'cos', pi/2, [15], [], 0);
D12 = spreading(101, 'cos', 0, [15], ST.w, 1);
STD1 = mkdspec(ST, D1);
STD12 = mkdspec(ST, D12);
```

The energy is divided between two peaks, corresponding to contributions from wind and swell. We shall also use the two directional spectra from Chapter 1 with frequency independent, `STD1`, and frequency dependent, `STD12`, spreading. \square

Crest period

Example 8. (contd.) (*Crest period*) We begin with the density of crest period, which (obviously) is identical for all three spectra `S1`, `SD1`, and `SD12`. The computed density is a result of a numerical integration of a theoretically derived formula, which is described, e.g., in [46]. The algorithm gives an upper bound (and, if requested, a lower bound too) for the density. Consequently, if the integral of the computed density, over all periods, is close to one it implies that the density is computed with high accuracy.

```

f_tc_4 = spec2tpdf(ST,[],'Tc',[0 12 61],[],4);
f_tc_1 = spec2tpdf(ST,[],'Tc',[0 12 61],[],-1);
pdfplot(f_tc_4,'-.'), hold on
pdfplot(f_tc_1), hold off
simpson(f_tc_4.x{1},f_tc_4.f)
simpson(f_tc_1.x{1},f_tc_1.f)

```

The crest period density is shown in Figure 4.1(a). The integral of the density `f_tc_4` computed using the function `simpson` is 1.005, showing the high accuracy of the approximation. The density `f_tc_1` uses another algorithm, which is faster, and it has the integral 0.9993. The computation time depends on the required accuracy and how broad banded the spectrum is. For example, the same accuracy is achieved for the JONSWAP spectrum in about half the time. The computation time increases if there is a considerable probability for long waves with low crests.

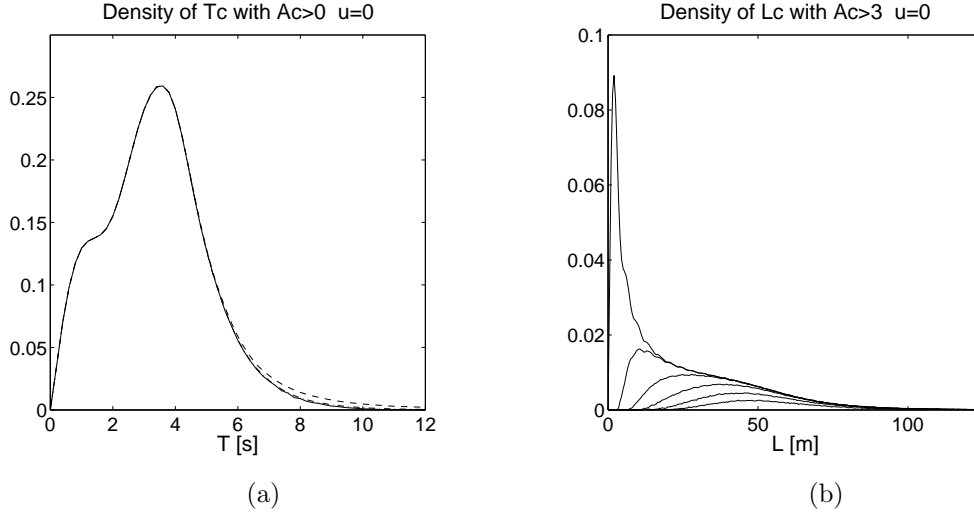


Figure 4.1: (a) Densities `f_tc_1` (solid), `f_tc_2` (dashed), and `f_tc_4` (dash dotted) of crest period T_c for Torsethaugen spectrum `ST`. (b) Densities of crest length L_c , (most peaked curve) compared to the density when restricted to waves with crest height Ac more than 10%, 20%, 30%, 40%, 50% of the significant wave height above the still water level, for Gaussian sea with the Torsethaugen spectrum with $H_s = 6$ [m]. Lowest curve corresponds to $Ac > 3$ [m]; the exact proportion is 10.2%, according to Table 4.1.

The last argument in the calls above to `spec2tpdf` is worth special attention, and we will later study its effect in detail. It controls the numerical algorithm that computes the density. Here, we only note that a positive choice, here 4, gives an upper bound to the density, more accurate and more time consuming the higher the value, while a negative value, here -1, given an almost unbiased value in much shorter time. \square

Crest length

Example 8. (contd.) (*Crest length*) We then turn to the density of crest length for the Torsethaugen spectrum. It can be computed using the same function `spec2tpdf`, we just change the input `def` variable `'Tc'` to `'Lc'`.

level [m]	0.6	1.2	1.5	1.8	2.4	3.0
proportion of crests above level	0.607	0.435	0.367	0.305	0.191	0.102
CDF of crest height A_c	0.391	0.563	0.630	0.693	0.806	0.895

Table 4.1: Second row: proportion of crest heights above a level, computed by `spec2tpdf`; Third row: CDF of crest height computed by `spec2Acdf`.

```
f_Lc = spec2tpdf(ST,[],'Lc',[0 100 151],[],-1);
pdfplot(f_Lc,'-.'), hold on
```

The crest length density has a sharp peak for very short waves – the wave-number spectrum is much more broad banded than the frequency spectrum; see [47] for a general comparison of wave period and wave length. However, the short waves have small crests and should be considered as ‘noise’ rather than as apparent waves. Consequently, we may wish to compute the proportion of waves that have crest higher than a certain proportion of the significant wave height, e.g. 25%, i.e. one standard deviation, $H_s/4 = 1.5$ [m], and give the density of the crest length for these waves. This can be done by specifying an extra argument `h = 1.5` in the call to `spec2tpdf`.

```
f_Lc_1 = spec2tpdf(ST,[],'Lc',[0 100 151],1.5,-1);
pdfplot(f_Lc_1)
```

Figure 4.1(b) presents the results when the crest height is restricted to more than 10%, 20%, 30%, 40%, 50% of the significant wave height. and we can see that all short waves in fact were small. (The algorithm produces some very small negative density values. These have been removed before the plotting; see the following section on numerical accuracy, Section 4.2.2.)

The proportion of waves with crests above 1.5 [m] (one standard deviation) is computed by the following commands.

```
simpson(f_Lc.x{1},f_Lc.f)
simpson(f_Lc_1.x{1},f_Lc_1.f)
```

Taking the ratio, we can see that more than half of the waves are small, about 37% of the waves have crests above 1.5 [m]. Similar calculations for the curves in Figure 4.1(b), give the proportions of crests above the levels in Table 4.1. \square

Crest height

From a statistical viewpoint the crest period distribution is uniquely defined as the empirical distribution of the time between mean level upcrossings and the following downcrossing. It is linked to a fixed observation point and an “infinite” observation interval. Similarly, crest length distribution is the empirical distribution of the distance between mean level up- and downcrossings. It is linked to a fixed time and a fixed, “infinitely long”, observation transect on the ocean surface. Discussing crest height distribution, the maximum height between an up- and a downcrossing, we obviously have to decide which observation scheme is used. Fortunately, the WAFO routine `spec2Acdf` handles both alternatives, depending on the type of spectrum we use..

Example 8. (contd.) (*Crest height*) The table of the proportion of high crest waves is related to the cumulative distribution function (cdf) of the crest height Ac in a natural way. The routine `spec2Acdf` computes and plots the cdf directly, both for the crest height over a crest period in time and for the crest height over a crest length in space. It also plots the Rayleigh approximation.

The following commands creates empirical and theoretical crest height distributions in time and in space for Gaussian waves with Torsethaugen frequency spectrum. The vector T contains 100 replicates of 400 seconds of time wave simulation, the vector L contains 100 replicates of 4000 meters of space wave simulation. AcT , AcL are the time and space observed crest heights, respectively.

```
clf; Hs = 6;
r = (0:0.12:1.1*Hs)';
F_Ac_s1_T = spec2Acdf(ST,[],'Tc',[0 12 61],r,-1); hold on
T = spec2sdat(ST,[40000,100],0.01);
[SteepT,HeightT,AcT] = dat2steep(T);
plotedf(AcT,'-.')
F_Ac_s1_L = spec2Acdf(ST,[],'Lc',[0 125 251],r,-1);
L = spec2sdat(spec2spec(ST,'k1d'),[40000 100],0.1);
[SteepL,HeightL,AcL] = dat2steep(L);
plotedf(AcL,'-.')
plot(r,1-exp(-8*r.^2/Hs^2)), hold off
```

Figure 4.2 shows the empirical distribution of Ac in a long simulation in time, and the theoretical distribution functions for crest height in time and in space computed by `spec2Acdf`, as well as the Rayleigh approximation from Section 3.3.3. The simulations contain 9255 space wave crests and 5823 time wave crests. The agreement between the empirical and theoretical distribution functions is very good. The Rayleigh distribution gives a good approximation of the time crest height for large crest values but over-estimates the smallest crests. It does not work for space waves.

The third row in Table 4.1 shows the cdf values for crest height in space computed by `spec2Acdf`. The sum of the second and third row should be one; here, all sums in the table are greater than 0.997. \square

Example 8. (contd.) (*Directional spreading*) We finish this example by considering the Torsethaugen spectrum with the two different spreading functions `STD1` and `STD12`. In Figures 1.5 and 1.6 we presented simulations of the sea surfaces with these spectra. From the figures we expect that the two crest length distributions should be different. (Obviously, the crest period densities are identical). In the directional sea we have to define the azimuth of the line for which the crest length should be computed (the default value is zero). Now, the directional spectra `STD1` and `STD12` have different main wave directions, 90° and 0° degrees, respectively, and hence we shall choose different azimuths for the two spectra. More precisely, for both cases we shall consider heading waves; this is achieved using the function `spec2spec`.

```
f_Lc_d1 = spec2tpdf(spec2spec(STD1,'rotmdir',pi/2),[],...
                    'Lc',[0 200 201],[],-1);
pdfplot(f_Lc_d1,'-.'), hold on
```

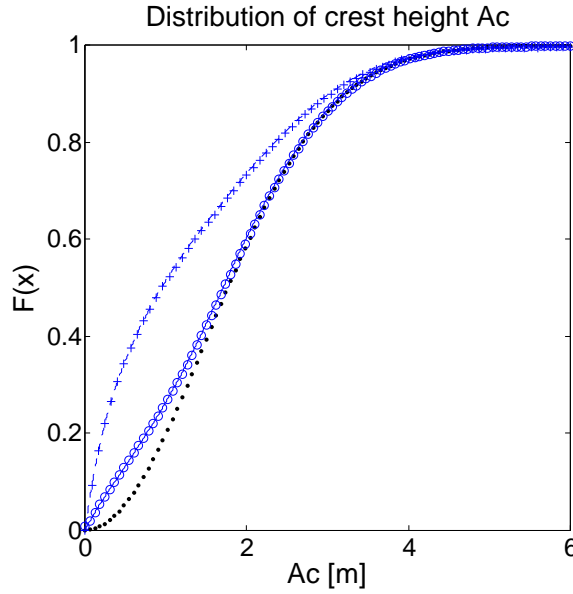


Figure 4.2: Cumulative distribution (cdf) for crest height Ac with Torsethaugen spectrum ST. Curves most to the left = theoretical (solid) and empirical (dash dotted) cdf for Ac over a crest length. Middle curves show theoretical and empirical cdf for Ac over a crest period. Curve most to the right is the cdf for the Rayleigh approximation.

```
f_Lc_d12 = spec2tpdf(STD12,[],'Lc',[0 200 201],[],-1);
pdfplot(f_Lc_d12), hold off

figure(2)
dx = f_Lc.x{1}(2)-f_Lc.x{1}(1);
dx1 = f_Lc_d1.x{1}(2)-f_Lc_d1.x{1}(1);
dx12 = f_Lc_d12.x{1}(2)-f_Lc_d12.x{1}(1);
plot(f_Lc.x{1},cumsum(f_Lc.f)*dx), hold on
plot(f_Lc_d1.x{1},cumsum(f_Lc_d1.f)*dx1,'-.' )
plot(f_Lc_d12.x{1},cumsum(f_Lc_d12.f)*dx12,'--'), hold off
```

As expected, after examination of the simulated sea surfaces in Figures 1.5 and 1.6, the crest length for the two directional spectra are different. The sea with frequency dependent spreading seems to be more irregular. We can see in Figure 4.3 that waves with frequency independent spreading are only slightly longer than the waves in unidirectional sea, while the crest length of both seas are much shorter than for frequency dependent spreading. \square

4.2.2 Numerical accuracy and computational speed

The basic algorithm in the routine `spec2tpdf` computes a finite-dimensional approximation to an "infinite-dimensional" normal expectation. The last input in all the previous calls to the routine is a parameter called `nit`, and it determines both the integration method and the dimensionality of the computed integral. Important references on how to compute normal probabilities are [5, 15, 16, 23, 24, 71].

The `nit` parameter can be positive, negative, and zero. Positive `nit` values use numeri-

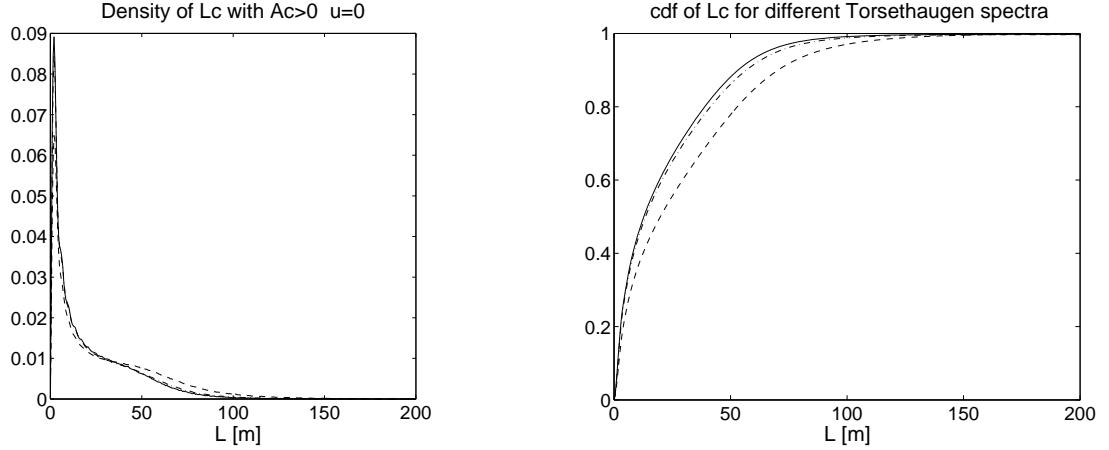


Figure 4.3: Computed pdf (left) and cdf (right) for L_c in Gaussian sea with Torsethaugen spectrum with different spreading: unidirectional spectrum $S1$ (solid line) ; frequency independent spreading $SD1$ (dash-dotted line); frequency dependent spreading $SD12$ (dashed line).

cal, deterministic, integration algorithms, while negative values use a simulation technique based on importance sampling; see [15, 16] for a review of different methods.

The methods with positive `nit` are very reliable and have been tested on different wave problems since the first version was used already in 1987; see [69]. As default, they give an upper bound to the densities. The integration methods corresponding to negative `nit` values are often much faster and also very accurate in cases when the deterministic method has troubles with too long execution times; see [41] for examples.

Although the method with negative `nit` is based on simulation, the accuracy is still controlled. If the number of simulations is too small to achieve the required accuracy the program gives an error statement with an estimate of the possible error in the computed density.

One should be aware that both positive and negative `nit` values can produce negative density values with `spec2tpdf`. This is the result of the way the densities are computed, namely as differences between "cumulative distribution type" functions. Then, small numerical variations may cause negative density estimates, mostly for very small density values.

The routine `spec2tpdf` is the MATLAB interface to a FORTRAN program. All programs computing exact densities of different wave characteristics can be reformulated in such a way that the density is written as a certain multidimensional integral of a function of Gaussian variables; see [46] for more details. This integral is computed using a FORTRAN module called `RIND`. There is also a MATLAB interface called `rind` which can be used to test programs for new wave characteristics.

An example is a function `spec2tpdf2` which uses the program `rind`. The program is slower than `spec2tpdf`, and it does not have an option that allows to choose waves with crest above some level, but on the other hand it is easier to use for experimentation, and it can also be used to learn how to create own programs.

Besides the parameter `nit`, the input parameter `speed` will also control the accuracy of the computations in module `trgauss`; see the help text to the routines for information.

Remark 4.4. The accuracy of the numerical computations depends on the parameters

`nit` and `speed` in a natural and predictable way. Of course, also the choice of grid size affects the accuracy; some of the algorithms are very sensitive to short time or space steps and can produce covariance matrices which are not positive definite.

MATLAB version, computer CPU, and RAM memory size, all affect speed. More subtle effects of hardware implementation can affect some computed small probabilities, of interest in applications. In the examples we present many numerical results and execution times, and the reader is advised to make own experiments to become familiar with these characteristics. \square

Example 8. (contd.) (*Numerical accuracy and the parameter `nit`*) We shall exemplify the use of the parameter `nit` by computing the crest length density for the directional spectrum with frequency independent spreading. We shall also use the slower program `spec2tpdf2` for illustration. We fix the speed and method by setting an option variable.

```
opt1 = rindoptset('speed',5,'method',3);
STD1r = rotspec(STD1,pi/2);
f_Lc_d1_5 = spec2tpdf(STD1r,[],'Lc',[0 200 201],[],5);
f_Lc_d1_3 = spec2tpdf(STD1r,[],'Lc',[0 200 201],[],3);
f_Lc_d1_2 = spec2tpdf(STD1r,[],'Lc',[0 200 201],[],2);
f_Lc_d1_0 = spec2tpdf(STD1r,[],'Lc',[0 200 201],[],0);
f_Lc_d1_neg = spec2tpdf(STD1r,[],'Lc',[0 200 201],[],-1);
f_Lc_d1_n4 = spec2tpdf2(STD1r,[],'Lc',[0 200 201],opt1);

pdfplot(f_Lc_d1_5), hold on
pdfplot(f_Lc_d1_2), pdfplot(f_Lc_d1_3)
pdfplot(f_Lc_d1_0), pdfplot(f_Lc_d1_neg)
pdfplot(f_Lc_d1_n4,'LineWidth',2,'-.-')
simpson(f_Lc_d1_n4.x{1},f_Lc_d1_n4.f)
```

The execution times for the densities were 150 seconds, 5.6 seconds, 1.3 seconds, 0.13 seconds, 2.4 seconds, and 3.7 seconds, respectively. In Figure 4.4(a) the different approximations are presented and we can see how the density decreases with increasing positive `nit`. The negative `nit` involves some random number integration methods, but we can hardly see that the computed density is actually a random function. Most problems are less numerical demanding and `nit=2` often suffices, but here clearly the negative `nit` is preferable.

In Figure 4.4(b) we compare an empirical density of crest length `Lc`, conditioned on crest height `Ac > 1.5[m]`, based on 500 000 observed waves, with the normalized density `f_Lc_1` from page 71, computed with `nit = -1`. The agreement is almost perfect. \square

4.2.3 Wave period and wave length

In the previous sections we described routines for the marginal distributions of crest and trough periods, and height, `Tc`, `Tt`, `Ac`, and the corresponding crest and trough lengths, `Lc`, `Lt`. We also showed how to limit the population to waves for which the crest (trough) amplitudes are above some predetermined threshold.

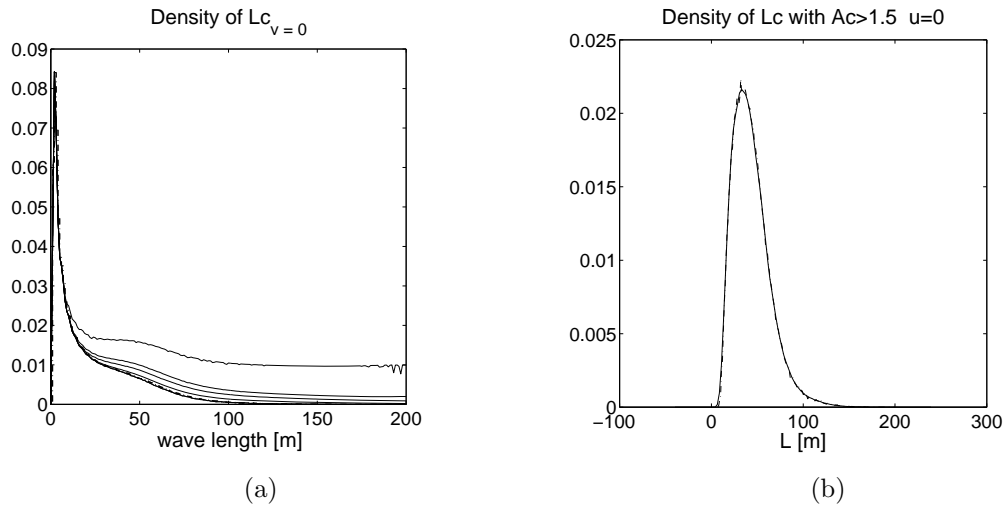


Figure 4.4: (a) Approximations by different methods and accuracy of the crest length for the directional spectrum STD1r with frequency independent spreading. The top solid curves are computed with positive `nit` = 0 (top), 2, 3, 5, and negative `nit` = -1 (bottom), in routine `spec2tpdf`, while the dash-dotted curve has negative `nit` with routine `spec2tpdf2`. (b) Solid curve = the empirical density of crest length L_c with crest height $Ac > 1.5$ [m], dash-dotted curve is the normalized computed density f_{Lc_1} .

We now turn to the wave period, $T_u = T_c + T_t$, which is the time between two successive upcrossings of the still water level u . It is related to, but not equal to, the crest-to-crest wave period T_{cc} , which is the time span between two successive crests. The density of T_u can be computed using the function `spec2tccpdf`. The wave length L_u or encountered wave period can also be computed by `spec2tccpdf`, with just a few inputs to be modified; see the help text. Hence, these variables shall not be discussed here any more.

The computations using `spec2tccpdf` are slower than those using `spec2tpdf`, since one needs to compute the joint density of T_c and T_t and then integrate the convolution to get $T_u = T_c + T_t$. It should be mentioned that, in addition to the methods to reduce computation time, one of the best methods to speed up computation is to cut off high frequencies in the spectrum. The syntax of `spec2tccpdf` is almost identical to that of `spec2tpdf`, and hence we limit ourselves to a few examples.

Example 9. (*Sea data wave distributions*) In order to make comparisons with the wave characteristic distributions in `sea.dat` we shall use the estimated spectrum `SS`, see Example 1 on pages 20 and 26. We first re-compute the spectrum estimate and the transformation to Gaussianness, and extract some characteristics.

```
xx = load('sea.dat');
x = xx;
x(:,2) = detrend(x(:,2));
SS = dat2spec(x);
si = sqrt(spec2mom(SS,1));
SS.tr = dat2tr(x);
Hs = 4*si
```

The estimated spectrum is plotted in Figure 4.5, together with pointwise 95% confidence intervals.

Note that the spectrum contains a transformation field `SS.tr`, and recall the IMPORTANT NOTE 1 on page 35. If you want to simulate new versions of `sea.dat` by `spec2sdat` you must normalise the spectrum to have $m_0 = 1$. \square

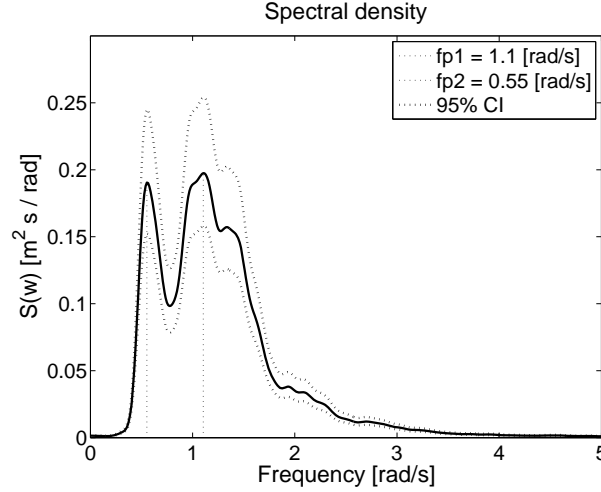


Figure 4.5: Estimated spectrum `SS` for data `sea.dat` with confidence bands.

Example 9. (contd.) (*Crest period*) We first consider the crest period, as we did in Example 8 on page 70, and also the proportion of crests with significant crest height, i.e. T_c when $A_c > H_s/2$, in the same way as we did for crest length. After that we will do the same for wave period and consider T_u when $A_c > H_s/2$. The proportion of crest periods with significant crest height should be the same as the proportion of wave periods with significant crest height, i.e. T_u when $A_c > H_s/2$. The difference between the two proportions gives an indication of the accuracy in the computation of the convolution $T_u = T_c + T_t$.

We can also compare the calculated proportion of significant crests with the proportion observed in data and with the approximative Rayleigh model. Finally, we estimate the density using KDE from data and compare to the theoretically computed one, based on the transformed Gaussian model.

For completeness we again estimate the transformation and find wave characteristics in the signal. The crest period, T_c , distribution, estimated from data, and the computed density are almost identical, except for very short waves; see Figure 4.6(a), obtained by the following commands. Note the last output variable `yn` in the call to `dat2steep`, which is an interpolated series, to be used later, when we need more exact values for the wave periods.

```
method = 0; rate = 2;
[S,H,Ac,At,Tcf,Tcb,z_ind,yn] = dat2steep(x,rate,method);
Tc = Tcf+Tcb;
t = linspace(0.01,8,200);
f_tc1emp = kde(Tc,{'L2',0},t);
pdfplot(f_tc1emp), hold on
```

```
f_tc1 = spec2tpdf(SS,[],'Tc',[0 8 81],0,4);
Chk1 = simpson(f_tc1.x{1},f_tc1.f) %Integral should be one
pdfplot(f_tc1,'-.'), hold off
```

We next compute the density of crest period, but now for waves with significant crest height, i.e. waves for which $Ac > Hs/2$. In the following call to `spec2tpdf` the restriction to $Ac > Hs/2$ is indicated by the argument `[Hs/2]`.

```
nit = 4;
f_tc2 = spec2tpdf(SS,[],'Tc',[0 8 81],[Hs/2],nit);
Pemp = sum(Ac>Hs/2)/sum(Ac>0)
      %Observed proportion of high crests
Chk2 = simpson(f_tc2.x{1},f_tc2.f)
      %Integral should be equal to probability of high crests
index = find(Ac>Hs/2);
f_tc2emp = kde(Tc(index),{'L2',0},t);
f_tc2emp.f = Pemp*f_tc2emp.f;
pdfplot(f_tc2emp), hold on
pdfplot(f_tc2,'-.'), hold off
```

The observed frequency of significant crests, `Pemp` = 0.1778 is close to the theoretically computed values, `Chk2` = 0.1802 with `nit` = 5 and `Chk2` = 0.1816 with `nit` = 4, obtained with computation times of 18 seconds and 4 seconds, respectively. A finer grid, `[0 8 161]` instead of `[0 8 81]` in `f_tc2`, will give an almost exact agreement with the empirical frequency with four times the computation time.

Observe that the Rayleigh approximation would give a probability equal to 0.1353. This is not surprising since crests in non-Gaussian sea tend to be higher than those in Gaussian sea.

Clearly, by changing the input `Hs/2` to any other fixed level `h`, and integrating the resulting density we obtain approximations to the probability $P(Ac > h)$. When `h` is a vector then it is more efficient to use the program `spec2Acdf` to compute $P(Ac > h)$, as in the crest height Example 8 on page 73. However, before using the program it is important to first use `spec2tpdf` and check that the computed density integrates to one. If not, the inputs `param` and `nit` have to be changed. Note that the integral `Chk1` is slightly greater than one.

Observe that in this section we are analysing apparent waves in time. If the input `'Tc'` in `spec2tpdf` is replaced by `'Lc'`, then we would consider waves in space and the proportion of significant crest would probably be very different. \square

Example 9. (contd.) (*Wave period for high-crest waves*) We turn now to the more difficult problem of wave period $Tu = Tc + Tt$, and compute the density for waves with significant crest height, $Ac > Hs/2$ and with $At > 0$. As mentioned, this differs from crest period Example 8 on page 70 in that it involves the distribution of the sum $Tc + Tt$ of two dependent random variables, with the same marginal distribution. Since the computations need to be done with high accuracy (the computed density is different for the unconditional wave period and for the period of waves with crest below a given threshold), we need to use a high positive `nit` value, so that the total sum of the density is close to 0.1789, or use a negative `nit`. We begin with negative `nit`, which gives faster results very close to the true density, and then take `nit` = 3.

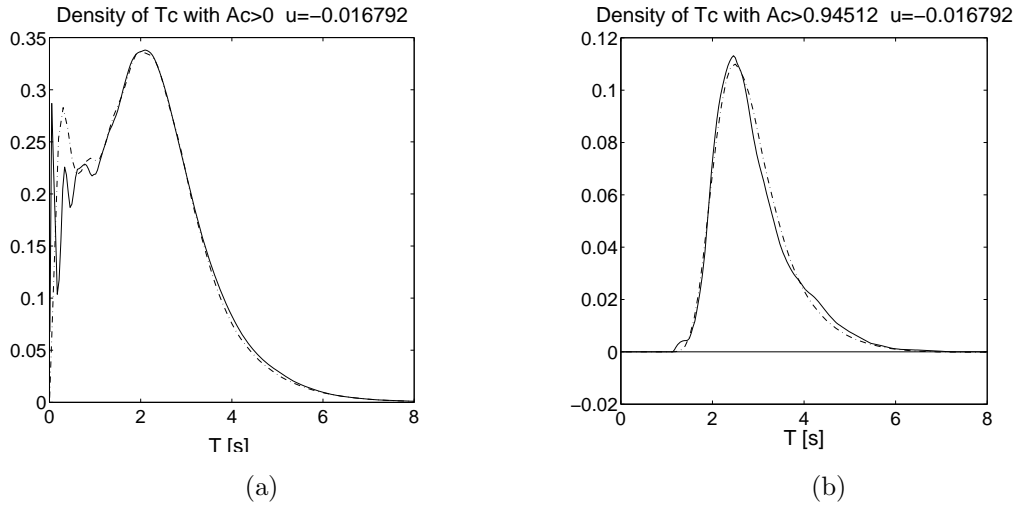


Figure 4.6: (a) Estimated density (KDE) of crest periods in `sea.dat` (solid line) compared with theoretically computed using `spec2tpdf` (dashed line). (b) The same for the waves with significant crest, i.e. $Ac > H_s/2$.

```
f_tun = spec2tccpdf(SS, [], 't>', [0 12 61], [Hs/2], [0], -1);
simpson(f_tun.x{1}, f_tun.f)
f_tu3 = spec2tccpdf(SS, [], 't>', [0 12 61], [Hs/2], [0], 3, 5);
simpson(f_tu3.x{1}, f_tu3.f)
pdfplot(f_tun), hold on
pdfplot(f_tu3, '--'), hold off
```

The integral of the density `f_tcn` is 0.1778, which is close to the previously computed value 0.1789. However, the execution time was 66 seconds, compared to 21 seconds for `f_t2`. The choice `nit=3` takes 3 minutes and give the integral 0.15. We have checked the program with `nit=5` (execution times 66 minutes), and the integrals was 0.17. The densities are shown in Figure 4.7(a). We can see that the density computed using `nit=-1` (dash-dotted line) is quite accurate, even if it slightly wiggly, being a random function with very small variance, and errors compensate each other giving almost perfect total probability mass. Note that another call of the program would give slightly different values and the total mass would also be changed. \square

Example 9. (contd.) (*Wave period for high-crest, deep-trough waves*) We finish the example with an even more interesting case, the density of wave period of waves with both significant crest and significant trough, i.e. really big waves. We first estimate the probability of such waves in the data; then we use the interpolated series `yn` from page 78.

```
[TC tc_ind v_ind] = dat2tc(yn, [], 'dw');
N = length(tc_ind);
t_ind = tc_ind(1:2:N);
c_ind = tc_ind(2:2:N);
Pemp = sum(yn(t_ind, 2) < -Hs/2 && ...
           yn(c_ind, 2) > Hs/2) / length(t_ind)
ind = find(yn(t_ind, 2) < -Hs/2 && yn(c_ind, 2) > Hs/2);
spwaveplot(yn, ind(2:4))
```

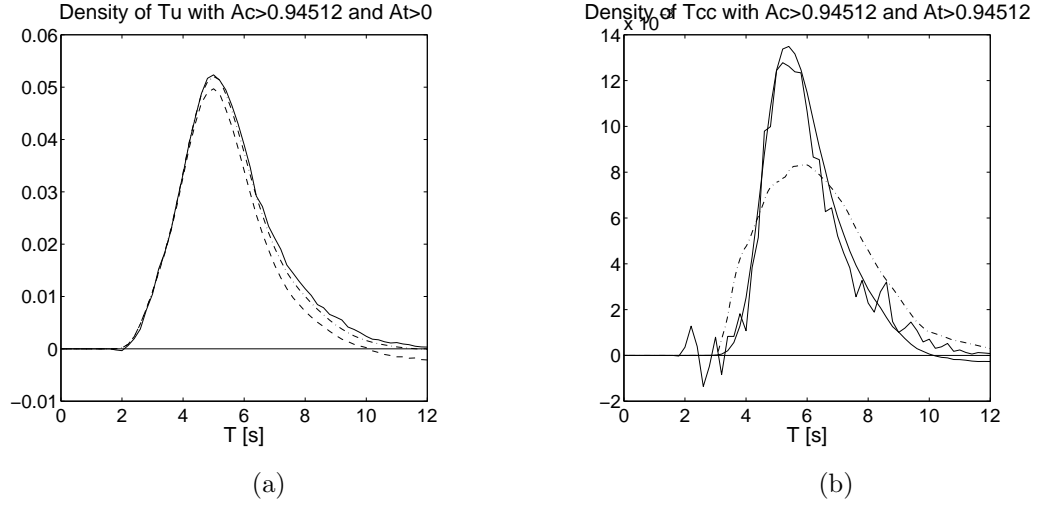


Figure 4.7: (a) Densities of upcrossing period T_u for waves with significant crest in the transformed Gaussian model for `sea.dat` computed with different degree of accuracy; (solid line) `nit=-1`; the dashed line is computed with `nit=5` and the dash dotted line with `nit=3`. (b) Densities of period T_u for waves with significant crest and trough in the same model; solid wiggled line `nit=-1`; solid smooth line `nit=4`; the dash dotted line is estimated from the data with KDE.

```
Tu = yn(v_ind(1+2*ind),1)-yn(v_ind(1+2*(ind-1)),1);
t = linspace(0.01,14,200);
f_tu2_emp = kde(Tcc,{'L2',0},t);
f_tu2_emp.f = Pemp*f_tu2_emp.f;
pdfplot(f_tu2_emp,'-.')
```

The probability is estimated to be $P_{\text{emp}} = 0.0370$, which is slightly higher than what we could expect if high crests and low troughs occur independently of each other (the probability would then be less than 0.025).

We turn now to computation of the probability using `spec2tccpdf` with `nit=-1`. However, we are here in a situation when the error in computations is of the order 10^{-3} , which is comparable to the values of the density itself. Hence the computed function will look very noisy.

```
f_tu2_n = spec2tccpdf(SS,[],'t>',[0 12 61],[Hs/2],[Hs/2],-1);
simpson(f_tu2_n.x{1},f_tu2_n.f), hold on
pdfplot(f_tu2_n), hold off
```

The execution time is less than one minute, and the computed probability with `nit = -1` is 0.0358, which is well in agreement with the number estimated from data. The more time-demanding `nit = 4` gives a much smoother pdf curve with almost the same integral, with an execution time of 15 minutes.

In Figure 4.7(b) we see the computed densities of wave period for these big waves. Those are well concentrated around the mean value. It is also compared to the KDE estimator. We have not tried to tune up the estimator that is based on only 20 values and hardly can be considered as accurate. \square

4.3 Joint density of crest period and crest height

In this section we shall present programs for joint characteristics of apparent waves. We shall be mostly concerned with crest period, crest position, and crest height. Since we also want to compare the theoretically derived densities with observations we wish to study a longer record of measurements than we did in the previous section. By doing so we will have more reliable statistical estimates of the densities, but on the other hand we face the problem that the sea state can change during the measured period – the process is simply not stationary.

The data come from the Gullfaks C platform, see Figure 4.8(a). See the help text of `gfaksr89` for a detailed description of the data and `northsea` for the instructions how the map showing location of the platform was drawn.

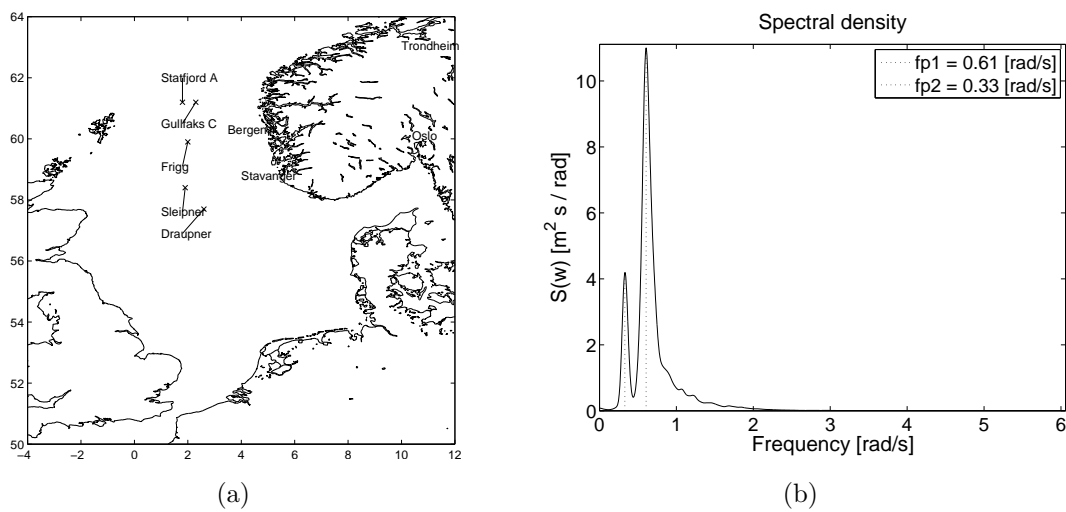


Figure 4.8: Location of Gullfaks C platform (a). The estimated spectrum (b).

WARNING: In the following examples we run the programs with maximum accuracy and hence we have long execution times. Usually one should use simpler and faster approximations at first experiments with complicated distributions. When one is satisfied with the results, one should compute the densities with the desired high accuracy. For testing own problems we recommend to start execution of programs with input parameter `speed = 9,8` (maximal speed is 9, the default is 4) and `nit = -1, 1`, (default is 2). These choices will produce fast but still useful approximations.

4.3.1 Preliminary analysis of data

Example 10. (*Analysis of Gullfaks data*) We begin with loading the data, estimating spectrum, finding the transformation `g`, and checking crest period density. Observe that the data is sampled with 2.5 [Hz], what may cause some interpolation errors in the estimated densities.

```
yy = load('gfaksr89.dat');
SG = dat2spec(yy);
si = sqrt(spec2mom(SG,1));
```



```

SG.tr = dat2tr(yy);
Hs = 4*si
v = gaus2dat([0 0],SG.tr); v = v(2)

```

The spectrum has two peaks, see Figure 4.8(b). We are not checking different options to estimate the spectrum, but use the default parameters.

We shall now extract some simple wave characteristics, $T_c, T_t, T_{cf}, A_c, A_t$. All these are column vectors containing crest period, trough period, position of crest, crest height, and trough height, respectively. All vectors are ordered by number of a wave, i.e. all vectors contain characteristic of the i 'th wave in their position i .

```

[TC tc_ind v_ind] = dat2tc(yy,v,'dw');
N = length(tc_ind);
t_ind = tc_ind(1:2:N);
c_ind = tc_ind(2:2:N);
v_ind_d = v_ind(1:2:N+1);
v_ind_u = v_ind(2:2:N+1);
T_d      = ecross(yy(:,1),yy(:,2),v_ind_d,v);
T_u      = ecross(yy(:,1),yy(:,2),v_ind_u,v);
Tc = T_d(2:end)-T_u(1:end);
Tt = T_u(1:end)-T_d(1:end-1);
Tcf = yy(c_ind,1)-T_u;
Ac = yy(c_ind,2)-v;
At = v-yy(t_ind,2);

```

Here we used the routine `ecross` to interpolate the data to find the exact level crossings. We then compute the crest period density from spectrum and compare it with that observed in data.

```

t = linspace(0.01,15,200);
kopt3 = kdeoptset('hs',0.25,'L2',0);
ftc1 = kde(Tc,kopt3,t);
ftt1 = kde(Tt,kopt3,t);
pdfplot(ftt1,'k'), hold on
pdfplot(ftc1,'k-')
f_tc4 = spec2tpdf(SG,[],'Tc',[0 12 81],0,4,5);
f_tcn = spec2tpdf(SG,[],'Tc',[0 12 81],0,-1);
pdfplot(f_tcn,'b'), hold off

```

We do not present the graphical result for this computations but simply comment that the agreement between theory and data is very good for both densities, except for observed long waves, which have somewhat longer periods (about 0.25 seconds) than theoretically computed. It is not much for a signal with 2.5 [Hz] sampling frequency. There is also the possibility that the swell peak in the spectrum is too much smoothed. \square

4.3.2 Joint distribution of crest period and height

We turn now to the joint density for the wave crest variables T_c, T_{cf}, A_c . We shall compute the empirical densities from the observations and compute the theoretical ones from the transformed Gaussian process with estimated spectrum and the transformation using the function `spec2thpdf`. This function computes many joint characteristics of the half wave, i.e. the part of the signal between the consecutive crossings of a still water level – most of them are simply functions of the triple T_c, T_{cf}, A_c . (Execute `help spec2thpdf` for a complete list).

In a special case, when the so called crest velocity is of interest, $V_{cf} = A_c/T_{cf}$, the joint density of V_{cf}, A_c is computed by the program `spec2vhpdf`, which is a simplified and modified `spec2thpdf` program.

Example 10. (contd.) (*Position and height of crest for wave with given period*) We shall first consider waves with crest period $T_c \approx 4.5$ seconds. Obviously the position of the crest of such waves is not constant, but varies from wave to wave. The following commands estimate the density of crest position and height for waves with $T_c \approx 4.5$ seconds, and plot the results in Figure 4.9(a).

```
ind = find(4.4 < Tc && Tc < 4.6);
f_AcTcf = kde([Tcf(ind) Ac(ind)], {'L2'}, [1 .5]);
plot(Tcf(ind), Ac(ind), '.'), hold on
pdfplot(f_AcTcf), hold off
```

Next, we compare the observed distribution with the theoretically computed joint density of T_c, T_{cf}, A_c for a fixed value of T_c . By this we mean that if we integrate the result we shall obtain the value of the density of T_c . Note that the distribution can also be computed using the program `spec2tpdf`.

```
opt1 = rindoptset('speed',5,'method',3);
opt2 = rindoptset('speed',5,'nit',2,'method',0);
f_tcfac1 = ...
    spec2thpdf(SG,[],'TcfAc',[4.5 4.5 46],[0:0.25:8],opt1);
f_tcfac2 = ...
    spec2thpdf(SG,[],'TcfAc',[4.5 4.5 46],[0:0.25:8],opt2);

pdfplot(f_tcfac1,'-.'), hold on
pdfplot(f_tcfac2)
plot(Tcf(ind), Ac(ind), '.'), hold off

simpson(f_tcfac1.x{1},simpson(f_tcfac1.x{2},f_tcfac1.f,1))
simpson(f_tcfac2.x{1},simpson(f_tcfac2.x{2},f_tcfac2.f,1))

f_tcf6 = spec2tpdf(SG,[],'Tc',[4.5 4.5 46],[0:0.25:8],6);
f_tc6.f(46)
```

We conclude that the densities `f_tcfac1` and `f_tcfac2` really integrate to the marginal density of T_c (`f_tc4.f(46)`), demonstrating the accuracy of the densities `f_tcfac1` and `f_tcfac2`. Note the difference in computation time.

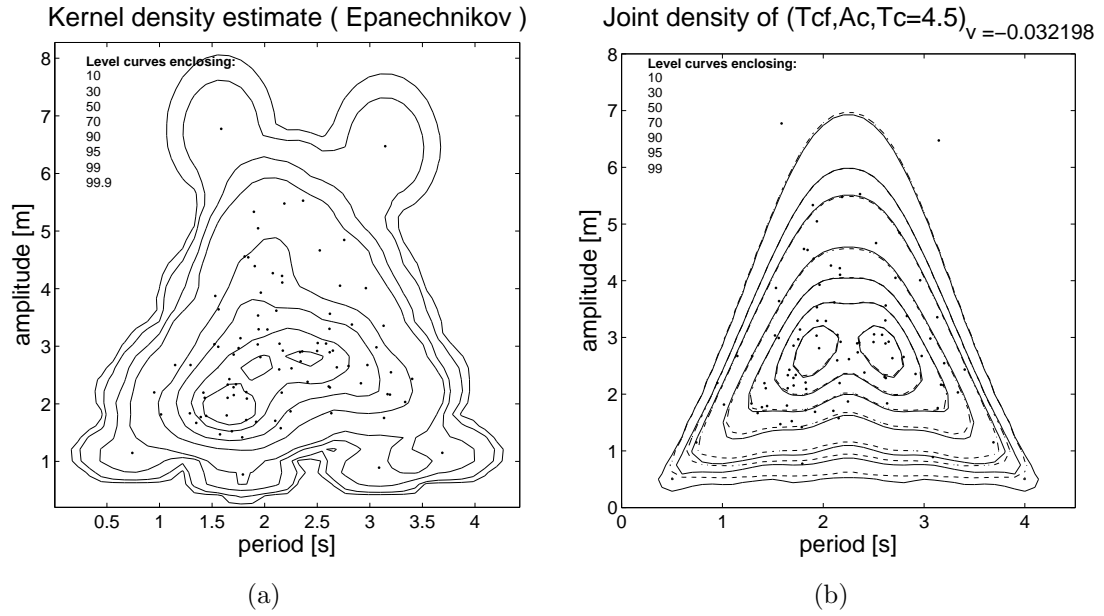


Figure 4.9: Distribution of crest position and crest height for Gullfaks waves with crest period $T_c = 4.5$ [s]. (a) The estimated (KDE) density of crest position and height together with observations (dots). (b) The theoretically computed density with `nit = -1, 2` and the data.

In Figure 4.9(a) the estimated (KDE) joint density is given and it should be compared with Figure 4.9(b), where the theoretical density is presented. Here we can really see the advantage of the theoretically computed densities. Even if we have here used a long record of wave data, there is not enough of waves to make a reliable estimate of the joint density, and in a standard 20 minutes records there would be far too few observations. \square

As we have mentioned already the integral over the crest position of the computed densities is equal to the joint density of crest period and height. So in order to get the whole density of T_c , Ac one needs to execute the previous program to obtain the density of T_c , T_{cf} , Ac for different values of T_c and integrate out the variable T_{cf} , and this will take some time. However, most time is spent on the computation of the density of long and small waves, and these are not interesting. Hence we can start to compute the joint density of T_c, Ac for significant waves.

Example 10. (contd.) (*Joint crest period/amplitude for significant waves*) We compute the joint density of T_c, Ac of significant waves in the Gullfaks data in order to compare the distribution with the Longuet-Higgins approximation; see Section 3.3.2. The following call takes substantial time (35 minutes), and gives the “exact” distribution. It is not included in the “fast” version of the command file `Chapter4.m`.

```
f_tcac_s = spec2thpdf(SG, [], 'TcAc', [0 12 81], [Hs/2:0.1:2*Hs], opt1);
```

Next, we find the modified Longuet-Higgins density, i.e. the density with transformed crest heights. The original LH-density underestimates the high crests with up to one meter. We can see that for significant waves and the present spectrum the modified Longuet-Higgins density is quite accurate.

```

mom = spec2mom(SS,4,[],0);
t = f_tcac_s.x{1}; h = f_tcac_s.x{2};
flh_g = lh83pdf(t',h',[mom(1),mom(2),mom(3)],SS.tr);
ind = find(Ac>Hs/2);
plot(Tc(ind), Ac(ind),'.''); hold on
pdfplot(flh_g,'k-.''); pdfplot(f_tcac_s); hold off

```

In Figure 4.10(a) the theoretical density is plotted with solid lines and the transformed LH-density with dash dotted lines. We can see that the simple approximation is working very well, even if it gives slightly too short periods.

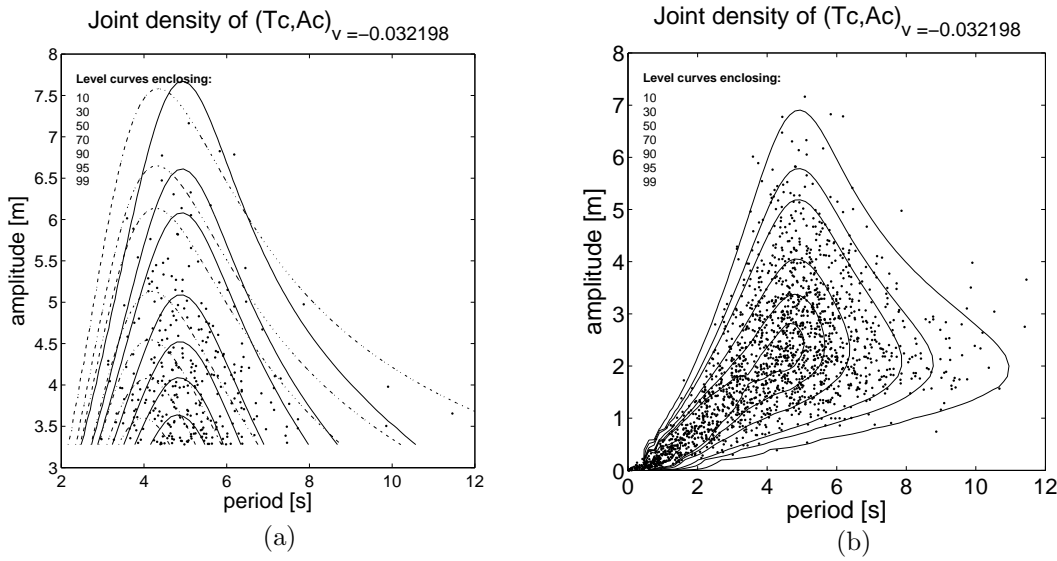


Figure 4.10: Joint density of T_c and A_c for the transformed Gaussian model of the sea measurements from Gullfaks C platform (solid line) compared with the transformed Longuet-Higgins density (dash dotted line) and the data (dots) for waves with significant crest.

Finally, we compute the density for all wave heights.

```

f_tcac = spec2thpdf(SG,[],'TcAc',[0 12 81],[0:0.2:8],opt1);
pdfplot(f_tcac)

```

In Figure 4.10(b) the theoretical density is compared with the data, and as we see, the agreement is again quite good. This routine take about 15 minutes to run, and it is not executed in the default version of the command file `Chapter4.m`. \square

4.3.3 Joint density of crest height and trough depth

In previous sections we presented programs that compute joint densities of different wave characteristics. We started with marginal densities of crest and trough periods T_c , T_t , and then the joint density of T_c, T_t was derived in order to get the full wave period T_u . Next, we considered T_c, T_{cr}, A_c , crest period, crest position, and crest height. (The same is possible for T_t, T_{tb}, A_t .) However, in order to fully describe a wave we should compute

the joint density of $T_c, T_{ac}, A_c, T_t, T_{at}, A_t$. It is possible to write a program that computes such six dimensional densities and it would not take more then 10 minutes of computer time to compute the density for 200, say, different combinations of the characteristics. But in order to describe a six dimensional density one needs may be 100 000 combinations of values and this is not practically possible yet. Observe that, by numerical differentiation, one can compute the joint density of T_c, A_c, T_t, A_t using `spec2tccpdf` (or `spec2AcAt`). This approach is rather time consuming, see [44].

There are however some alternatives. From previous studies we know that very high crests (troughs) occur at the local maximum (minimum) closest to a zero crossing. We also know that it is the derivative at the crossing that mainly determines the height of the wave crest. Consequently, the steepness of a wave is mainly determined by the height and location of *the last minimum before* and *the first maximum after* an upcrossing of the still water level. This particular type of min-to-max wave is called a *mean separated minimum-to-maximum* wave. In general, we can introduce a *v-level separated min-to-max wave* to be the last minimum before and the first maximum after a level v upcrossing. The distance between the mean-level separated minima and maxima, denoted T_{mM} can be used to compute steepness of a wave, see [15, 16] for details. The function `spec2mmtpdf` computes the joint density of v-separated wave length and other characteristics of the v-separated minima and maxima. It also computes the joint density of all pairs of local minima, maxima and the distance in between; see [44] for examples.

4.3.4 Min-to-max distributions – Markov method

We shall now investigate another wave characteristic, the min-to-max wave distribution, including the min-to-max period and amplitude. This requires the joint density of the height of a local minimum (maximum) and the following maximum (minimum). The WAFO routine that handles this is called `spec2mmtpdf`, and calculates, i.a. the joint density of the height of a maximum and the following minimum; see the help text to `spec2mmtpdf`.

One important application of the min-to-max distribution is for approximation of the joint density of A_c, A_t , the crest and trough amplitudes, by approximating the sequence of local extremes in a transformed Gaussian model by a Markov chain; see [73] for detailed description of the algorithm. The approximation has been checked on many different sea data giving very accurate results, and it is also relatively fast. There is another program `spec2cmat` which is somewhat less accurate but even faster. It is used in Chapter 5 to compute Markov matrices and rainflow matrices used in fatigue.

Example 11. (*min-max problems with Gullfaks data*) In this example we continue the analysis of the Gullfaks C platform data. First we shall retrieve the sequence of turning points, i.e. the minima and maxima, in `yy` and calculate the theoretical distribution.

```
opt2 = rindoptset('speed',5,'nit',2,'method',0);
tp = dat2tp(yy);
Mm = fliplr(tp2mm(tp));
fmm = kde(Mm);
f_mM = spec2mmtpdf(SG,[],'mm',[],[-7 7 51],opt2);
pdfplot(f_mM,'-.'), hold on
pdfplot(fmm,'k-'), hold off
```

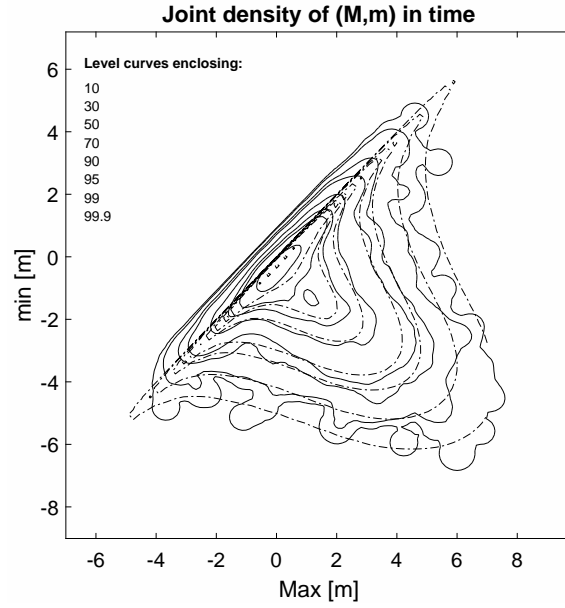


Figure 4.11: Joint density of maximum and the following minimum for the transformed Gaussian model of the sea measurements from Gullfaks C (dash-dotted lines) compared with the estimated (KDE) density from data (solid lines).

In Figure 4.11 we can see that the theoretically computed density agrees very well with the estimated one, even with an as low a `nit` as 2. \square

Example 12. (*Crest-trough distribution from min-max transitions*) We turn now to the joint density of crest and trough. We first compute the exact distribution with the help of `spec2mmtpdf`, and then compare the result with that obtained by means of the Markov approximation for the stillwater-separated min-max sequence; see Section 5.2.3.

```
ind = find(Mm(:,1)>v && Mm(:,2)<v);
Mmv = abs(Mm(ind,:)-v);
fmmv = kde(Mmv,'epan');
f_vmm = spec2mmtpdf(SG,[],'vmm',[],[-7 7 51],opt2);
pdfplot(fmmv,'k-'), hold on
pdfplot(f_vmm,'-.'), hold off
```

Then we compute the joint density of crest and trough using the Markov approximation to the sequence of local extremes (sequence of turning points `tp`).

```
facat = kde([Ac At]);
f_acat = spec2mmtpdf(SG,[],'AcAt',[],[-7 7 51],opt2);
pdfplot(f_acat,'-.'), hold on
pdfplot(facat,'k-'), hold off
```

Now we are in the position to check our two methods, the Markov method, where the min-to-max sequence is approximated by a Markov chain, and the replacement of the true min-to-max transition probabilities by the transition probabilities that are valid for the stillwater-separated min-to-max values. The results are presented in Figure 4.12. We see

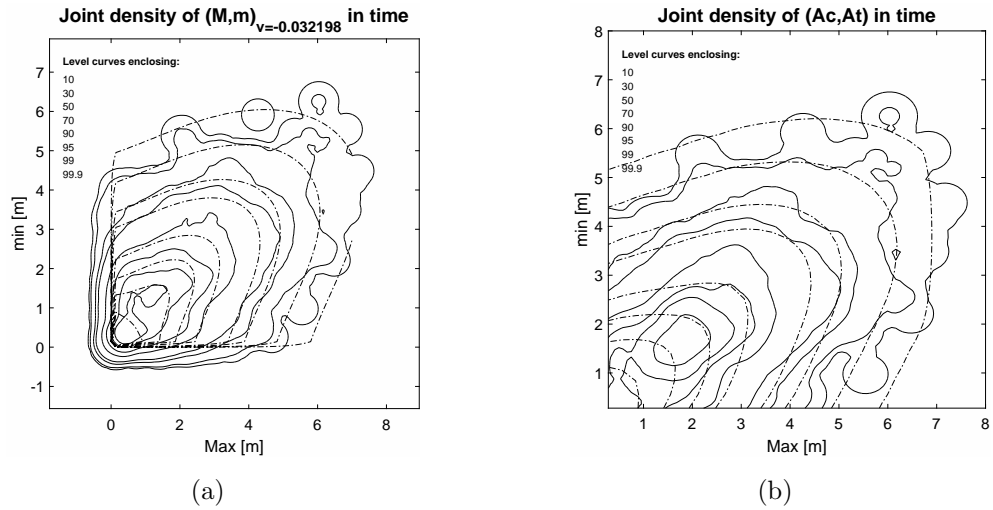


Figure 4.12: Estimated joint density (KDE) of stillwater-separated min-to-max values for the measurements from Gullfaks C (solid line) compared with: (a) the transformed Gaussian model for the measurements (dash-dotted line). (b) Markov approximation for the joint density of crest and trough height A_c, A_t (dash-dotted line).

in (a) that the stillwater-separated min-to-max distribution miss a considerable number of min-to-max values, which fall on the same side of the still water level. On the other hand, figure (b) indicates that the Markov assumption is acceptable. \square

4.4 WAFO wave characteristics routines

help trgauss

Module TRGAUSS in WAFO Toolbox.

Version 2.5.2 07-Feb-2011

Readme - New features, bug fixes, and changes in TRGAUSS.

Misc

createpdf - PDF struct constructor.
 pdfplot - Plot contents of pdf structures.
 trplot - Plots transformation, g, eg. estimated with dat2tr.

Transforms and non-linearities

dat2gaus - Transforms x using the transformation g.
 gaus2dat - Transforms xx using the inverse of g.
 testgaussian - Test if a stochastic process is Gaussian.
 spec2skew - Estimates the moments of 2'nd order non-linear waves.
 trangood - Makes a transformation that is suitable for efficient transforms.
 tranproc - Transforms process X and up to four derivatives.
 trmak - Put together a transformation object.
 troptset - Create or alter TRANSFORM OPTIONS structure.
 trunmak - Split a transformation object into its pieces.

Transformed Gaussian model estimation

cdf2tr - Estimate transformation, g, from observed CDF.
 dat2tr - Estimate transformation, g, from data.
 hermitetr - Estimate transformation, g, from the first 4 moments.
 ochitr - Estimate transformation, g, from the first 3 moments.
 lc2tr - Estimate transformation, g, from observed crossing intensity.
 lc2tr2 - Estimate transformation, g, from observed crossing intensity, version 2.

Gaussian probabilities and expectations

cdfnorm2d - Bivariate normal cumulative distribution function.
 prbnorm2d - Bivariate normal probability.
 prbnormnd - Multivariate normal probability by Genz' algorithm.
 prbnormndpc - Multivariate normal probabilities with product correlation.
 prbnormtnd - Multivariate normal or T probability by Genz' algorithm.
 prbnormtndpc - Multivariate normal or T probability with product correlation structure.

- rind - Computes multivariate normal expectations.
- rindoptset - Create or alter RIND OPTIONS structure.

Probability density functions (pdf) or intensity matrices

- chitwo2lc_sorm - SORM-approximation of crossing intensity, noncentral χ^2 process.
- chitwo2lc_sp - Saddlepoint approximation of crossing intensity, noncentral χ^2 process.
- dirsp2chitwo - Parameters in non-central CHI-TWO process for directional Stokes waves.
- iter - Calculates a Markov matrix given a rainflow matrix.
- iter_mc - Calculates a kernel of a MC given a rainflow matrix.
- mc2rfc - Calculates a rainflow matrix given a Markov chain with kernel f_{xy} .
- mctp2rfc - Rainflow matrix given a Markov matrix of a Markov chain of turning points.
- mctp2tc - Calculates frequencies for the upcrossing troughs and crests.
- nt2fr - Calculates the frequency matrix given the counting distribution matrix.
- spec2cmat - Joint intensity matrix for cycles (max,min)-, rainflow- and (crest,trough).
- spec2mmtpdf - Joint density of Maximum, minimum and period.
- spec2tccpdf - Density of crest-to-crest wave-period or -length.
- spec2thpdf - Joint density of amplitude and period/wave-length characteristics.
- spec2tpdf - Density of crest/trough- period or length.
- spec2tpdf2 - Density of crest/trough- period or length, version 2.
- specq2lc - Saddlepoint approximation of crossing intensity for quadratic sea.
- th2vhpdf - Transform joint T-H density to V-H density.

Cumulative distribution functions (cdf)

- cdflomax - CDF for local maxima for a zero-mean Gaussian process.
- spec2AcAt - Survival function for crests and troughs, $R(h1,h2)=P(Ac>h1,At>h2)$.
- spec2Acdf - CDF for crests $P(Ac\leq h)$ or troughs $P(At\leq h)$.

CHAPTER 5

Fatigue load analysis and rain-flow cycles

This chapter contains some elementary facts about random fatigue and how to compute expected fatigue damage from a stochastic, stationary load process. The commands can be found in `Chapter5.m`, taking a few seconds to run.

5.1 Random fatigue

5.1.1 Random load models

This chapter presents some tools from WAFO for analysis of random loads in order to assess random fatigue damage. A complete list of fatigue routines can be obtained from the help function on `fatigue`.

We shall assume that the load is given by one of three possible forms:

1. As measurements of the stress or strain function with some given sampling frequency in Hz. Such loads will be called measured loads and denoted by $x(t)$, $0 \leq t \leq T$, where t is time and T is the duration of the measurements.
2. In the frequency domain (that is important in system analysis) as a power spectrum. This means that the signal is represented by a Fourier series

$$x(t) \approx m + \sum_{i=1}^{[T/2]} a_i \cos(\omega_i t) + b_i \sin(\omega_i t)$$

where $\omega_i = i \cdot 2\pi/T$ are angular frequencies, m is the mean of the signal and a_i, b_i are Fourier coefficients. The properties are summarized in a spectral density as in described in Section 2.2.

3. In the rainflow domain, i.e. the measured load is given in the form of a rainflow matrix.

We shall now review some simple means to characterize and analyze loads which are given in any of the forms (1)–(3), and show how to derive characteristics, important for fatigue evaluation and testing.

We assume that the reader has some knowledge about the concept of cycle counting, in particular rainflow cycles, and damage accumulation using Palmgren-Miners linear damage accumulation hypotheses. The basic definitions are given in the end of this introduction. Another important property is the crossing spectrum $\mu(u)$, introduced in Section 2.1, defined as the intensity of upcrossings of a level u by $x(t)$ as a function of u .

The process of damage accumulation depends only on the values and the order of the local extremes (maxima and minima), in the load. The sequence of local extremes is called the *sequence of turning points*. The irregularity factor α measures how dense the local extremes are relatively to the mean frequency f_0 . For a completely regular function there would be only one local maximum between upcrossings of the mean level, giving irregularity factor equal to one. In the other extreme case, there are infinitely many local extremes giving irregularity factor zero. However, if the crossing intensity $\mu(u)$ is finite, most of those local extremes are irrelevant for the fatigue and should be disregarded by means of some smoothing device.

A particularly useful filter is the so-called *rainflow filter* that removes all local extremes that build rainflow cycles with amplitude smaller than a given threshold. We shall always assume that the signals are rainflow filtered; see Section 5.2.1.

If more accurate predictions of fatigue life are needed, then more detailed models are required for the sequence of turning points. Here the Markov chain theory has shown to be particularly useful. There are two reasons for this:

- the Markov models constitute a broad class of processes that can accurately model many real loads,
- for Markov models, the fatigue damage prediction using rainflow method is particularly simple, [70] and [33].

In the simplest case, the necessary information is the intensity of pairs of local maxima and the following minima, summarized in the so-called Markov matrix or min-max matrix. The dependence between other extremes is modelled using Markov chains, see [77] and [22].

5.1.2 Damage accumulation in irregular loads

In laboratory experiments, one often subjects a specimen of a material to a constant amplitude load, e.g. $L(t) = s \sin(\omega t)$, where s and ω are the constant amplitude and frequency, and one counts the number of cycles (periods) until the specimen breaks. The number of load cycles until failure, $N(s)$, as well as the amplitudes s are recorded. For small amplitudes, $s < s_\infty$, the fatigue life is often very large, and is set to infinity, $N(s) \approx \infty$, i.e. no damage will be observed even during an extended experiment. The amplitude s_∞ is called *the fatigue limit* or *the endurance limit*. In practice, one often uses a simple model for the S-N curve, also called the Wöhler curve, i.e. the relation between the amplitude s and $N(s)$,

$$N(s) = \begin{cases} K^{-1} s^{-\beta}, & s > s_\infty, \\ \infty, & s \leq s_\infty, \end{cases} \quad (5.1)$$

where K and β are material dependent parameters. Often K is considered as a random variable, usually lognormally distributed, i.e. with $K^{-1} = E\epsilon^{-1}$ where $\ln E \in N(0, \sigma_E^2)$, and ϵ, β are fixed constants.

For irregular loads, also called variable amplitude loads, one often combines the S-N curve with a cycle counting method by means of the *Palmgren-Miner linear damage accumulation theory*, to predict fatigue failure time. A cycle counting procedure is used to form equivalent load cycles, which are used in the life prediction.

If the k :th cycle in an irregular load has amplitude s_k then it is assumed that it causes a damage equal to $1/N(s_k)$. The total damage at time t is then

$$D(t) = \sum_{t_k \leq t} \frac{1}{N(s_k)} = K \sum_{t_k \leq t} s_k^\beta = K D_\beta(t), \quad (5.2)$$

where the sum contains all cycles that have been completed up to time t . Then, the fatigue life time T^f , say, is shorter than t if the total damage at time t exceeds 1, i.e. if $D(t) > 1$. In other words, T^f is defined as the time when $D(t)$ crosses level 1 for the first time.

A very simple predictor of T^f is obtained by replacing $K = E^{-1}\epsilon$ in Eq. (5.2) by a constant, for example the median value of K , which is equal to ϵ , under the lognormal assumption. For high cycle fatigue, the time to failure is long, more than $10^5/f_0$, and then for stationary (and ergodic and some other mild assumptions) loads, the damage $D_\beta(t)$ can be approximated by its mean $E(D_\beta(t)) = d_\beta \cdot t$. Here d_β is the *damage intensity*, i.e. how much damage is accumulated per unit time. This leads to a very simple predictor of fatigue life time,

$$\hat{T}^f = \frac{1}{\epsilon d_\beta}. \quad (5.3)$$

5.1.3 Rainflow cycles and hysteresis loops

The now commonly used cycle counting method is the rainflow counting, which was introduced 1968 by Matsuishi and Endo in [54]. It was designed to catch both slow and rapid variations of the load by forming cycles by pairing high maxima with low minima even if they are separated by intermediate extremes. Each local maximum is used as the maximum of a *hysteresis loop* with an amplitude that is computed by the rainflow algorithm. A new definition of the rainflow cycle, equivalent to the original definition, was given 1987 by Rychlik, [68]. The formal definition is also illustrated in Figure 5.1.

Definition 5.1 (Rainflow cycle) *From each local maximum M_k one shall try to reach above the same level, in the backward (left) and forward (right) directions, with an as small downward excursion as possible. The minima, m_k^- and m_k^+ , on each side are identified. The minimum that represents the smallest deviation from the maximum M_k is defined as the corresponding rainflow minimum m_k^{RFC} . The k :th rainflow cycle is defined as (m_k^{RFC}, M_k) .*

If t_k is the time of the k :th local maximum and the corresponding rainflow amplitude is $s_k^{\text{RFC}} = M_k - m_k^{\text{RFC}}$, i.e. the amplitude of the attached hysteresis loop, then the total damage at time t is

$$D(t) = \sum_{t_k \leq t} \frac{1}{N(s_k^{\text{RFC}})} = K \sum_{t_k \leq t} (s_k^{\text{RFC}})^\beta = K D_\beta(t), \quad (5.4)$$

where the sum contains all rainflow cycles that have been completed up to time t .

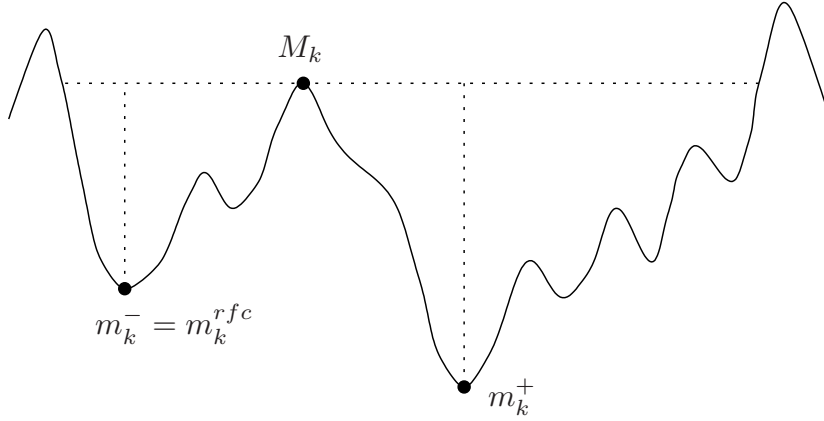


Figure 5.1: Definition of the rainflow cycle as given by [68].

To use Eq. (5.3) to predict the fatigue life we need the damage intensity d_β , i.e. the damage per time unit caused by the rainflow cycles. If there are on the average f_0 maxima¹ per time unit, after rainflow filtering, and equally many rainflow cycles, and each rainflow cycle causes an expected damage $\epsilon E(1/N_{\text{SRFC}})$ it is clear that the damage intensity is equal to

$$d_\beta = f_0 E \left((S^{\text{RFC}})^\beta \right).$$

Thus, an important parameter for prediction of fatigue life is the distribution of the rainflow amplitudes and in particular the expected value of the rainflow amplitudes raised to the material dependent power parameter β . WAFO contains a number of routines for handling the rainflow cycles in observed load data and in theoretical load models.

5.2 Load cycle characteristics

5.2.1 Rainflow filtered load data

In previous chapters we have presented models for sea wave data, treated as functions of time. The models can be used in response analysis for marine structures to wave forces or to compute wave characteristics for specified random wave models, e.g. those defined by their power spectrum.

Measured wave or load signals are often very noisy and need to be smoothed before further analysis. A common practice is to use a bandpass filters to exclude high frequencies from the power spectrum and to filter out slow trends. If the function is modelled by a transformed Gaussian process \mathbf{xx} , as described in Section 2.2.4, such a filtration is performed on the inverse transformed signal $\mathbf{yy} = \mathbf{g}(\mathbf{xx})$. Obviously, one should not over-smooth data since that will affect the height of extreme waves or cycles. Consequently, if the signal is still too irregular even after smoothing, this is an indication that one should use the trough-to-crest wave concept, defined as in Table 3.1, instead of the simpler min-to-max cycles. Chapter 4 of this tutorial was aimed at showing how one can compute the crest-to-trough wave characteristics from a Gaussian or transformed Gaussian model.

¹We have defined f_0 as the mean level upcrossing frequency, i.e. the mean number of times per time unit that the load upcrosses the mean level. Thus there are in fact at least f_0 local maxima per time unit. Since the rainflow filter reduces the number of cycles, we let f_0 here be *defined as* the average number of rainflow cycles per time unit.

The trough-to-crest cycle concept is a nonlinear means to remove small irregularities from a load series. Another nonlinear method to remove small cycles from data is the rainflow filtering, introduced in [72], and included in the WAFO toolbox. For completeness, we describe the algorithm of the rainflow filter.

In this tutorial we have used a simple definition of rainflow cycles that is convenient for functions with finitely many local maxima and minima. However, rainflow filters and rainflow cycles can be defined for very irregular functions, like a sample function of Brownian motion, where there are infinitely many local extremes in any finite interval, regardless how small. This is accomplished by defining the rainflow minimum $m^{\text{RFC}}(t)$ for all time points t of a function $x(t)$ in such a way that the rainflow amplitude $x(t) - m^{\text{RFC}}(t)$ is zero if the point $x(t)$ is not a strict local maximum of the function; see [72] for more detailed discussion. Now, a *rainflow filter with threshold h* , extracts all rainflow cycles $(m^{\text{RFC}}(t), x(t))$ such that $x(t) - m^{\text{RFC}}(t) > h$. Consequently, if $h < 0$ then the signal is unchanged by the filter, if $h = 0$ we obtain a sequence of turning points, and, finally, if $h > 0$, all small oscillations are removed, see Figure 5.7 for an example.

5.2.2 Oscillation count and the rainflow matrix

The rainflow count is a generalization of the crossing count. The crossing spectrum counts the number of times a signal upcrosses any level u . More important for fatigue damage is the *oscillation count*, $N^{\text{OSC}}(u, v)$ that counts the number of times a signal upcrosses an interval $[u, v]$. The oscillation count is thus a function of two variables, u and v , and is plotted as a bivariate count. The oscillation count is a counting distribution for the rainflow cycles. Consequently, if the matrix **Nosc** with elements $N^{\text{OSC}}(u_j, u_i)$ is known, for a discrete set of levels, $u_1 \leq u_2 \leq \dots \leq u_n$, we can compute the frequency (or rather histogram) matrix of the rainflow count by means of the WAFO-function **nt2fr** and obtain the matrix **Frfc** = **nt2fr(Nosc)**, in fatigue practice called the *rainflow matrix*. Knowing the rainflow matrix of a signal one can compute the oscillation count by means of the inverse function **fr2nt**.

The rainflow matrix will play an important role in the analysis of a rainflow filtered signal. Let $x(t)$ be a measured signal and denote by $x_h(t)$ the rainflow filtered version, filtered with threshold h . Now, if we know a rainflow matrix **Frfc**, say, of x , then the rainflow matrix of x_h is obtained by setting some sub-diagonals of **Frfc** to zero, since there are no cycles in x_h with amplitudes smaller than h . Thus, the oscillation count of x_h can be derived from the oscillation count of x .

Note that extracting a sequence of troughs and crests $(m_i^{\text{TC}}, M_i^{\text{TC}})$ from the signal is closely related to rainflow filtering. Given a reference level u^{TC} , the sequence $(m_i^{\text{TC}}, M_i^{\text{TC}})$ can be obtained by first removing all rainflow cycles (m_j^{RFC}, M_j) such that $M_j < u^{\text{TC}}$ or $m_j^{\text{RFC}} > u^{\text{TC}}$ and then finding the min-to-max pairs in the filtered signal.

Clearly, the oscillation count is an important characteristic of irregularity of a sea level function, and similarly, the expected oscillation count, also called an *oscillation intensity matrix*, is an important characteristic of the random processes used as a model for the data. Consequently we face two problems: how to compute the oscillation intensity for a specified model, and if knowing the oscillation intensity, how can one find an explicit and easy way to handle random processes with this intensity. Note that by solving these two problems one increases the applicability of rainflow filters considerably. Since then,

given a random process, one can find its oscillation intensity, and next one can compute the oscillation intensity of the rainflow filtered random process, and finally, find a random process model for the filtered signal.

5.2.3 Markov chain of turning points, Markov matrix

An upcrossing of an interval $[u, v]$ occurs if the process, after an upcrossing of the level u , passes the higher level v before it returns below u . Therefore, the oscillation intensity is closely related to a special first passage problem, and it can be practically handled if some Markov structure of the process is assumed. While Gaussian processes are an important class of models for linear filtering, Markov processes are the appropriate models as far as rainflow filtering is concerned. In this section a class of models, the so called Markov chain of turnings points will be introduced.

For any load sequence we shall denote by TP the sequence of turning points. The sequence TP will be called a *Markov chain of turning points* if it forms a Markov chain, i.e. if the distribution of a local extremum, given all previous extrema, depends only on the value and type (minimum or maximum) of the most recent previous extremum. The elements in the histogram matrix of min-to-max cycles and max-to-min cycles are equal to the observed number of transitions from a minimum (maximum) to a maximum (minimum) of specified height. Consequently, the probabilistic structure of the Markov chain of turning points is fully defined by the expected histogram matrix of min-to-max and max-to-min cycles; sometimes called *Markov matrices*. Note that for a transformed Gaussian process, a Markov matrix for min-to-max cycles was computed in Section 4.3.4 by means of the WAFO function `spec2mmtpdf`. In WAFO there is also an older version of that program, called `spec2cmat`, which we shall use in this chapter. The max-to-min matrix is obtained by symmetry.

Next, the function `mctp2tc` (= Markov Chain of Turning Points to Trough Crests), computes the trough2crest intensity, using a Markov matrix to approximate the sequence of turning points by a Markov chain. This approximation method is called the *Markov method*. Be aware that the Markov matrix is not the transition matrix of the Markov chain of turning points, but the intensity of different pairs of turning points.

Figure 5.2 shows the general principle of a Markov transition count between turning points of local maxima and minima. The values have been discretized to levels labeled 1, ..., n, from smallest to largest.

Finding the expected rainflow matrix is a difficult problem and explicit results are known only for special classes of processes, e.g. if \mathbf{x} is a stationary diffusion, a Markov chain or a function of a vector valued Markov chain. Markov chains are very useful in wave analysis since they form a broad class of processes and for several sea level data, as well as for transformed Gaussian processes, one can observe a very good agreement between the observed or simulated rainflow matrix and that computed by means of the Markov method. Furthermore, Markov chains can be simulated in a very efficient way. However, the most important property is that, given a rainflow matrix or oscillation count of a Markov chain of turning points one can find its Markov matrix. This means that a Markov chain of turning points can be defined by either a Markov matrix \mathbf{FmM} or by its rainflow matrix \mathbf{Frfc} , and these are connected by the following nonlinear equation

$$\mathbf{Frfc} = \mathbf{FmM} + \mathcal{F}(\mathbf{FmM}), \quad (5.5)$$

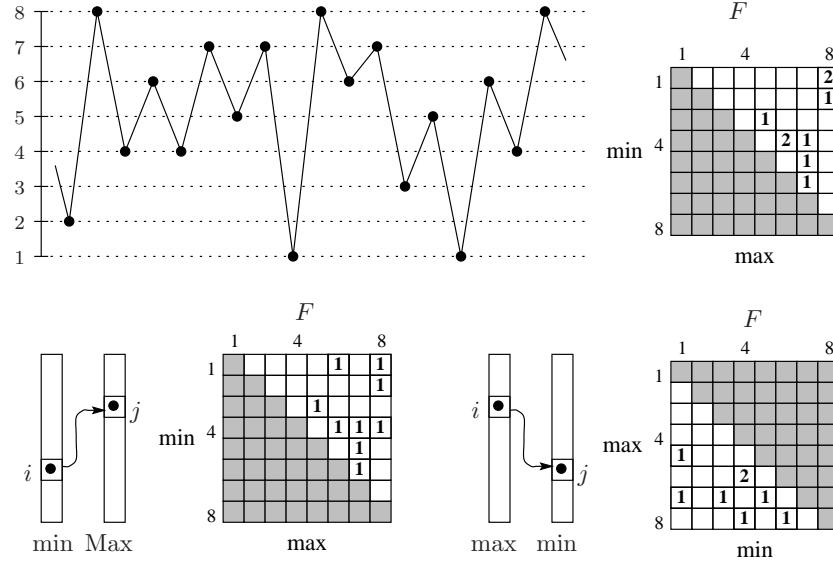


Figure 5.2: Part of a discrete load process where turning points are marked with \bullet . The scale to the left is the discrete levels. The transitions from minimum to maximum and from maximum to minimum are collected in the min-max matrix, F and max-min matrix, \hat{F} , respectively. The rainflow cycles are collected in the rainflow matrix, F^{RFC} . The numbers in the squares are the number of observed cycles and the grey areas are by definition always zero.

where \mathcal{F} is a matrix valued function, defined in [72], where also an algorithm to compute the inverse $(\mathcal{I} + \mathcal{F})^{-1}$ is given. The WAFO functions for computing Frfc from FmM are `mctp2rfm` and `mctp2rfc`, while the inverse, i.e. FmM as a function of Frfc , is computed by `arfm2mctp`. It might be a good idea to check the modules `cycles` and `trgauss` in WAFO for different routines for handling these matrices.

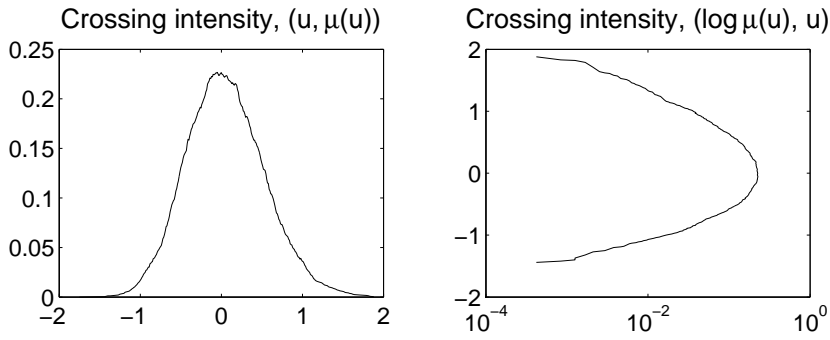
5.3 Cycle analysis with WAFO

In this section we shall demonstrate how WAFO can be used to extract rainflow cycles from a load sequence, and how the corresponding fatigue life can be estimated. The Markov method is used for simulation and approximation of real load sequences. We shall use three load examples, the deep water sea load, a simulated transformed Gaussian model, and a load sequence generated from a special Markov structure.

5.3.1 Crossing intensity

Basic to the analysis is the crossing intensity function $\mu(u)$, i.e. the number of times per time unit that the load up-crosses the level u , considered as a function of u . We illustrate the computations on the deep water sea waves data.

```
xx_sea = load('sea.dat');
tp_sea = dat2tp(xx_sea);
lc_sea = tp2lc(tp_sea);
T_sea = xx_sea(end,1)-xx_sea(1,1);
```

Figure 5.3: Level crossing intensity for `sea.dat`

```
lc_sea(:,2) = lc_sea(:,2)/T_sea;
subplot(221), plot(lc_sea(:,1),lc_sea(:,2))
title('Crossing intensity, (u, \mu(u))')
subplot(222), semilogx(lc_sea(:,2),lc_sea(:,1))
title('Crossing intensity, (log \mu(u), u)')
```

The routines `dat2tp` and `tp2lc` take a load sequence and extracts the turning points, and from this calculates the number of up-crossings as a function of level. The plots produced, Figure 5.3, show the crossing intensity plotted in two common modes, lin-lin of $(u, \mu(u))$ and log-lin of $(\log \mu(u), u)$.

We shall also have use for the *mean frequency* f_0 , i.e. the number of mean level up-crossings per time unit, and the *irregularity factor*, α , which is the mean frequency divided by the mean number of local maxima per time unit. Thus $1/\alpha$ is the average number of local maxima that occur between the mean level upcrossings.

To compute f_0 we use the MATLAB function `interp1`, (make help `interp1`), to find the crossing intensity of the mean level.

```
m_sea = mean(xx_sea(:,2));
f0_sea = interp1(lc_sea(:,1),lc_sea(:,2),m_sea,'linear')
extr_sea = length(tp_sea)/(2*T_sea);
alfa_sea = f0_sea/extr_sea
```

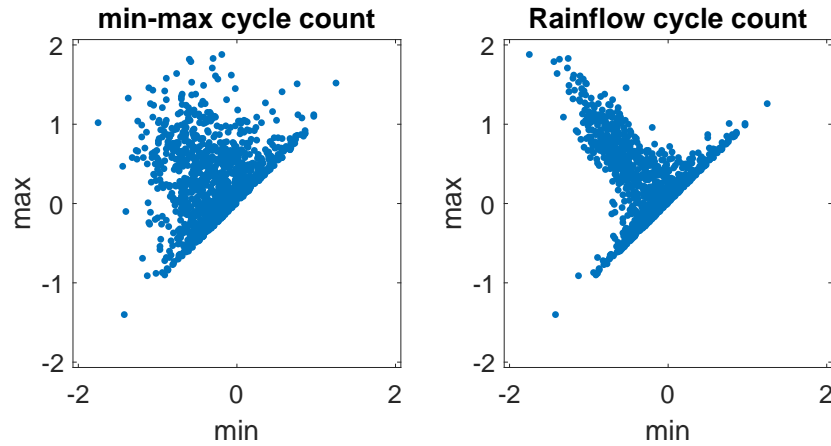
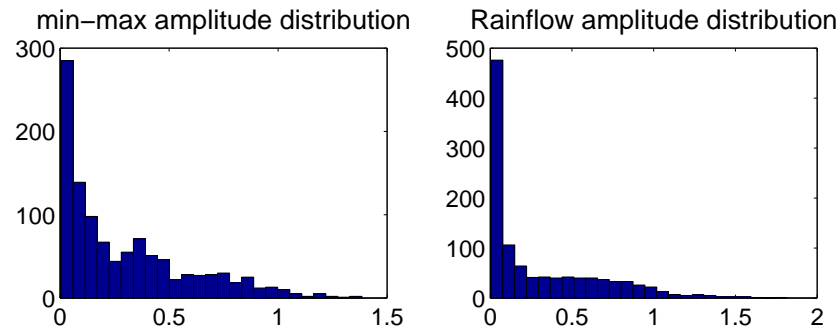
5.3.2 Extraction of rainflow cycles

We start by a study of rainflow cycles in the deep water sea data. Recall the definition of rainflow and min-max cycle counts. The demo program `democc` illustrates these definitions. To use it to identify the first few rainflow and min-max cycles, just use,

```
proc = xx_sea(1:500,:);
democc
```

Two windows will appear. In Demonstration Window 1, first mark the turning points by the button TP. Then choose a local maximum (with the buttons marked +1, -1, +5, -5) and find the corresponding cycle counts, using the buttons RFC, PT. The cycles are visualized in the other window.

We shall now examine cycle counts in the load `xx_sea`. From the sequence of turning points `tp` we find the rainflow and min-max cycles in the data set,

Figure 5.4: Rainflow and min-max cycle plots for `sea.dat`.Figure 5.5: min-max and rainflow cycle distributions for `sea.dat`.

```
RFC_sea = tp2rfc(tp_sea);
mM_sea = tp2mm(tp_sea);
```

Since each cycle is a pair of a local maximum and a local minimum in the load, a cycle count can be visualized as a set of pairs in the \mathbb{R}^2 -plane. This is done by the routine `ccplot`. Compare the rainflow and min-max counts in the load in Figure 5.4 obtained by the following commands.

```
subplot(121), ccplot(mM_sea)
title('min-max cycle count')
subplot(122), ccplot(RFC_sea)
title('Rainflow cycle count')
```

Observe that RFC contains more cycles with high amplitudes, compared to mM. This becomes more evident in an amplitude histogram as seen in Figure 5.5.

```
ampmM_sea = cc2amp(mM_sea);
ampRFC_sea = cc2amp(RFC_sea);
subplot(221), hist(ampmM_sea,25);
title('min-max amplitude distribution')
subplot(222), hist(ampRFC_sea,25);
title('Rainflow amplitude distribution')
```

5.3.3 Simulation of rainflow cycles

Simulation of cycles in a Markov model

The most simple cycle model assumes that the sequence of turning points forms a Markov chain. Then the model is completely defined by the min-max matrix, \mathbf{G} . The matrix has dimension $n \times n$, where n is the number of discrete levels (e.g. 32 or 64). In this example the discrete levels \mathbf{u} are chosen in the range from -1 to 1 . The matrix \mathbf{G} will contain the probabilities of transitions between the different levels in \mathbf{u} ; see the help function for `mktestmat` for the generation of \mathbf{G} .

```
n = 41; param_m = [-1 1 n];
u_markov = levels(param_m);
G_markov = mktestmat(param_m, [-0.2 0.2], 0.15, 1);
```

The model is easy to simulate and this is performed by the simulation routine `mctpsim`. This routine simulates only the sequence of turning points and not the intermediate load values.

```
T_markov = 5000;
xxD_markov = mctpsim({G_markov []}, T_markov);
xx_markov = [(1:T_markov)' u_markov(xxD_markov)'];
```

Here `xxD_markov` takes values $1, \dots, n$, and by changing the scale, as in the third command line, we get the load `xx_markov`, with TP-number in first column load values between -1 and 1 in second column. The first 50 samples of the simulation is plotted in Figure 5.6 by

```
plot(xx_markov(1:50,1),xx_markov(1:50,2))
```

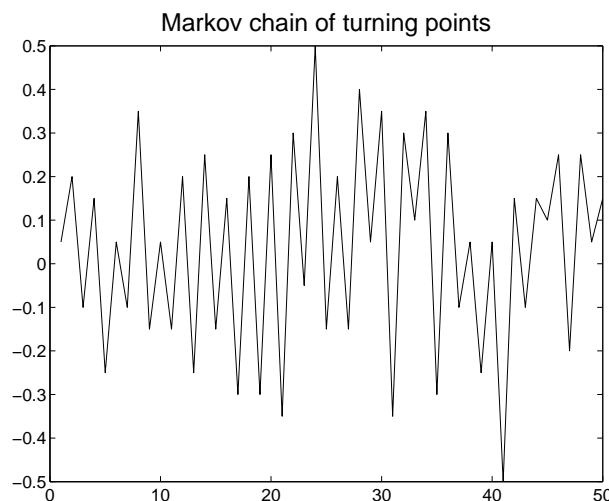


Figure 5.6: Simulated Markov sequence of turning points.

We shall later use the matrix $\mathbf{G}_{\text{markov}}$ to calculate the theoretical rainflow matrix, but first we construct a similar sequence of turning points from a transformed Gaussian model.

Rainflow cycles in a transformed Gaussian model

In this example we shall consider a sea-data-like series obtained as a transformed Gaussian model with JONSWAP spectrum. Since that spectrum contains also rather high frequencies a JONSWAP load will contain many cycles with small amplitude. These are often uninteresting and can be removed by a rainflow filter as follows.

Let g be the Hermite transformation proposed by Winterstein, which we used in Chapter 2. Suppose the spectrum is of the JONSWAP type. To get the transform we need as input the approximative higher moments, skewness and kurtosis, which are automatically calculated from the spectrum by the routine `spec2skew`. We define the spectrum structure, including the transformation, and simulate the transformed Gaussian load `xx_herm`. The routine `dat2dtp` extracts the turning points discretized to the levels specified by the parameter vector `param`.

Note that when calling the simulation routine `spec2sdat` with a spectrum structure including a transformation, the input spectrum must be normalized to have standard deviation 1, i.e. one must divide the spectral values by the variance sa^2 .

```
me = mean(xx_sea(:,2));
sa = std(xx_sea(:,2));
Hm0_sea = 4*sa;
Tp_sea = 1/max(lc_sea(:,2));
SJ = jonswap([], [Hm0_sea Tp_sea]);

[sk, ku] = spec2skew(SJ);
SJ.tr = hermitetr([], [sa sk ku me]);
param_h = [-1.5 2 51];
SJnorm = SJ;
SJnorm.S = SJnorm.S/sa^2;
xx_herm = spec2sdat(SJnorm, [2^15 1], 0.1);
h = 0.2;
[dtp, u_herm, xx_herm_1] = dat2dtp(param_h, xx_herm, h);
plot(xx_herm(:,1), xx_herm(:,2), 'k', 'LineWidth', 2);
hold on;
plot(xx_herm_1(:,1), xx_herm_1(:,2), 'k--', 'Linewidth', 2);
axis([0 50 -1 1]), hold off;
title('Rainflow filtered wave data')
```

The rainflow filtered data `xx_herm_1` contains the turning points of `xx_herm` with rainflow cycles less than $h=0.2$ removed. In Figure 5.7 the dashed curve connects the remaining turning points after filtration.

Try different degree of filtering on the Ochi transformed sequence and see how it affects the min-max cycle distribution. You can use the following sequence of commands, with different h -values; see Figure 5.8 for the results. Note that the rainflow cycles have their original values in the left figure but that they have been discretized to the discrete level defined by `param_h` in the right figure.

```
tp_herm=dat2tp(xx_herm);
RFC_herm=tp2rfc(tp_herm);
```

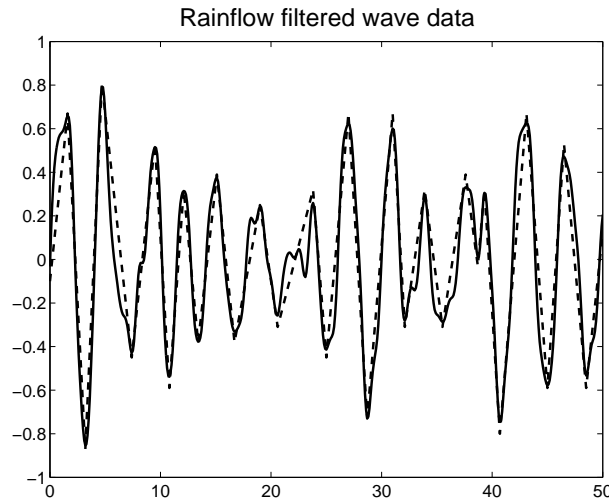


Figure 5.7: Hermite transformed wave data together with rainflow filtered turning points, $h = 0.2$.

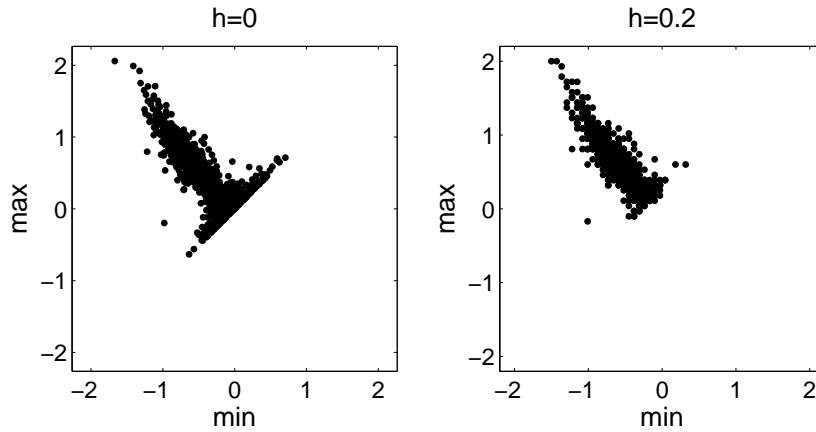


Figure 5.8: Rainflow cycles and rainflow filtered rainflow cycles in the transformed Gaussian process.

```

mM_herm=tp2mm(tp_herm);
h=0.2;
[dtu,u,tp_herm_1]=dat2dtp(param_h,xx_herm,h);
RFC_herm_1 = tp2rfc(tp_herm_1);
subplot(121), ccplot(RFC_herm)
title('h=0')
subplot(122), ccplot(RFC_herm_1)
title('h=0.2')

```

5.3.4 Calculating the Rainflow Matrix

We have now shown how to extract rainflow cycles from a load sequence and to perform rainflow filtering in measured or simulated load sequences. Next we shall demonstrate how the expected (theoretical) rainflow matrix can be calculated in any random load or wave model, defined either as a Markov chain of turning points, or as a stationary random process with some spectral density. We do this by means of the Markov method based on

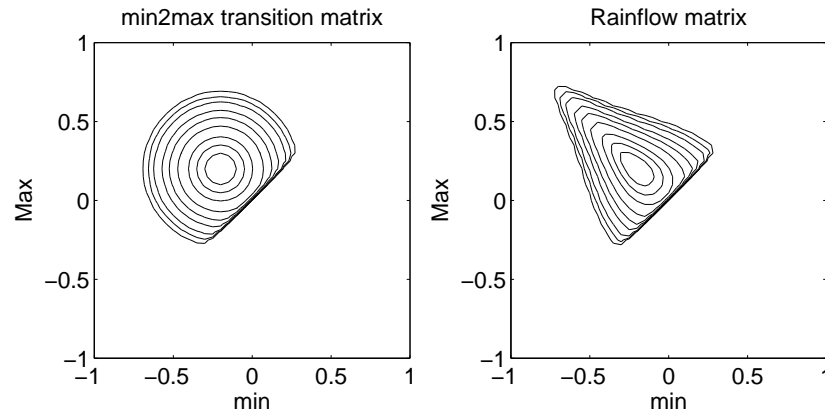


Figure 5.9: min-max-matrix and theoretical rainflow matrix for test Markov sequence.

the max-min transition matrix for the sequence of turning points. This matrix can either be directly estimated from or assigned to a load sequence, or it can be calculated from the correlation or spectrum structure of a transformed Gaussian model by the methods described in Section 4.3.4.

Calculation of rainflow matrix in the Markov model

The theoretical rainflow matrix `Grfc` for the Markov model is calculated in WAFO by the routine `mctp2rfm`. Let `G_markov` be as in Section 5.3.3 and calculate the theoretical rainflow matrix by

```
Grfc_markov=mctp2rfm({G_markov []});
```

A cycle matrix, e.g. a min-max or rainflow matrix, can be plotted by `cmatplot`. Now we will compare the min-max and the rainflow matrices.

```
subplot(121),cmatplot(u_markov,u_markov,G_markov),...
    axis('square')
subplot(122),cmatplot(u_markov,u_markov,Grfc_markov),...
    axis('square')
```

Both 2D- and 3D-plots can be drawn; see the help on `cmatplot`. It is also possible to plot many matrices in one call.

```
cmatplot(u_markov,u_markov,{G_markov Grfc_markov},3)
```

A plot with `method = 4` gives contour lines; see Figure 5.9. Note that for high maxima and low minima, the rainflow matrix has a pointed shape while the min-max matrix has a more rounded shape.

```
cmatplot(u_markov,u_markov,{G_markov Grfc_markov},4)
subplot(121), axis('square'),...
    title('min2max transition matrix')
subplot(122), axis('square'), title('Rainflow matrix')
```

We now compare the theoretical rainflow matrix with an observed rainflow matrix obtained in the simulation. In this case we have simulated a discrete Markov chain of turning points with states $1, \dots, n$ and put them in the variable `xxD_markov`. It is turned into a rainflow matrix by the routine `dtp2rfm`. The comparison in Figure 5.10 between the observed rainflow matrix and the theoretical one is produced as follows.

```
n = length(u_markov);
Frfc_markov = dtp2rfm(xxD_markov,n);
cmatplot(u_markov,u_markov,...
         {Frfc_markov Grfc_markov*T/2},3)
subplot(121), axis('square')
         title('Observed rainflow matrix')
subplot(122), axis('square')
         title('Theoretical rainflow matrix')
```

Note that in order to compare the observed matrix `Frfc_markov` with the theoretical matrix `Grfc_markov` we have to multiply the latter by the number of cycles in the simulation which is equal to $T/2$.

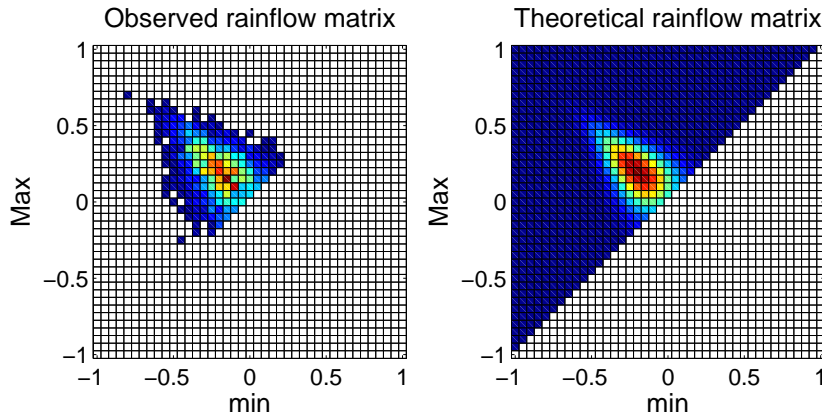


Figure 5.10: Observed and theoretical rainflow matrix for test Markov sequence.

We end this section by an illustration of the rainflow smoothing operation. The observed rainflow matrix is rather irregular, due to the statistical variation in the finite sample. To facilitate comparison with the theoretical rainflow matrix we smooth it by the built in smoothing facility in the routine `cc2cmat`. To see how it works for different degrees of smoothing we calculate the rainflow cycles by `tp2rfc`.

```
tp_markov = dat2tp(xx_markov);
RFC_markov = tp2rfc(tp_markov);
h = 0.2;
Frfc_markov_smooth = cc2cmat(param_m,RFC_markov,[],1,h);
cmatplot(u_markov,u_markov,...
         {Frfc_markov_smooth Grfc_markov*T/2},4)
subplot(121), axis('square')
         title('Smoothed observed rainflow matrix')
```

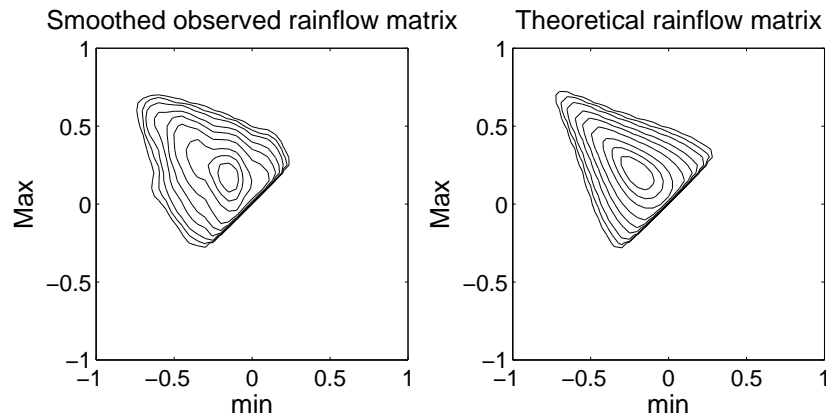



Figure 5.11: Smoothed observed and calculated rainflow matrix for test Markov sequence.

```
subplot(122), axis('square')
        title('Theoretical rainflow matrix')
```

Here, the smoothing is done as a kernel smoother with a bandwidth parameter `h = 1`. The effect of the smoothing is shown in Figure 5.11.

Rainflow matrix from spectrum

We are now ready to demonstrate how the rainflow matrix can be calculated in a load or wave model defined by its correlation or spectrum structure. We chose the transformed Gaussian model with the Hermite transform `xx_herm` which was studied in Section 5.3.3. This model was defined by its JONSWAP spectrum and the standard Hermite transform for asymmetry.

We first need to find the structure of the turning points, which is defined by the min-to-max density by the methods in Section 4.3.4. We start by computing an approximation, `GmM3_herm`, of the min-max density by means of the cycle routine `spec2cmat` (as an alternative one can use `spec2mmtpdf`). The type of cycle is specified by a cycle parameter, in this case `'Mm'`.

```
GmM3_herm = spec2cmat(SJ, [], 'Mm', [], param_h, 2);
```

The result is seen in Figure 5.12.

Then, we approximate the distribution of the turning points by a Markov chain with transitions between extrema calculated from `GmM3_herm`, and compute the rainflow matrix by Eq. (5.5).

```
Grfc_herm = mctp2drfm({GmM3_herm.f, []});
```

In WAFO, the rainflow matrix can be calculated directly from the spectrum by the cycle distribution routine `spec2cmat` by specifying the cycle parameter to `'rfc'`.

```
Grfc_direct_herm = spec2cmat(SJ, [], 'rfc', [], [], 2);
```

The output is a structure array which contains the rainflow matrix in the cell `.f`.

The min-max matrix `GmM3_herm` and the rainflow matrix `Grfc_herm` are shown together in Figure 5.12, obtained using the following commands.

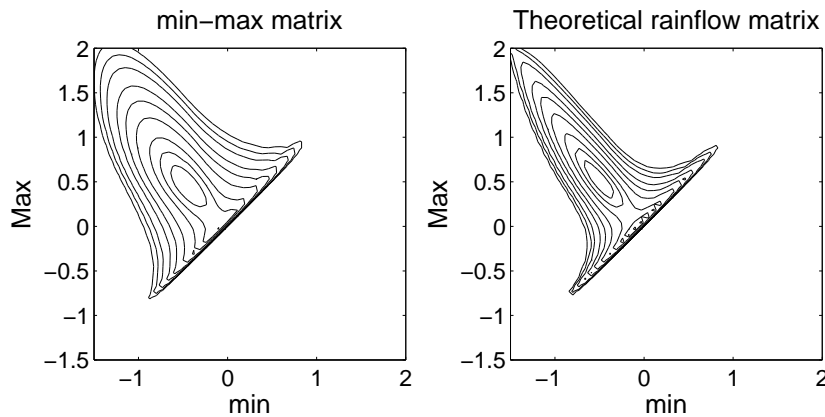


Figure 5.12: min-max matrix and theoretical rainflow matrix for Hermite transformed Gaussian waves.

```
u_herm = levels(param_h);
cmatplot(u_herm,u_herm,{GmM3_herm.f Grfc_herm},4)
subplot(121), axis('square'),...
    title('min-max matrix')
subplot(122), axis('square'),...
    title('Theoretical rainflow matrix')
```

We can also compare the theoretical min-max matrix with the observed cycle count and the theoretical rainflow matrix with the observed one. In both comparisons we smooth the observed matrix to get a more regular structure. We also illustrate the multi-plotting capacity of the routine `cmatplot`.

```
tp_herm = dat2tp(xx_herm);
RFC_herm = tp2rfc(tp_herm);
mM_herm = tp2mm(tp_herm);
h = 0.2;
FmM_herm_smooth = cc2cmat(param_o,mM_herm,[],1,h);
Frfc_herm_smooth = cc2cmat(param_o,RFC_herm,[],1,h);
T_herm=xx_herm(end,1)-xx_herm(1,1);
cmatplot(u_herm,u_herm,{FmM_herm_smooth ...
    GmM3_herm.f*T_herm/2;...
    Frfc_herm_smooth Grfc_herm*T_herm/2},4)
subplot(221), axis('square')
    title('Observed smoothed min-max matrix')
subplot(222), axis('square')
    title('Theoretical min-max matrix')
subplot(223), axis('square')
    title('Observed smoothed rainflow matrix')
subplot(224), axis('square')
    title('Theoretical rainflow matrix')
```

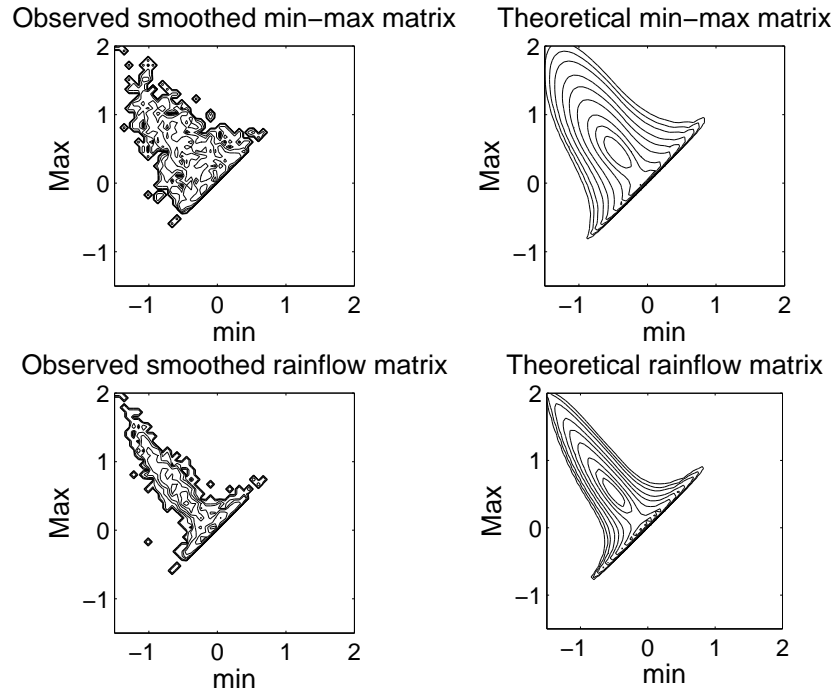


Figure 5.13: Observed smoothed and theoretical min-max matrix, and observed smoothed and theoretical rainflow matrix for Hermite transformed Gaussian waves.

5.3.5 Simulation from crossings structure

In fatigue experiments it is important to generate load sequences with a prescribed rainflow or other crossing property. Besides the previously used simulation routines for Markov loads and spectrum loads, WAFO contains algorithms for generation of random load sequences that have a specified average rainflow distribution or a specified irregularity and crossing spectrum. We illustrate the crossing structure simulation by means of the routine `lc2sdat`. Simulation from a rainflow distribution can be achieved by first calculating the corresponding Markov matrix and then simulate by means of `mctpsim`.

The routine `lc2sdat` simulates a load with specified irregularity factor and crossing spectrum. We first estimate these quantities in the simulated Hermite transformed Gaussian load, and then simulate series with the same crossing spectrum but with varying irregularity factor. The sampling variability increases with decreasing irregularity factor, as is seen in Figure 5.14. The figures were generated by the following commands.

```
cross_herm = dat2lc(xx_herm);
alpha1 = 0.25;
alpha2 = 0.75;
xx_herm_sim1 = lc2sdat(cross_herm,500,alpha1);
cross_herm_sim1 = dat2lc(xx_herm_sim1);
subplot(211)
plot(cross_herm(:,1),cross_herm(:,2)/max(cross_herm(:,2)))
hold on
stairs(cross_herm_sim1(:,1),...
       cross_herm_sim1(:,2)/max(cross_herm_sim1(:,2)))
hold off
```

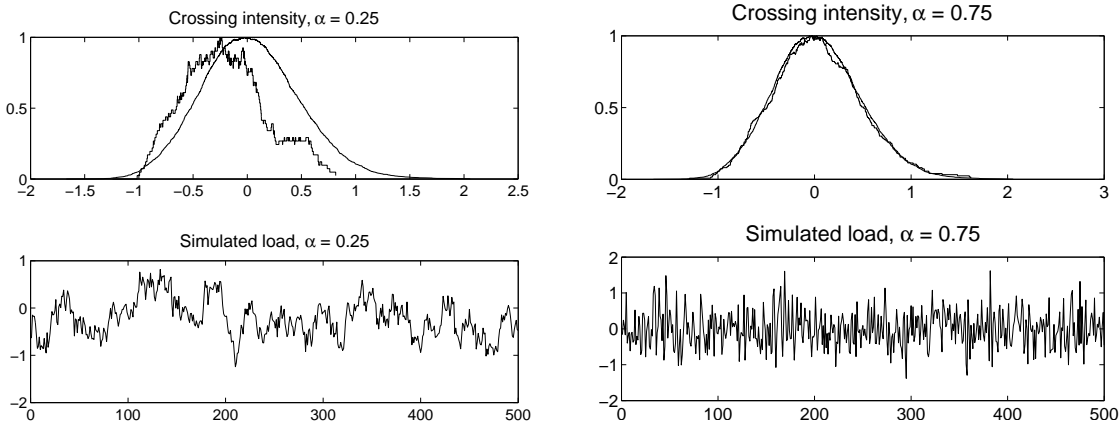


Figure 5.14: Upper figures show target crossing spectrum (smooth curve) and obtained spectrum (wiggled curve) for simulated process shown in lower figures. Irregularity factor: left $\alpha = 0.25$, right $\alpha = 0.75$.

```

title('Crossing intensity, \alpha = 0.25')
subplot(212)
plot(xx_herm_sim1(:,1),xx_herm_sim1(:,2))
title('Simulated load, \alpha = 0.25')

xx_herm_sim2 = lc2sdat(500,alpha2,cross_herm);
cross_herm_sim2 = dat2lc(xx_herm_sim2);
subplot(211)
plot(cross_herm(:,1),cross_herm(:,2)/max(cross_herm(:,2)))
hold on
stairs(cross_herm_sim2(:,1),...
       cross_herm_sim2(:,2)/max(cross_herm_sim2(:,2)))
hold off
title('Crossing intensity, \alpha = 0.75')
subplot(212)
plot(xx_herm_sim2(:,1),xx_herm_sim2(:,2))
title('Simulated load, \alpha = 0.75')

```

5.4 Fatigue damage and fatigue life distribution

5.4.1 Introduction

We shall now give a more detailed account of how WAFO can be used to estimate and bound the fatigue life distribution under random loading. The basic assumptions are the Wöhler curve Eq. (5.1) and the Palmgren-Miner damage accumulation rule Eq. (5.2),

$$N(s) = \begin{cases} K^{-1}s^{-\beta}, & s > s_{\infty}, \\ \infty, & s \leq s_{\infty}, \end{cases} \quad (5.6)$$

$$D(t) = \sum_{t_k \leq t} \frac{1}{N(s_k)} = K \sum_{t_k \leq t} s_k^{\beta} = K D_{\beta}(t). \quad (5.7)$$

Here $N(s)$ is the expected fatigue life from constant amplitude test with amplitude s , and $D(t)$ is the total damage at time t caused by variable amplitude cycles s_k , completed before time t . The damage intensity $d_\beta = D(t)/t$ for large t is the amount of damage per time unit.

Most information is contained in the cycle amplitude distribution, in particular in the rainflow cycles, in which case (5.7) becomes,

$$D(t) = \sum_{t_k \leq t} \frac{1}{N_{s_k}} = K \sum_{t_k \leq t} (S_k^{\text{RFC}})^\beta, \quad S_k^{\text{RFC}} = (M_k - m_k^{\text{RFC}}) / 2.$$

The rainflow cycle count **RFC** can be directly used for prediction of expected fatigue life. The expression Eq. (5.3) gives the expected time to fatigue failure in terms of the material constant ϵ and the expected damage d_β per time unit. The parameters ϵ and β can be estimated from an S-N curve. In the examples here we will use $\epsilon = 5.5 \cdot 10^{-10}$, $\beta = 3.2$; see Section 5.4.4. For our sea load **xx_sea**, the computations go directly from the rainflow cycles as follows.

```
beta=3.2; gam=5.5E-10; T_sea=xx_sea(end,1)-xx_sea(1,1);
d_beta=cc2dam(RFC_sea,beta)/T_sea;
time_fail=1/gam/d_beta/3600
```

giving the time to failure **5.9693e+006** when time to failure is counted in hours (= 3600 sec). Obviously, this load causes little damage to the material with the specified properties, since the failure time is almost 700 years – of course, the sea wave data is not a fatigue load sequence, so the example is meaningless from a fatigue point of view.

5.4.2 Level Crossings

We have in Section 5.3.5 seen how the crossing intensity contains information about the load sequence and how it can be used for simulation. We shall now investigate the relation between the crossing intensity, the rainflow cycles, and the expected fatigue life.

We use the Markov model from Section 5.3.3 for the sequence of turning points as an example. First we go from the rainflow matrix to the crossing intensity.

```
mu_markov = cmat2lc(param_m,Grfc_markov);
mu0bs_markov = cmat2lc(param_m,Frfc_markov/(T_markov/2));
plot(mu_markov(:,1),mu_markov(:,2),...
      mu0bs_markov(:,1),mu0bs_markov(:,2),'--')
title('Theoretical and observed crossing intensity ')
```

The plot in Figure 5.15 compares the theoretical upcrossing intensity **mu_markov** with the observed upcrossing intensity **mu0bs_markov**, as calculated from the theoretical and observed rainflow matrices, respectively.

5.4.3 Damage

The **WAFO** toolbox contains a number of routines to compute and bound the damage, as defined by (5.7), inflicted by a load sequence. The most important routines are **cc2dam** and **cmat2dam**, which give the total damage from a cycle count and from a cycle matrix,

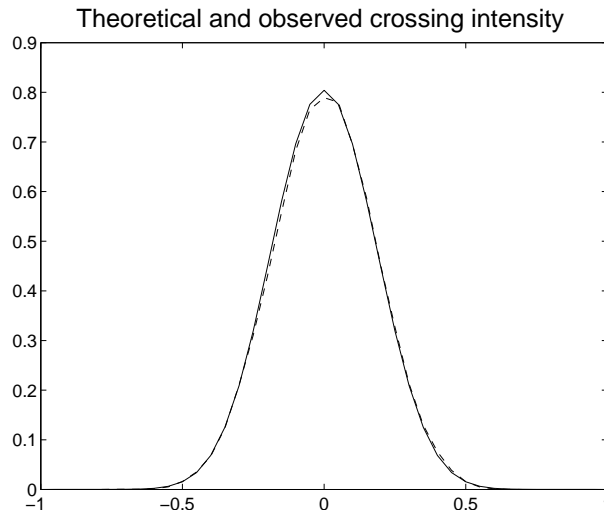


Figure 5.15: Crossing intensity as calculated from the Markov observed rainflow matrix (solid curve) and from the observed rainflow matrix (dashed curve).

respectively. More detailed information is given by `cmat2dmat`, which gives a damage matrix, separated for each cycle, from a cycle matrix. An upper bound for total damage from level crossings is given by `lc2dplus`.

We first calculate the damage by the routines `cc2dam` for a cycle count (e.g. rainflow cycles) and `cmat2dam` for a cycle matrix (e.g. rainflow matrix).

```
beta = 4;
Dam_markov = cmat2dam(param_m,Grfc_markov,beta)
DamObs1_markov = ...
    cc2dam(u_markov(RFC_markov),beta)/(T_markov/2)
DamObs2_markov = ...
    cmat2dam(param_m,Frfc_markov,beta)/(T_markov/2)
```

Here, `Dam_markov` is the theoretical damage per cycle in the assumed Markov chain of turning points, while `DamObs1` and `DamObs2` give the observed damage per cycle, calculated from the cycle count and from the rainflow matrix, respectively. For this model the result should be `Dam_markov = 0.0073` for the theoretical damage and very close to this value for the simulated series.

The damage matrix is calculated by `cmat2dmat`. It shows how the damage is distributed among the different cycles as illustrated in Figure 5.16. The sum of all the elements in the damage matrix gives the total damage.

```
Dmat_markov = cmat2dmat(param_m,Grfc_markov,beta);
DmatObs_markov = cmat2dmat(param_m,...
    Frfc_markov,beta)/(T_markov/2);}
subplot(121), cmatplot(u_markov,u_markov,Dmat_markov,4)
title('Theoretical damage matrix')
subplot(122), cmatplot(u_markov,u_markov,DmatObs_markov,4)
title('Observed damage matrix')
sum(sum(Dmat_markov))
sum(sum(DmatObs_markov))
```

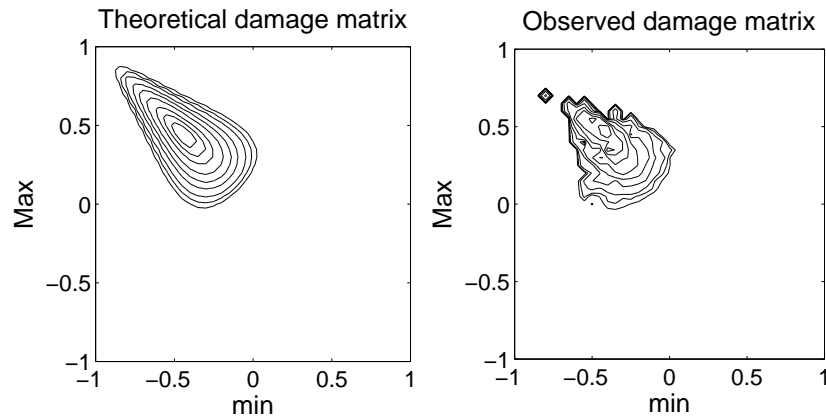


Figure 5.16: Distribution of damage from different RFC cycles, from calculated theoretical and from observed rainflow matrix.

It is possible to calculate an upper bound on the damage intensity from the crossing intensity only, without using the rainflow cycles. This is done by the routine `lc2dplus`, which works on any theoretical or observed crossing intensity function.

```
Damplus_markov = lc2dplus(mu_markov,beta)
```

5.4.4 Estimation of S-N curve

WAFO contains routines for computation of parameters in the basic S-N curve (5.1), for the relation between the load cycle amplitude s and the fatigue life $N(s)$ in fixed amplitude tests, defined by (5.6). The variation of the material dependent variable K is often taken to be random with a lognormal distribution,

$$K = E\epsilon^{-1},$$

where ϵ is a fixed parameter, depending on material, and $\ln E$ has a normal distribution with mean 0 and standard deviation σ_E . Thus, there are three parameters, ϵ , β , σ_E , to be estimated from an S-N experiment. Taking logarithms in (5.1) the problem turns into a standard regression problem,

$$\ln N(s) = -\ln E - \ln \epsilon - \beta \ln s,$$

in which the parameters can easily be estimated.

The WAFO toolbox contains a data set `sn.dat` with fatigue lives from 40 experiments with $s = 10, 15, 20, 25$, and 30 MPa, stored in a variable `N`, in groups of five. The estimation routine is called `snplot`, which performs both estimation and plotting; see `help snplot`.

First load SN-data and plot in log-log scale.

```
SN = load('sn.dat');
s = SN(:,1); N = SN(:,2);
loglog(N,s,'o'), axis([0 14e5 10 30])
```

To further check the assumptions of the S-N-model we plot the results for each s -level separately on normal probability paper. As seen from Figure 5.17 the assumptions seem acceptable since the data fall on almost parallel straight lines.

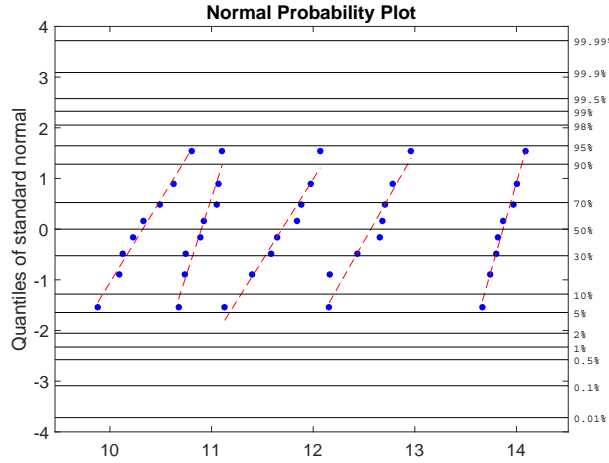


Figure 5.17: Check of S-N-model on normal probability paper.

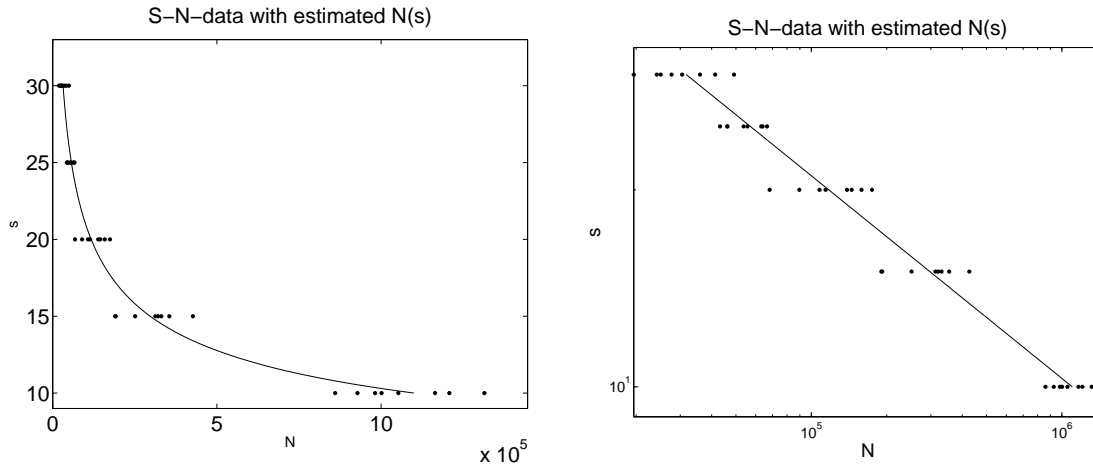


Figure 5.18: Estimation of S-N-model on linear and log-log scale.

```
plotnorm(reshape(log(N),8,5))
```

The estimation is performed and fitted lines plotted in Figure 5.18, with linear and log-log plotting scales:

```
[e0,beta0,s20] = snplot(s,N,12);
title('S-N-data with estimated N(s)')
```

gives linear scale and

```
[e0,beta0,s20] = snplot(s,N,14);
title('S-N-data with estimated N(s)')
```

gives log-log scales.

5.4.5 From S-N-curve to fatigue life distribution

The Palmgren-Miner hypothesis states that fatigue failure occurs when the accumulated damage exceeds one, $D(t) > 1$. Thus, if the fatigue failure time is denoted by T_f , then

$$P(T_f \leq t) = P(D(t) \geq 1) = P(K \leq \epsilon D_\beta(t)).$$

Here $K = E^{-1}\epsilon$ takes care of the uncertainty in the material. In the previous section we used and estimated a lognormal distribution for the variation of K around ϵ , when we assumed that $\ln K = \ln \epsilon - \ln E$ is normal with mean $\ln \epsilon$ and standard deviation σ_E .

The cycle sum $D_\beta(t)$ is the sum of a large number of damage terms, only dependent on the cycles. For loads with short memory one can assume that $D_\beta(t)$ is approximately normal,

$$D_\beta(t) \approx N(d_\beta t, \sigma_\beta^2 t),$$

where

$$d_\beta = \lim_{t \rightarrow \infty} \frac{D_\beta(t)}{t} \quad \text{and} \quad \sigma_\beta^2 = \lim_{t \rightarrow \infty} \frac{V(D_\beta(t))}{t}.$$

Thus the fatigue life distribution can be computed by combining the lognormal distribution for K with the normal distribution for $D_\beta(t)$. Denoting the standard normal density and distribution functions by $\phi(x)$ and $\Phi(x)$, respectively, an approximate explicit expression for the failure probability within time t is

$$P(T^f \leq t) \approx \int_{-\infty}^{\infty} \Phi \left(\frac{\ln \epsilon + \ln d_\beta t + \ln(1 + \frac{\sigma_\beta}{d_\beta \sqrt{t}} z)}{\sigma_E} \right) \phi(z) dz. \quad (5.8)$$

We have already estimated the material dependent parameters $\epsilon = \mathbf{e0}$, $\beta = \mathbf{beta0}$, and $\sigma_E^2 = \mathbf{s20}$, in the S-N data, so we need the damage intensity d_β and its variability σ_β for the acting load.

We first investigate the effect of uncertainty in the β -estimate.

```
beta = 3:0.1:8;
DRFC = cc2dam(RFC_sea,beta);
dRFC = DRFC/T_sea;
plot(beta,dRFC), axis([3 8 0 0.25])
title('Damage intensity as function of \beta')
```

The plot in Figure 5.19 shows the increase in damage with increasing β .

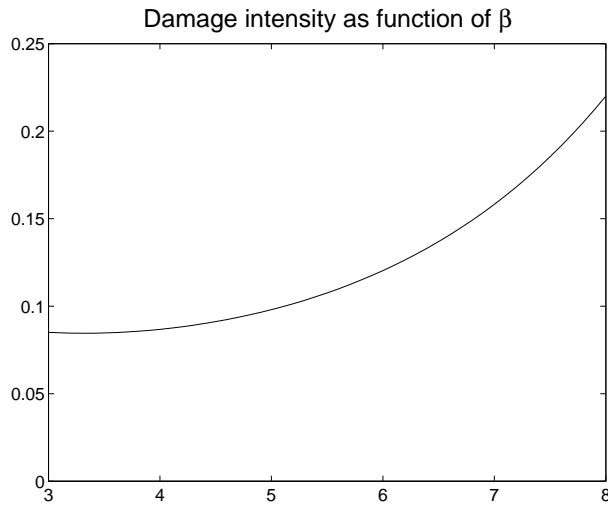


Figure 5.19: Increasing damage intensity from sea-load with increasing β .

Next, we shall see how the load variability affects the fatigue life. We use three different values for σ_β^2 , namely 0, 0.5, and 5. With $\mathbf{beta0}$, $\mathbf{e0}$, $\mathbf{s20}$ estimated in Section 5.4.4, we compute and plot the following three possible fatigue life distributions.

```

dam0 = cc2dam(RFC_sea,beta0)/T_sea;
[t0,F0] = ftf(e0,dam0,s20,0.5,1);
[t1,F1] = ftf(e0,dam0,s20,0,1);
[t2,F2] = ftf(e0,dam0,s20,5,1);
plot(t0,F0,t1,F1,t2,F2)

```

Here, the fourth parameter is the value of σ_β^2 used in the computation; see `help ftf`.

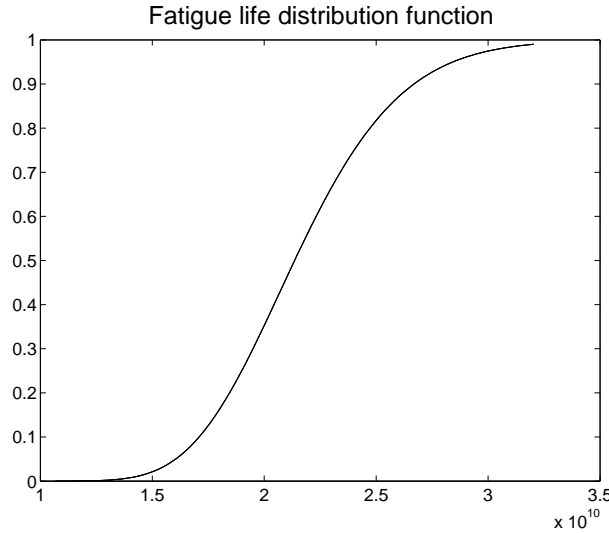


Figure 5.20: Fatigue life distribution with sea load.

The resulting fatigue life distribution function is shown in Figure 5.20. As seen, the curves are identical, indicating that the correct value of σ_β^2 is not important for such small ϵ -values as are at hand here. Hence, one can use $\sigma_\beta^2 = 0$, and assume that the damage accumulation process is proportional to time.

5.4.6 Fatigue analysis of complex loads

Loads which cause fatigue are rarely of the homogeneous and stationary character as the loads used in the previous sections. On the contrary, typical load characteristics often change their value during the life time of a structure, for example, load spectra on an airplane part have very different fatigue properties during the different stages of an air mission. Marine loads on a ship are quite different during loading and unloading, compared to a loaded ocean voyage, and the same holds for any road vehicle.

The WAFO toolbox can be used to analyse also loads of complex structure and we shall illustrate some of these capabilities in this section. To be eligible for WAFO-analysis, the loads have to have a piecewise stationary character, for example the mean level or the standard deviation may take two distinct levels and change abruptly, or the frequency content can alternate between two modes, one irregular and one more regular. Such processes are called *switching processes*. A flexible family of switching loads are those where the change between the different stationary states is governed by a Markov chain. WAFO contains a special package of routines for analysis of such switching Markov loads, based on methods by Johannesson, [32, 33].

In the following example the load alternates between two different mean levels, corresponding to one heavy-load state (1) and one light-load state (2). In Figure 5.21 the

observed load is shown in the upper part. The alternating curve in the lower part shows the switches between the two states.

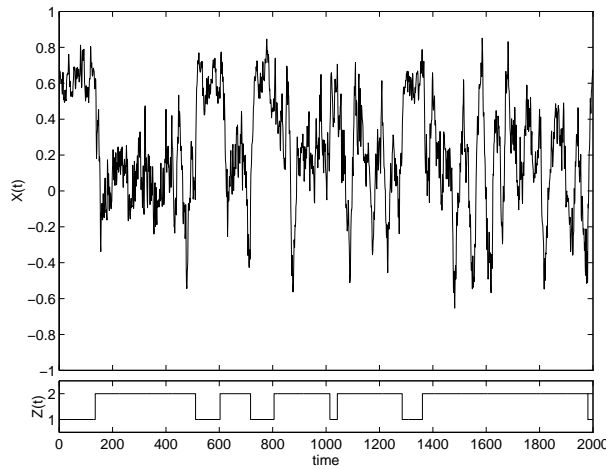


Figure 5.21: Simulated switching load with two states. Upper graph shows the load, and the states are indicated in the lower graph.

As long as the load is in one of the states, the rainflow cycles are made up of alternations between turning points belonging only to that part of the load. When the state changes there is introduced extra rainflow cycles with larger amplitudes. These extra cycles can be seen in the total rainflow matrix, shown in Figure 5.22. The two large groups of cycles around $(\min, \max) = (0.5, 0.75)$ and $(\min, \max) = (0, 0)$ come from states (1) and (2), respectively. The contribution from the switching is seen in the small assembly of cycles around $(\min, \max) = (-0.5, 1)$.

More details on how to analyse and model switching loads can be found in [31].

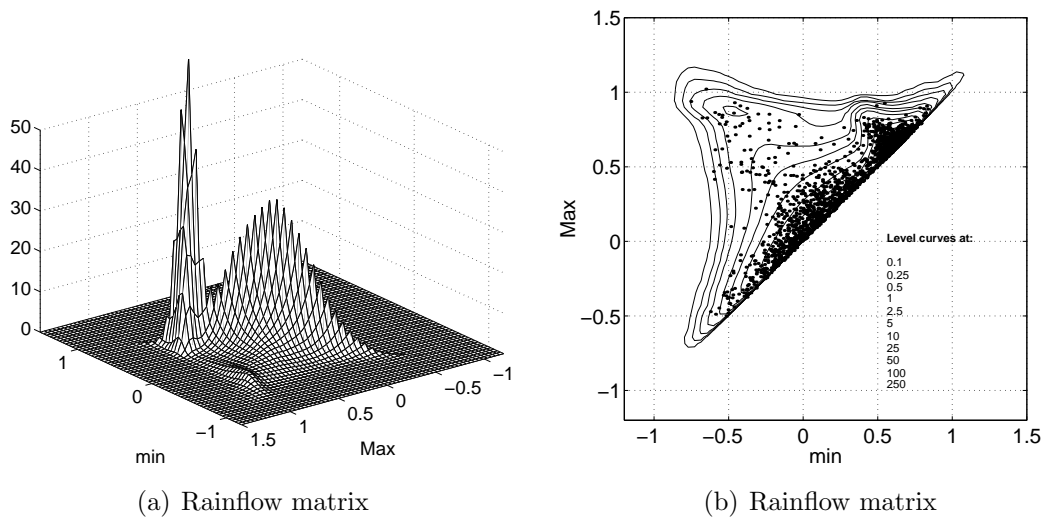


Figure 5.22: 3D-plot (left) and isolines (right) of calculated rainflow matrix for switching load in Figure 5.21. The dots in the right figure are the observed rainflow cycles.

CHAPTER 6

Extreme value analysis

Of particular interest in wave analysis is how to find extreme quantiles and extreme significant values for a wave series. Often this implies going outside the range of observed data, i.e. to predict, from a limited number of observations, how large the extreme values might be. Such analysis is commonly known as *Weibull analysis* or *Gumbel analysis*, from the names of two familiar extreme value distributions. Both these distributions are part of a general family of extreme value distributions, known as the *Generalized Extreme Value Distribution*, (GEV). The *Generalized Pareto Distribution* (GPD) is another distribution family, particularly adapted for *Peaks Over Threshold* (POT), analysis. WAFO contains routines for fitting of such distributions, both for the Weibull and Gumbel distributions, and for the two more general classes of distributions. For a general introduction to statistical extreme value analysis, the reader is referred to [19].

This chapter illustrates how WAFO can be used for elementary extreme value analysis in the direct GEV method and in the POT method. The example commands in `Chapter6.m` take a few seconds to run. We start with a simple application of the classical Weibull and Gumbel analysis before we turn to the general techniques.

6.1 Weibull and Gumbel papers

The Weibull and Gumbel distributions, the latter sometimes also called “the” *extreme value distribution*, are two extreme value distributions with distribution functions, respectively,

$$\text{Weibull:} \quad F_W(x; a, c) = 1 - e^{-(x/a)^c}, \quad x > 0, \quad (6.1)$$

$$\text{Gumbel:} \quad F_G(x; a, b) = \exp\left(-e^{-(x-b)/a}\right), \quad -\infty < x < \infty. \quad (6.2)$$

The Weibull distribution is often used as distribution for random quantities which are the *minimum* of a large number of independent (or weakly dependent) identically distributed random variables. In practice it is used as a model for random strength of material, in which case it was originally motivated by the principle of *weakest link*. Similarly, the Gumbel distribution is used as a model for values which are *maxima* of a large number of independent variables.

Since one gets the minimum of variables x_1, x_2, \dots, x_n by changing the sign of the maximum of the sequence $-x_1, -x_2, \dots, -x_n$, one realises that distributions suitable for the analysis of maxima can also be used for analysis of minima. Both the Weibull and the Gumbel distribution are members of the class of Generalized Extreme Value distributions (GEV), which we shall describe in Section 6.2.

6.1.1 Estimation and plotting

We begin here with an example of Weibull and Gumbel analysis, where we plot data and empirical distribution and also estimate the parameters a, b, c in Eqs. (6.1) and (6.2). The file `atlantic.dat` is included in WAFO, and it contains significant wave-height data recorded approximately 14 times a month in the Atlantic Ocean in December to February during seven years and at two locations. The data are stored in the vector `Hs`. We try to fit a Weibull distribution to this data set, by the WAFO-routine `plotweib`, which performs both the estimation and the plotting.

```
Hs = load('atlantic.dat');
wei = plotweib(Hs)
```

This will result in a two element vector `wei = [ahat chat]` with estimated values of the parameters (a, c) in (6.1). The empirical distribution function of the input data is plotted automatically in a Weibull diagram with scales chosen to make the Weibull distribution function equal to a straight line. The horizontal scale is logarithmic in the observations x , and the vertical scale is linear in the *reduced variable* $\log(-\log(1 - F(x)))$; see Figure 6.1(a). Obviously, a Weibull distribution is not very well suited to describe the significant wave-height data.

To illustrate the use of the Gumbel distribution we plot and estimate the parameters (a, b) in the Gumbel distribution (6.2) for the data in `Hs`. The command

```
gum = plotgumb(Hs)
```

results in a vector `gum` with estimated values `[ahat bhat]` and the plot in Figure 6.1(b). Here the horizontal axis is linear in the observations x and the vertical axis carries the reduced variable $-\log(-\log(F(x)))$. The data shows a much better fit to the Gumbel than to a Weibull distribution.

A distribution that is often hard to distinguish from the Gumbel distribution is the Lognormal distribution, and making a Normal probability plot of the logarithm of `Hs` in Figure 6.1(c) also shows a good fit.

```
plotnorm(log(Hs), 1, 0);
```

The parameter estimation in `plotgumb` and `plotweib` is done by fitting a straight line to the empirical distribution functions in the diagrams and using the relations

$$\log\{-\log[1 - F_W(x; a, c)]\} = c \log(x) - c \log(a), \quad (6.3)$$

and

$$-\log\{-\log[F_G(x; a, b)]\} = x/a - b/a, \quad (6.4)$$

to relate parameters to intercepts and slopes of the estimated lines. In the following section we shall describe some more statistical techniques for parameter estimation in the Generalized Extreme Value distribution.

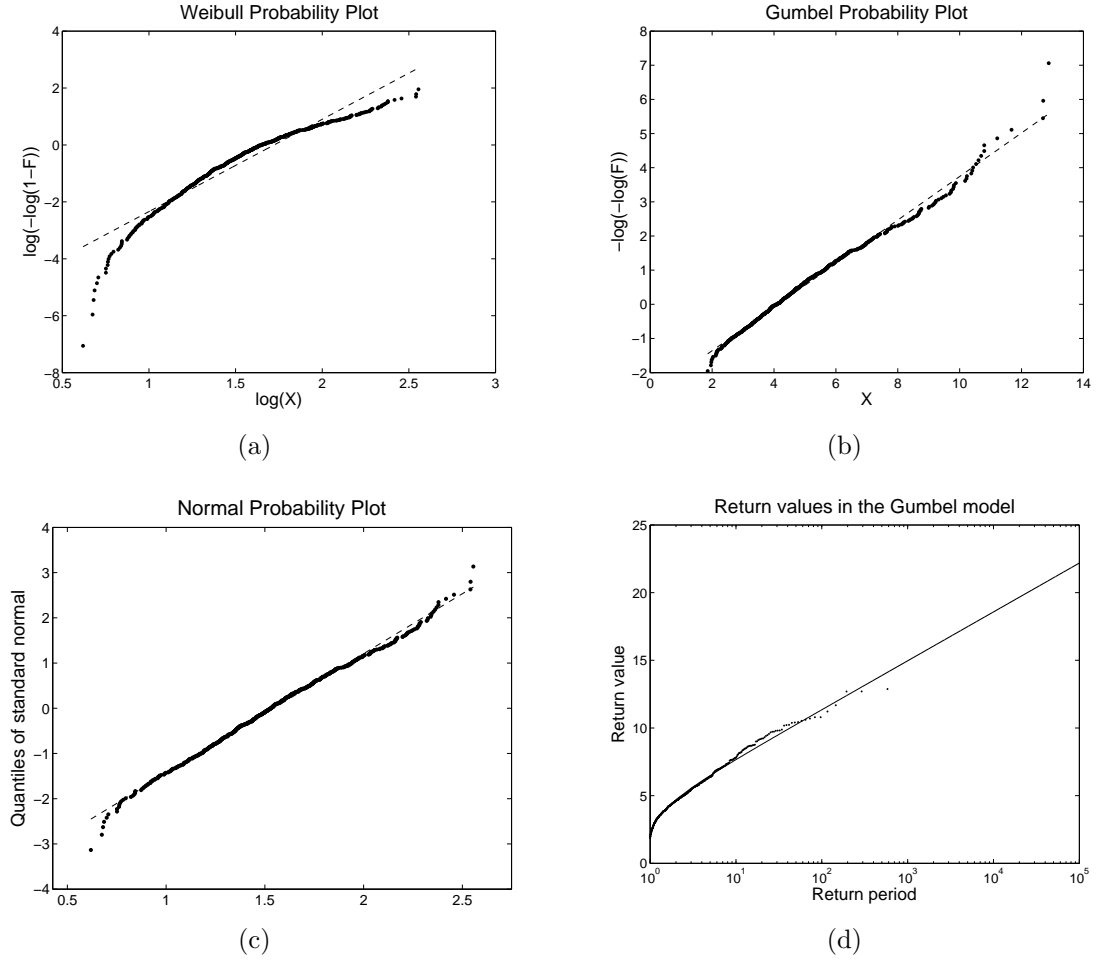


Figure 6.1: Significant wave-height data: (a) on Weibull paper, (b) on Gumbel paper, (c) logarithm of data on Normal probability paper, and (d) return values calculated in the Gumbel model with observed data.

6.1.2 Return value and return period

The results of an extreme value analysis is often expressed in terms of *return values* or *return levels*, which are simply related to the quantiles of the distribution. A return value is always coupled to a *return period*, expressed in terms of the length of an observation period, or the number of (independent) observations of a random variable.

Suppose we are interested in the return levels for the largest significant wave height that is observed during one year at a measuring site. Denote by $M_{H_s}^k$ the maximum during year number k and let its distribution function be $F(x)$. Then the N -year return level, s_N , is defined by

$$F(s_N) = 1 - 1/N. \quad (6.5)$$

For example, $P(H_s > s_{100}) = 1 - F(s_{100}) = 1/100$, which means that,

- the probability that the level s_{100} is exceeded during one particular year is 0.01,
- on the average, the yearly maximum significant wave height exceeds s_{100} one year in 100 years, (note that there may be several exceedances during that particular year),

- the probability that s_{100} is exceeded *at least* one time during a time span of 100 years is $1 - (1 - 0.01)^{100} \approx 1 - 1/e = 0.6321$, provided years are independent.

To make it simple, we consider the Gumbel distribution, and get, from (6.5), the T -year return value for the yearly maximum in the Gumbel distribution (6.2):

$$s_T = b - a \log(-\log(1 - 1/T)) \approx b + a \log T, \quad (6.6)$$

where the last approximation is valid for large T -values.

As an example we show a return value plot for the Atlantic data, as if they represented a sequence of yearly maxima. Figure 6.1(d) gives the return values as a function of the return period for the Atlantic data. The WAFO-commands are:

```
T = 1:100000;
sT = gum(2) - gum(1)*log(-log(1-1./T));
semilogx(T,sT), hold on
N = 1:length(Hs); Nmax = max(N);
plot(Nmax./N,sort(Hs,'descend'),'.')
title('Return values in the Gumbel model')
xlabel('Return priod')
ylabel('Return value'), hold off
```

In the next section we shall see a more realistic example of return value analysis. The Atlantic data did not represent yearly maxima and the example was included only as an alternative way to present the result of a Gumbel analysis.

6.2 The GPD and GEV families

The Generalized Pareto Distribution (GPD) has the distribution function

$$\text{GPD:} \quad F(x; k, \sigma) = \begin{cases} 1 - (1 - kx/\sigma)^{1/k}, & \text{if } k \neq 0, \\ 1 - \exp\{-x/\sigma\}, & \text{if } k = 0, \end{cases} \quad (6.7)$$

for $0 < x < \infty$, if $k \leq 0$, and for $0 < x < \sigma/k$, if $k > 0$. The Generalized Extreme Value distribution (GEV) has distribution function

$$\text{GEV:} \quad F(x; k, \mu, \sigma) = \begin{cases} \exp\{-(1 - k(x - \mu)/\sigma)^{1/k}\}, & \text{if } k \neq 0, \\ \exp\{-\exp\{-(x - \mu)/\sigma\}\}, & \text{if } k = 0, \end{cases} \quad (6.8)$$

for $k(x - \mu) < \sigma$, $\sigma > 0$, k, μ arbitrary. The case $k = 0$ is interpreted as the limit when $k \rightarrow 0$ for both distributions.

Note that the Gumbel distribution is a GEV distribution with $k = 0$ and that the Weibull distribution is equal to a reversed GEV distribution with $k = 1/c$, $\sigma = a/c$, and $\mu = -a$, i.e. if W has a Weibull distribution with parameters (a, c) then $-W$ has a GEV distribution with $k = 1/c$, $\sigma = a/c$, and $\mu = -a$.

The estimation of parameters in the GPD and GEV distributions is not a simple matter, and no general method exists, which has uniformly good properties for all parameter combinations. WAFO contains algorithms for plotting of distributions and estimation of parameters with four different methods, suitable in different regions.

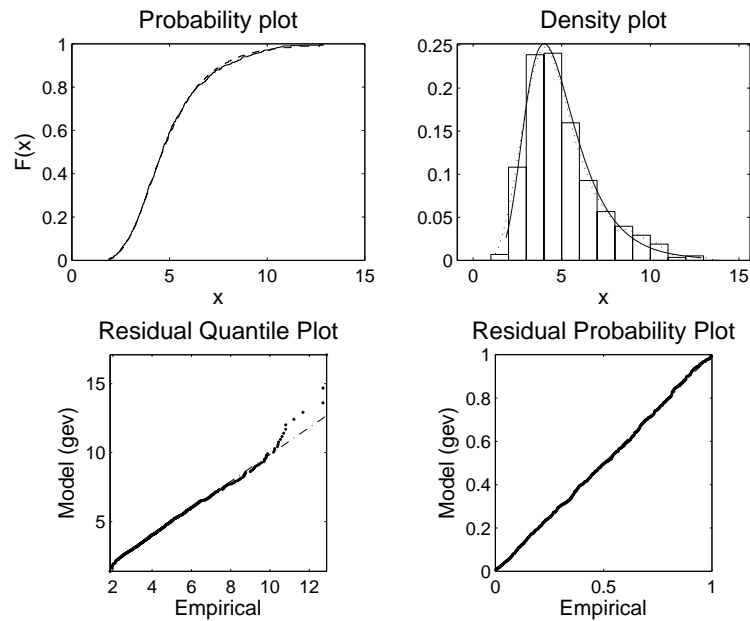


Figure 6.2: Empirical distribution (solid), cdf and pdf, of significant wave-height in atlantic data, with estimated (dashed) Generalized Extreme Value distribution, and two diagnostic plots of goodness of fit.

6.2.1 Generalized Extreme Value distribution

For the Generalized Extreme Value (GEV) distribution the estimation methods used in the WAFO toolbox are the Maximum Likelihood (ML) method and the method with Probability Weighted Moments (PWM), described in [66] and [29]. The programs have been adapted to MATLAB from a package of S-Plus routines described in [10].

We start with the significant wave-height data for the Atlantic data, stored in `Hs`. The command

```
gev = fitgev(Hs,'plotflag',2)
```

will give estimates `gev.params = [khat sigmahat muhat]` of the parameters (k, σ, μ) in the GEV distribution (6.8). The output matrix field `gev.covariance` will contain the estimated covariance matrix of the estimates. The program also gives a plot of the empirical distribution together with the best fitted distribution and two diagnostic plots that give indications of the goodness of fit; see Figure 6.2.

The routine `plotkde`, which is a simplified version of the kernel density estimation routines in `kdetools`, is used to compare the GEV density given estimated parameters with a non-parametric estimate (note that `plotkde` can be slow for large data sets like `Hs`). The commands

```
clf
x = linspace(0,14,200);
plotkde(Hs,[x;pdfgev(x,gev)]')
```

will give the upper right diagram in Figure 6.2.

The default estimation algorithm for the GEV distribution is the method with Probability Weighted Moments (PWM). An optional second argument, `fitgev(Hs, method)`,

allows a choice between the PWM-method (when `method = 'pwm'`) and the alternative ML-method (when `method = 'ml'`). The variances of the ML estimates are usually smaller than those of the PWM estimates. However, it is recommended that one first uses the PWM method, since it works for a wider range of parameter values.

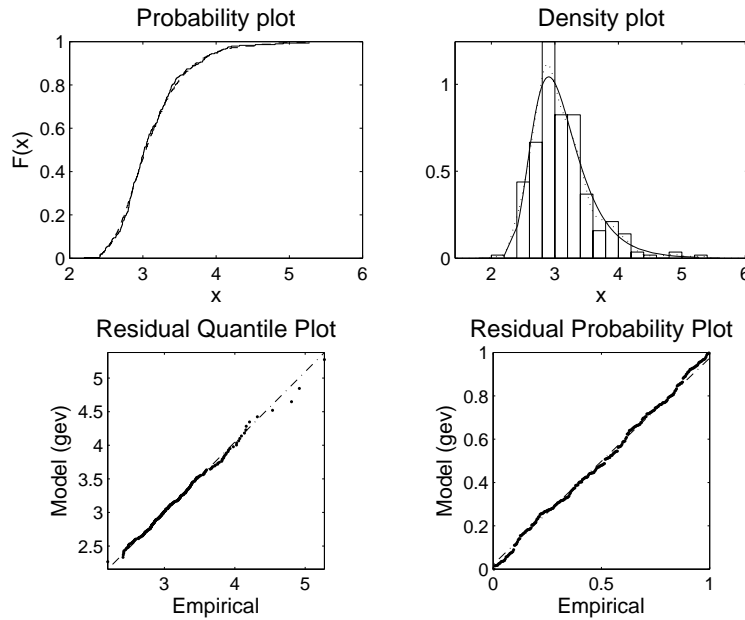


Figure 6.3: GEV analysis of 285 maxima over 5 minute intervals of sea level data Yura87.

Example 13. (*Wave data from the Yura station*) The WAFO toolbox contains a data set `yura87` of more than 23 hours of water level registrations at the Poseidon platform in the Japan Sea; see `help yura87`. Sampling rate is 1 Hz and to smooth data we interpolate to 4 Hz, and then group the data into a matrix with 5 minutes of data in each column, leaving out the last, unfinished period.

```
xn = load('yura87.dat');
XI = 0:0.25:length(xn);
N = length(XI); N = N-mod(N,4*60*5);
YI = interp1(xn(:,1),xn(:,2),XI(1:N),'spline');
YI = reshape(YI,4*60*5,N/(4*60*5)); % Each column holds
                                     % 5 minutes of interpolated data.
```

It turns out that the mean value and standard deviation change slowly during the measuring period, and we therefore standardize each column to zero mean and unit variance, before we take the maximum over each 5 minute interval and perform the GEV analysis; compare the results with those in the simpler analysis in Section 1.4.5.

```
Y5 = (YI-ones(1200,1)*mean(YI))./(ones(1200,1)*std(YI));
Y5M = max(Y5);
Y5gev = fitgev(Y5M,'plotflag',2)
```

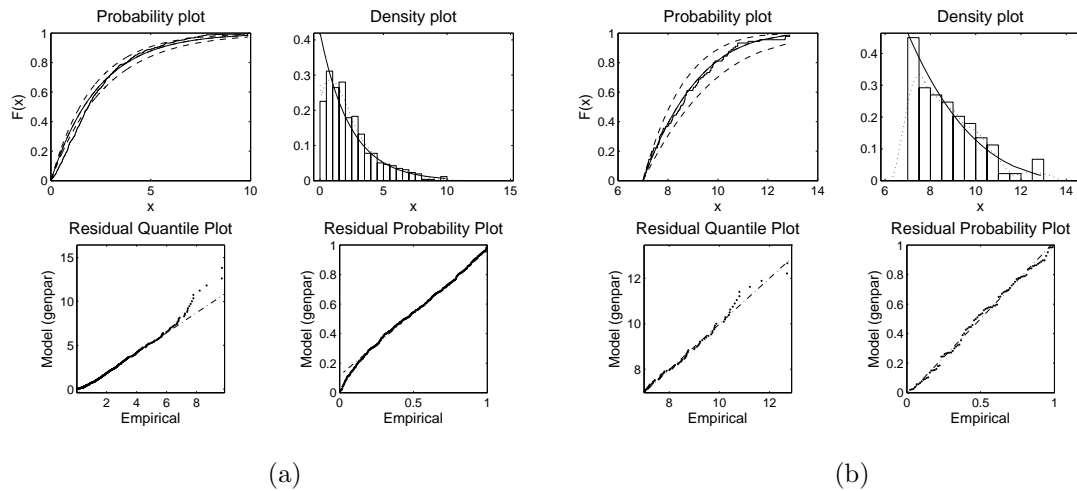


Figure 6.4: (a) Exceedances of significant wave-height data over level 3, (b) Significant wave-height over level 7, in atlantic data

The estimated parameters in `Y5gev.params` are $k = -0.314$ with a 95% confidence interval of $(-0.12, 0.06)$, indicating that a Gumbel distribution might be an acceptable choice. Location and scale are estimated to $\mu = 2.91$ and $\sigma = 0.34$. Figure 6.3 shows a good fit to the GEV model for the series of 5 minute maxima in the (standardized) Yura series, except for the few largest values, which are underestimated by the model. This is possibly due to a few short periods with very large variability in the data. \square

6.2.2 Generalized Pareto distribution

For the Generalized Pareto distribution (GPD) the WAFO uses the method with Probability Weighted Moments (PWM), described in [28], and the standard Method of Moments (MOM), as well as a general method suggested by Pickands, in [61]. S-Plus routines for these methods are described in [10].

The GPD is often used for exceedances over high levels, and it is well suited as a model for significant wave heights. To fit a GPD to the exceedances in the `atlantic` H_s series over of thresholds 3 and 7, one uses the commands

```
gpd3 = fitgenpar(Hs(Hs>3)-3,'plotflag',1);
figure
gpd7 = fitgenpar(Hs(Hs>7),'fixpar',...
                 [nan,nan,7],'plotflag',1);
```

This will give estimates `gpd.params = [khat sigma_hat]` of the parameters (k, σ) in the Generalized Pareto distribution (6.7) based on exceedance data $H_s(H_s > u) - u$. The optional output matrix `gpd.covariance` will contain the estimated covariance matrix of the estimates. The program also gives a plot of the empirical distribution together with the best fitted distribution; see Figure 6.4. The fit is better for exceedances over level 7 than over 3, but there are less data available, and the confidence bounds are wider.

The choice of estimation method is rather dependent on the actual parameter values. The default estimation algorithm in WAFO for estimation in the Generalized Pareto

distribution is the Maximum Product of Spacings (MPS) estimator since it works for all values of the shape parameter and have the same asymptotic properties as the Maximum Likelihood (ML) method (when it is valid). The Pickands' (PKD) and Least Squares (LS) estimator also work for any value of the shape parameter k in Eq. (6.7). The ML method is only useful when $k \leq 1$, the PWM when $k > -0.5$, the MOM when $k > -0.25$. The variances of the ML estimates are usually smaller than those of the other estimators. However, for small sample sizes it is recommended to use the PWM, MOM or MPS if they are valid.

It is possible to simulate independent GEV and GPD observations in WAFO. The command series

```
Rgev = rndgev(0.3,1,2,1,100);
gp = fitgev(Rgev,'method','pwm');
gm = fitgev(Rgev,'method','ml','start',gp.params,...
            'plotflag',0);
x=sort(Rgev);
plottedf(Rgev,gp,{'-','r-'}); hold on
plot(x,cdfgev(x,gm),'--'); hold off
```

simulates 100 values from the GEV distribution with parameters (0.3, 1, 2), then estimates the parameters using two different methods and plots the estimated distribution functions together with the empirical distribution. Similarly for the GPD distribution.

```
Rgpd = rndgenpar(0.4,1,0,1,100);
plottedf(Rgpd); hold on
gp = fitgenpar(Rgpd,'method','pkd','plotflag',0);
x=sort(Rgpd);
plot(x,cdfgenpar(x,gp))
gw = fitgenpar(Rgpd,'method','pwm','plotflag',0);
plot(x,cdfgenpar(x,gw),'g:')
gml = fitgenpar(Rgpd,'method','ml','plotflag',0);
plot(x,cdfgenpar(x,gml),'--')
gmps = fitgenpar(Rgpd,'method','mps','plotflag',0);
plot(x,cdfgenpar(x,gmps),'r-.'); hold off
```

with four different methods of parameter estimation. The results are shown in Figure 6.5(a) and (b).

6.2.3 Return value analysis

As in the Gumbel model, one can calculate the return levels in the GEV by inverting (6.5) with the GEV distribution function (6.8). The return level corresponding to return period N satisfies $1 - F(s_N) = 1/N$, so when F is a GEV distribution function with shape parameter $k \neq 0$,

$$s_N = \mu + \frac{\sigma}{k} \left(1 - (-\log(1 - 1/N))^k \right) \approx \mu + \frac{\sigma}{k} \left(1 - N^{-k} \right), \quad (6.9)$$

where the last expression holds for N large, so one can use $-\log(1 - 1/N) \approx 1/N$. As always in practice, the parameters in the return level have to be replaced by their estimated values, which introduces uncertainties in the computed level.

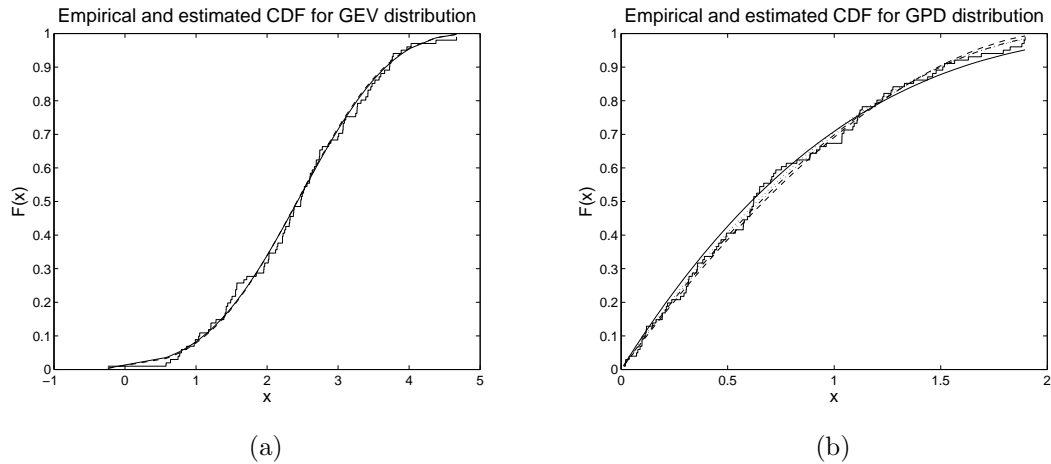


Figure 6.5: Empirical (solid) distributions and estimated (dashed) distribution functions for 100 observations of GEV (a) and GPD (b) variables.

Example 13. (contd.) Applied to the *yura87* data and the estimated GEV-model, we perform the return level extrapolation by the commands,

```
T = 1:100000;
k = Y5gev.params(1); mu=Y5gev.params(3);
sigma = Y5gev.params(2);
sT = mu + sigma/k*(1-(log(1-1./T))^k);
semilogx(T,sT), hold
N = 1:length(Y5M); Nmax=max(N);
plot(Nmax./N,sort(Y5M,'descend'),'.'')
title('Return values in the GEV model')
xlabel('Return priod')
ylabel('Return value')
grid on; hold off
```

The result is shown in Figure 6.6, consistent with the quantile plot in Figure 6.3. \square

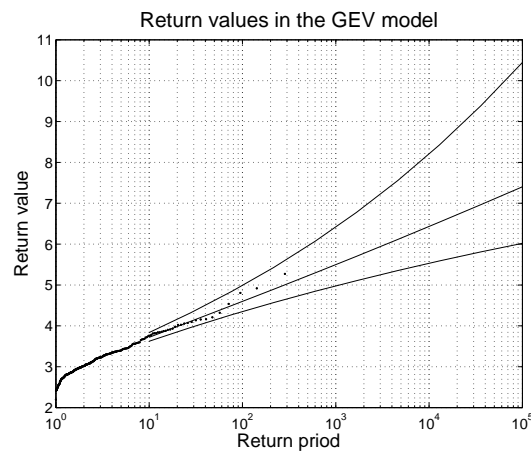


Figure 6.6: Return level extrapolation in *yura87* data depends on the good fit in the main part of the distribution. A few deviating large observations are disturbing.

6.3 POT-analysis

Peaks Over Threshold analysis (POT) is a systematic way to analyse the distribution of the exceedances over high levels in order to estimate extreme quantiles outside the range of observed values. The method is based on the observation that the extreme tail of a distribution often has a rather simple and standardized form, regardless of the shape of the more central parts of the distribution. One then fits such a simple distribution only to those observations that exceed some suitable level, with the hope that this fitted distribution gives an accurate fit to the real distribution also in the more extreme parts. The level should be chosen high enough for the tail to have approximately the standardized form, but not so high that there remains too few observations above it. After fitting a tail distribution one estimates the distribution of the (random) number of exceedances over the level, and then combines the tail distribution of the individual exceedances with the distribution for the number of exceedances to find the total tail distribution.

6.3.1 Expected exceedance

The simplest distribution to fit to the exceedances over a level u is the Generalized Pareto distribution, GPD, with distribution function (6.7). Note that if a random variable X follows a Generalized Pareto distribution $F(x; k, \sigma)$, then the exceedances over a level u is also GPD with distribution function $F(x; k, \sigma - ku)$, with the same k -parameter but with different (if $k \neq 0$) scale parameter $\sigma - ku$,

$$P(X > u + y \mid X > u) = \frac{(1 - k \frac{u+y}{\sigma})^{1/k}}{(1 - k \frac{u}{\sigma})^{1/k}} = \left(1 - k \frac{y}{\sigma - ku}\right)^{1/k}.$$

Another important property of the Generalized Pareto Distribution is that if $k > -1$, then the mean exceedance over a level u is a linear function of u :

$$E(X - u \mid X > u) = \frac{\sigma - ku}{1 + k}.$$

Plotting the mean exceedance as a function of u can help on decide on a proper threshold value. The resulting plot is called *Mean residual life plot*, also referred to as mean excess plots in statistical literature. The following command illustrate this for the significant wave height `atlantic` data:

```
plotreslife(Hs, 'umin', 2, 'umax', 10, 'Nu', 200);
```

The result is plotted in Figure 6.7, and it seems to exhibit an almost linear relationship for $u \geq 7$.

6.3.2 Poisson + GPD = GEV

If one is successful in fitting a Generalized Pareto distribution to the tail of data, one would like to use the GPD to predict how extreme values might occur over a certain period of time. One could, for example, want to predict the most extreme wave height that will appear during a year. If the distribution of the individual significant wave height exceedances is GPD one can easily find e.g., the distribution of the largest value of a fixed number of exceedances. However, the number of exceedances is not fixed but random, and

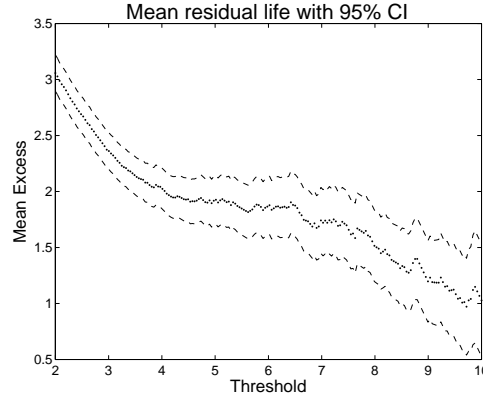


Figure 6.7: Expected exceedance over level u of **atlantic** data as function of u .

then one has to combine the distribution of the random size of individual exceedances with the random number of exceedances N , before one can say anything about the total maximum. If the level u is high we can, due to the Poisson approximation of the Binomial distribution and neglecting the dependence of nearby values, assume N to have an approximate Poisson distribution.

Now there is a nice relationship between the Generalized Pareto distribution and the Generalized Extreme Value distribution in this respect: *the maximum of a Poisson distributed number of independent GPD variables has a GEV distribution*. This follows by simple summation of probabilities: if N is a Poisson distributed random variable with mean μ , and $M_N = \max(X_1, X_2, \dots, X_N)$ is the maximum of N independent GPD variables then,

$$\begin{aligned} P(M_N \leq x) &= \sum_{n=0}^{\infty} P(N = n) \cdot P(X_1 \leq x, X_2 \leq x, \dots, X_n \leq x) \\ &= \sum_{n=0}^{\infty} e^{-\mu} \frac{\mu^n}{n!} \cdot \left(1 - \left(1 - k \frac{x}{\sigma}\right)^{1/k}\right)^n \\ &= \exp \left\{ -\left(1 - k(x - a)/b\right)^{1/k} \right\}, \end{aligned}$$

which is the Generalized Extreme Value distribution with $b = \sigma/\mu^k$ and $a = \sigma(1 - \mu^{-k})/k$.

This means that we can estimate the distribution of the maximum significant wave height during a winter (December – February) months from our data set **Hs** by fitting a GPD to the exceedances over some level u , estimating μ by the number of exceedances N divided by the number of months ($7 \times 3 \times 2 = 42$) and use the above relation to fit a GEV distribution:

```
gpd7 = fitgenpar(Hs(Hs>7)-7,'method','pwm','plotflag',0);
khat = gpd7.params(1);
sigmahat = gpd7.params(2);
muhat = length(Hs(Hs>7))/(7*3*2);
bhat = sigmahat/muhat^khat;
ahat = 7-(bhat-sigmahat)/khat;
x = linspace(5,15,200);
plot(x,cdfgev(x,khat,bhat,ahat))
```

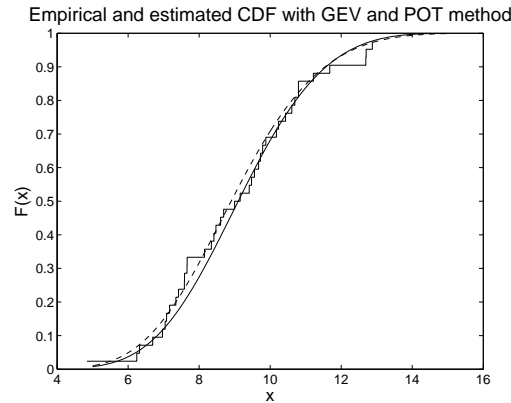


Figure 6.8: Estimated distribution functions of monthly maxima with the POT method (solid), fitting a GEV (dashed) and the empirical distribution.

We have here used the threshold $u = 7$ since the exceedances over this level seem to fit well to a GPD distribution in Figures 6.4(b) and 6.7. A larger value will improve the Poisson approximation to the number of exceedances but give us less data to estimate the parameters.

Since we have approximately 14 data points for 41 complete months, we can compute the monthly maxima `mm` and fit a GEV distribution directly:

```
mm = zeros(1,41);
for i=1:41
    % Last month is not complete
    mm(i) = max(Hs(((i-1)*14+1):i*14));
end
gev = fitgev(mm);
plotcdf(mm), hold on
plot(x,cdfgev(x,gev),'--'), hold off
```

The results of the two methods agree very well in this case as can be seen in Figure 6.8, where the estimated distributions are plotted together with the empirical distribution of `mm`.

6.3.3 Declustering

The POT method relies on two properties of peaks over the selected threshold: they should occur randomly in time according to an approximate Poisson process, and the exceedances should have an approximate GPD distribution and be approximately independent. In practice, one does not always find a Poisson distribution for the number of exceedances. Since extreme values sometimes have a tendency to cluster, some declustering algorithm could be applied to identify the largest value in each of the clusters, and then use a Poisson distribution for the number of clusters. The selected peaks should be sufficiently far apart for the exceedances to be independent. The WAFO toolbox contains the routine `decluster` to perform the declustering.

To select the clusters and check the Poisson character one can use the *dispersion index*, which is the ratio between the variance and the expectation of the number of peaks. For a Poisson distribution this ratio is equal to one. An acceptable peak separation should give a dispersion index near one.

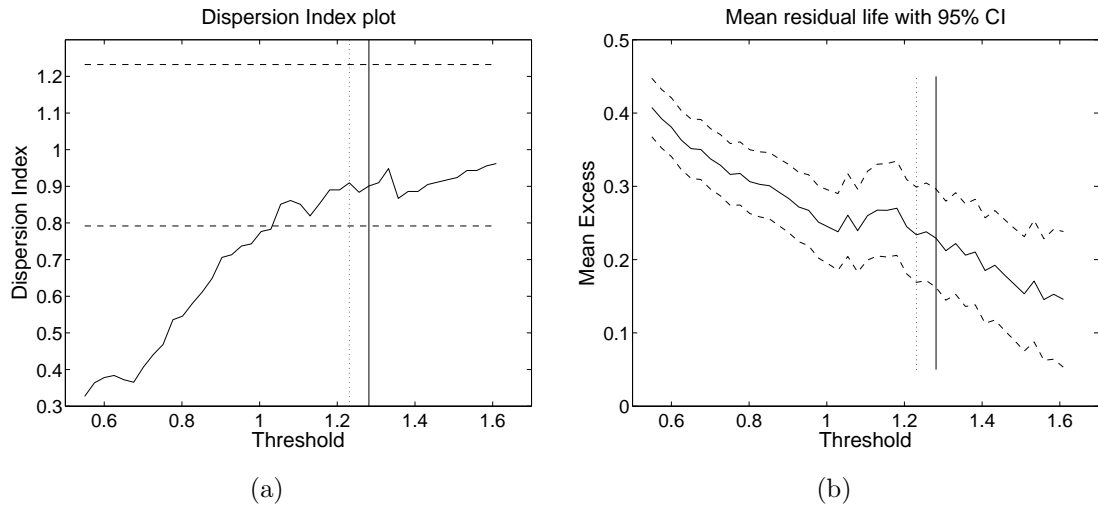


Figure 6.9: Threshold selection in POT analysis. Dashed vertical line indicates threshold selected by the dispersion index, solid line by the residual life analysis.

Example 14. (*Declustering sea data*) We will extract peaks over threshold in the `sea.dat`, which is a recording of almost 40 minutes of sea level data, sampled at a rate of 4[Hz].

We first define some parameters, `Nmin`, `Tmin`, `Tb`, to control the declustering, and to identify the peaks that exceed 90% of the median peak size and are separated by at least `Tmin`.

```

Nmin = 7; % minimum number of extremes
Tmin = 5; % minimum dist between extremes
Tb = 15; % block period
xx = load('sea.dat');
timeSpan = (xx(end,1)-xx(1,1))/60; % in minutes
dt = xx(2,1)-xx(1,1); % in seconds
tc = dat2tc(xx);
umin = median(tc(tc(:,2)>0,2));
Ie0 = findpot(tc, 0.9*umin, Tmin);
Ev = sort(tc(Ie0,2));
Ne = numel(Ev)
if Ne>Nmin && Ev(Ne-Nmin)>umin, umax = Ev(Ne-Nmin);
else umax = umin;
end

```

Next, we calculate the expected residual life and the dispersion index for thresholds between `umin` and `umax` and select an interval which is compatible with the Poisson distribution for the number of peaks.

```

Nu = floor((umax-umin)/0.025)+1;
u = linspace(umin,umax,Nu);
mrl = reslife(Ev, 'u',u);
umin0 = umin;

```

```

for io = numel(mrl.data):-1:1,
    CI = mrl.dataCI(io:end,:);
    if ~(max(CI(:,1))<=mrl.data(io) && mrl.data(io)<=min(CI(:,2))),
        umin0 = mrl.args(io); break;
    end
end
[di, threshold, ok_u] = ...
    disprsnidx(tc(Ie0,:), 'Tb', Tb, 'alpha',0.05, 'u',u);

```

The plots from the following commands are shown in Figure 6.9. It seems as if `threshold = 1.23[m]` is a suitable threshold.

```

figure(1); plot(di)
vline(threshold)      % Threshold from dispersion index
vline(umin0,'g')      % Threshold from mean residual life plot
figure(2); plot(mrl)
vline(threshold)      % Threshold from dispersion index
vline(umin0,'g')      % Threshold from mean residual life plot

```

A GPD fit for peaks above 1.23[m] with diagnostic plot is obtained by the commands

```

Ie = findpot(tc, threshold, Tmin);
lambda = numel(Ie)/timeSpan; % # Y>threshold per minute
varLambda = lambda*(1-(dt/60)*lambda)/timeSpan;
stdLambd = sqrt(varLambda)
Ev = tc(Ie,2);
phat = fitgenpar(Ev, 'fixpar',[nan,nan,threshold], 'method','mps');
figure(3); phat.plotfitsumry() % check fit to data

```

The diagnostic plots are found in Figure 6.10. The last step is to calculate the numerical value and some confidence intervals for a return level, and we do so for a three hour period, 180 min.

```

Tr = 3*60          % Return period in minutes
[xr,xrlo,xrup] = invgenpar(1./(lambda*Tr),phat,...
    'lowertail',false,'alpha', 0.05) % return level + 95%CI
[xr,xrlo5,xrup5] = invgenpar(1./(lambda*Tr),phat,...
    'lowertail',false,'alpha', 0.5)  % return level + 50%CI

```

The three hour return level is thus estimated to `xr = 2.02[m]` with a 95% confidence interval (1.30, 10.08). The 50% confidence bounds are (1.58, 3.05); as expected, a high confidence leads to a very high upper limit. \square

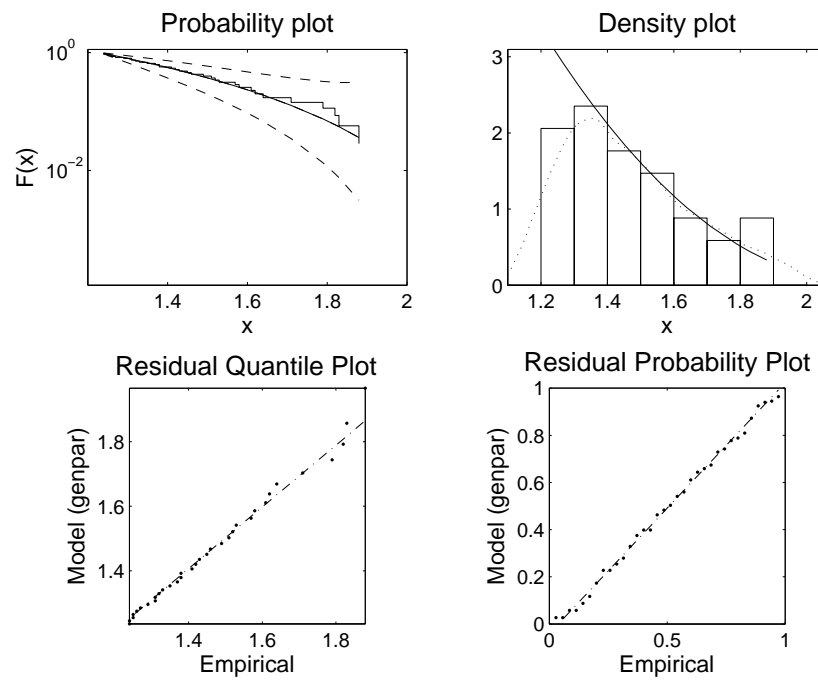


Figure 6.10: Diagnostic GPD plot for sea data return levels.

6.4 Summary of statistical procedures in WAFO

The extreme value analysis presented in this chapter is part of a comprehensive library of statistical routines for random number generation, probability distributions, and parameter and density estimation and likelihood analysis, etc.

help statistics

Module STATISTICS in WAFO Toolbox.

Version 2.5.2 07-Feb-2011

What's new

Readme - New features, bug fixes, and changes
in STATISTICS.

Parameter estimation

fitbeta	- Parameter estimates for Beta data
fitchi2	- Parameter estimates for Chi squared data
fitexp	- Parameter estimates for Exponential data
fitgam	- Parameter estimates for Gamma data
fitgengam	- Parameter estimates for Generalized Gamma data
fitgenpar	- Parameter estimates for Generalized Pareto data
fitgenparml	- Internal routine for fitgenpar (ML estimates for GPD data)
fitgenparrange	- Parameter estimates for GPD model over a range of thresholds
fitgev	- Parameter estimates for GEV data
fitgumb	- Parameter estimates for Gumbel data
fitinvnorm	- Parameter estimates for Inverse Gaussian data
fitlognorm	- Parameter estimates for Lognormal data
fitmarg2d	- Parameter estimates for MARG2D data
fitmargcnd2d	- Parameter estimates for DIST2D data
fitnorm	- Parameter estimates for Normal data
fitray	- Parameter estimates for Rayleigh data
fitraymod	- Parameter estimates for Truncated Rayleigh data
fitt	- Parameter estimates for Student's T data
fitweib	- Parameter estimates for Weibull data
fitweib2d	- Parameter estimates for 2D Weibull data
fitweibmod	- Parameter estimates for truncated Weibull data

<code>cdfdiscrete</code>	- Discrete CDF
<code>cdfempirical</code>	- Empirical CDF
<code>cdfmarg2d</code>	- Joint 2D CDF due to Plackett
<code>cdfmargcnd2d</code>	- Joint 2D CDF computed as $\int F(X_1 < v X_2 = x_2) \cdot f(x_2) dx_2$
<code>cdfmargcnd2dfun</code>	- is an internal function to <code>cdfmargcnd2d</code> and <code>prbmargcnd2d</code> .
<code>cdfnormnd</code>	- Multivariate normal CDF
<code>cdfweib2d</code>	- Joint 2D Weibull CDF
<code>cdfbeta</code>	- Beta CDF
<code>cdfbin</code>	- Binomial CDF
<code>cdfchi2</code>	- Chi squared CDF
<code>cdfexp</code>	- Exponential CDF
<code>cdff</code>	- Snedecor's F CDF
<code>cdffrech</code>	- Frechet CDF
<code>cdfgam</code>	- Gamma CDF
<code>cdfgengam</code>	- Generalized Gamma CDF
<code>cdfgengammod</code>	- Modified Generalized Gamma CDF
<code>cdngenpar</code>	- Generalized Pareto CDF
<code>cdngev</code>	- Generalized Extreme Value CDF
<code>cdfgumb</code>	- Gumbel CDF
<code>cdfhyge</code>	- The hypergeometric CDF
<code>cdfinvnorm</code>	- Inverse Gaussian CDF
<code>cdflognorm</code>	- Lognormal CDF
<code>cdfmargcnd2d</code>	- Joint 2D CDF computed as $\int F(X_1 < v X_2 = x_2) \cdot f(x_2) dx_2$
<code>cdfnorm</code>	- Normal CDF
<code>cdfray</code>	- Rayleigh CDF
<code>cdfraymod</code>	- Modified Rayleigh CDF
<code>cdft</code>	- Student's T CDF
<code>cdfpois</code>	- Poisson CDF
<code>cdfweib</code>	- Weibull CDF
<code>cdfweibmod</code>	- Truncated Weibull CDF
<code>edf</code>	- Empirical Distribution Function
<code>edfcnd</code>	- Empirical Distribution Function conditioned on $X \geq c$
<code>prbmargcnd2d</code>	- returns the probability for rectangular regions
<code>prbweib2d</code>	- returns the probability for rectangular regions
<code>margcnd2dsmfun</code>	- Smooths the MARGCND2D distribution parameters
<code>margcnd2dsmfun2</code>	- Smooths the MARGCND2D distribution parameters

Inverse cumulative distribution functions

invbeta	- Inverse of the Beta CDF
invbin	- Inverse of the Binomial CDF
invcauchy	- Inverse of the Cauchy CDF
invchi2	- Inverse of the Chi squared CDF
invcmarg2d	- Inverse of the conditional CDF of X2 given X1
invcweib2d	- Inverse of the conditional 2D weibull CDF of X2 given X1
invdiscrete	- Discrete quantile
invempirical	- Empirical quantile
invexp	- Inverse of the Exponential CDF
invf	- Inverse of Snedecor's F CDF
invfrech	- Inverse of the Frechet CDF
invgam	- Inverse of the Gamma CDF
invgengam	- Inverse of the Generalized Gamma CDF
invgengammod	- Inverse of the Generalized Gamma CDF
invgenpar	- Inverse of the Generalized Pareto CDF
invgev	- Inverse of the Generalized Extreme Value CDF
invgumb	- Inverse of the Gumbel CDF
invhyge	- Inverse of the Hypergeometric CDF
invinvnorm	- Inverse of the Inverse Gaussian CDF
invlognorm	- Inverse of the Lognormal CDF
invnorm	- Inverse of the Normal CDF
invray	- Inverse of the Rayleigh CDF
invrt	- Inverse of the Student's T CDF
invweib	- Inverse of the Weibull CDF
invpois	- Inverse of the Poisson CDF
invraymod	- Inverse of the modified Rayleigh CDF
invweibmod	- Inverse of the modified Weibull CDF

Random number generators

rndalpha	- Random matrices from a symmetric alpha-stable distribution
rndbeta	- Random matrices from a Beta distribution
rndbin	- Random numbers from the binomial distribution
rndboot	- Simulate a bootstrap resample from a sample
rndcauchy	- Random matrices a the Cauchy distribution
rndchi2	- Random matrices from a Chi squared distribution
rnddiscrete	- Random sample

<code>rndempirical</code>	- Bootstrap sample
<code>rndexp</code>	- Random matrices from an Exponential distribution
<code>rndf</code>	- Random matrices from Snedecor's F distribution
<code>rndfrech</code>	- Random matrices from a Frechet distribution
<code>rndgam</code>	- Random matrices from a Gamma distribution
<code>rndgengam</code>	- Random matrices from a Generalized Gamma distribution.
<code>rndgengammod</code>	- Random matrices from a Generalized Modified Gamma distribution.
<code>rndgenpar</code>	- Random matrices from a Generalized Pareto Distribution
<code>rndgev</code>	- Random matrices from a Generalized Extreme Value distribution
<code>rndgumb</code>	- Random matrices from a Gumbel distribution
<code>rndhyge</code>	- Random numbers from the Hypergeometric distribution
<code>rndinvnorm</code>	- Random matrices from a Inverse Gaussian distribution
<code>rndlognorm</code>	- Random matrices from a Lognormal distribution.
<code>rndmarg2d</code>	- Random points from a MARG2D distribution
<code>rndmargcnd2d</code>	- Random points from a MARGCND2D distribution
<code>rndnorm</code>	- Random matrices from a Normal distribution
<code>rndnormnd</code>	- Random vectors from a multivariate Normal distribution
<code>rndpois</code>	- Random matrices from a Poisson distribution
<code>rndray</code>	- Random matrices from a Rayleigh distribution
<code>rndraymod</code>	- Random matrices from modified Rayleigh distribution
<code>rndt</code>	- Random matrices from a Student's T distribution
<code>rndweib</code>	- Random matrices a the Weibull distribution
<code>rndweibmod</code>	- Random matrices from the modified Weibull distribution
<code>rndweib2d</code>	- Random numbers from the 2D Weibull distribution

Moments

mombeta	- Mean and variance for the Beta distribution
mombin	- Mean and variance for the Binomial distribution
momchi2	- Mean and variance for the Chi squared distribution
momexp	- Mean and variance for the Exponential distribution
momf	- Mean and variance for Snedecor's F distribution
momfrech	- Mean and variance for the Frechet distribution
momgam	- Mean and variance for the Gamma distribution
momgengam	- Mean and variance for the Generalized Gamma distribution
momgenpar	- Mean and variance for the Generalized Pareto distribution
momgev	- Mean and variance for the GEV distribution
momgumb	- Mean and variance for the Gumbel distribution
momhyge	- Mean and variance for the Hypergeometric distribution
mominvnorm	- Mean and variance for the Inverse Gaussian distribution
momlognorm	- Mean and variance for the Lognormal distribution
mommarg2d	- Mean and variance for the MARG2D distribution
mommargcnd2d	- Mean and variance for the MARGCND2D distribution
momnorm	- Mean and variance for the Normal distribution
mompois	- Mean and variance for the Poisson distribution
momray	- Mean and variance for the Rayleigh distribution
momt	- Mean and variance for the Student's T distribution
momweib	- Mean and variance for the Weibull distribution
momweib2d	- Mean and variance for the 2D Weibull distribution

Profile log likelihood functions

lnkexp	- Link for x,F and parameters of Exponential distribution
lnkgenpar	- Link for x,F and parameters of Generalized Pareto distribution
lnkgev	- Link for x,F and parameters of Generalized Extreme value distribution
lnkgumb	- Link for x,F and parameters of Gumbel distribution
lnkgumbtrnc	- Link for x,F and parameters of truncated Gumbel distribution
lnkray	- Link for x,F and parameters of Rayleigh distribution
lnkweib	- Link for x,F and parameters of Weibull distribution
loglike	- Negative Log-likelihood function
logps	- Moran's negative log Product Spacings statistic
ciproflog	- Confidence Interval using Profile Log-likelihood or Product Spacing- function
proflog	- Profile Log- likelihood or Product Spacing-function
findciproflog	- Find Confidence Interval from proflog function

Extremes

decluster	- Decluster peaks over threshold values
extremalidx	- Extremal Index measuring the dependence of data
findpot	- Find indices to Peaks over threshold values
fitgev	- Parameter estimates for GEV data
fitgenpar	- Parameter estimates for Generalized Pareto data
prb2retper	- Return period from Probability of exceedance
retper2prb	- Probability of exceedance from return period

Threshold selection

fitgenparrange	- Parameter estimates for GPD model vs thresholds
disprsnidx	- Dispersion Index vs threshold
reslife	- Mean Residual Life, i.e., mean excesses vs thresholds

- plotdisprsnidx - Plot Dispersion Index vs thresholds
- plotreslife - Plot Mean Residual Life
(mean excess vs thresholds)

Regression models

- logit - Logit function.
- logitinv - Inverse logit function.
- regglm - Generalized Linear Model regression
- reglm - Fit multiple Linear Regression Model.
- reglogit - Fit ordinal logistic regression model.
- regnonlm - Non-Linear Model Regression
- regstepmlm - Stepwise predictor subset selection for
Linear Model regression

Factor analysis

- princomp - Compute principal components of X

Descriptive Statistics

- ranktrf - Rank transformation of data material.
- spearman - Spearman's rank correlation coefficient
- mean - Computes sample mean (Matlab)
- median - Computes sample median value (Matlab)
- std - Computes standard deviation (Matlab)
- var - Computes sample variance (Matlab)
- var2corr - Variance matrix to correlation matrix
conversion
- cov - Computes sample covariance matrix
(Matlab)
- corrcoef - Computes sample correlation coefficients
(Matlab toolbox)
- skew - Computes sample skewness
- kurt - Computes sample kurtosis
- lmoment - L-moment based on order statistics
- percentile - Empirical quantile (percentile)
- iqr - Computes the Inter Quartile Range
- range - Computes the range between the maximum
and minimum values

Statistical plotting

- clickslct - Select points in a plot by clicking
with the mouse
- histgram - Plot histogram
- plotbox - Plot box-and-whisker diagram
- plotdensity - Plot density.
- plotexp - Plot data on Exponential distribution
paper

plotedf	- Plot Empirical Distribution Function
plotedfcnd	- Plot Empirical Distribution Function CoNDitioned that $X \geq c$
plotfitsumry	- Plot diagnostic of fit to data
plotgumb	- Plot data on Gumbel distribution paper
plotkde	- Plot kernel density estimate of PDF
plotmarg2dcdf	- Plot conditional CDF of X_1 given $X_2=x_2$
plotmarg2dmom	- Plot conditional mean and standard deviation
plotmargcnd2dcdf	- Plot conditional empirical CDF of X_1 given $X_2=x_2$
plotmargcnd2dfit	- Plot parameters of the conditional distribution
plotmargcnd2dmom	- Plot conditional mean and standard deviation
plotnorm	- Plot data on a Normal distribution paper
plotqq	- Plot empirical quantile of X vs empirical quantile of Y
plotray	- Plot data on a Rayleigh distribution paper
plotresprb	- Plot Residual Probability
plotresq	- Plot Residual Quantile
plotscatr	- Pairwise scatter plots
plotweib	- Plot data on a Weibull distribution paper
plotweib2dcdf	- Plot conditional empirical CDF of X_1 given $X_2=x_2$
plotweib2dmom	- Plot conditional mean and standard deviation

Hypothesis Tests

anovan	- multi-way analysis of variance (ANOVA)
testgumb	- Tests if shape parameter in a GEV is equal to zero
testmean1boot	- Bootstrap t-test for the mean equal to 0
testmean1n	- Test for mean equals 0 using one-sample T-test
testmean2n	- Two-sample t-test for mean(x) equals mean(y)
testmean1r	- Wilcoxon signed rank test for H_0 : mean(x) equals 0
testmean2r	- Wilcoxon rank-sum test for H_0 : mean(x) equals mean(y)

Confidence interval estimation

ciboot	- Bootstrap confidence interval.
ciquant	- Nonparametric confidence interval for quantile

momci1b - Moment confidence intervals using
 Bootstrap

Bootstrap & jackknife estimates

covboot - Bootstrap estimate of the variance of
 a parameter estimate.

covjack - Jackknife estimate of the variance of
 a parameter estimate.

stdboot - Bootstrap estimate of the
 standard deviation of a parameter

stdjack - Jackknife estimate of the
 standard deviation of a parameter

Design of Experiments

yates - Calculates main and interaction effects
 using Yates' algorithm.

ryates - Reverse Yates' algorithm to give
 estimated responses

fitmodel - Fits response by polynomial

alias - Alias structure of a fractional design

cdr - Complete Defining Relation

cl2cnr - Column Label to Column Number

cnr2cl - Column Number to Column Label

ffd - Two-level Fractional Factorial Design

getmodel - Return the model parameters

sudg - Some Useful Design Generators

plotresponse - Cubic plot of responses

nplot - Normal probability plot of effects

Misc

comnsize - Calculates common size of all non-scalar
 arguments

dgammainc - Incomplete gamma function with derivatives

gammaincln - Logarithm of incomplete gamma function.

parsestatsinput - Parses inputs to pdfxx, prbxx, invxx and
 rndxx functions

createfdata - Distribution parameter struct constructor

getdistname - Return the distribution name

stdize - Standardize columns to have mean 0 and
 standard deviation 1

center - Recenter columns to have mean 0

Demo

demofitgenpar - Script to check the variance of estimated
 parameters

APPENDIX A

Kernel density estimation

Histograms are among the most popular ways to visually present data. They are particular examples of density estimates and their appearance depends on both the choice of origin and the width of the intervals (bins) used. In order for the histogram to give useful information about the true underlying distribution, a sufficient amount of data is needed. This is even more important for histograms in two dimensions or higher. Also the discontinuity of the histograms may cause problems, e.g., if derivatives of the estimate are required.

An effective alternative to the histogram is the kernel density estimate (KDE), which may be considered as a “smoothed histogram”, only depending on the bin-width and not depending on the origin, see [80].

A.1 The univariate kernel density estimator

The univariate KDE is defined by

$$\hat{f}_X(x; h_s) = \frac{1}{n h_s} \sum_{j=1}^n K_d \left(\frac{x - X_j}{h_s} \right), \quad (\text{A.1})$$

where n is the number of datapoints, X_1, X_2, \dots, X_n , is the data set, and h_s is the smoothing parameter or window width. The kernel function K_d is usually a unimodal, symmetric probability density function. This ensures that the KDE itself is also a density. However, kernels that are not densities are also sometimes used [see 92], but these are not implemented in the WAFO toolbox.

To illustrate the method, consider the kernel estimator as a sum of “bumps” placed at the observations. The shape of the bumps are given by the kernel function while the width is given by the smoothing parameter, h_s . Fig. A.1 shows a KDE constructed using 7 observations from a standard Gaussian distribution with a Gaussian kernel function. One should note that the 7 points used here, is purely for clarity in illustrating how the kernel method works. Practical density estimation usually involves much higher number of observations.

Fig. A.1 also demonstrates the effect of varying the smoothing parameter, h_s . A too small value for h_s may introduce spurious bumps in the resulting KDE (top), while a

too large value may obscure the details of the underlying distribution (bottom). Thus the choice of value for the smoothing parameter, h_s , is very important. How to select one will be elaborated further in the next section.

The particular choice of kernel function, on the other hand, is not very important since suboptimal kernels are not suboptimal by very much, [see 92, pp. 31]. However, the kernel that minimizes the mean integrated square error is the Epanechnikov kernel, and is thus chosen as the default kernel in the software, see Eq. (A.8). For a discussion of other kernel functions and their properties, see [92].

A.1.1 Smoothing parameter selection

The choice of smoothing parameter, h_s , is very important, as exemplified in Fig.A.1. In many situations it is satisfactory to select the smoothing parameter subjectively by eye, i.e., look at several density estimates over a range of bandwidths and selecting the density that is the most “pleasing” in some sense. However, there are also many circumstances where it is beneficial to use an automatic bandwidth selection from the data. One reason is that it is very time consuming to select the bandwidth by eye. Another reason, is that, in many cases, the user has no prior knowledge of the structure of the data, and does not have any feeling for which bandwidth gives a good estimate. One simple, quick and commonly used automatic bandwidth selector, is the bandwidth that minimizes the mean integrated square error (MISE) asymptotically. As shown in [92, Section 2.5 and 3.2.1], the one dimensional AMISE¹-optimal normal scale rule assuming that the underlying density is Gaussian, is given by

$$h_{AMISE} = \left[\frac{4}{3n} \right]^{1/5} \hat{\sigma}, \quad (\text{A.2})$$

where $\hat{\sigma}$ is some estimate of the standard deviation of the underlying distribution. Common choices of $\hat{\sigma}$ are the sample standard deviation, $\hat{\sigma}_s$, and the standardized interquartile range (denoted IQR):

$$\hat{\sigma}_{IQR} = (\text{sample IQR}) / (\Phi^{-1}(3/4) - \Phi^{-1}(1/4)) \approx (\text{sample IQR}) / 1.349, \quad (\text{A.3})$$

where Φ^{-1} is the standard normal quantile function. The use of $\hat{\sigma}_{IQR}$ guards against outliers if the distribution has heavy tails. A reasonable approach is to use the smaller of $\hat{\sigma}_s$ and $\hat{\sigma}_{IQR}$ in order to lessen the chance of oversmoothing, [see 80, pp. 47].

Various other automatic methods for selecting h_s are available and are discussed in [80] and in more detail in [92].

A.1.2 Transformation kernel density estimator

Densities close to normality appear to be the easiest for the kernel estimator to estimate. The estimation difficulty increases with skewness, kurtosis and multimodality [92, Chap. 2.9].

Thus, in the cases where the random sample X_1, X_2, \dots, X_n , has a density, f , which is difficult to estimate, a transformation, t , might give a good KDE, i.e., applying a transformation to the data to obtain a new sample Y_1, Y_2, \dots, Y_n , with a density g that more

¹AMISE = asymptotic mean integrated square error

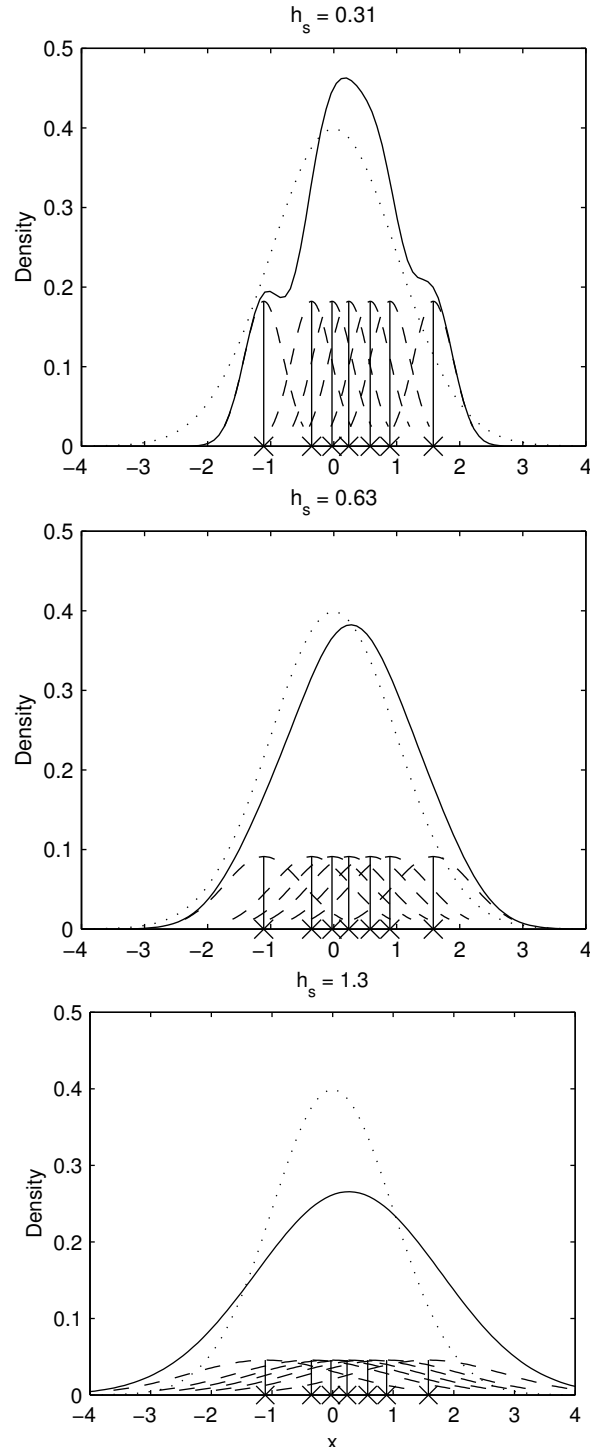


Figure A.1: Smoothing parameter, h_s , impact on KDE: True density (dotted) compared to KDE based on 7 observations (solid) and their individual kernels (dashed).

easily can be estimated using the basic KDE. One would then backtransform the estimate of g to obtain the estimate for f .

Suppose that $Y_i = t(X_i)$, where t is an increasing differentiable function defined on the support of f . Then a standard result from statistical distribution theory is that

$$f(x) = g(t(x)) t'(x), \quad (\text{A.4})$$

where $t'(x)$ is the derivative. Backtransformation of the KDE of g based on Y_1, Y_2, \dots, Y_n , leads to the explicit formula

$$\hat{f}_X(x; h_s, t) = \frac{1}{n h_s} \sum_{j=1}^n K_d \left(\frac{t(x) - t(X_j)}{h_s} \right) t'(x) \quad (\text{A.5})$$

A simple illustrative example comes from the problem of estimating the Rayleigh density. This density is very difficult to estimate by direct kernel methods. However, if we apply the transformation $Y_i = \sqrt{X_i}$ to the data, then the normal plot of the transformed data, Y_i , becomes approximately linear. Fig. A.2 shows that the transformation KDE is a better estimate around 0 than the ordinary KDE.

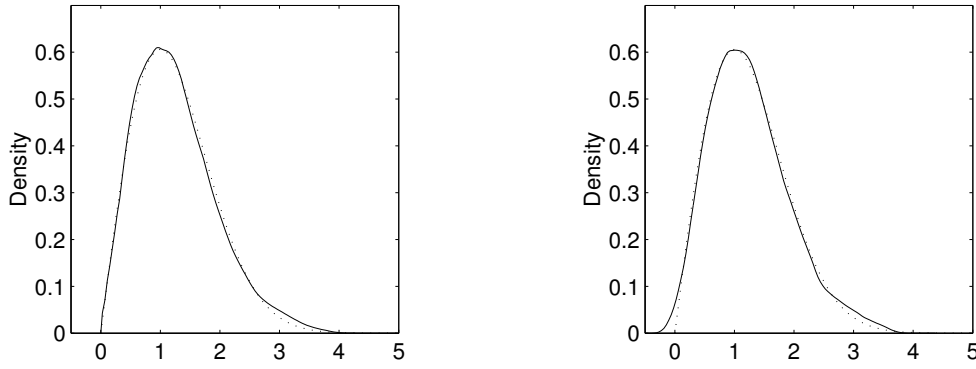


Figure A.2: True Rayleigh density (dotted) compared to transformation KDE (solid, left) and ordinary KDE (solid, right) based on 1000 observations.

A.2 The multivariate kernel density estimator

The multivariate kernel density estimator is defined in its most general form by

$$\hat{f}_{\mathbf{X}}(\mathbf{x}; \mathbf{H}) = \frac{|\mathbf{H}|^{-1/2}}{n} \sum_{j=1}^n K_d \left(\mathbf{H}^{-1/2}(\mathbf{x} - \mathbf{X}_j) \right), \quad (\text{A.6})$$

where \mathbf{H} is a symmetric positive definite $d \times d$ matrix called the *bandwidth matrix*. A simplification of Eq. (A.6) can be obtained by imposing the restriction $\mathbf{H} = \text{diag}(h_1^2, h_2^2, \dots, h_d^2)$. Then Eq. (A.6) reduces to

$$\hat{f}_{\mathbf{X}}(\mathbf{x}; \mathbf{h}) = \frac{1}{n \prod_{i=1}^d h_i} \sum_{j=1}^n K_d \left(\frac{x - X_{j1}}{h_1}, \frac{x - X_{j2}}{h_2}, \dots, \frac{x - X_{jd}}{h_d} \right), \quad (\text{A.7})$$

and is, in combination with a transformation, a reasonable solution to visualize multivariate densities.

The multivariate Epanechnikov kernel also forms the basis for the optimal spherically symmetric multivariate kernel and is given by

$$K_d(\mathbf{x}) = \frac{d+2}{2v_d} (1 - \mathbf{x}^T \mathbf{x}) \mathbf{1}_{\mathbf{x}^T \mathbf{x} \leq 1}, \quad (\text{A.8})$$

where $v_d = 2\pi^{d/2}/(\Gamma(d/2)d)$ is the volume of the unit d -dimensional sphere.

In this tutorial we use the KDE to find a good estimator of the central part of the joint densities of wave parameters extracted from time series. Clearly, such data are dependent, so it is assumed that the time series are ergodic and short range dependent to justify the use of KDE:s, [see 92, Chap. 6]. Usually, KDE gives poor estimates of the tail of the distribution, unless large amounts of data is available. However, a KDE gives qualitatively good estimates in the regions of sufficient data, i.e., in the main parts of the distribution. This is good for visualization, e.g. detecting modes, symmetries of distributions.

The kernel density estimation software is based on `KDETOOL`, which is a MATLAB toolbox produced by Christian Beardah, [9], which has been totally rewritten and extended to include the transformation kernel estimator and generalized to cover any dimension for the data. The computational speed has also been improved.

APPENDIX B

Standardized wave spectra

Knowledge of which kind of spectral density is suitable to describe sea state data are well established from experimental studies. Qualitative considerations of wave measurements indicate that the spectra may be divided into 3 parts, (see Fig. B.1):

1. Sea states dominated by wind sea but significantly influenced by swell components.
2. More or less pure wind seas or, possibly, swell component located well inside the wind frequency band.
3. Sea states more or less dominated by swell but significantly influenced by wind sea.

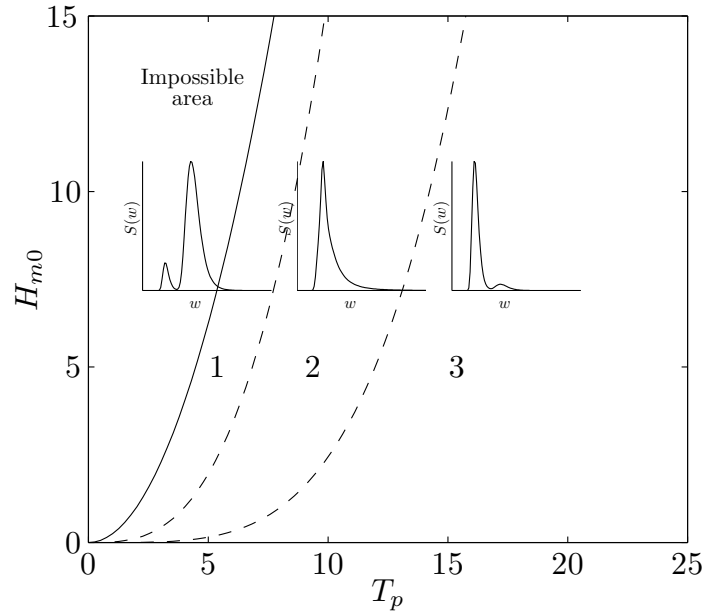


Figure B.1: Qualitative indication of spectral variability.

One often uses some parametric form of the spectral density. The three most important parametric spectral densities implemented in WAFO will be described in the following sections.

B.1 JONSWAP spectrum

The JONSWAP (JOint North Sea Wave Project) spectrum of [26] is a result of a multinational project to characterize standardized wave spectra for the Southeast part of the North Sea. The spectrum is valid for not fully developed sea states. However, it is also used to represent fully developed sea states. It is particularly well suited to characterize wind sea when $3.6\sqrt{H_{m0}} < T_p < 5\sqrt{H_{m0}}$. The JONSWAP spectrum is given in the form:

$$S^+(\omega) = \frac{\alpha g^2}{\omega^M} \exp\left(-\frac{M}{N} \left(\frac{\omega_p}{\omega}\right)^N\right) \gamma^{\exp\left(\frac{-(\omega/\omega_p-1)^2}{2\sigma^2}\right)}, \quad (\text{B.1})$$

where

$$\begin{aligned} \sigma &= \begin{cases} 0.07 & \text{if } \omega < \omega_p, \\ 0.09 & \text{if } \omega \geq \omega_p, \end{cases} \\ M &= 5, \quad N = 4, \\ \alpha &\approx 5.061 \frac{H_{m0}^2}{T_p^4} \left\{ 1 - 0.287 \ln(\gamma) \right\}. \end{aligned}$$

A standard value for the peakedness parameter, γ , is 3.3. However, a more correct approach is to relate γ to H_{m0} and T_p , and use

$$\gamma = \exp\left\{ 3.484 \left(1 - 0.1975 (0.036 - 0.0056 T_p / \sqrt{H_{m0}}) T_p^4 / H_{m0}^2 \right) \right\}. \quad (\text{B.2})$$

Here γ is limited by $1 \leq \gamma \leq 7$. This parameterization is based on qualitative considerations of deep water wave data from the North Sea; see [89] and [27].

The relation between the peak period and mean zero-upcrossing period may be approximated by

$$T_{m02} \approx T_p / (1.30301 - 0.01698 \gamma + 0.12102 / \gamma) \quad (\text{B.3})$$

The JONSWAP spectrum is identical with the two-parameter Pierson-Moskowitz, Bretschneider, ITTC (International Towing Tank Conference) or ISSC (International Ship and Off-shore Structures Congress) wave spectrum, given H_{m0} and T_p , when $\gamma = 1$. (For more properties of this spectrum, see the WAFO function `jonswap.m`.)

B.2 Torsethaugen spectrum

Torsethaugen, [86, 87, 88], proposed to describe bimodal spectra by

$$S^+(\omega) = \sum_{i=1}^2 S_J^+(\omega; H_{m0,i}, \omega_{p,i}, \gamma_i, N_i, M_i, \alpha_i) \quad (\text{B.4})$$

where S_J^+ is the JONSWAP spectrum defined by Eq. (B.1). The parameters $H_{m0,i}$, $\omega_{p,i}$, N_i , M_i , and α_i for $i = 1, 2$, are the significant wave height, angular peak frequency, spectral shape and normalization parameters for the primary and secondary peak, respectively.

These parameters are fitted to 20 000 spectra divided into 146 different classes of H_{m0} and T_p obtained at the Statfjord field in the North Sea in the period from 1980 to 1989. The measured H_{m0} and T_p values for the data range from 0.5 to 11 meters and from 3.5 to 19 seconds, respectively.

Given H_{m0} and T_p these parameters are found by the following steps. The borderline between wind dominated and swell dominated sea states is defined by the fully developed sea, for which

$$T_p = T_f = 6.6 H_{m0}^{1/3}, \quad (\text{B.5})$$

while for $T_p < T_f$, the local wind sea dominates the spectral peak, and if $T_p > T_f$, the swell peak is dominating.

For each of the three types a non-dimensional period scale is introduced by

$$\epsilon_{lu} = \frac{T_f - T_p}{T_f - T_{lu}},$$

where

$$T_{lu} = \begin{cases} 2\sqrt{H_{m0}} & \text{if } T_p \leq T_f \quad (\text{Lower limit}), \\ 25 & \text{if } T_p > T_f \quad (\text{Upper limit}), \end{cases}$$

defines the lower or upper value for T_p . The significant wave height for each peak is given as

$$H_{m0,1} = R_{pp} H_{m0} \quad H_{m0,2} = \sqrt{1 - R_{pp}^2} H_{m0},$$

where

$$R_{pp} = (1 - A_{10}) \exp\left(-\left(\frac{\epsilon_{lu}}{A_1}\right)^2\right) + A_{10},$$

$$A_1 = \begin{cases} 0.5 & \text{if } T_p \leq T_f, \\ 0.3 & \text{if } T_p > T_f, \end{cases} \quad A_{10} = \begin{cases} 0.7 & \text{if } T_p \leq T_f, \\ 0.6 & \text{if } T_p > T_f. \end{cases}$$

The primary and secondary peak periods are defined as

$$T_{p,1} = T_p,$$

$$T_{p,2} = \begin{cases} T_f + 2 & \text{if } T_p \leq T_f, \\ \left(\frac{M_2 (N_2/M_2)^{(N_2-1)/M_2} / \Gamma((N_2-1)/M_2)}{1.28 (0.4)^{N_2} \{1 - \exp(-H_{m0,2}/3)\}} \right)^{1/(N_2-1)} & \text{if } T_p > T_f, \end{cases}$$

where the spectral shape parameters are given as

$$N_1 = N_2 = 0.5 \sqrt{H_{m0}} + 3.2,$$

$$M_i = \begin{cases} 4 \left(1 - 0.7 \exp\left(\frac{-H_{m0}}{3}\right)\right) & \text{if } T_p > T_f \text{ and } i = 2, \\ 4 & \text{otherwise.} \end{cases}$$

The peakedness parameters are defined as

$$\gamma_1 = 35 \left(1 + 3.5 \exp(-H_{m0})\right) \gamma_T, \quad \gamma_2 = 1,$$

where

$$\gamma_T = \begin{cases} \left(\frac{2\pi H_{m0,1}}{g T_p^2}\right)^{0.857} & \text{if } T_p \leq T_f, \\ (1 + 6 \epsilon_{lu}) \left(\frac{2\pi H_{m0}}{g T_f^2}\right)^{0.857} & \text{if } T_p > T_f. \end{cases}$$

Finally the normalization parameters α_i ($i = 1, 2$) are found by numerical integration so that

$$\int_0^\infty S_J^+(\omega; H_{m0,i}, \omega_{p,i}, \gamma_i, N_i, M_i, \alpha_i) d\omega = H_{m0,i}^2/16.$$

Preliminary comparisons with spectra from other areas indicate that the empirical parameters in the Torsethaugen spectrum can be dependent on geographical location. This spectrum is implemented as a matlab function `torsethaugen.m` in the WAFO toolbox.

B.3 Ochi-Hubble spectrum

Ochi and Hubble [59], suggested to describe bimodal spectra by a superposition of two modified Bretschneider (Pierson-Moskovitz) spectra:

$$S^+(\omega) = \frac{1}{4} \sum_{i=1}^2 \frac{((\lambda_i + 1/4) \omega_{p,i}^4)^{\lambda_i}}{\Gamma(\lambda_i)} \frac{H_{m0,i}^2}{\omega^{4\lambda_i + 1}} \exp\left(-\frac{(\lambda_i + 1/4) \omega_{p,i}^4}{\omega^4}\right),$$

where $H_{m0,i}$, $\omega_{p,i}$, and λ_i for $i = 1, 2$, are significant wave height, angular peak frequency, and spectral shape parameter for the low and high frequency components, respectively.

The values of these parameters are determined from an analysis of data obtained in the North Atlantic. The source of the data is the same as that for the development of the Pierson-Moskowitz spectrum, but analysis is carried out on over 800 spectra including those in partially developed seas and those having a bimodal shape. In contrast to the JONSWAP and Torsethaugen spectra, which are parameterized as function of H_{m0} and T_p , Ochi and Hubble, [59] gave, from a statistical analysis of the data, a family of wave spectra consisting of 11 members generated for a desired sea severity (H_{m0}) with the coefficient of 0.95.

The values of the six parameters as functions of H_{m0} are given as:

$$\begin{aligned} H_{m0,1} &= R_{p,1} H_{m0}, \\ H_{m0,2} &= \sqrt{1 - R_{p,1}^2} H_{m0}, \\ \omega_{p,i} &= a_i \exp(-b_i H_{m0}), \\ \lambda_i &= c_i \exp(-d_i H_{m0}), \end{aligned}$$

where $d_1 = 0$ and the remaining empirical constants a_i , b_i ($i = 1, 2$), and d_2 , are given in Table B.1. (See also the function `ochihubble.m` in the WAFO toolbox.)

Member no. 1 given in Table B.1 defines the most probable spectrum, while member no. 2 to 11 define the 0.95 percent confidence spectra.

A significant advantage of using a family of spectra for design of marine systems is that one of the family members yields the largest response such as motions or wave induced forces for a specified sea severity, while another yields the smallest response with confidence coefficient of 0.95.

Rodrigues and Soares [67], used the Ochi-Hubble spectrum with 9 different parameterizations representing 3 types of sea state categories: swell dominated (a), wind sea dominated (b) and mixed wind sea and swell system with comparable energy (c). Each category is represented by 3 different inter-modal distances between the swell and the

Member no.	$R_{p,1}$	a_1	a_2	b_1	b_2	c_1	c_2	d_2
1	0.84	0.70	1.15	0.046	0.039	3.00	1.54	0.062
2	0.84	0.93	1.50	0.056	0.046	3.00	2.77	0.112
3	0.84	0.41	0.88	0.016	0.026	2.55	1.82	0.089
4	0.84	0.74	1.30	0.052	0.039	2.65	3.90	0.085
5	0.84	0.62	1.03	0.039	0.030	2.60	0.53	0.069
6	0.95	0.70	1.50	0.046	0.046	1.35	2.48	0.102
7	0.65	0.61	0.94	0.039	0.036	4.95	2.48	0.102
8	0.90	0.81	1.60	0.052	0.033	1.80	2.95	0.105
9	0.77	0.54	0.61	0.039	0.000	4.50	1.95	0.082
10	0.73	0.70	0.99	0.046	0.039	6.40	1.78	0.069
11	0.92	0.70	1.37	0.046	0.039	0.70	1.78	0.069

Table B.1: Empirical parameter values for the Ochi-Hubble spectral model.

wind sea spectral components. These three subgroups are denoted by I, II and III, respectively. The exact values for the six parameters are given in Table B.2. (See the function `ohspec3.m` in the WAFO toolbox.)

Sea state type	Sea state group	$H_{m0,1}$	$H_{m0,2}$	$\omega_{p,1}$	$\omega_{p,2}$	λ_1	λ_2
a	I	5.5	3.5	0.440	0.691	3.0	6.5
	II	6.5	2.0	0.440	0.942	3.5	4.0
	III	5.5	3.5	0.283	0.974	3.0	6.0
b	I	2.0	6.5	0.440	0.691	3.0	6.5
	II	2.0	6.5	0.440	0.942	4.0	3.5
	III	2.0	6.5	0.283	0.974	2.0	7.0
c	I	4.1	5.0	0.440	0.691	2.1	2.5
	II	4.1	5.0	0.440	0.942	2.1	2.5
	III	4.1	5.0	0.283	0.974	2.1	2.5

Table B.2: Target spectra parameters for mixed sea states.

APPENDIX C

Wave models

Generally the wind generated sea waves is a non-linear random process. Non-linearities are important in the wave-zone, i.e., from the crest to 1-2 wave amplitudes below the trough. Below this zone linear theory is acceptable. However, there are unsolved physical problems associated with the modelling of breaking waves. In practice, linear theory is used to simulate irregular sea and to obtain statistical estimates. Often a transformation of the linear model is used to emulate the non-linear behavior of the sea surface, but as faster computers are becoming available also higher order approximations will become common in ocean engineering practice. In the following sections we will outline these wave models. Only long-crested sea is used here either recorded at a fixed spatial location or at a fixed point in time.

C.1 The linear Gaussian wave model

Gaussian random surface can be obtained as a first order approximation of the solutions to differential equations based on linear hydrodynamic theory of gravity waves. The first order component is given by the following Fourier series

$$\eta_l(x, t) = \sum_{n=-N}^N \frac{A_n}{2} e^{i\psi_n} \quad (\text{C.1})$$

where the phase functions are

$$\psi_n = \omega_n t - k_n x \quad (\text{C.2})$$

If η_l is assumed to be stationary and Gaussian then the complex amplitudes A_j are also Gaussian distributed. The mean square amplitudes are related to the one-sided wave spectrum $S_{\eta\eta}^+(\omega)$ by

$$E[|A_n|^2] = 2 S_{\eta\eta}^+ (|\omega_n|) \Delta\omega \quad (\text{C.3})$$

The individual frequencies, ω_n and wavenumbers, k_n are related through the linear dispersion relation

$$\omega^2 = g k \tanh(k d) \quad (\text{C.4})$$

where g and d are the acceleration of gravity and water depth, respectively. For deep water Eq. (C.4) simplifies to

$$\omega^2 = gk \quad (\text{C.5})$$

It implies the following relation between the wave frequency spectrum and the wave number spectrum

$$S_{\eta\eta}^+(\omega) = \frac{2\omega}{g} S_{\eta\eta}^+(k) \quad (\text{C.6})$$

Without loss of generality it is assumed that η_l has zero expectation. It is also assumed that η is ergodic, i.e., any ensemble average may be replaced by the corresponding time-space average. This means that one single realization of η is representative of the random field. Here it is also assumed $\omega_{-j} = -\omega_j$, $k_{-j} = -k_j$ and $A_{-j} = \bar{A}_j$ where \bar{A}_j is the complex conjugate of A_j . The matlab program `spec2sdat.m` in WAFO use the Fast Fourier Transform (FFT) to evaluate Eq. (C.1).

C.2 The Second order non-linear wave model

Real wave data seldom follow the linear Gaussian model perfectly. The model can be corrected by including quadratic terms. Following [36] the quadratic correction η_q is given by

$$\eta_q(x, t) = \sum_{n=-N}^N \sum_{m=-N}^N \frac{A_n A_m}{4} E(\omega_n, \omega_m) e^{i(\psi_n + \psi_m)} \quad (\text{C.7})$$

where the quadratic transferfunction (QTF), $E(\omega_n, \omega_m)$ is given by

$$E(\omega_i, \omega_j) = \frac{\frac{gk_i k_j}{\omega_i \omega_j} - \frac{1}{2g}(\omega_i^2 + \omega_j^2 + \omega_i \omega_j) + \frac{g}{2} \frac{\omega_i k_j^2 + \omega_j k_i^2}{\omega_i \omega_j (\omega_i + \omega_j)}}{1 - g \frac{k_i + k_j}{(\omega_i + \omega_j)^2} \tanh((k_i + k_j)d)} - \frac{gk_i k_j}{2\omega_i \omega_j} + \frac{1}{2g}(\omega_i^2 + \omega_j^2 + \omega_i \omega_j) \quad (\text{C.8})$$

For deep water waves the QTF simplifies to

$$E(\omega_i, \omega_j) = \frac{1}{2g}(\omega_i^2 + \omega_j^2), \quad E(\omega_i, -\omega_j) = -\frac{1}{2g}|\omega_i^2 - \omega_j^2| \quad (\text{C.9})$$

where ω_i and ω_j are positive and satisfies the same relation as in the linear model.

However, if the spectrum does not decay rapidly enough towards zero, the contribution from the 2nd order wave components at the upper tail can be very large and unphysical. The predicted non-linearities are sensitive to how the input spectrum is treated (cut-off) as shown by [83].

One method to ensure convergence of the perturbation series is to truncate the upper tail of the spectrum at ω_{max} in the calculation of the 1st and 2nd order wave components. The [56] program *WAVSIM* set $\omega_{max} = \sqrt{2.0g/(0.95H_{m0})}$. [13] showed that this will have the side effect of giving the medium to low wave-heights a too low steepness (which may not be too serious in real application). However, using the truncation method the spectrum for the simulated series will deviate from the target spectrum in 2 ways: (1) no energy or wave components exist above the upper frequency limit ω_{max} , (2) the energy in the spectrum below ω_{max} will be higher than the target spectrum. In order to retain energy above ω_{max} in the spectrum, one may only truncate the upper tail of the spectrum for the calculation of the 2nd order components. However, in a real application one usually wants

the simulated data to have a prescribed target spectrum. Thus a more correct approach is to eliminate the second order effects from the spectrum before using it in the non-linear simulation. One way to do this is to extract the linear components from the spectrum by a fix-point iteration on the spectral density using the non-linear simulation program so that the simulated data will have approximately the prescribed target spectrum. This method is implemented as matlab function `spec2linsec.m` available in the WAFO toolbox. To accomplish convergence, the same seed is used in each call of the non-linear simulation program.

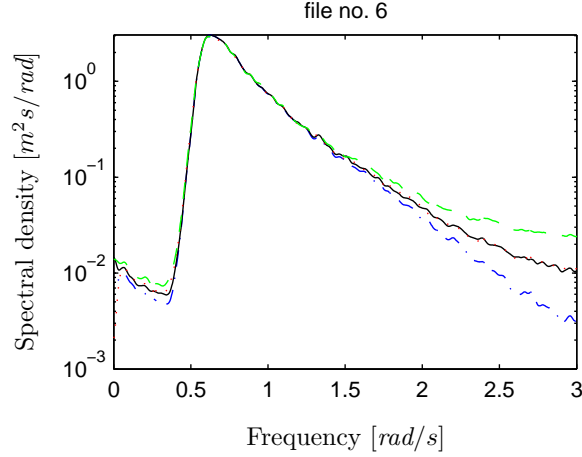


Figure C.1: Target spectrum, $S_T(\omega)$, (solid) and its linear component, $S_L(\omega)$ (dash-dot) compared with S_T^{NLS} (dash) and S_L^{NLS} (dot), i.e., spectra of non-linearly simulated data using input spectrum $S_T(\omega)$ (method 1) and $S_L(\omega)$ (method 2), respectively.

Fig.C.1 demonstrates the differences in the spectra obtained from data simulated using these methods. The solid line is the target spectrum, $S_T(\omega)$, and the dash-dotted line is its linear component, $S_L(\omega)$, obtained using method 2. The spectra S_T^{NLS} (dashed) and S_L^{NLS} (dotted) are estimated from non-linearly simulated data using the $S_T(\omega)$ and $S_L(\omega)$ spectra, respectively. As expected S_T^{NLS} is higher than S_T , while S_L^{NLS} is indistinguishable from S_T . It is also worth noting that the difference between the spectra is small, but have some impact on the higher order moments. For instance, the ϵ_2 and ϵ_4 parameters calculated from S_T^{NLS} increase with 6.1% and 2.5%, respectively. The corresponding values calculated from S_L^{NLS} increase with only 0.5% and 0.2%, respectively.

The small difference between $S_T(\omega)$ and $S_L(\omega)$ also lends some support to the view noted earlier, that the difference frequency effect can not fully explain the high values of the spectrum in the lower frequency part as found by [97].

The effects these methods have are discussed further in [15] and especially on wave steepness parameters. The second order non-linear model explained here is implemented in WAFO as `spec2nlsdat.m`. This is a very efficient implementation that calculate Eqs. (C.7) to (C.9) in the bi-frequency domain using a one-dimensional *FFT*. This is similar to the *WAVSIM* program of [56], but is made even more efficient by summing over non-zero spectral values only and by eliminating the need for saving the computed results to the hard drive. *WAVSIM* use 40 s to evaluate a transform with 32000 time steps/frequencies compared with 2 s for `spec2nlsdat.m` on a Pentium M 1700 MHz with 1 GB of RAM. Thus

the use of second order random waves should now become common in ocean engineering practice.

`spec2nlsdat.m` also allows finite water depth and any spectrum as input, in contrast to *WAVSIM*, which only uses infinite water depth and the JONSWAP spectrum.

C.3 Transformed linear Gaussian model

An alternative and faster method than including the quadratic terms to the linear model, is to use a transformation. The non-Gaussian process, $\eta(x, t)$, is then a function of a single Gaussian process, $\eta_l(x, t)$

$$\eta(x, t) = G(\eta_l(x, t)) \quad (\text{C.10})$$

where $G(\cdot)$ is a continuously differentiable function with positive derivative.

There are several ways to proceed when selecting the transformation. The simplest alternative is to estimate $G(\cdot)$ by some parametric or non-parametric means (see e.g. [94, 57, 73]).

The parametric formulas proposed by [57] as well as [94] use the moments of $\eta_l(x, t)$ to compute $G(\cdot)$. Information about the moments can be obtained directly from data or by using theoretical models. [52] derived an expression for the skewness and kurtosis of narrow banded Stokes waves to the leading order and used these to define the transformation. [95] fitted a parametric model to skewness and kurtosis of a second order model with a JONSWAP spectrum.

[50] studied the performance of 6 transformation methods including those mentioned above and concluded that the Hermite method in general produces very good results.

C.3.1 Hermite model

The Hermite transformation model proposed by [93] approximates the true process by the following transformation of a standard normal process $Y(t)$:

$$G(y) = \mu + K \sigma [y + c_3(y^2 - 1) + c_4(y^3 - 3y)] \quad (\text{C.11})$$

$$K = 1/\sqrt{1 + 2c_3^2 + 6c_4^2} \quad (\text{C.12})$$

where μ and σ are the mean and standard deviation, respectively, of the true process. The unitless coefficients c_3 and c_4 are chosen so that the transformed model match the skewness, ρ_3 , and excess, ρ_4 , of the true process. [96] improved the parameterizations by minimizing lack-of-fit errors on ρ_3 and ρ_4 , giving

$$c_3 = \frac{\rho_3}{6} \frac{1 - 0.015|\rho_3| + 0.3\rho_3^2}{1 + 0.2\rho_4} \quad (\text{C.13})$$

$$c_4 = 0.1 \left((1 + 1.25\rho_4)^{1/3} - 1 \right) c_{41} \quad (\text{C.14})$$

$$c_{41} = \left(1 - \frac{1.43\rho_3^2}{\rho_4} \right)^{1-0.1(\rho_4+3)^{0.8}} \quad (\text{C.15})$$

These results apply for $0 \leq 3/2\rho_3^2 < \rho_4 < 12$, which include most cases of practical interest. One may then estimate c_3 and c_4 using the sample skewness, $\hat{\rho}_3$, but restrict ρ_4 so that $\rho_4 = \min(\max(3\hat{\rho}_3^2/2, \hat{\rho}_4), \min(4(4\hat{\rho}_3/3)^2, 12))$. $\hat{\rho}_4$ is the sample excess and $(4\hat{\rho}_3/3)^2$ is the leading excess contribution for narrow banded Stokes waves as found by [52].

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