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Highly Thermally Conductive Polymer Composite Originated from Assembly of Boron Nitride at Oil Water Interface

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Highly Thermally Conductive Polymer Composite Originated from Assembly of Boron Nitride at Oil Water Interface

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Keywords: Oil-water interface; Boron nitride; Thermal conductivity; Thermally
conductive polymer; Polystyrene

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4 ABSTRACT Thermally conductive polymer packaging material is of great
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6 significance for the thermal management of electronics. Inorganic thermally
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8 conductive fillers have been demonstrated as a convenient approach to achieve this
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10 goal, however, sacrificing the lightweight and processability of the polymer. To
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12 address this problem, effective 3D boron nitride (BN) network was constructed as
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14 heat conduction pathway in polystyrene (PS) matrix based on oil-water interface
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16 assembly in this work. Styrene oil droplets were stabilized by BN sheets in water
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18 phase to form Pickering emulsions, and then the *in-situ* polymerization was triggered to
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20 synthesize PS microspheres with ultrathin BN layer covered surface (PS@BN
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22 microspheres). Composite substrates were fabricated through hot-compressing the
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24 PS@BN microspheres to form BN networks based on the original microsphere
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26 template. Benefited from the network structure, the maximum thermal conductivity of
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28 composite substrate reached 0.94 W/mK at 33.3 wt% BN, which is 626% folds of that
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30 of pure polystyrene. It was also demonstrated that the storage modulus and thermal
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32 stability of the composite substrate were dramatically improved by the BN network.
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34 The reported composite substrate and its fabrication strategy are promising in the
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36 development of thermal management of electronics.
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1. Introduction

With the fast development of the electronics industry, power density of the electronics increases rapidly, resulting in severe heat accumulation problems. Insufficient heat dissipation performance of electronic packaging materials seriously threatens the working stability and lifespan of electronic products.¹⁻⁶ Polymers currently hold an absolutely dominant share in electronic packaging materials due to their electrical insulation, low cost, facile processability, and lightweight. However, the inherent thermal conductivity of polymer materials is rather low, only about 0.1-0.3 W/mK, which is difficult to meet the heat dissipation requirements of electronic packaging materials.⁷⁻¹² Therefore, development of polymer material with high thermal conductivity is on urgent demand.

Introduction of thermally conductive fillers such as boron nitride (BN), aluminum oxide, carbon, is a promising method to improve the thermal conductivity of polymer matrix.¹³ However, it is still a huge challenge to optimize the distribution of thermally conductive fillers in the polymer matrix to form an effective heat conduction pathway.^{3, 11, 14, 15} Three-dimensional (3D) networks of thermally conductive fillers have been proven as an efficient structure for thermal conductivity enhancement of polymer matrix. Various methods for construction of 3D thermally conductive networks have been developed based on the assembly of the fillers. The techniques for filler assembly could be roughly classified as following: (1) **Chemical modification enabled assembly**.^{3, 16, 17} Strong interaction between the filler and polymer is introduced through chemical modification, guiding the assembly of the

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4 filler to form thermally conductive networks. For example, Gu et al. reported that the
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6 NH₂-POSS functionalization of BN fillers increased the thermal conductivity
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8 coefficient of BN/polyimide composites from 0.69 W/mK to 0.71 W/mK at 30 wt%
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10 BN content.¹⁸ Jiang et al. reported thermally conductive BN network construction
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12 based on hydrogen bond between hydroxy modified BN particles and polyvinyl
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14 alcohol.³ (2) **External field assisted assembly.**¹⁹⁻²¹ Magnetic field regulated
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16 self-assembly of the magnetic filler is an efficient method to form network. Our group
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18 previously reported that the orientations of iron oxide modified magnetically
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20 responsive BN could be controlled by external magnetic field in polymer matrix,
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22 obtaining a 3D interconnected network of BN platelets and carbon nanotubes.¹³ (3)
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24 **Phase separation induced self-assembly.** Phase separation such as icing²² or other
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26 crystallization²³ caused nucleation from homogeneous solution, which provided
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28 template for the assembly of the fillers. Hu et al. reported 3D-BN network from
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30 ice-templating self-assembly of BN, epoxy composites was then fabricated as thermal
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32 interfacial materials by infiltration technology.²² (4) **Microsphere template assisted**
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34 **assembly.**^{8, 24-28} Thermally conductive fillers and microspheres are physically mixed
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36 at the beginning, further processing such as hot-compression will be applied to
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38 convert the microspheres into polymer matrix, forming polymer matrix with thermally
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40 conductive filler network. Wang et al.⁸ reported that BN nanosheets and PS
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42 microspheres formed composite microspheres *via* strong electrostatic interactions for
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44 the thermal interface material fabrication based on latex blending and subsequent
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46 compression molding. Our group demonstrated that porous silicon carbide nanowires
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4 (SiCw) skeleton could be formed based on polystyrene microspheres templates and
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6 epoxy-based composites with structurally segregated SiCw manufactured after
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8 sintering and infiltrating.²⁵
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11 Water-oil interface is a desired platform for the self-assembly of colloidal/nano
12 particles. For example, Pickering emulsions are kinetically stabilized by solid
13 particles instead of surfactant.^{29, 30} Pickering emulsions, stabilized by 2D materials
14 such as graphene oxide, BN nanosheets,³¹ have been widely reported and Pickering
15 emulsion could be employed as soft templates for the preparation of functional hybrid
16 materials.^{30, 32-35} Among other 2D materials, BN shows excellent thermal
17 conductivity, good electrical insulation and low dielectric constant,³⁶⁻³⁸ which was
18 highly desirable for the electronic packaging materials.
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32 In this work, self-assembly of BN at water/styrene interface was employed to
33 prepare BN-coated PS (PS@BN) microspheres by *in-situ* emulsion polymerization.
34 PS@BN microspheres were hot-compressed into composite substrates and thermal
35 conductivity and mechanical properties of which were investigated. To the best of
36 our knowledge, this work is the first time to propose emulsion templet method in
37 the field of thermally conductive filler network construction. Compared to the
38 reported methods in the literatures, assembly of BN on emulsion templet offers an
39 ultrathin layer of close packed BN network in polymer matrix, enabling highly
40 thermally conductive composite PS substrate. The proposed preparation method
41 also avoids any surfactants or chemical modification, which is a facile and green
42 route for the fabrication of functional materials. The explored relation between
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the BN distribution in matrix and thermal/mechanical properties of composite substrate will shed new light on the design of electronic packaging polymers.

2. Materials and experiment

2.1 Materials

BN particles (Chemical Abstracts Service Registry Number (CAS No.) : 10043-11-5, purity : 98.5%, average diameters : 1 μm) were provided by Shanghai Macklin Biochemical Co., Ltd. BN particles (CAS No. : 10043-11-5; purity: 98%, average diameters : 3 μm and 5 μm) were provided by Dandong Rijin Science and Technology Co., Ltd. Sodium hydroxide (CAS No.:1310-73-2, purity: $\geq 96.0\%$) was purchased from Sinopharm Chemical Reagent Co., Ltd. Styrene (CAS No.:100-42-5, Analytical Reagent (AR), supplied by Shanghai Aladdin biochemical Co., Ltd) was washed by 5 wt% of sodium hydroxide solution before use. Benzoyl peroxide (CAS No.: 94-36-0, AR) was purchased from Shanghai Aladdin biochemical Co., Ltd. Deionized water was purified by the Milli-Q water purification system.

Table 1. The recipe of the Pickering emulsion for the preparation of PS@BN microspheres

Sample name	Weight of BN (g)	BN ratio in the Feed (wt%)
PS@BN -9.09%	2.0	9.09
PS@BN -14.9%	3.5	14.9
PS@BN -25.9%	7.0	25.9
PS@BN -33.3%	10.0	33.3

2.2 Preparation of Pickering emulsion

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4 0.20 g of benzoyl peroxide was dissolved in 20.0 mL of styrene to form an oil
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6 phase. The specified amount of the BN powder in the Table 1 was dispersed in 200.0
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8 mL deionized water. The mixture of BN and water was sonicated for 30 min to obtain
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10 uniform water dispersion. The water dispersion and oil phase were mixed and
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12 emulsified with the aid of emulsification machine (FLUKO, Germany) for 2 min at
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14 the rotating speed of 10000 rpm. Then a stable Pickering emulsion was obtained.
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19 **2.3 Preparation of PS@BN microspheres**

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22 The as-formed Pickering emulsion was transferred into a 500 mL three-neck round
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24 bottom flask. Nitrogen was introduced to the flask to replace the air for 30 min, then
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26 the flask was placed into a 70 °C water bath to trigger the *in-situ* polymerization. The
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28 polymerization lasted for 10 hours without any stirring. The products were collected
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30 by centrifugation at 9000 rpm and the precipitate was washed by ethanol for 4~5
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32 times to remove the excessive styrene monomer. The products were dried in vacuum
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34 oven at 40 °C for 24 hours. The obtained composites were named as PS@BN
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36 microspheres.
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43 **2.4 Preparation of composite substrate**

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45 The composite substrates were prepared with the aid of Hot-compressing Machine
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47 (WuHan QiEn Science and Technology Development Co., Ltd, China). 3.0 g PS@BN
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49 microspheres were placed in a mould (25 mm×25 mm×2 mm). The mould was
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51 preheated to the investigated temperature (80 °C or 95 °C) and the sample inside was
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53 compressed at certain pressure (10 MPa or 25 MPa) for 15 min. The composite was
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55 formed after another pressing for 5 min when the whole system was cooled to 25 °C.
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2.5 Characterization

Pickering emulsions were observed with an optical microscope (Olympus BX53, Japan). The morphology of PS@BN and cross-section of composites substrate were examined by scanning electron microscopy (SEM, Sirion-200 FEI, America). The element distribution of the samples was investigated by the energy dispersive spectroscopy (EDS) detector equipped in SEM. The size distribution of PS@BN microspheres was obtained from statistics based on counting over 200 samples with the aid of the software Nanomeasurer. The XRD (X-ray diffraction) analyses of BN and PS@BN were carried out with a Philips X' Pert Pro MPD X-ray diffractometer with Cu K α radiation ($\lambda = 0.154$ nm, 40 kV, 40 mA). The thermal stabilities of the composites were studied by Thermogravimetric Analysis (TGA, Perkin-Elmer, USA, Pyris1) from 20 to 900 °C at a heating rate of 10 °C/min in air atmosphere. The thermal conductivity of composite substrate was measured by Hot Disk instrument (TPS 2200, AB Corporation, Sweden) in isotropic mode. The storage modulus and loss factor ($\tan\delta$) of composite substrate were performed on a dynamic mechanical analyzer (Diamond DMA, Perkin-Elmer, USA). The samples were tested from room temperature to 150 °C with a heating rate of 2 °C/min and a testing frequency of 1 Hz. The composite substrate was heated from 25 °C to 70 °C placed on a homemade programmable point heating device and a Handheld infrared camera (CEM DT-980, Huashengchang, China) was applied to visualize the temperature distribution evolution of the substrate during this process. 5 μ L deionized water or styrene was added on a BN tablet (diameter: 12.5 mm, thickness: 1.5 mm) made from

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4 compressing the BN powder, and the contact angle of the droplet was measured by
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6 Data Physics optical Contact Angle (CA-100&D, Shanghai Innuo Precision
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8 Instruments Co., Ltd, China). The stability of emulsion was assessed by emulsion
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10 stability index (ESI). The ESI was measured by the height of the separated oil phase
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12 relative to the height of the remaining emulsion, which was calculated as the
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14 percentage ratio of the emulsion height to the sum of the emulsion height plus the
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16 height of separated oil phase³⁹. The X-ray photoelectron spectra (XPS) was performed
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18 on ESCALAB 250 (Thermo-VG Scientific) for analyzing the elemental compositions
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25 at the surface of samples.

26 **3. Results and discussion**

27 **3.1 Formation of Pickering Emulsion**

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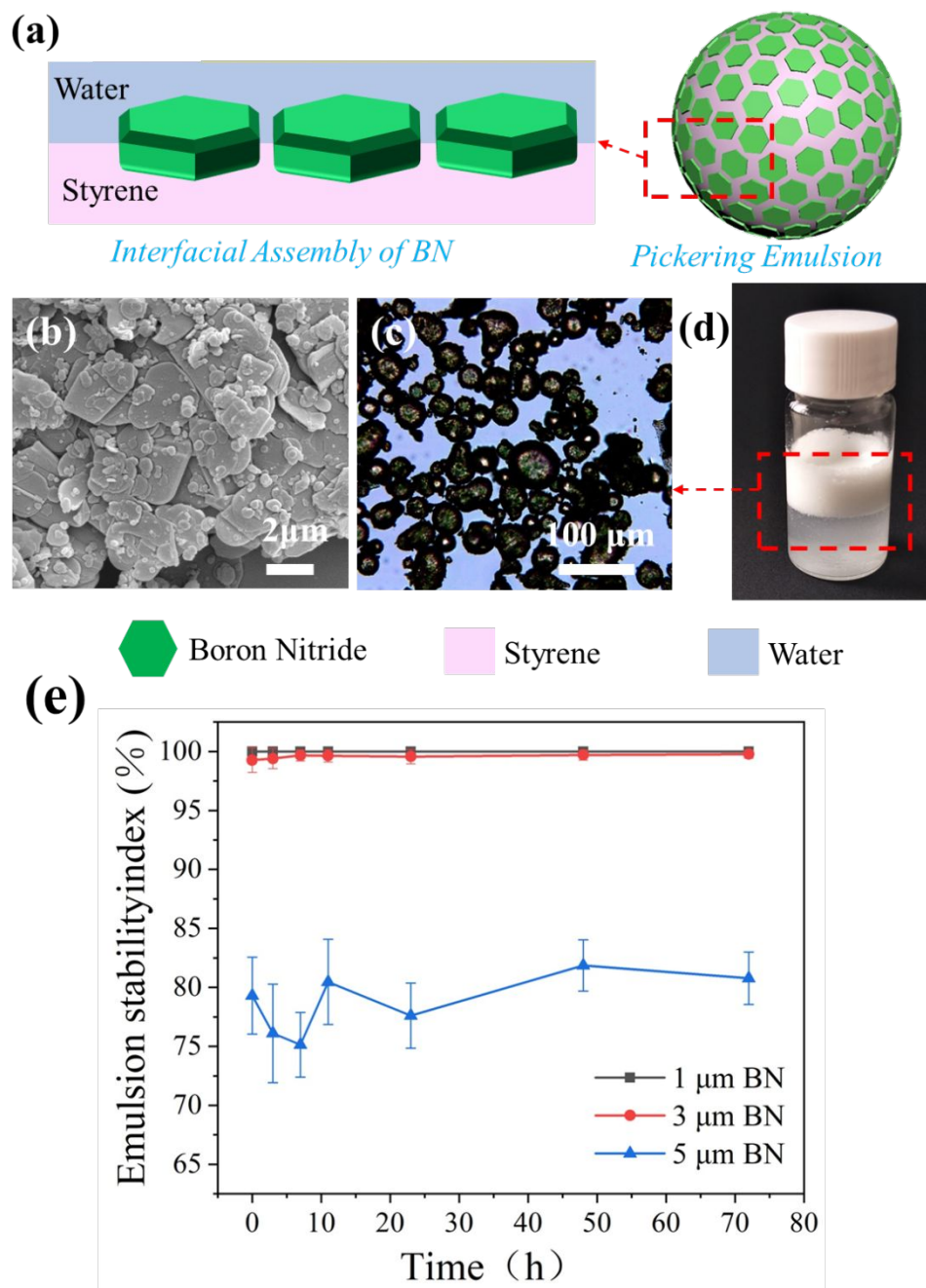


Fig. 1 (a) Schematic of Pickering emulsion, (b) SEM image of BN particles with mean size of 3 μm (c) the optical microscopy image of Pickering emulsions; (d) photograph of typical Pickering emulsion stabilized by BN ; and (e) Emulsion stability index (ESI) as a function of time for Pickering emulsion stabilized by BN particles.

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4 The process of Pickering emulsion formation is schematically described in Fig. 1a.
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6 The oil and water phases were sufficiently emulsified at the 10000 rpm. Due to the
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8 massive shear force from the emulsification, a large area of bare oil-water interfaces
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10 was created. These bare oil-water interfaces were energetically unfavorable, tending
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12 to adsorb BN particles (Fig. 1b and Fig. S2 in the supporting information) for the free
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14 energy minimization of the system. As a result, the as formed emulsions were
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16 stabilized by BN particles in the form of that a layer of the BN particles were
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18 adsorbed at the oil-water interface. The emulsion droplets ranging from several
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20 micrometers to several tens of micrometers were observed from the optical
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22 microscope image (Fig. 1c). The dark edge of the emulsion droplets confirmed that
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24 the emulsion was stabilized by the opaque BN sheets. The density of the oil phase
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26 (styrene) is 0.906 g/mL at 20 °C, which is lower than that of water, thus the obtained
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28 milky oil-in-water emulsion floated above the transparent water phase (Fig. 1d) after a
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30 short period of standing. Emulsion stabilized by 1 μm and 3 μm BN showed excellent
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32 stability based on the ESI in Fig. 1e, indicating that the emulsion is stable during the
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34 10 hour polymerization. In contrast, the emulsion stabilized by 5 μm BN exhibited a
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36 low ESI with large fluctuation. The photographs of emulsion evolution were shown in
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38 Fig. S1 in Supporting Information, where obvious oil phase separation could be found
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40 in emulsion stabilized by 5 μm BN.
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52 **3.2 Preparation of PS@BN composite microspheres**

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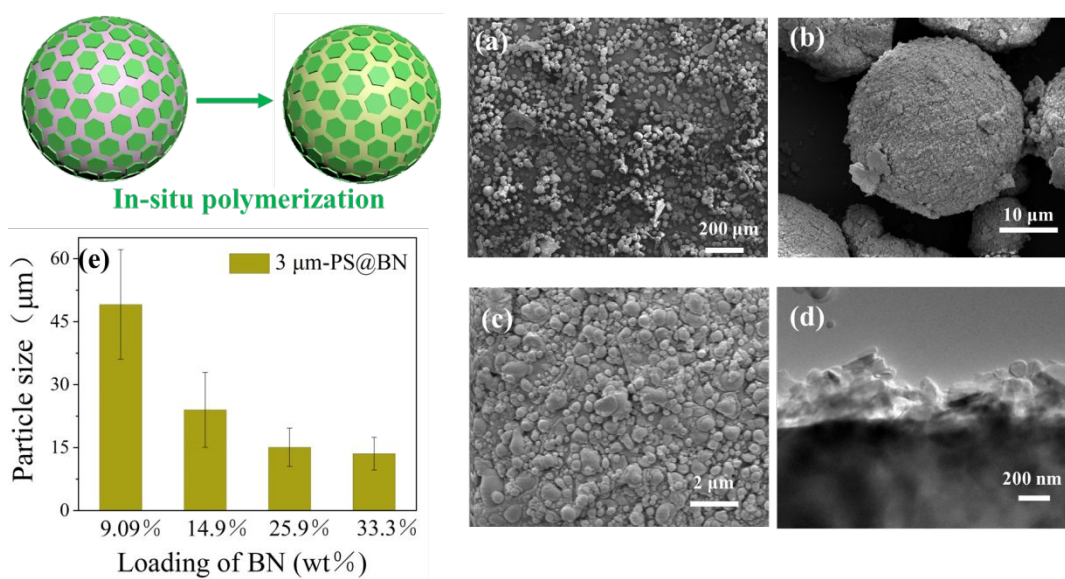


Fig. 2 The cartoon illustrates the formation of PS@BN microspheres from *in-situ* polymerization of Pickering emulsion. (a) SEM image of PS@BN microspheres stabilized by 3 μm BN sheets. SEM images of a typical PS@BN microsphere with (b) low and (c) high magnifications; (d) TEM image, (e) particle size distribution

PS@BN composite microspheres were fabricated by the *in-situ* polymerization of styrene monomer in the emulsion. The solubility of the initiator determined polymerization position. The water-soluble initiator ammonium persulfate (APS) could start the polymerization of the diffused styrene in water phase, leading to PS microspheres without any BN coating (Fig S3 in Supporting Information). The oil-soluble benzoyl peroxide (BPO) was employed in this study to achieve an emulsion template polymerization. BPO was dissolved in the monomer in the separated phases in the emulsion. The polymerization took place inside the emulsion droplets, which were stabilized by the BN sheets, ensuring that the surface of the formed PS microspheres was covered by BN sheets. The obtained microspheres

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4 exhibited a uniform size distribution with an average diameter around several tens of
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6 microns (Fig. 2a and 2b), that was consistent with the mean diameter of emulsion
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8 droplets observed by optical microscopy. Compared with smooth surface of pure
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10 polystyrene microspheres (Fig. S4), PS@BN microspheres exhibited a rough surface
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12 due to the coexistence of BN sheets and PS structure (Fig. 2c). The thickness of the
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14 BN layer was less than 1 micrometer according to the TEM image (Fig. 2d). This is
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16 because that only the BN adsorbed at the oil-water interface could be anchored at the
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18 surface of PS microspheres. This ultrathin BN layer raised the possibility for
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20 achieving high thermal conductivity in relatively low BN loading, which will be
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22 discussed in the following sections. The size of the PS@BN microspheres decreased
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24 with the BN content in the feed during the polymerization (Fig. 2e). It was attributed
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26 that the increasing amount of BN sheet provided more stabilized interfaces during the
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28 emulsification. For the identical amount of oil phase, more interface area of the
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30 emulsion droplets led to smaller droplets size. It suggested that BN content could be
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32 used to control the size of the PS@BN microspheres.
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42 **3.3 Mechanism of the PS@BN microspheres formation**

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45 The formation of PS@BN microspheres relied on the BN assembly on the oil-water
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47 interface. The stability of the colloidal particles was mainly determined by the
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49 hydrophobicity and size.⁴⁰ The powder of BN sheets was compressed into tablet to
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51 investigate its wettability. Fig 3a illustrates the configuration of contact angle
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53 measurement. The tablets from BN with mean size of 1 μm , 3 μm and 5 μm BN
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55 showed a mean contact angle of $26.8 \pm 0.3^\circ$, $52.3 \pm 0.7^\circ$ and $67.6 \pm 0.5^\circ$ (Fig. 3c-3e),
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4 respectively, indicating good water wettability of BN.^{41, 42} The good water wettability
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6 of BN was attributed to the -OH at surface, which was confirmed by the
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8 high-resolution XPS spectra of 3 μm BN (Fig. 3l). The peak at 190.6 eV is assigned to
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10 B-N bond while the peak at 191.3 eV is assigned to the B-O bond (Fig. 3m).⁴³⁻⁴⁵ The
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12 -OH on the BN also could be observed from the FTIR spectrum (Fig. S4). All the
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14 contact angles of styrene droplets on the tablets made from different sized BN sheets
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16 were closed to 0° in Fig. 3f-3h, indicating a strong interaction between BN and
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18 styrene. It was attributed to that delocalized electrons from hexagonal BN and the
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20 aromatic structure of styrene formed a strong, noncovalent bond *via* π - π stacking (Fig
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22 3b) and van der Waals interactions.^{12, 46, 47} Since BN sheets could be wet by both
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24 water and styrene, they were able to firmly anchor at the interface. After the
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26 polymerization in the oil droplets, the interfacial BN sheets were bonded to the PS
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28 microsphere, as shown in Fig 2d.
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38 The desorption energy of BN from the interface increases with its size,
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40 indicating that the increasing BN size improved the stability of the emulsion
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42 (Fig.S1a-b). However, the gravitational force gradually played an important role,
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44 promoting the desorption of BN from the interfaces. Composite microspheres
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46 prepared from BN sheets with average size of 1 μm and 3 μm as stabilizer (Fig. 3i
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48 and 3j) showed spherical morphology with desired BN and PS distribution.
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51 Further increase of BN size led to BN attached anomalous particles mixed with
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53 irregularly shaped fragments (Fig. 3k). The phenomenon indicated that emulsion
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55 showed less stability when it was stabilized by BN nanosheets with average size
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larger than 5 μm (Fig.S1c.)

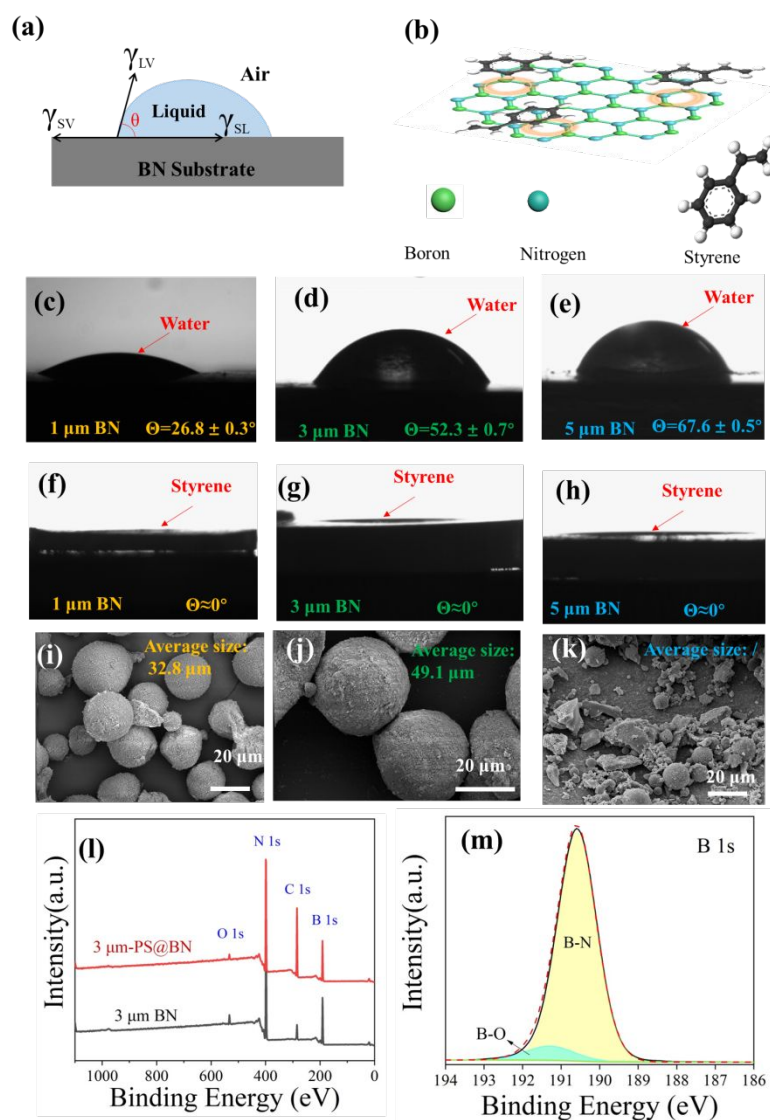


Fig.3 (a) Schematic configuration of contact angle measurements; (b) schematic illustration of interaction between BN and PS, the orange ring denotes the π - π stacking effects; (c-e) contact angles of water droplet on the tablets made of BN with various sizes; (f-h) contact angles of styrene droplet on the tablets made of BN with various sizes; SEM images of PS@BN microspheres obtained by BN sheets with mean size of (i) 1 μm , (j) 3 μm and (k) 5 μm . (l) XPS spectra of the 3 μm BN and 3 μm -PS@BN microspheres; (m) B 1s high-resolution spectrum of 3 μm BN. The content of BN in feed was 9.09 wt% for the preparation of all the above samples.

3.4 Preparation of composite substrate

The composite substrates were prepared by hot-compressing the PS@BN microspheres. The DSC (Fig. S5) curves suggested that the glass transition temperature of the PS@BN was between 90.5 - 93.3 °C. The fluidity of PS increased above the glass transition temperature and PS@BN microspheres would merge together to form the composite substrate under physical pressure. Pores between the microsphere units in the cross-section of composite substrate (Fig. 4c) were observed for the sample hot-compressed at 80 °C, 25 MPa, indicating incomplete contact between the BN and PS matrix. When the temperature of hot-press reached to 95 °C, PS microspheres merged into a complete polymer matrix while BN located at the interfaces of the original microspheres, forming a three-dimensional network (Fig. 4d). Fig. 4a-4b showed the Carbon (C) and Nitrogen (N) element distribution at the surface of PS@BN composite microspheres and cross-section of composite substrate. The C and N elements maps complementary with each other, indicating BN and PS were co-existed on the surface of the microspheres. After hot-compressing, ultra-thin network of Nitrogen element (Fig. 4b) was observed in the PS matrix. The X-ray diffraction peaks (Fig. 4f) of the composite substrate at approximate 26.7° and 41.3° were associated with the (002) and (100) planes of BN, respectively. The compression could cause the re-orientation of the BN in the polymer matrix, according to the literature, in which the value of $I(002)/I(100)$ could reach 1057.⁴⁸ The value of $I(002)/I(100)$ of our composite substrate increased from 3.2 to 18.9 when the BN content was increased from 9.09 to 33.3 wt%, much smaller than that of the literature,

indicating a negligible deformation during the compression, thus the integrity of BN network could be maintained.

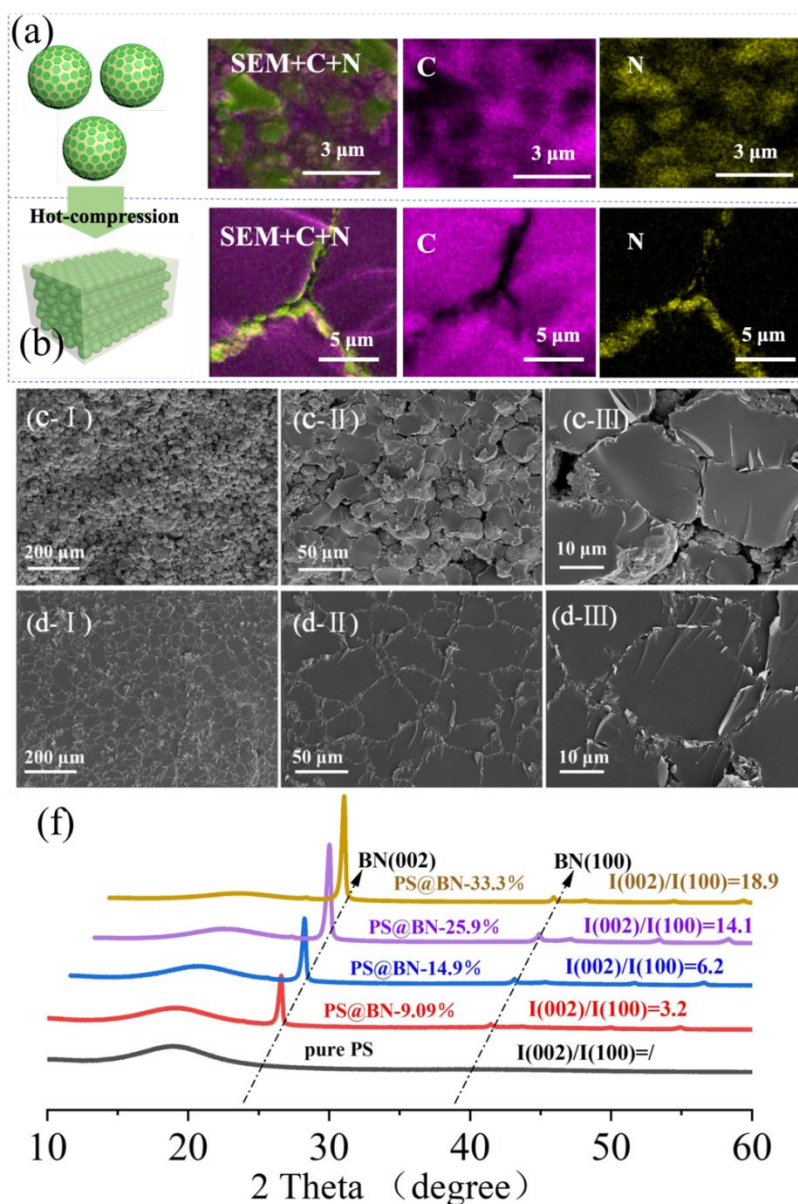


Fig. 4 EDS elemental mapping images of (a) the surface of PS@BN composite microspheres and (b) cross-section of composite substrate; cross-section SEM images of composite substrate under different conditions of hot-pressing: (c) 80°C, 25MPa; (d) 95°C, 25Mpa; I, II, III represent the SEM at different magnifications,

respectively; (f) XRD patterns of the composite substrates made from PS@BN microspheres with varies BN loadings.

3.5 Mechanical properties and thermal stability of the composite substrates

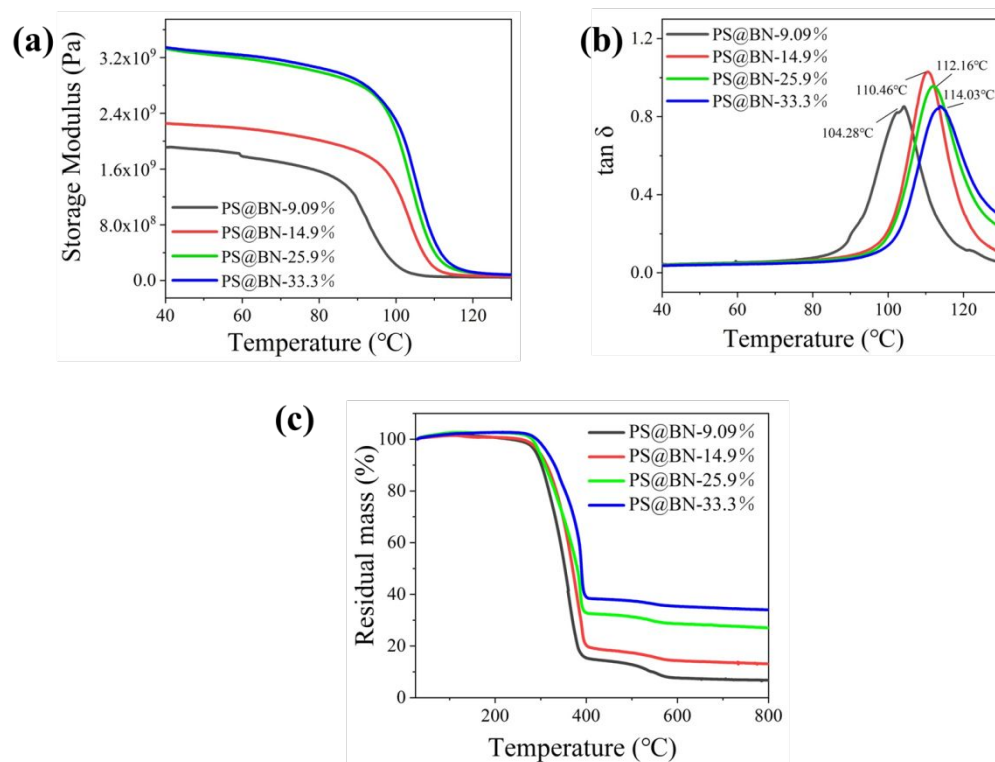


Fig. 5 Dynamic mechanical analysis (DMA) of the PS@BN composite substrates, (a) storage modulus and (b) loss tangent ($\tan \delta$) versus temperature of the composite substrates; (c) thermogravimetric analysis of PS@BN composite substrates with increased content of BN.

Distribution and volume fraction of inorganic filler in polymer matrix could affect the viscoelastic properties of polymeric materials dramatically.^{2, 49} As depicted in Fig. 5a, the composite substrate with larger content of BN exhibited a higher storage modulus at the low temperature region, indicating that the mechanical strength of the substrate could be enhanced by BN. The rigidity of the polymer matrix increased due

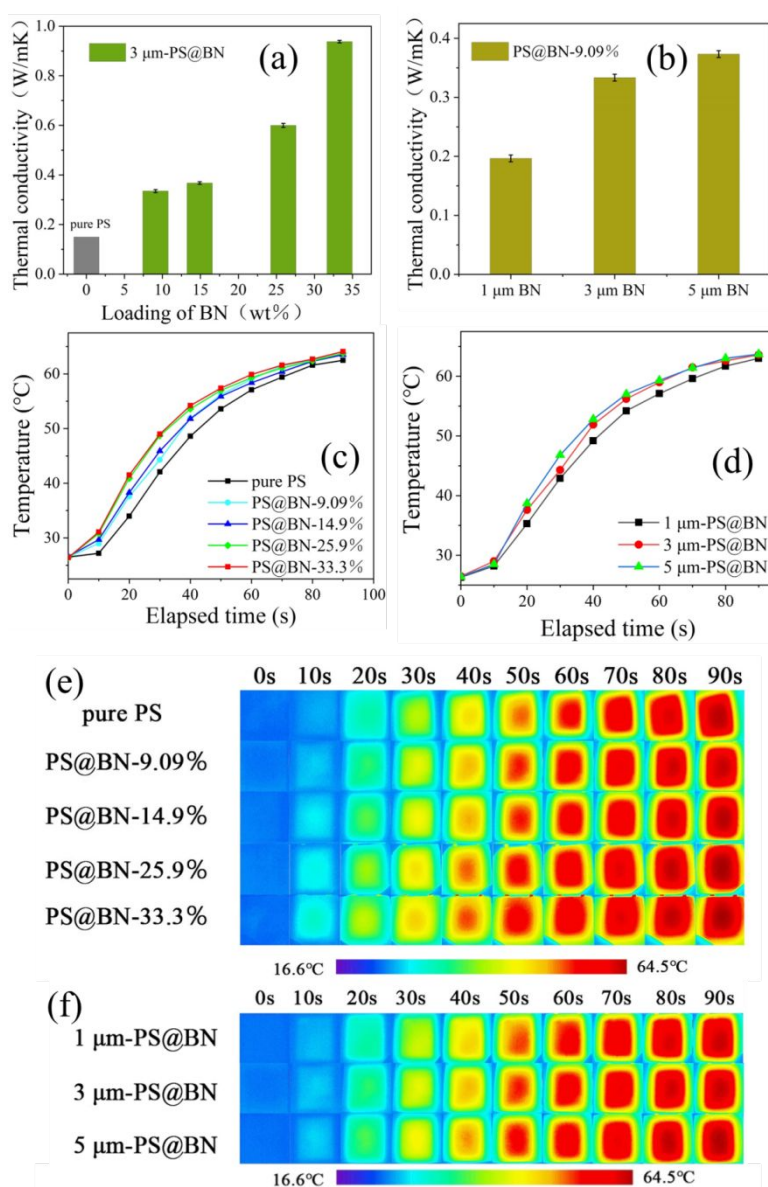
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4 to the blending of rigid inorganic fillers. When the temperature was higher than 120
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6 °C, the mobility of the polymer chains was significantly improved, limiting the role of
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8 rigid filler in the polymer matrix, thus causing a sharp drop in the storage modulus of
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10 the material.
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14 The loss tangent ($\tan \delta$) is the ratio of loss modulus to the storage modulus. As
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16 shown in Fig. 5b, the glass transition temperature (T_g) of composite was considered
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18 to be the temperature corresponding to the peak value of $\tan \delta$.^{25, 50} T_g values of
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20 PS@BN composites with 9.09 wt%, 14.9 wt%, 25.9 wt%, 33.3 wt% BN contents
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22 were 104.28, 110.46, 112.16, 114.03 °C, respectively, shifting to higher temperatures
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24 with the increasing content of BN sheet. As the content of the rigid inorganic filler
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26 increased, the movement of the polymer segment was limited. Polymer chains
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28 required excess energy to overcome the induced resistance to achieve chain motion.²
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51 Therefore, the glass transition temperature of the material gradually increased when
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41 The thermogravimetric analysis curves of the composites are shown in Fig. 5c. The
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43 residual value of the composite was roughly used as the BN content, assuming that
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45 the PS was totally decomposed while the BN maintained stable during heating. The
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47 residual mass of BN was converted to a volume fraction,⁵² as shown in Table S1. The
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49 thermal residual value confirmed that only part of the thermally conductive fillers was
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51 coated in PS@BN microspheres. According to Table S1 in Supporting Information,
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53 thermal decomposition temperatures at 5% of the weight loss (T_5) of the composite
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55 increased with BN content, suggesting that the initial decomposition temperature of

the composites could be increased by incorporation of inorganic thermal fillers. The phenomenon indicated that thermal stability of the composite would be enhanced by gradually adding inorganic fillers. T50 stands for the thermal decomposition temperatures at 50% of the weight loss, the relation between T50 and BN loading showed similar trend with that of T5, confirming that the thermal stability of the composite could be enhanced by the BN sheets.

3.6 Thermal conductivity of the composite substrate



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4 Fig. 6 (a) Thermal conductivity of composite substrate against the BN content; (b)
5
6 thermal conductivity of composite substrate against the size of BN; surface
7
8 temperature evolution with elapsed time of the composite made with different BN (c)
9
10 loadings and (d) sizes; infrared images taken by each 10 seconds for the composite
11
12 substrate made with different BN contents (e) and different BN sizes (f)
13
14
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18 The loading ratio and the mean size of BN sheets were found to be two important
19
20 factors controlling the thermal conductivity of the composite substrate. The thermal
21
22 conductivity of the composite substrate was 0.38 W/mK at BN loading of 9.09 wt%,
23
24 253% improvement compared to the pure polystyrene (0.15 W/mK⁵³). It was
25
26 attributed to that the thermally conductive 3D BN network dramatically improved
27
28 thermal conductivity of PS matrix. Thermal conductivity increased from 0.38 to 0.94
29
30 W/mK when the content of BN was lifted from 9.09 wt% to 33.3 wt% (Fig. 6a). High
31
32 physical BN loading is one of the reason for the thermal conductivity enhancement,
33
34 the other reason is that the mean size of the PS@BN microspheres decreased with the
35
36 BN loading (Fig 2e). The smaller PS@BN microsphere led to a denser BN 3D
37
38 network in the composite substrate, thereby facilitating heat transfer and improving
39
40 the overall thermal conductivity of the material. Heat transportation along large sized
41
42 BN experienced less interfacial thermal resistances in the composite substrate, as a
43
44 result, the thermal conductivity of the composite substrate increased with BN size
45
46 (Fig. 6b). It is noteworthy that even emulsion stabilized by 5 μm showed relatively
47
48 low ESI and some irregular shaped composite particles could be found after the
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50 polymerization (Fig 3k). The composite microspheres made from 5 μm BN showed
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4 highest thermal conductivity. It indicated that regardless of the imperfect shape, the
5
6 surface attached BN at PS particles also could form thermally conductive network
7
8
9 after hot-compression (Fig. 6b).

10
11 The heat conduction performance of the composite substrate was demonstrated by
12
13 upside surface temperature monitoring during the downside heating. The temperature
14
15 increased faster of the substrate with high BN loadings (Fig. 6c) at the beginning,
16
17 agreeing well with the trend of thermal conductivity. The temperature difference
18
19 gradually converged after 40s (Fig. 6c) because the heat conduction tended to reach
20
21 equilibrium after a certain time. The surface temperature of composite substrate made
22
23 from larger sized BN responded faster to the heating compared to that made of
24
25 smaller sized BN, as shown in Fig 6d. The temperature evolution (Fig. 6e and 6f) of
26
27 composite during heat showed well agreement with the results of thermal conductivity
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29 measurements, suggesting the improved heat conduction performance of the PS
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31 matrix after the introduction of BN network.
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40 Polymer composites usually require high thermally conductive filler loadings to
41
42 achieve high thermal conductivity,³ sacrificing the advantage of the polymer such as
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44 light weight and ease processability and so on. Therefore, improving thermal
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46 conductivity of polymer at low filler content is still a challenge. This work
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48 demonstrated that composite substrate fabricated from emulsion template method is
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50 comparable to the polymer materials prepared from other recently developed
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56 methods.
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Table 2 Comparison of thermal conductivity of polymer composites from recent literatures

Typical Sample	Filler loading	Thermal Conductivity (W/mK)	Filler Size (μm)	Year
BNNS/PVA	10 wt%	0.7321	1.0–2.0	2019 ⁴⁴
BN@PS/(PP/PS)	About 15 wt%	About 0.45	50	2018 ⁵⁴
BN/CPS	15.9 wt%	0.692	/	2016 ²⁷
AlN/PS	25 wt%	0.418	2	2016 ⁵⁵
Epoxy/BN	40 vol%	1.98	13	2019 ⁵¹
PS/BN	St/BNNS=5:1	1.1	/	2015 ⁵⁶
Epoxy/BN- Al_2O_3	26.5 vol%	0.808	3	2014 ⁵⁷
PS@BN	33.3 wt%	0.94	3	This work

4. Conclusion

In summary, a facile method for fabricating PS@BN composite microspheres from *in-situ* polymerization based on emulsion template was reported. PS substrate with embedded 3D inorganic BN network was obtained by further hot compression of PS@BN microspheres at 95 °C. Due to the 3D thermally conductive BN network from the self-assembly of BN at oil-water interface, the BN/PS composite substrate exhibited a maximum thermal conductivity of 0.94 W/mK at BN loading of 33.3 wt%. The mechanical strength and thermal stability of the composite microspheres were also dramatically enhanced by the introduction of BN. BN network constructed from

1
2
3
4 interfacial assembly for the fabrication of potential electronic packaging material has
5
6 been demonstrated.
7

8 9 ASSOCIATED CONTENT

10 11 **Supporting Information**

12 Stability of Pickering emulsion stabilized by BN; Morphologies of BN particles and
13
14 PS microspheres; FTIR spectrum of BN particles; Differential scanning calorimetry
15
16 (DSC) of PS@BN microspheres; and Thermogravimetric Analysis (TGA) of
17
18 PS@BNPS@BN microspheres could be found in Supporting Information which is
19
20 available free of charge.
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36 37 **Notes**

38
39 The authors declare no competing financial interest.
40
41
42

43 44 **Author Contributions**

45
46 The authors contributed equally.
47

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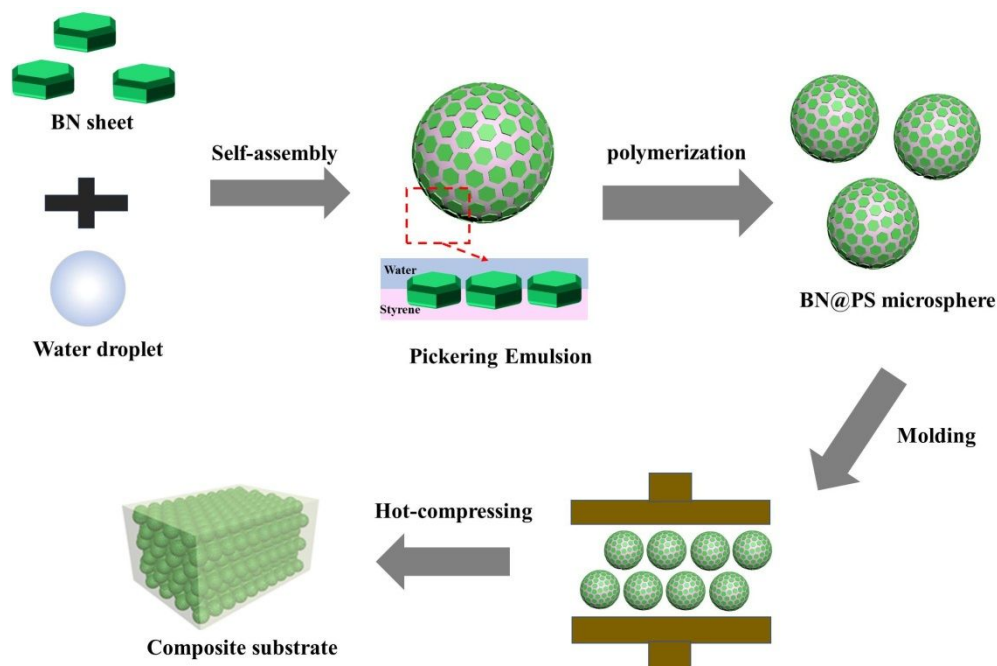
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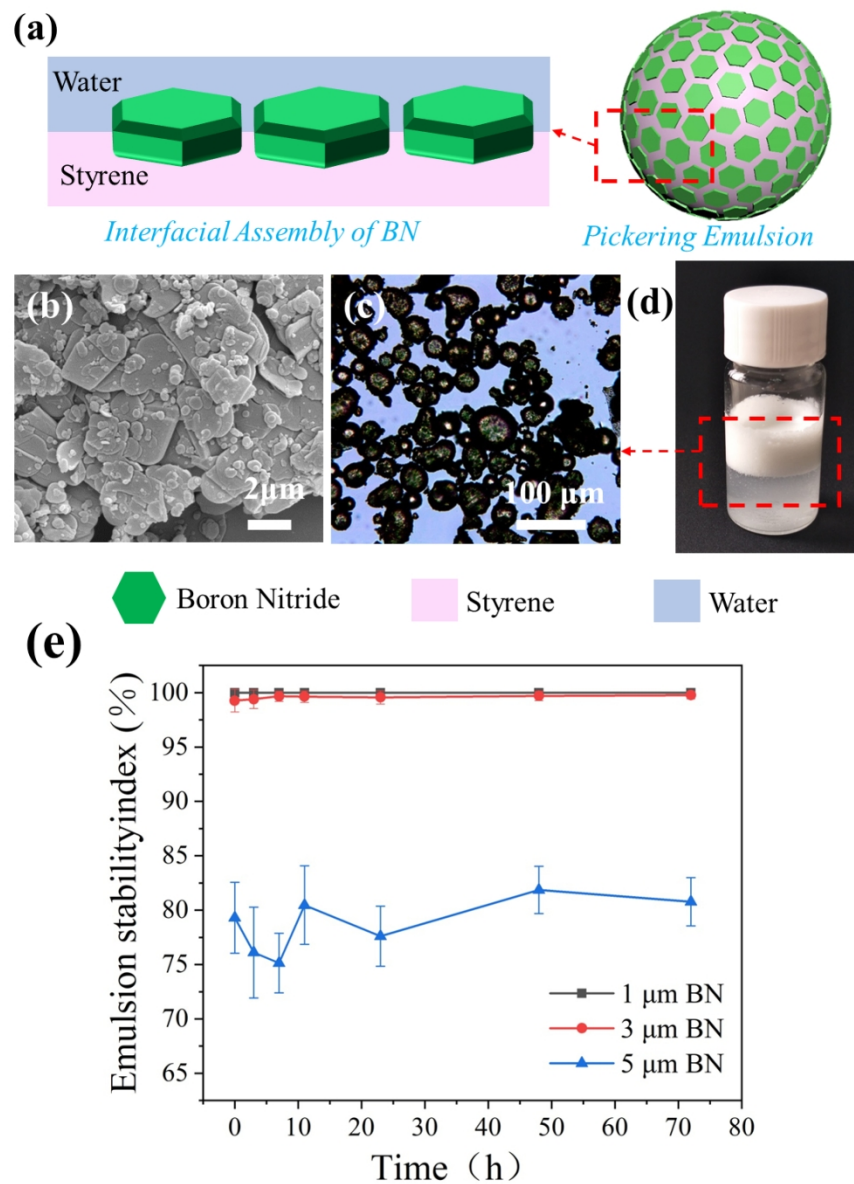
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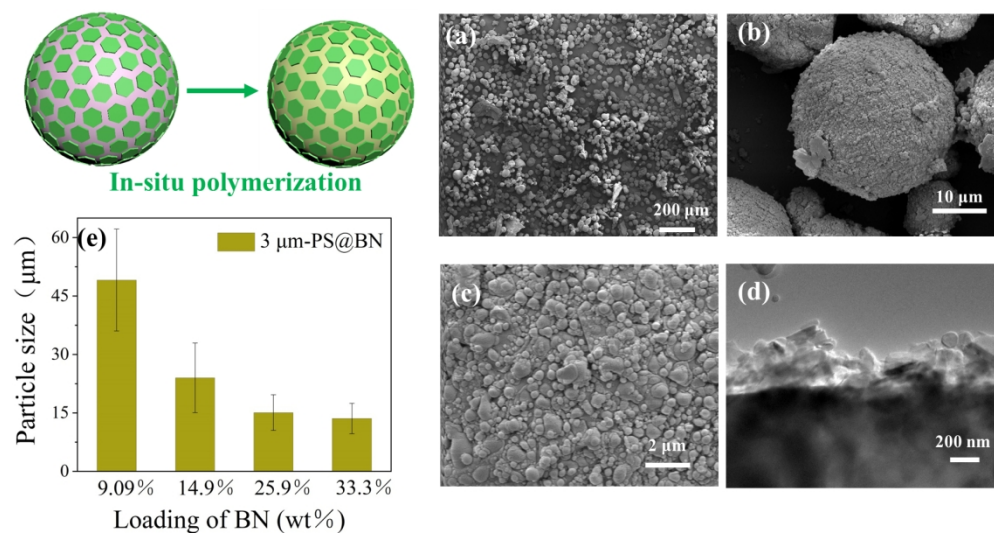


The Highly Thermally Conductive Polymer Composite is fabricated by
Assembly of Boron Nitride at Oil Water Interface



45 Fig. 1 (a) Schematic of Pickering emulsion, (b) SEM image of BN particles with mean size of 3 μm (c) the
46 optical microscopy image of Pickering emulsions; (d) photograph of typical Pickering emulsion stabilized by
47 BN ; and (e) Emulsion stability index (ESI) as a function of time for Pickering emulsion stabilized by BN
48 particles.

49 191x262mm (150 x 150 DPI)



24 Fig. 2 The cartoon illustrates the formation of PS@BN microspheres from in-situ polymerization of Pickering
25 emulsion. (a) SEM image of PS@BN microspheres stabilized by 3 μm BN sheets. SEM images of a typical
26 PS@BN microsphere with (b) low and (c) high magnifications; (d) TEM image, (e) particle size distribution

27 316x167mm (150 x 150 DPI)

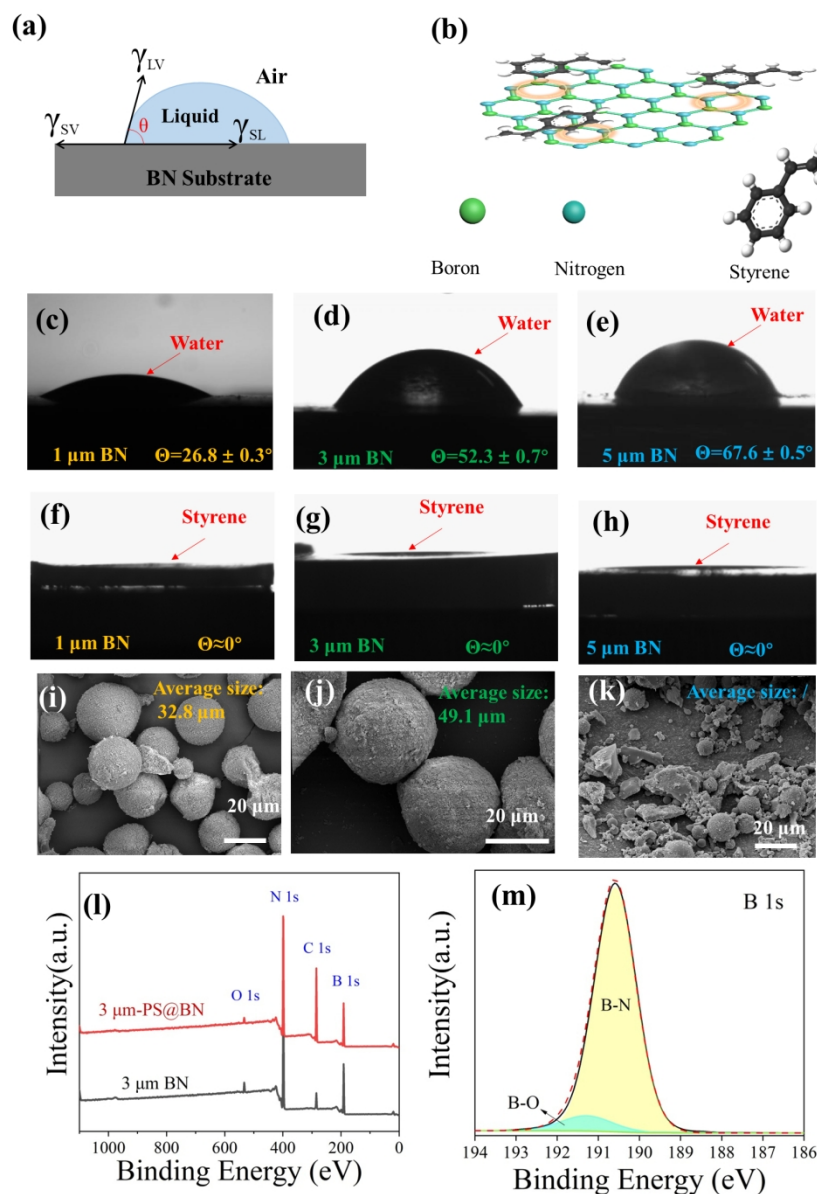


Fig.3 (a) Schematic configuration of contact angle measurements; (b) schematic illustration of interaction between BN and PS, the orange ring denotes the π - π stacking effects; (c-e) contact angles of water droplet on the tablets made of BN with various sizes; (f-h) contact angles of styrene droplet on the tablets made of BN with various sizes; SEM images of PS@BN microspheres obtained by BN sheets with mean size of (i) 1 μm , (j) 3 μm and (k) 5 μm . (l) XPS spectra of the 3 μm BN and 3 μm -PS@BN microspheres; (m) B 1s high-resolution spectrum of 3 μm BN. The content of BN in feed was 9.09 wt% for the preparation of all the above samples.

274x384mm (150 x 150 DPI)

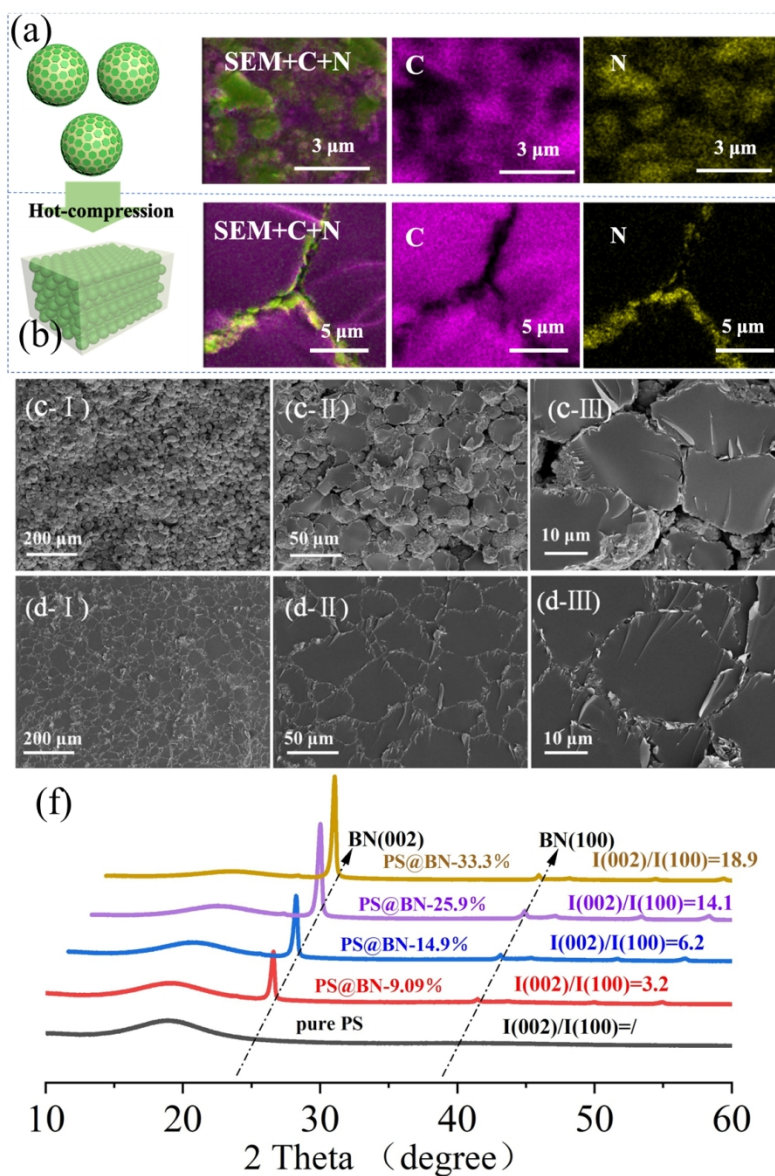


Fig. 4 EDS elemental mapping images of (a) the surface of PS@BN composite microspheres and (b) cross-section of composite substrate; cross-section SEM images of composite substrate under different conditions of hot-pressing: (c) 80°C, 25MPa; (d) 95°C, 25MPa; I, II, III represent the SEM at different magnifications, respectively; (f) XRD patterns of the composite substrates made from PS@BN microspheres with varies BN loadings.

205x302mm (150 x 150 DPI)

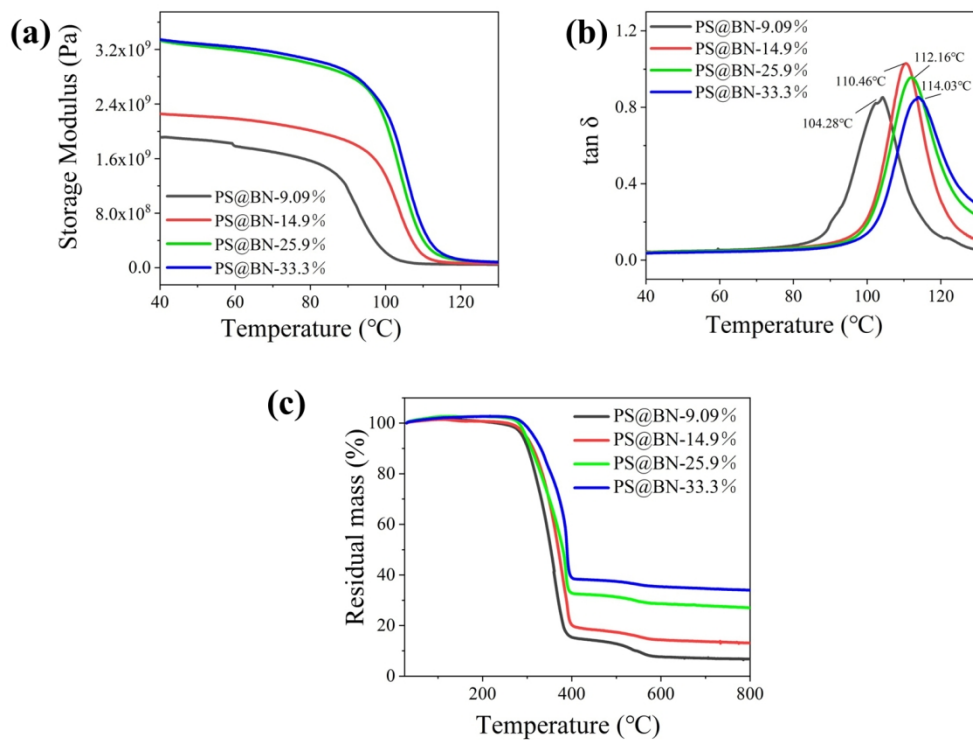


Fig. 5 Dynamic mechanical analysis (DMA) of the PS@BN composite substrates, (a) storage modulus and (b) loss tangent ($\tan \delta$) versus temperature of the composite substrates; (c) thermogravimetric analysis of PS@BN composite substrates with increased content of BN.

275x205mm (150 x 150 DPI)

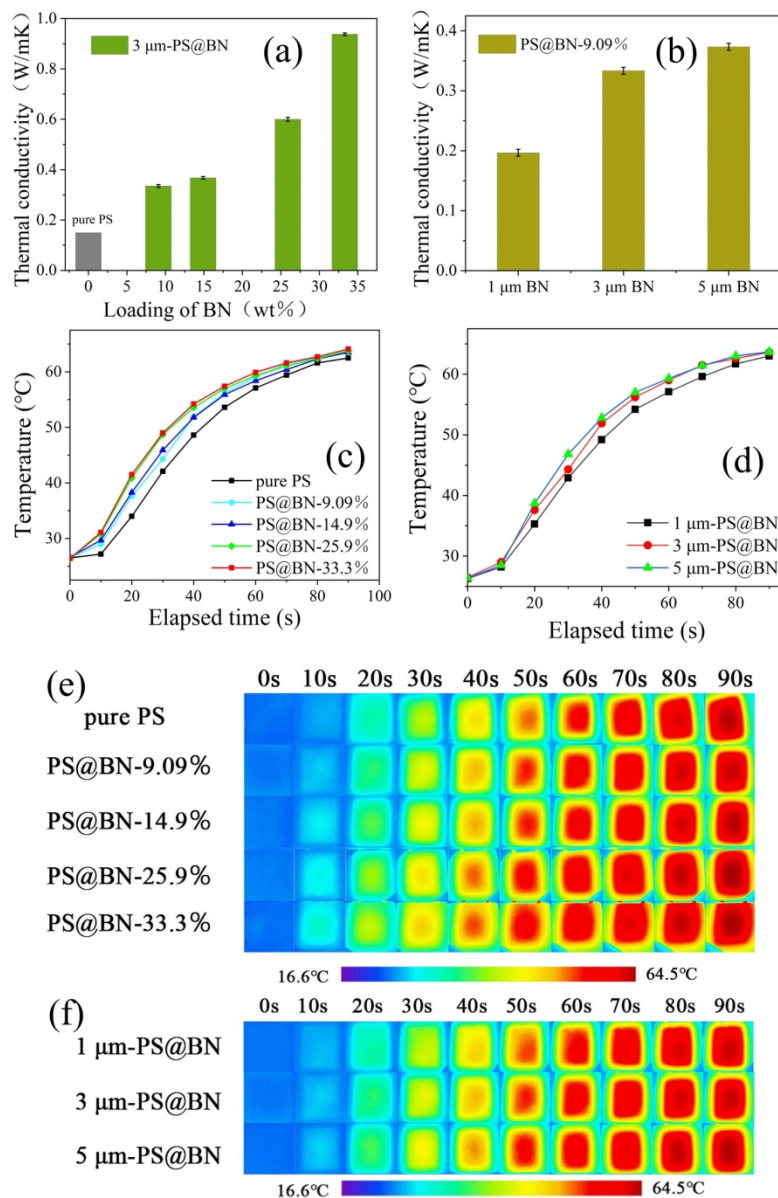


Fig. 6 (a) Thermal conductivity of composite substrate against the BN content; (b) thermal conductivity of composite substrate against the size of BN; surface temperature evolution with elapsed time of the composite made with different BN (c) loadings and (d) sizes; infrared images taken by each 10 seconds for the composite substrate made with different BN contents (e) and different BN sizes (f)

243x368mm (150 x 150 DPI)