

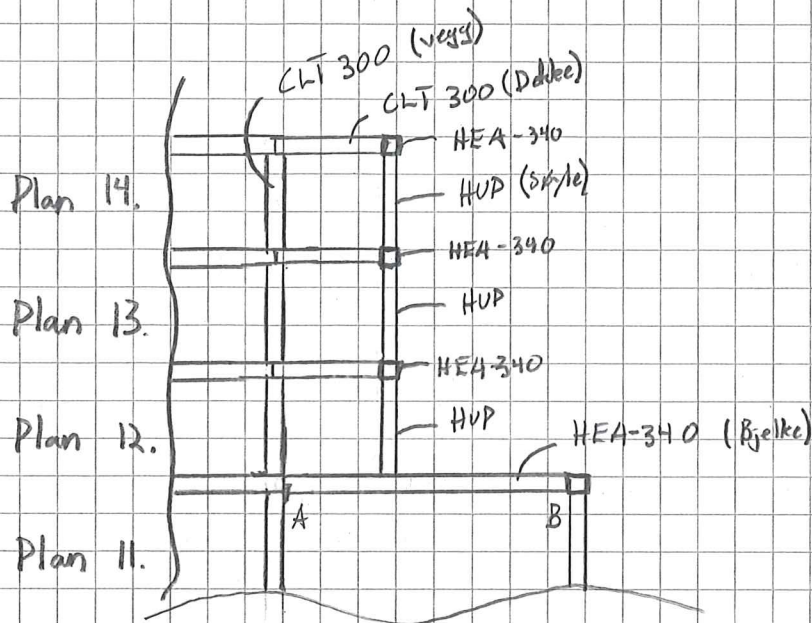
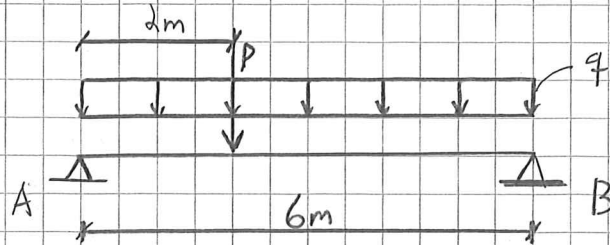
Vedlegg 19

Håndberegningskontroll av bjelke

Beregning Bjelke

HEA - 340

$L = 6\text{ m}$



Laster : (Alle håndberegninger vil resultere i mindre utnyttelse)
en del som egentlig er tilfelle

Dekke (CLT 300) :

$$500 \text{ kg/m}^3 \cdot 0,300 \text{ m} = 150 \text{ kg/m}^2 \Rightarrow 1,5 \text{ kN/m}^2$$

Påstøp :

$$2500 \text{ kg/m}^3 \cdot 0,05 \text{ m} = 125 \text{ kg/m}^2 \Rightarrow 1,25 \text{ kN/m}^2$$

Himling, membran, lettregger, fyllmasse etc :

$$50 \text{ kg/m}^2 \Rightarrow 0,5 \text{ kN/m}^2$$

Terrasselast : $4,0 \text{ kN/m}^2$

Snølast : $S_k = 3,0 \text{ kN/m}^2$

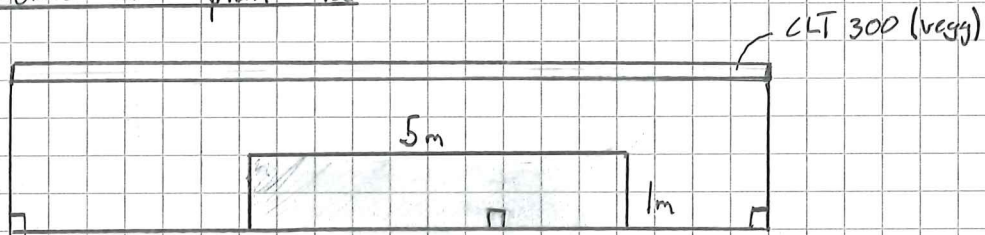
Formfaktor for flatt tak er $\mu_1 = 0,8$

$$S = S_k \cdot \mu_1$$

$$= 3,0 \text{ kN/m}^2 \cdot 0,8 = 2,4 \text{ kN/m}^2$$

Finne punktlasten P :

Dekke over plan 12:



$$\text{Lastareal: } 5\text{m} \times 1\text{m} = 5\text{m}^2$$

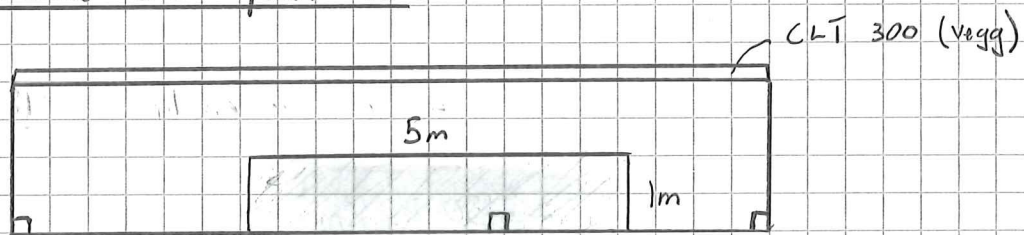
$$g_T = 1,5 \text{ kN/m}^2 + 1,25 \text{ kN/m}^2 + 0,5 \text{ kN/m}^2 = 3,25 \text{ kN/m}^2$$

$$n_T = 4,0 \text{ kN/m}^2$$

$$G_{12} = 3,25 \text{ kN/m}^2 \cdot 5\text{m}^2 = 16,25 \text{ kN}$$

$$N_{12} = 4,0 \text{ kN/m}^2 \cdot 5\text{m}^2 = 20 \text{ kN}$$

Dekke over plan 13:



$$\text{Lastareal: } 5\text{m} \times 1\text{m} = 5\text{m}^2$$

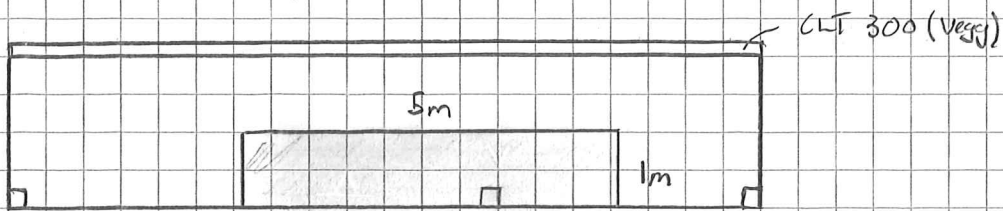
$$g_T = 1,5 \text{ kN/m}^2 + 1,25 \text{ kN/m}^2 + 0,5 \text{ kN/m}^2 = 3,25 \text{ kN/m}^2$$

$$n_T = 4,0 \text{ kN/m}^2$$

$$G_{13} = 3,25 \text{ kN/m}^2 \cdot 5\text{m}^2 = 16,25 \text{ kN}$$

$$N_{13} = 4,0 \text{ kN/m}^2 \cdot 5\text{m}^2 = 20 \text{ kN}$$

Dekke over plan 14:



$$\text{Lastareal} = 5\text{m} \times 1\text{m} = 5\text{m}^2$$

$$g_T = 1,5 \text{ kN/m}^2 + 1,25 \text{ kN/m}^2 + 0,5 \text{ kN/m}^2 = 3,25 \text{ kN/m}^2$$

$$S = 2,4 \text{ kN/m}^2$$

$$G_{14} = 3,25 \text{ kN/m}^2 \cdot 5\text{m}^2 = 16,25 \text{ kN}$$

$$S_{14} = 2,4 \text{ kN/m}^2 \cdot 5\text{m}^2 = 12 \text{ kN}$$

Totalt 3 etasjer:

$$G_{12,13,14} = G_{12} + G_{13} + G_{14}$$

$$= 16,25 \text{ kN} + 16,25 \text{ kN} + 16,25 \text{ kN} = \underline{48,75 \text{ kN}}$$

$$N_{12,13,14} = N_{12} + N_{13} + S_{14}$$

$$= 20 \text{ kN} + 20 \text{ kN} + 12 \text{ kN} = \underline{52 \text{ kN}}$$

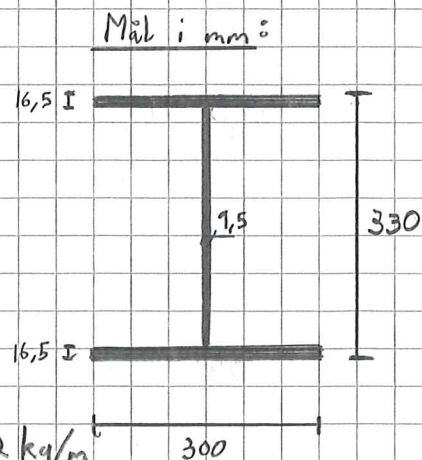
Egenvekt stålbjelke:

HEA-340

Stål: 7850 kg/m^3

$$A = 0,0134 \text{ m}^2$$

$$L = 5\text{m}$$



$$7850 \text{ kg/m}^3 \cdot 0,0134 \text{ m}^2 = 105,2 \text{ kg/m}$$

$$\Rightarrow 1,05 \text{ kN/m}$$

$$1,05 \text{ kN/m} \cdot 5\text{m} = 5,25 \text{ kN/etasje}$$

$$G_{\text{bjelke}} = 5,25 \text{ kN/etasje} \cdot 3 \text{ etasjer} = \underline{15,75 \text{ kN}}$$

③

Egenvekt stålsøyler:

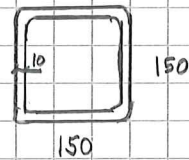
HVP $150 \times 150 \times 10$

Stål: 7850 kg/m^3

$A = 0,0055 \text{ m}^2$

$L = 2,8 \text{ m}$

Mål: mm:



$$7850 \text{ kg/m}^3 \cdot 0,0055 \text{ m}^2 = 43,2 \text{ kg/m} \\ \Rightarrow 0,43 \text{ kN/m}$$

$$0,43 \text{ kN/m} \cdot 2,8 \text{ m} = 1,2 \text{ kN/søyle}$$

$$G_{\text{søyle}} = 1,2 \text{ kN/søyle} \cdot 3 \text{ søyler} = \underline{3,6 \text{ kN}}$$

Total punktlast P_s

$$G = G_{12,13,14} + G_{\text{betong}} + G_{\text{søyle}}$$

$$= 48,75 \text{ kN} + 15,75 \text{ kN} + 3,6 \text{ kN} = \underline{68,1 \text{ kN}} \text{ (Bruksgrense)}$$

$$N = N_{12,13,14} = \underline{52 \text{ kN}} \text{ (Bruksgrense)}$$

$$B1: \gamma_G \cdot G + \gamma_Q \cdot N$$

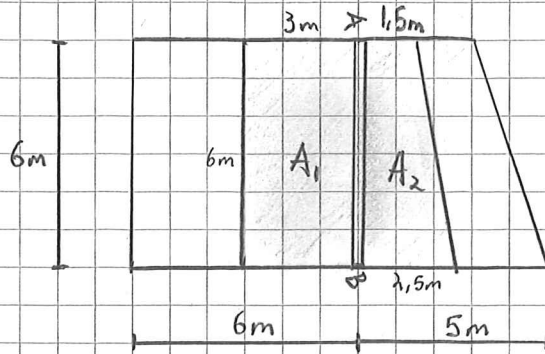
$$= 1,35 \cdot 68,1 \text{ kN} + 1,05 \cdot 52 \text{ kN} = \underline{146,5 \text{ kN}} \text{ (Bruddgrense)}$$

$$B2: \gamma_G \cdot G + \gamma_Q \cdot N$$

$$= 1,2 \cdot 68,1 \text{ kN} + 1,5 \cdot 52 \text{ kN} = \underline{159,7 \text{ kN}} \text{ (Bruddgrense)}$$

$$\text{Bruker } B2: \underline{P = 159,7 \text{ kN}}$$

Finne q (jevnt fordelt last) :



(Lengd bjelke 6m)

$$\text{Lastareal} = \underbrace{6\text{m} \times 3\text{m}}_{A_1} + \left(6\text{m} \times 1,5\text{m} + \frac{1\text{m} \times 6\text{m}}{2} \right) = 30\text{ m}^2$$

$$\text{CLT 300 (Dekke)} : 1,5\text{ kN/m}^2$$

$$\text{Påstøp} : 1,25\text{ kN/m}^2$$

$$\text{Himling, membran, lettregger, fyllmasse etc} : 0,5\text{ kN/m}^2$$

$$\text{Terrasselast} : 4,0\text{ kN/m}^2$$

$$G_1 = (1,5 + 1,25 + 0,5)\text{ kN/m}^2 \cdot 30\text{ m}^2 = 97,5\text{ kN}$$

$$N_1 = 4,0\text{ kN/m}^2 \cdot 30\text{ m}^2 = 120\text{ kN}$$

$$G = \frac{97,5\text{ kN}}{6\text{m}} = 16,25\text{ kN/m} \quad (\text{Bruksgrense})$$

$$N = \frac{120\text{ kN}}{6\text{m}} = 20\text{ kN/m} \quad (\text{Bruksgrense})$$

$$B1: \gamma_G \cdot G + \gamma_Q \cdot N$$

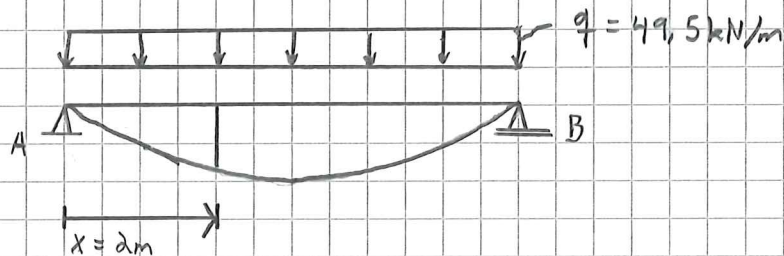
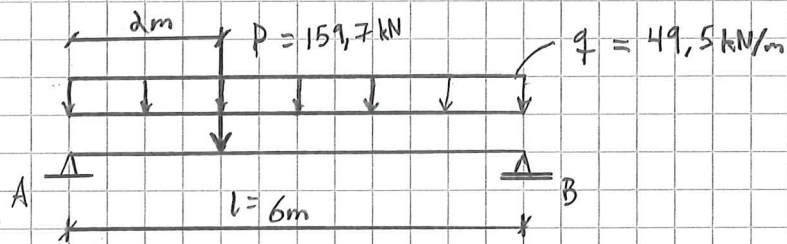
$$= 1,35 \cdot 16,25\text{ kN/m} + 1,05 \cdot 20\text{ kN/m} = 42,9\text{ kN/m} \quad (\text{Bruksgrense})$$

$$B2: \gamma_G \cdot G + \gamma_Q \cdot N$$

$$= 1,2 \cdot 16,25\text{ kN/m} + 1,5 \cdot 20\text{ kN/m} = 49,5\text{ kN/m} \quad (\text{Bruksgrense})$$

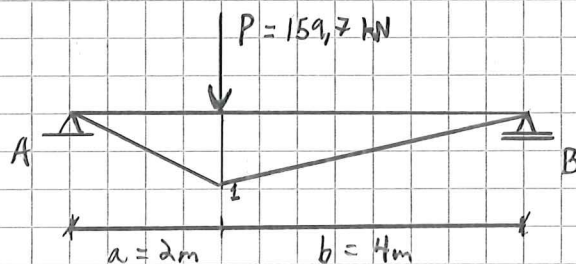
$$\text{Bruker } B2 : \underline{q = 49,5\text{ kN/m}}$$

Finne M_{max} :



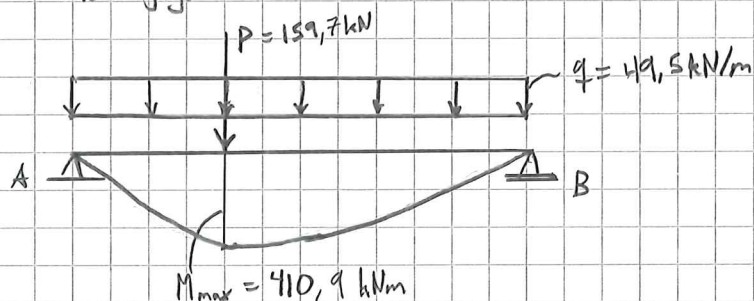
$$M_x = \frac{q \cdot l \cdot x}{2} - \frac{q \cdot x^2}{2}$$

$$= \frac{49,5 \text{ kN/m} \cdot 6\text{m} \cdot 2\text{m}}{2} - \frac{49,5 \text{ kN/m} \cdot (2\text{m})^2}{2} = 198 \text{ kNm}$$



$$M_1 = \frac{P \cdot a \cdot b}{l} = \frac{159,7 \text{ kN} \cdot 2\text{m} \cdot 4\text{m}}{6\text{m}} = 212,9 \text{ kNm}$$

Samlet figur 6



$$M_{max} = M_x + M_1 = 198 \text{ kNm} + 212,9 \text{ kNm} = 410,9 \text{ kNm}$$

Kontroll bjelkespenningen:

$$\sigma = \frac{M_{\max}}{W_p} = \frac{410,9 \cdot 10^6 \text{ Nmm}}{1850 \cdot 10^3 \text{ mm}^3} = 222,1 \text{ N/mm}^2 = 222,1 \text{ MPa}$$

$$f_{bd} = \frac{f_d}{\gamma_m} = \frac{355 \text{ MPa}}{1,05} = 338,1 \text{ MPa}$$

$$\sigma \leq f_{bd}$$

$$\underline{222,1 \text{ MPa} < 338,1 \text{ MPa} \Rightarrow \text{OK!}}$$

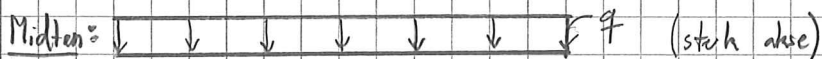
$$\frac{222,1 \text{ MPa}}{338,1 \text{ MPa}} = \underline{0,66} \text{ utfyllt}$$

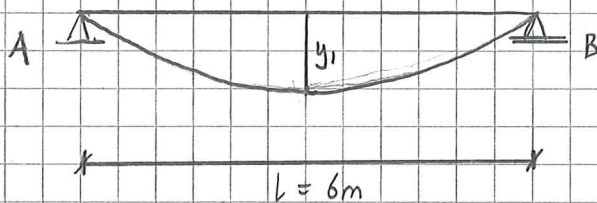
Kontroll nedbøyning:

Nedbøyning blir beregnet i bruksgrensetilstand $\gamma_G = 1,0$

$$P = G + N = 68,1 \text{ kN} + 52 \text{ kN} = \underline{120,1 \text{ kN}} \text{ (Bruksgrense)} \quad \gamma_Q = 1,0$$

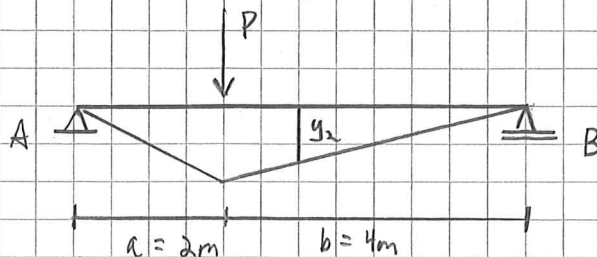
$$q = G + N = 16,25 \text{ kN/m} + 20 \text{ kN/m} = \underline{36,25 \text{ kN/m}} \text{ (Bruksgrense)}$$

Midten:  (statisk akse)



$$y_1 = \frac{5 \cdot q \cdot l^4}{384 \cdot E \cdot I_y}$$

$$= \frac{5 \cdot 36,25 \text{ kN/m} \cdot (6000 \text{ mm})^4}{384 \cdot 2,1 \cdot 10^5 \text{ N/mm}^2 \cdot 2,769 \cdot 10^8 \text{ mm}^4} = \underline{10,52 \text{ mm}}$$



$$y_2 = \frac{P \cdot a (3 \cdot l^2 - 4 \cdot a^2)}{48 \cdot E \cdot I_y}$$

$$= \frac{120,1 \cdot 10^3 \text{ N} \cdot 2000 \text{ mm} \cdot (3 \cdot (6000 \text{ mm})^2 - 4 \cdot (2000 \text{ mm})^2)}{48 \cdot 2,1 \cdot 10^5 \text{ N/mm}^2 \cdot 2,769 \cdot 10^8 \text{ mm}^4}$$

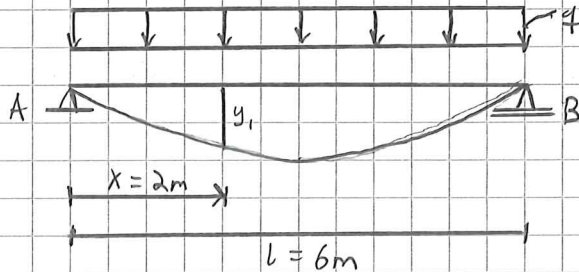
$$= \underline{7,92 \text{ mm}}$$

$$y_T = y_1 + y_2 = 10,52 \text{ mm} + 7,92 \text{ mm} = \underline{18,44 \text{ mm}}$$

$$\text{Max nedbøjning: } \frac{6000 \text{ mm}}{250} = \underline{24 \text{ mm}}$$

$$\underline{18,44 \text{ mm} < 24 \text{ mm} \Rightarrow \text{OK!}}$$

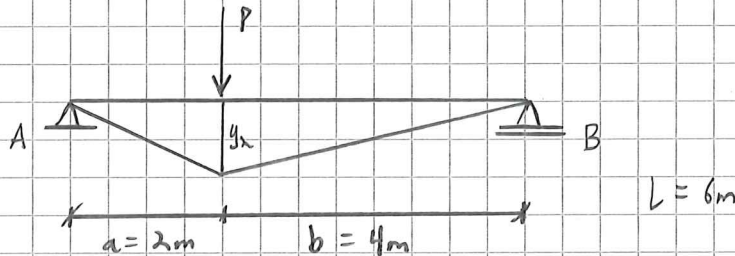
Spalte nedbøjning ved punktlast:



$$y_1 = \frac{q \cdot l^3 \cdot x}{24 \cdot E \cdot I_y} \cdot \left(1 - 2 \cdot \frac{x^2}{l^2} + \frac{x^3}{l^3} \right)$$

$$= \frac{36,25 \text{ N/mm} \cdot (6000 \text{ mm})^3 \cdot (2000 \text{ mm})^2}{24 \cdot 2,1 \cdot 10^5 \text{ N/mm}^2 \cdot 2,769 \cdot 10^8 \text{ mm}^4} \cdot \left(1 - 2 \cdot \frac{(2000 \text{ mm})^2}{(6000 \text{ mm})^2} + \frac{(2000 \text{ mm})^3}{(6000 \text{ mm})^3} \right)$$

$$= \underline{9,14 \text{ mm}}$$



$$y_2 = \frac{P \cdot a^2 \cdot b^2}{3 \cdot E \cdot I_y \cdot l}$$

$$= \frac{120,1 \cdot 10^3 \text{ N} \cdot (2000 \text{ mm})^2 \cdot (4000 \text{ mm})^2}{3 \cdot 2,1 \cdot 10^5 \text{ N/mm}^2 \cdot 2,769 \cdot 10^8 \text{ mm}^4 \cdot 6000 \text{ mm}}$$

$$= \underline{7,34 \text{ mm}}$$

$$y_T = y_1 + y_2 = 9,14 \text{ mm} + 7,34 \text{ mm} = \underline{16,48 \text{ mm}}$$

$$\underline{16,48 \text{ mm} < 24 \text{ mm} \Rightarrow \text{OK!}}$$