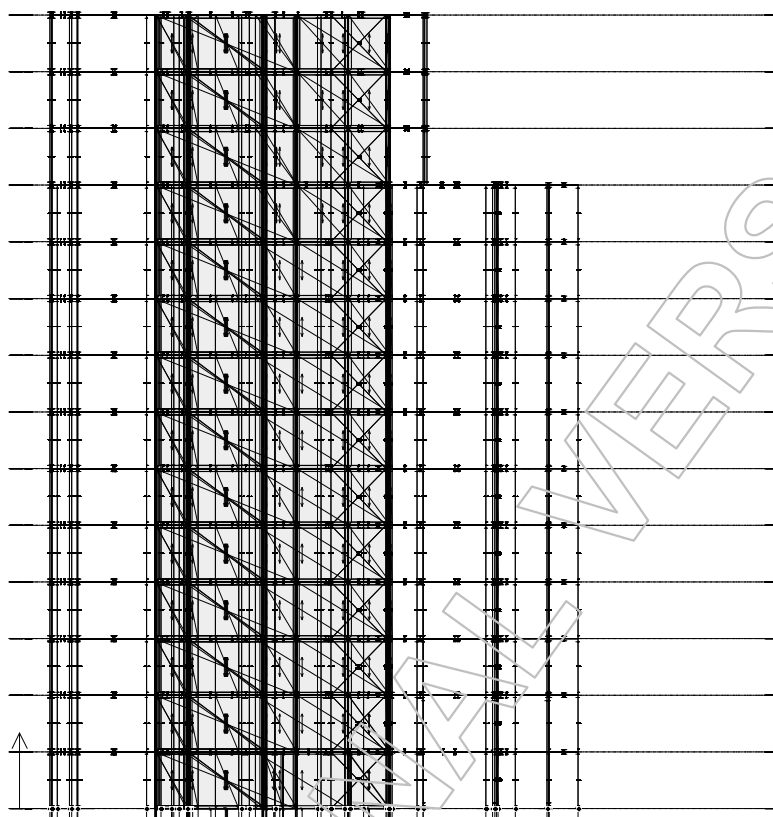


# Vedlegg 10

Dimensjonering av konstruksjon i FEM-Design

Eurocode (NA: Norwegian)



Project:

Fri Sikt

Customer:

Bacheloroppgave 2019

Description:

Dimensjonering i FEM-Design

FEM-Design © StruSoft

Designed: Marius Ove Bjørkavåg, Martin Mork Breivik

Date: 15.05.2019

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# Dokument

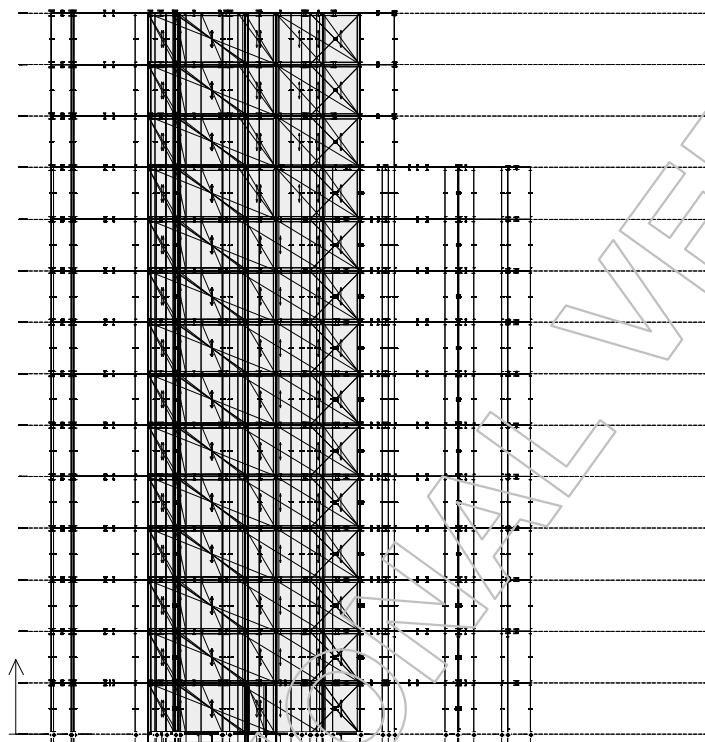
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# 1 Statisk modell

## 1.1 Geometri

Eurocode (NA: Norwegian)





## 2 Laster

### 2.1 Load cases

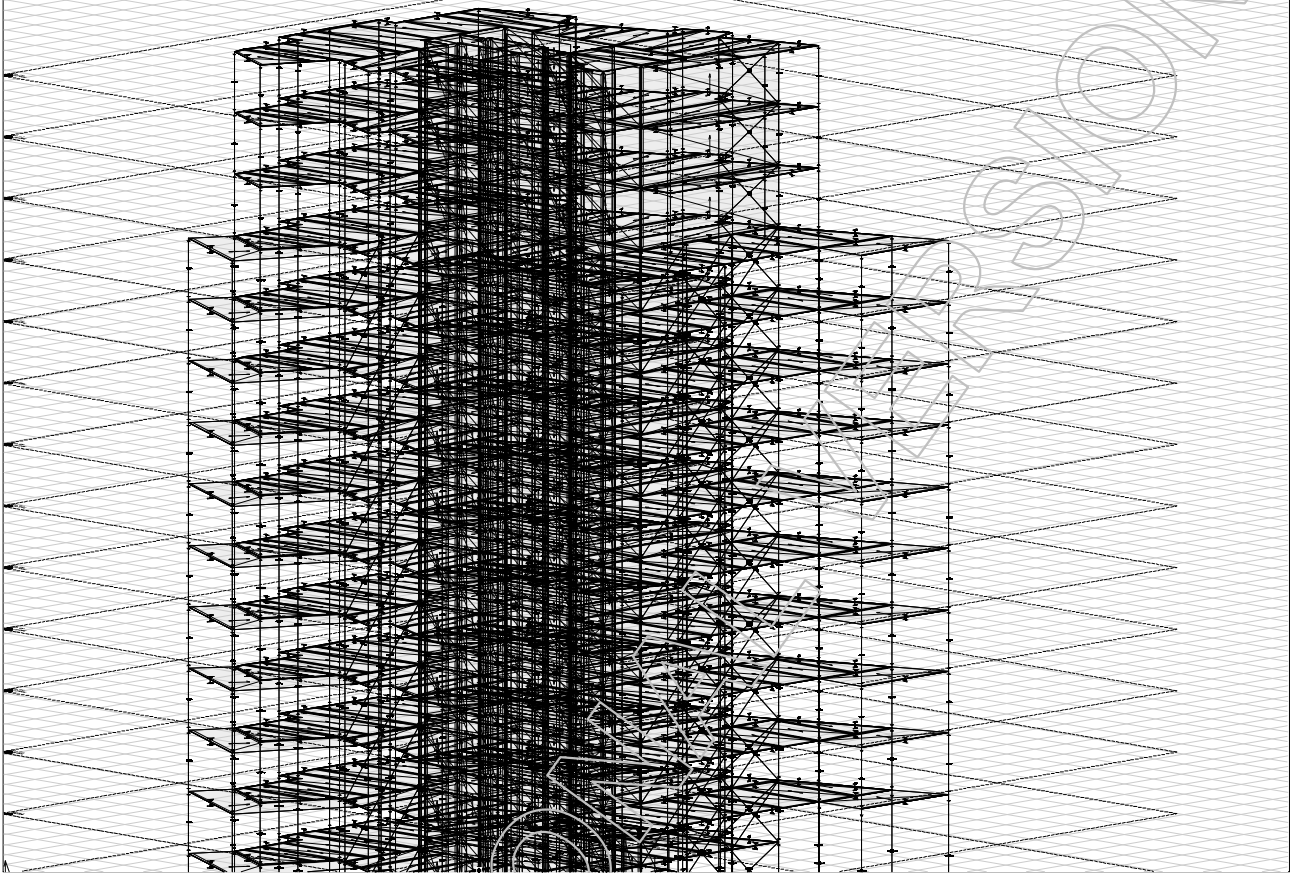
Load cases

No.	Name	Type
1	Auto Egenlast	+Struc. dead load
2	Egenlast Påført	Ordinary
3	Nyttelast Bolig	Ordinary
4	Nyttelast Terrasse	Ordinary
5	Snølast	Ordinary
6	Vind Y	Ordinary
7	Vind X	Ordinary
8	Deviation X+ (Generated by 1.00xLC...	Deviation load
9	Deviation Y+ (Generated by 1.00xLC...	Deviation load

Duration class
Permanent
Permanent
Medium-term
Short-term
Short-term
Short-term
Short-term
Permanent
Permanent

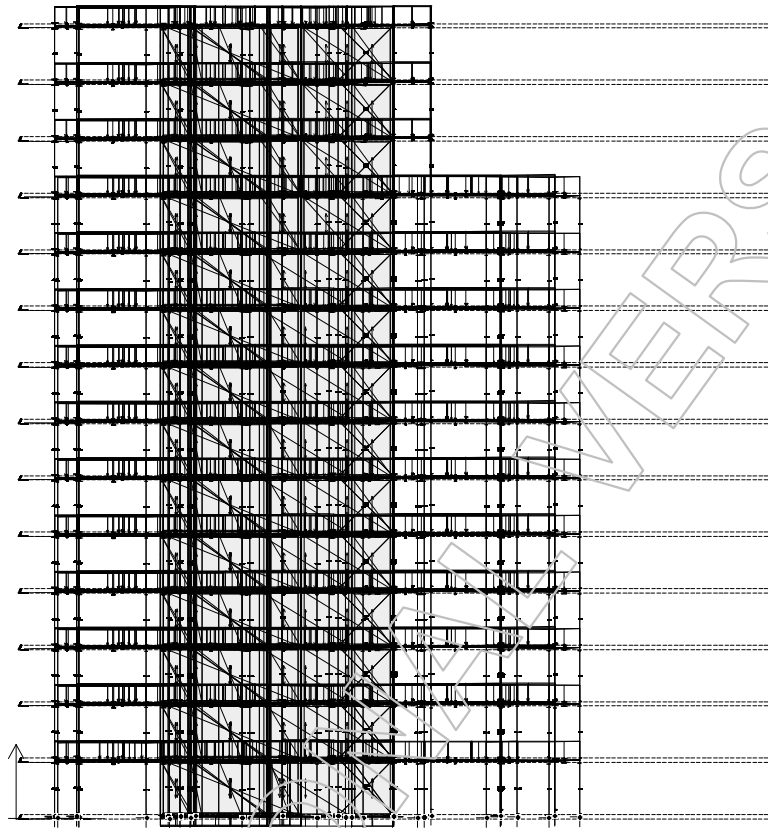
Auto Egenlast

Eurocode (NA: Norwegian)



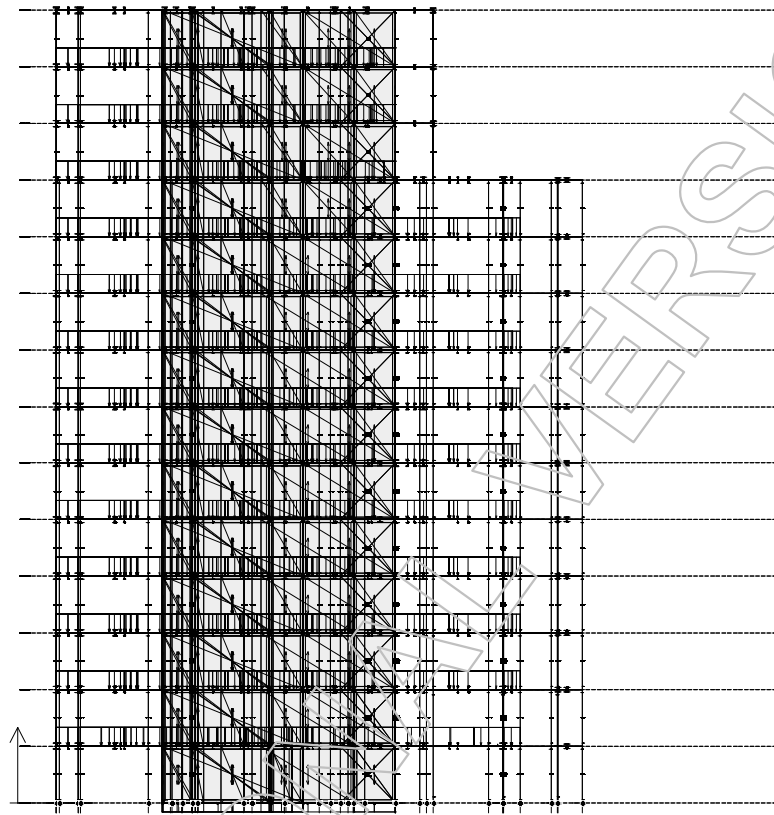
# Egenlast Påført

Eurocode (NA: Norwegian)



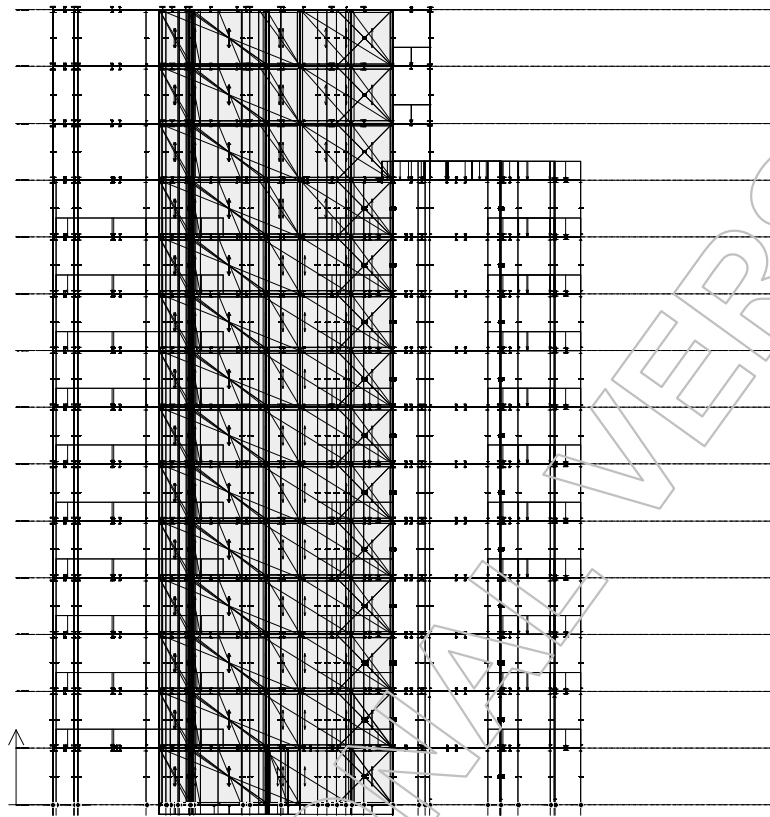
## Nyttelast Bolig

Eurocode (NA: Norwegian)



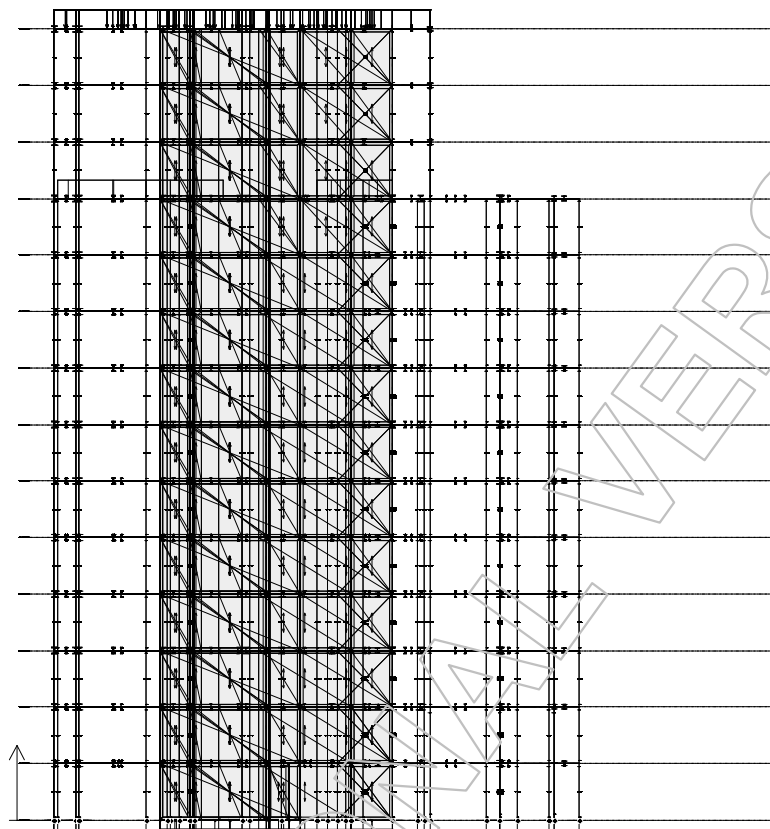
# Nyttelast Terrasse

Eurocode (NA: Norwegian)

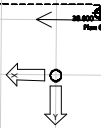


## Snølast

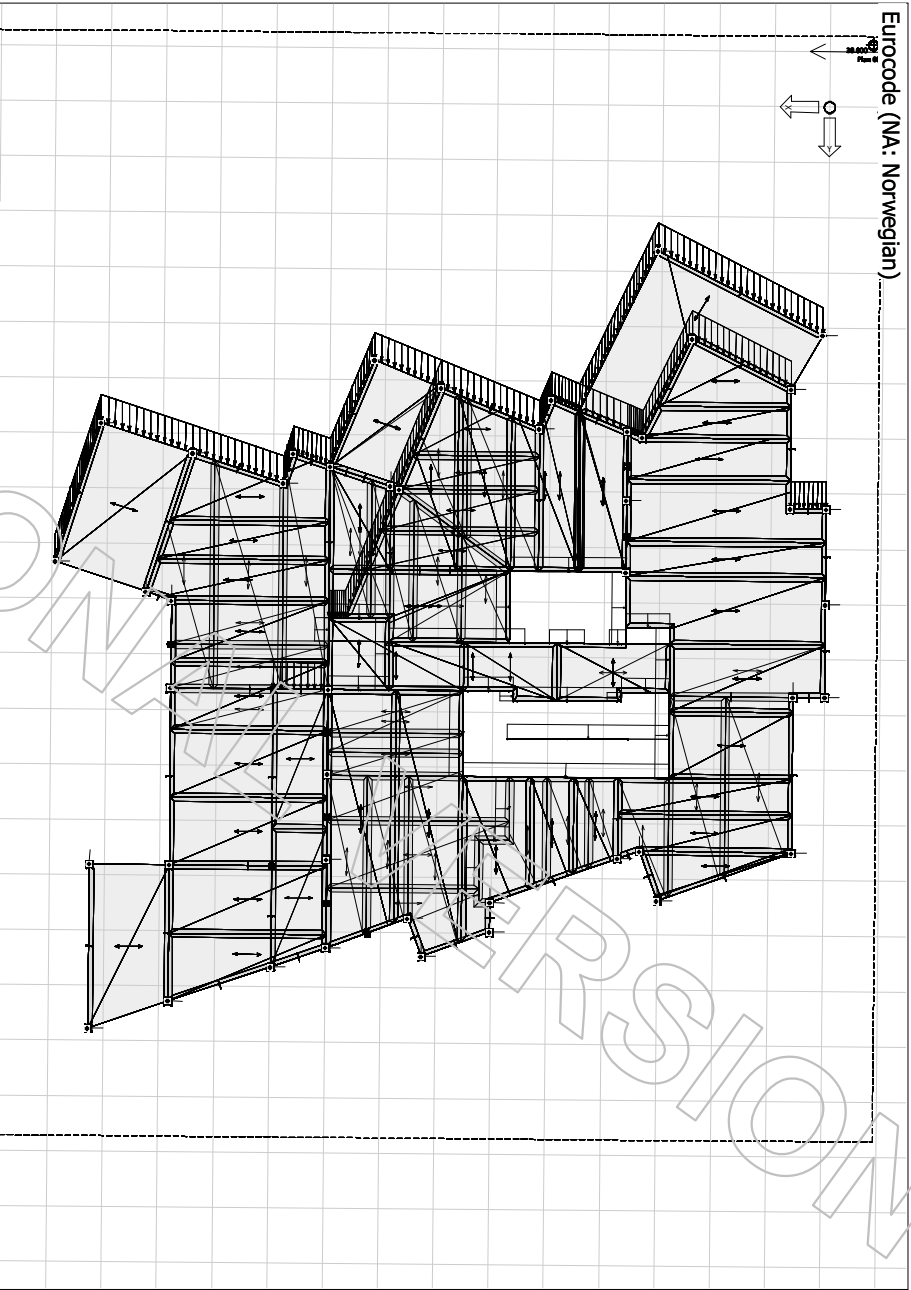
Eurocode (NA: Norwegian)



Eurocode (NA: Norwegian)

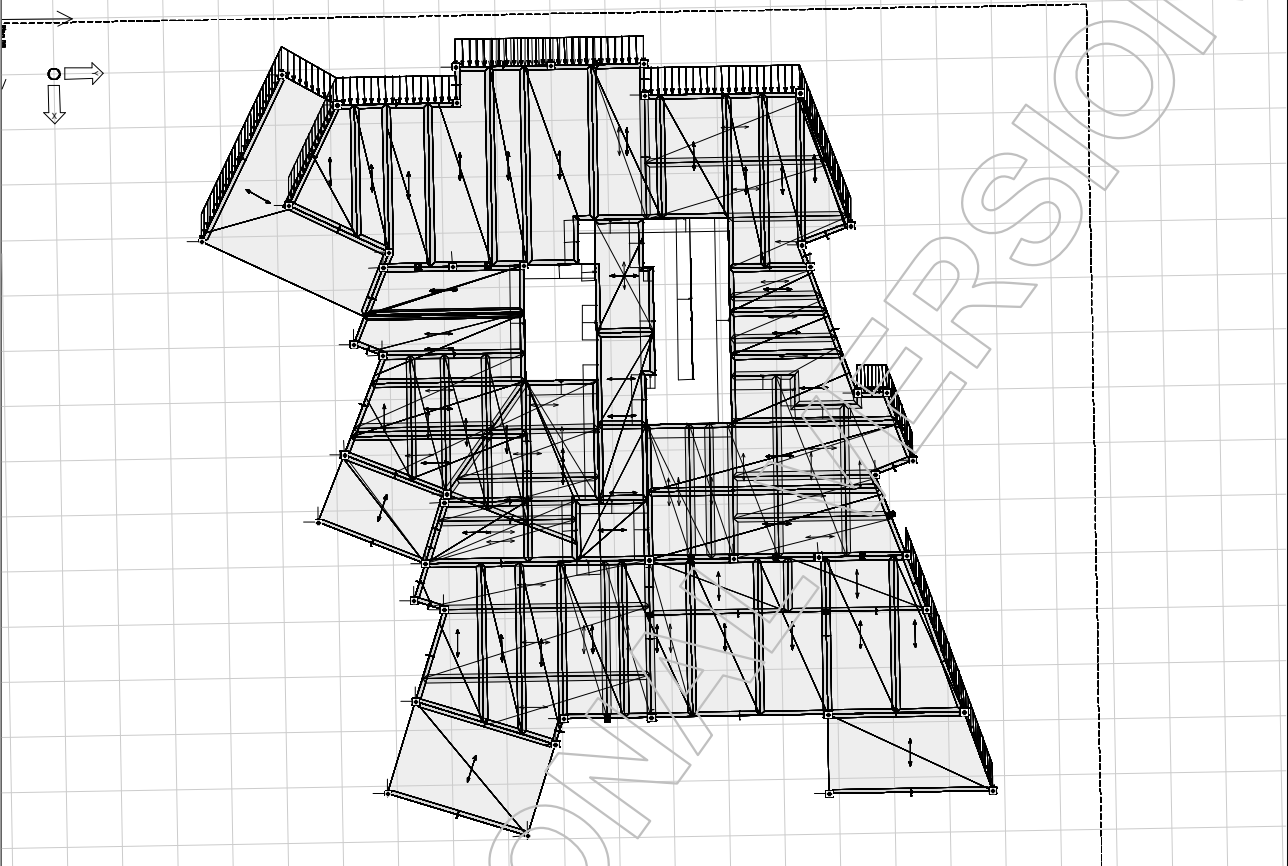


Vind Y



Vind X

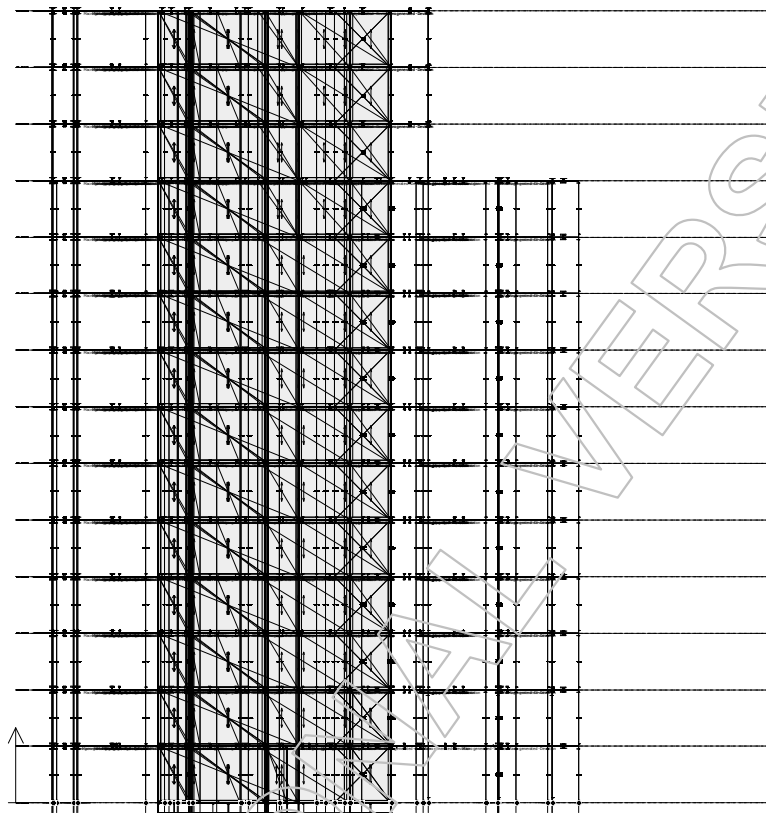
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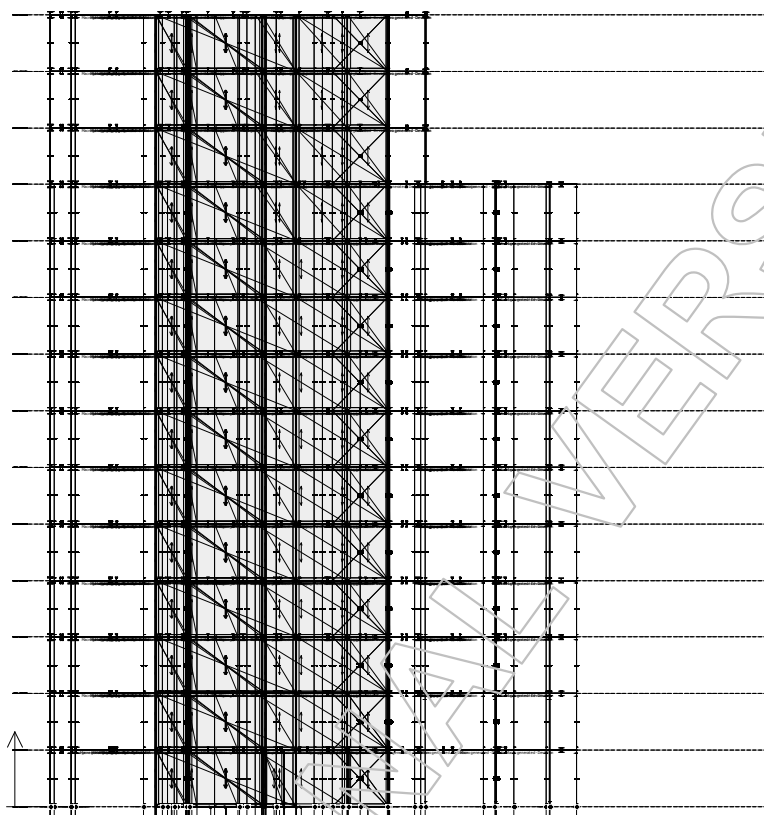
Deviation X+

Eurocode (NA: Norwegian)



Deviation Y+

Eurocode (NA: Norwegian)



## 2.2 Load combinations

Load combinations

No.	Name	Type	Factor
1	Bruddgr...	Ultimate	1.350
			1.050
			1.050
			1.050
			1.350
			0.900
			0.900
			1.350
			1.350
			1.350
2	Bruddgr...	Ultimate	1.350
			1.050
			1.050
			1.050
			1.350
			-0.900
			-0.900
			-1.350
3	Bruddgr...	Ultimate	-1.350
			1.200
			1.500

Load cases
Auto Egenlast (+Struc. dead load)
Nyttelast Bolig
Nyttelast Terrasse
Snølast
Egenlast Påført
Vind X
Vind Y
Deviation X+ (Generated by 1.00xLC.1+1.0...
Deviation Y+ (Generated by 1.00xLC.1+1.0...
Auto Egenlast (+Struc. dead load)
Nyttelast Bolig
Nyttelast Terrasse
Snølast
Egenlast Påført
Vind X
Vind Y
Deviation X+ (Generated by 1.00xLC.1+1.0...
Deviation Y+ (Generated by 1.00xLC.1+1.0...
Auto Egenlast (+Struc. dead load)
Nyttelast Bolig

No.	Name	Type	Factor
4	Bruddgr...	Ultimate	1.500
			1.050
			1.200
			1.050
			1.050
			1.200
			1.200
			1.200
			1.500
			1.500
			1.050
			1.200
			-1.050
			-1.050
5	Bruksgr...	Frequent	-1.200
			-1.200
			1.000
			0.700
			0.700
			0.700
			1.000

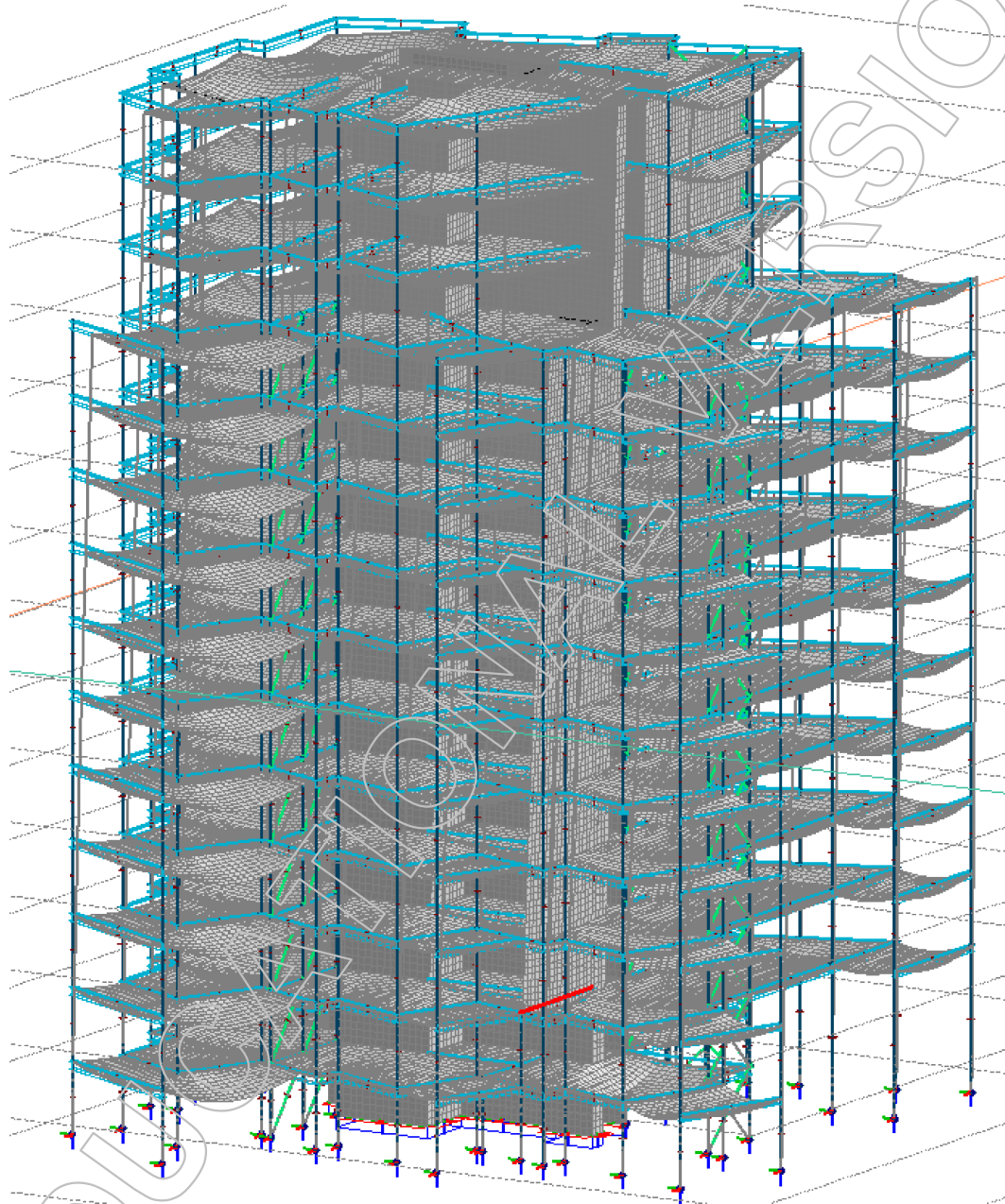
Load cases
Nyttelast Terrasse
Snølast
Egenlast Påført
Vind X
Vind Y
Deviation X+ (Generated by 1.00xLC.1+1.0...
Deviation Y+ (Generated by 1.00xLC.1+1.0...
Auto Egenlast (+Struc. dead load)
Nyttelast Bolig
Nyttelast Terrasse
Snølast
Egenlast Påført
Vind X
Vind Y
Deviation X+ (Generated by 1.00xLC.1+1.0...
Deviation Y+ (Generated by 1.00xLC.1+1.0...
Auto Egenlast (+Struc. dead load)
Nyttelast Bolig
Nyttelast Terrasse
Snølast
Egenlast Påført

No.	Name	Type	Factor
6	Egenlast	Frequent	1.000
			1.000
			1.000
			1.000
7	Vind +	Ultimate	1.000
			1.000
			1.200
			1.200
8	Vind -	Ultimate	1.000
			1.000
			1.200
			1.200

Load cases
Deviation X+ (Generated by 1.00xLC.1+1.0...
Deviation Y+ (Generated by 1.00xLC.1+1.0...
Auto Egenlast (+Struc. dead load)
Egenlast Påført
Auto Egenlast (+Struc. dead load)
Egenlast Påført
Vind X
Vind Y
Auto Egenlast (+Struc. dead load)
Egenlast Påført
Vind X
Vind Y

## 2.3 Bruddgrensetilstand

### 2.3.1 Mest belastet bjelke



Den mest belastede bjelke er markert i rødt. Bjelken er av typen HEA 340, og har en spennvidde på 5.49 meter

[illegible]

Utnyttelsesgrad

## B.58.1

### Maximum of load combinations

#### S 355

$$E = 210000 \text{ N/mm}^2$$

$$G = 80769 \text{ N/mm}^2$$

$$Y_{M0,ult} = 1.05$$

$$Y_{M0,acc/seis} = 1.00$$

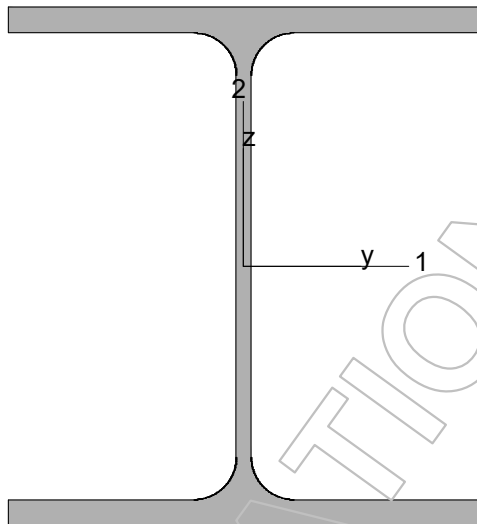
$$Y_{M1,ult} = 1.05$$

$$Y_{M1,acc/seis} = 1.00$$

$$Y_{M2,ult} = 1.25$$

$$Y_{M2,acc/seis} = 1.00$$

#### HE-A 340



P	=	1795	mm	$f_y$	=	355	N/mm <sup>2</sup>
A	=	13347	mm <sup>2</sup>	$\epsilon$	=	0.81	
$I_y$	=	2.769e+08	mm <sup>4</sup>	$\lambda_1$	=	76.40	
$I_z$	=	7.436e+07	mm <sup>4</sup>				
$i_1$	=	2.769e+08	mm <sup>4</sup>				
$I_2$	=	7.436e+07	mm <sup>4</sup>				
$W_{pl,1}$	=	1.850e+06	mm <sup>3</sup>				
$W_{pl,2}$	=	7.560e+05	mm <sup>3</sup>				
$W_{el,min,1}$	=	1.678e+06	mm <sup>3</sup>				
$W_{el,min,2}$	=	4.957e+05	mm <sup>3</sup>				
$i_1$	=	144	mm				
$i_2$	=	75	mm				
$I_t$	=	1.287e+06	mm <sup>4</sup>				
$I_w$	=	1.790e+12	mm <sup>6</sup>				



### Shear resistance, 1-1 - Part 1-1: 6.2.6, 6.2.8

LC: 'Vind +',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$V_{1,pl,Rd} = \frac{A_{1,v} \cdot f_y}{\sqrt{3} \cdot Y_{M0}} = \frac{10526 \cdot 355}{\sqrt{3} \cdot 1.05} = 2054.63 \text{ kN} \quad (6.18)$$

$$\begin{aligned} V_{1,pl,T,Rd} &= \sqrt{1 - \frac{T_{t,Ed}}{1.25 \left( f_y / \sqrt{3} \right) / Y_{M0}}} \cdot V_{1,pl,Rd} = \\ &= \sqrt{1 - \frac{0.88}{1.25 \left( 355 / \sqrt{3} \right) / 1.05}} \cdot 2054.63 = 2050.91 \text{ kN} \quad (6.26) \end{aligned}$$

$$\frac{V_{1,Ed}}{V_{1,pl,T,Rd}} = \frac{33.68}{2050.91} = 0.02 \leq 1.00 \quad (6.25) - \text{OK}$$

### Shear resistance, 2-2 - Part 1-1: 6.2.6, 6.2.8

LC: 'Bruddgrense 4 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$V_{2,pl,Rd} = \frac{A_{2,v} \cdot f_y}{\sqrt{3} \cdot Y_{M0}} = \frac{4495 \cdot 355}{\sqrt{3} \cdot 1.05} = 877.43 \text{ kN} \quad (6.18)$$

$$\begin{aligned} V_{2,pl,T,Rd} &= \sqrt{1 - \frac{T_{t,Ed}}{1.25 \left( f_y / \sqrt{3} \right) / Y_{M0}}} \cdot V_{2,pl,Rd} = \\ &= \sqrt{1 - \frac{2.05}{1.25 \left( 355 / \sqrt{3} \right) / 1.05}} \cdot 877.43 = 873.72 \text{ kN} \quad (6.26) \end{aligned}$$

$$\frac{V_{2,Ed}}{V_{2,pl,T,Rd}} = \frac{607.42}{873.72} = 0.70 \leq 1.00 \quad (6.25) - \text{OK}$$

### Torsional resistance - Part 1-1: 6.2.7

LC: 'Bruddgrense 4 Nytte',  $x = 3737$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$T_{\max,unit} = 21.48 \frac{\text{N/mm}^2}{\text{kN m}} \text{ is calculated by FEM analysis.}$$

$$T_{Rd} = \frac{f_y}{\sqrt{3} \cdot T_{\max,unit} \cdot Y_{M0}} = \frac{355}{\sqrt{3} \cdot 21.48 \cdot 1.05} = 9.09 \text{ kN m}$$

$$\frac{T_{Ed}}{T_{Rd}} = \frac{0.10}{9.09} = 0.01 \leq 1.00 \quad (6.23) - \text{OK}$$

### Shear stress - Part 1-1: 6.2.6

Not relevant

### Normal stress - Part 1-1: 6.2.1

Not relevant

### Normal capacity - Part 1-1: 6.2

LC: 'Brudgrense 3 Nytte',  $x = 3737$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$V_{1,Ed} = 10.75 \text{ kN} \leq 0.5 \cdot V_{1,pl,T,Rd} = 0.5 \cdot 2047.32 = 1023.66 \text{ kN} \rightarrow \rho_1 = 0.00$$

$$V_{2,Ed} = 60.44 \text{ kN} \leq 0.5 \cdot V_{2,pl,T,Rd} = 0.5 \cdot 874.31 = 437.15 \text{ kN} \rightarrow \rho_1 = 0.00$$

$$\frac{N_{Ed}}{N_{Rd}} + \frac{M_{1,Ed}}{M_{1,Rd}} + \frac{M_{2,Ed}}{M_{2,Rd}} = \frac{104.45}{4512.65} + \frac{112.51}{625.64} + \frac{5.63}{255.60} = 0.23 \leq 1.00 \quad (6.2) - \text{OK}$$

### Flexural buckling, 1-1 - Part 1-1: 6.3.1

LC: 'Brudgrense 4 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$\bar{\lambda}_1 = \frac{L_{cr,1}}{i_1 \cdot \lambda_1} = \frac{2011}{144 \cdot 76.40} = 0.18 \quad (6.50)$$

$$\alpha_1 = 0.34 \quad (\text{Buckling curve: b})$$

$$\begin{aligned} \varphi_1 &= 0.5 \left[ 1 + \alpha_1 \cdot (\bar{\lambda}_1 - 0.2) + \bar{\lambda}_1^2 \right] = \\ &= 0.5 \left[ 1 + 0.34 \cdot (0.18 - 0.2) + 0.18^2 \right] = 0.51 \end{aligned}$$

$$\begin{aligned} \chi_1 &= \min \left( \frac{1}{\varphi_1 + \sqrt{\varphi_1^2 - \bar{\lambda}_1^2}}, 1.0 \right) = \\ &= \min \left( \frac{1}{0.51 + \sqrt{0.51^2 - 0.18^2}}, 1.0 \right) = 1.00 \quad (6.49) \end{aligned}$$

$$N_{b,Rd,1} = \frac{\chi_1 \cdot A \cdot f_y}{\gamma_{M1}} = \frac{1.00 \cdot 13347 \cdot 355}{1.05} = 4512.65 \text{ kN} \quad (6.47)$$

$$\frac{N_{Ed}}{N_{b,Rd,1}} = \frac{31.82}{4512.65} = 0.01 \leq 1.00 \quad (6.46) - \text{OK}$$

### Flexural buckling, 2-2 - Part 1-1: 6.3.1

LC: 'Bruddgrense 4 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$\bar{\lambda}_2 = \frac{L_{cr,2}}{i_2 \cdot \lambda_1} = \frac{2011}{75 \cdot 76.40} = 0.35 \quad (6.50)$$

$\alpha_2 = 0.49$  (Buckling curve: c)

$$\begin{aligned} \varphi_2 &= 0.5 \left[ 1 + \alpha_2 \cdot (\bar{\lambda}_2 - 0.2) + \bar{\lambda}_2^2 \right] = \\ &= 0.5 \left[ 1 + 0.49 \cdot (0.35 - 0.2) + 0.35^2 \right] = 0.60 \end{aligned}$$

$$\begin{aligned} \chi_2 &= \min \left( \frac{1}{\varphi_2 + \sqrt{\varphi_2^2 - \bar{\lambda}_2^2}}, 1.0 \right) = \\ &= \min \left( \frac{1}{0.60 + \sqrt{0.60^2 - 0.35^2}}, 1.0 \right) = 0.92 \quad (6.49) \end{aligned}$$

$$N_{b,Rd,2} = \frac{\chi_2 \cdot A \cdot f_y}{\gamma_{M1}} = \frac{0.92 \cdot 13347 \cdot 355}{1.05} = 4161.13 \text{ kN} \quad (6.47)$$

$$\frac{N_{Ed}}{N_{b,Rd,2}} = \frac{31.82}{4161.13} = 0.01 \leq 1.00 \quad (6.46) \quad - \text{OK}$$

### Torsional-flexural buckling - Part 1-1: 6.3.1

LC: 'Bruddgrense 4 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$i_0 = \sqrt{i_1^2 + i_2^2 + y_0^2 + z_0^2} = \sqrt{144^2 + 75^2 + 0^2 + 0^2} = 162 \text{ mm}$$

$$N_{cr,1} = \frac{\pi^2 \cdot E \cdot I_1}{L_{cr,1}^2} = \frac{\pi^2 \cdot 210000 \cdot 276931124}{2011^2} = 141947.67 \text{ kN}$$

$$N_{cr,2} = \frac{\pi^2 \cdot E \cdot I_2}{L_{cr,2}^2} = \frac{\pi^2 \cdot 210000 \cdot 74359990}{2011^2} = 38114.99 \text{ kN}$$

$$N_{cr,T} = \frac{1}{i_0^2} \left( G \cdot I_t + \frac{\pi^2 \cdot E \cdot I_w}{L_t^2} \right) =$$

$$= \frac{1}{162^2} \left( 80769 \cdot 1.287e+06 + \frac{\pi^2 \cdot 210000 \cdot 1.790e+12}{2011^2} \right) = 38814.96 \text{ kN}$$

$$i_0^2 (N - N_{cr,1}) (N - N_{cr,2}) (N - N_{cr,T}) - N^2 y_0^2 (N - N_{cr,2}) - N^2 z_0^2 (N - N_{cr,1}) =$$

$$= 162^2 (N - 141947.67) (N - 38114.99) (N - 38814.96) - N^2 0^2 (N - 38114.99) - N^2 0^2 (N - 141947.67) = 0$$

Smallest root of the above equation related to the torsional-flexural buckling:

$$N_{cr,TF} = 38814.96 \text{ kN}$$

$$N_{cr} = \min(N_{cr,T}, N_{cr,TF}) = \min(38814.96, 38814.96) = 38814.96 \text{ kN}$$

$$\bar{\lambda}_T = \sqrt{\frac{A \cdot f_y}{N_{cr}}} = \sqrt{\frac{13347 \cdot 355}{38814.96}} = 0.35 \quad (6.53)$$

$$\alpha_T = 0.49 \quad (\text{Buckling curve: c})$$

$$\varphi_T = 0.5 \left[ 1 + \alpha_T (\bar{\lambda}_T - 0.2) + \bar{\lambda}_T^2 \right] =$$

$$= 0.5 \left[ 1 + 0.49 \cdot (0.35 - 0.2) + 0.35^2 \right] = 0.60$$

$$\chi_T = \min \left( \frac{1}{\varphi_T + \sqrt{\varphi_T^2 - \bar{\lambda}_T^2}}, 1.0 \right) =$$

$$= \min \left( \frac{1}{0.60 + \sqrt{0.60^2 - 0.35^2}}, 1.0 \right) = 0.92 \quad (6.49)$$

$$N_{b,Rd,T} = \frac{\chi_T \cdot A \cdot f_y}{Y_{M1}} = \frac{0.92 \cdot 13347 \cdot 355}{1.05} = 4168.71 \text{ kN} \quad (6.47)$$

$$\frac{N_{Ed}}{N_{b,Rd,T}} = \frac{31.82}{4168.71} = 0.01 \leq 1.00 - \text{OK}$$

### Lateral torsional buckling, top flange - Part 1-1: 6.3.2.2

LC: 'Bruddgrense 4 Nytte',  $x = 804$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$N_{cr,LT} = \frac{\pi^2 \cdot E \cdot I_z}{(k_z \cdot L_{cr})^2} = \frac{\pi^2 \cdot 2.100e+05 \cdot 7.436e+07}{(1.00 \cdot 2011)^2} = 38114.99 \text{ kN}$$

Loaded on top edge.

$$Z = (C_2 \cdot z_g - C_3 \cdot z_j) = (0.41 \cdot 165 - 0.75 \cdot 0) = 67.56 \text{ mm}$$

$$\begin{aligned} M_{cr} &= C_1 \cdot N_{cr,LT} \cdot \left\{ \left[ \left( \frac{k_z}{k_w} \right)^2 \cdot \frac{I_w}{I_z} + \frac{G \cdot I_t}{N_{cr,LT}} + Z^2 \right]^{0.5} - Z \right\} \\ &= 1.18 \cdot 3.811e+07 \cdot \left\{ \left[ \left( \frac{1.00}{1.00} \right)^2 \cdot \frac{1.790e+12}{7.436e+07} + \frac{8.077e+04 \cdot 1.287e+06}{3.811e+07} + 67.56^2 \right]^{0.5} - 67.56 \right\} \\ &= 4917.63 \text{ kN m} \end{aligned}$$

$$\bar{\lambda}_{LT} = \sqrt{\frac{W_y \cdot f_y}{M_{cr}}} = \sqrt{\frac{1850478 \cdot 355}{4.918e+09}} = 0.37$$

$\alpha_{LT} = 0.21$  (Buckling curve: a)

$$\begin{aligned} \varphi_{LT} &= 0.5 \left[ 1 + \alpha_{LT} \cdot (\bar{\lambda}_{LT} - 0.2) + \bar{\lambda}_{LT}^2 \right] = \\ &= 0.5 \left[ 1 + 0.21 \cdot (0.37 - 0.2) + 0.37^2 \right] = 0.58 \end{aligned}$$

$$\begin{aligned} X_{LT} &= \min \left( \frac{1}{\varphi_{LT} + \sqrt{\varphi_{LT}^2 - \bar{\lambda}_{LT}^2}}, 1.0 \right) = \\ &= \min \left( \frac{1}{0.58 + \sqrt{0.58^2 - 0.37^2}}, 1.0 \right) = 0.96 \quad (6.56) \end{aligned}$$

$$M_{y,b,Rd} = \frac{X_{LT} \cdot W_y \cdot f_y}{\gamma_{M1}} = \frac{0.96 \cdot 1850478 \cdot 355}{1.05} = 601.65 \text{ kN m} \quad (6.55)$$

$$\frac{M_{1,Ed}}{M_{y,b,Rd}} = \frac{109.40}{601.65} = 0.18 \leq 1.00 \quad (6.54) \text{ - OK}$$

### Lateral torsional buckling, bottom flange - Part 1-1: 6.3.2.2

LC: 'Bruddgrense 3 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$N_{cr,LT} = \frac{\pi^2 \cdot E \cdot I_z}{(k_z \cdot L_{cr})^2} = \frac{\pi^2 \cdot 2.100e+05 \cdot 7.436e+07}{(1.00 \cdot 2011)^2} = 38114.99 \text{ kN}$$

Loaded on top edge.

$$Z = (C_2 \cdot z_g - C_3 \cdot z_j) = (0.45 \cdot 165 - 0.75 \cdot 0) = 74.44 \text{ mm}$$

$$\begin{aligned} M_{cr} &= C_1 \cdot N_{cr,LT} \cdot \left\{ \left[ \left( \frac{k_z}{k_w} \right)^2 \cdot \frac{I_w}{I_z} + \frac{G \cdot I_t}{N_{cr,LT}} + Z^2 \right]^{0.5} - Z \right\} \\ &= 1.29 \cdot 3.811e+07 \cdot \left\{ \left[ \left( \frac{1.00}{1.00} \right)^2 \cdot \frac{1.790e+12}{7.436e+07} + \frac{8.077e+04 \cdot 1.287e+06}{3.811e+07} + 74.44^2 \right]^{0.5} - 74.44 \right\} \\ &= 5195.87 \text{ kN m} \end{aligned}$$

$$\bar{\lambda}_{LT} = \sqrt{\frac{W_y \cdot f_y}{M_{cr}}} = \sqrt{\frac{1850478 \cdot 355}{5.196e+09}} = 0.36$$

$\alpha_{LT} = 0.21$  (Buckling curve: a)

$$\begin{aligned} \varphi_{LT} &= 0.5 \left[ 1 + \alpha_{LT} \cdot (\bar{\lambda}_{LT} - 0.2) + \bar{\lambda}_{LT}^2 \right] = \\ &= 0.5 \left[ 1 + 0.21 \cdot (0.36 - 0.2) + 0.36^2 \right] = 0.58 \end{aligned}$$

$$\begin{aligned} X_{LT} &= \min \left( \frac{1}{\varphi_{LT} + \sqrt{\varphi_{LT}^2 - \bar{\lambda}_{LT}^2}}, 1.0 \right) = \\ &= \min \left( \frac{1}{0.58 + \sqrt{0.58^2 - 0.36^2}}, 1.0 \right) = 0.96 \quad (6.56) \end{aligned}$$

$$M_{y,b,Rd} = \frac{X_{LT} \cdot W_y \cdot f_y}{\gamma_{M1}} = \frac{0.96 \cdot 1850478 \cdot 355}{1.05} = 603.20 \text{ kN m} \quad (6.55)$$

$$\frac{M_{1,Ed}}{M_{y,b,Rd}} = \frac{84.27}{603.20} = 0.14 \leq 1.00 \quad (6.54) \text{ - OK}$$

### Interaction between normal force and bending 1. - Part 1-1: 6.3.3

LC: 'Bruddgrense 3 Nytte',  $x = 3737$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$k_{ij}$  factors are calculated according to Method 1

$$C_{my} = 1.00 \quad C_{yy} = 1.00$$

$$C_{mz} = 1.00 \quad C_{yz} = 1.00$$

$$C_{mLT} = 1.00 \quad C_{zy} = 1.00$$

$$C_{zz} = 0.92$$

$$M_{2,Rk} = f_y \cdot W_{pl,2} = 355 \cdot 755986 = 268.38 \text{ kN m}$$

$$\begin{aligned} \frac{N_{Ed}^{comp}}{N_{b,Rd,1}} + k_{11} \cdot \frac{M_{1,Ed}}{M_{y,b,Rd}} + k_{12} \cdot \frac{M_{2,Ed}}{M_{2,Rk}} &= \\ &= \frac{0.00}{4512.65} + 1.00 \cdot \frac{112.51}{625.64} + 0.70 \cdot \frac{5.63}{\frac{268.38}{1.05}} = 0.20 \leq 1.00 \quad (6.61) - \text{OK} \end{aligned}$$

### Interaction between normal force and bending 2. - Part 1-1: 6.3.3

LC: 'Bruddgrense 3 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$k_{ij}$  factors are calculated according to Method 1

$$C_{my} = 1.00 \quad C_{yy} = 1.00$$

$$C_{mz} = 1.00 \quad C_{yz} = 0.99$$

$$C_{mLT} = 1.00 \quad C_{zy} = 1.00$$

$$C_{zz} = 0.67$$

$$M_{2,Rk} = f_y \cdot W_{pl,2} = 355 \cdot 755986 = 268.38 \text{ kN m}$$

$$\begin{aligned} \frac{N_{Ed}^{comp}}{N_{b,Rd,2}} + k_{21} \cdot \frac{M_{1,Ed}}{M_{y,b,Rd}} + k_{22} \cdot \frac{M_{2,Ed}}{M_{2,Rk}} &= \\ &= \frac{0.00}{4161.13} + 0.52 \cdot \frac{84.27}{603.20} + 1.50 \cdot \frac{8.74}{\frac{268.38}{1.05}} = 0.12 \leq 1.00 \quad (6.62) - \text{OK} \end{aligned}$$

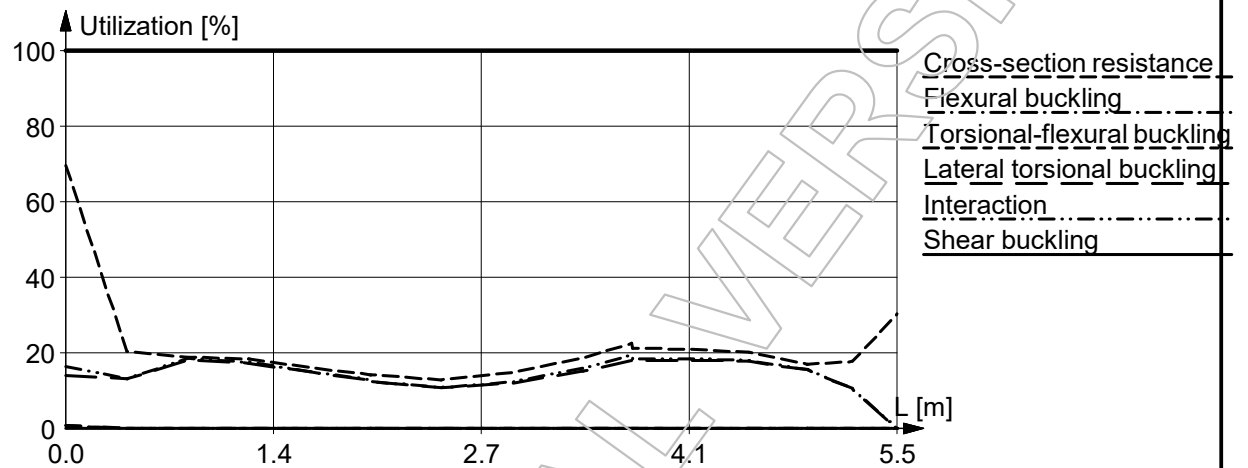
### Interaction between normal force and bending, 2nd order - Part 1-1: 6.3.3

Not relevant

### Shear buckling - Part 1-5: 5

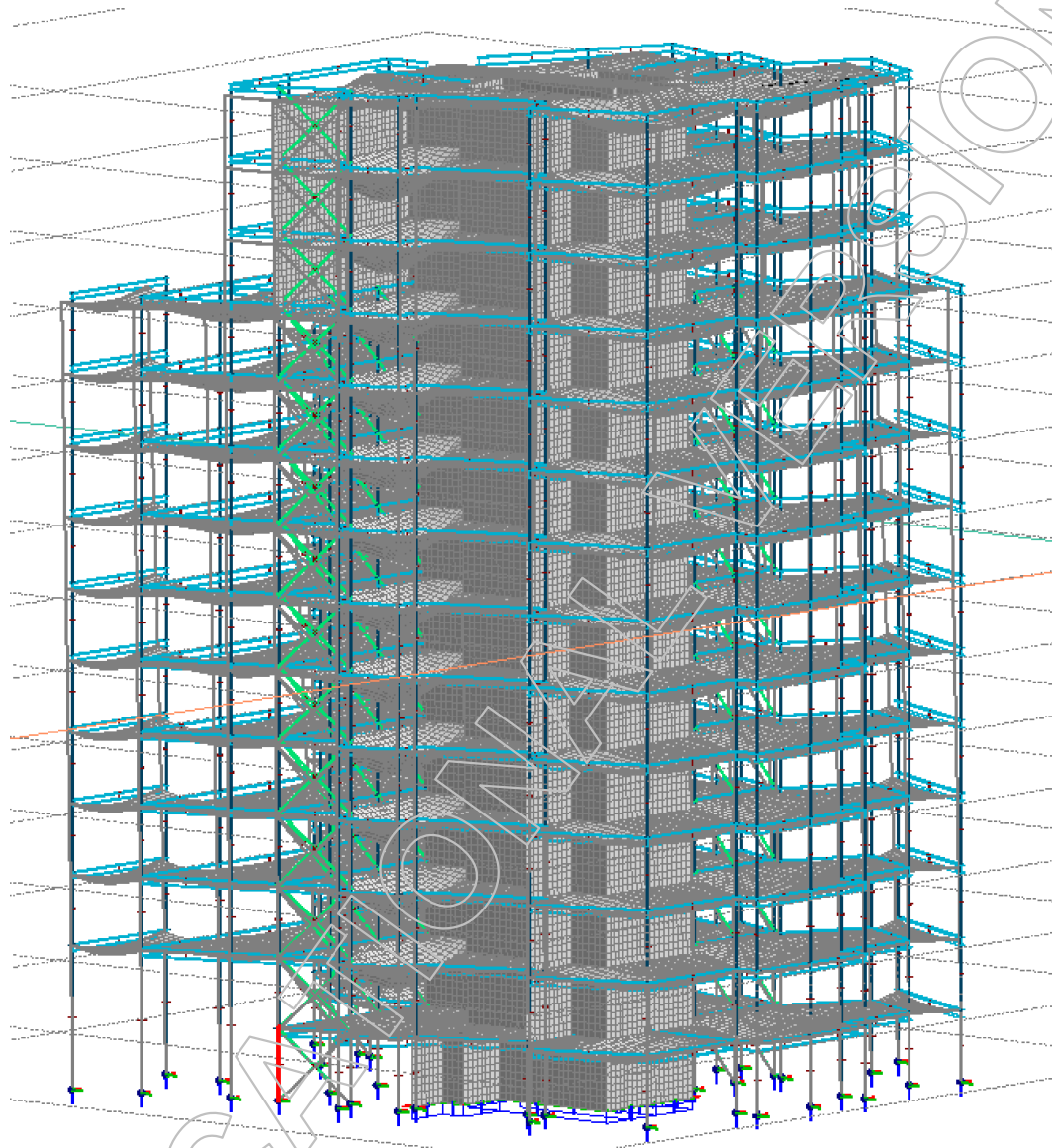
$$\frac{h_w}{t} = \frac{297}{10} = 31.3 \leq \frac{72}{\eta} \cdot \varepsilon = \frac{72}{1.20} \cdot 0.81 = 48.8 \rightarrow \text{Not relevant}$$

### Summary





### 2.3.2 Mest belastet søyle



Den mest belastede søylen er markert i rødt. Søylen er av typen KKR 300x300x10, og har en høyde på 3m

### Indre kræfter og diagrammer

Utnyttelsesgrad

### C.30.1

#### Maximum of load combinations

##### S 355

$$E = 210000 \text{ N/mm}^2$$

$$G = 80769 \text{ N/mm}^2$$

$$Y_{M0,ult} = 1.05$$

$$Y_{M0,acc/seis} = 1.00$$

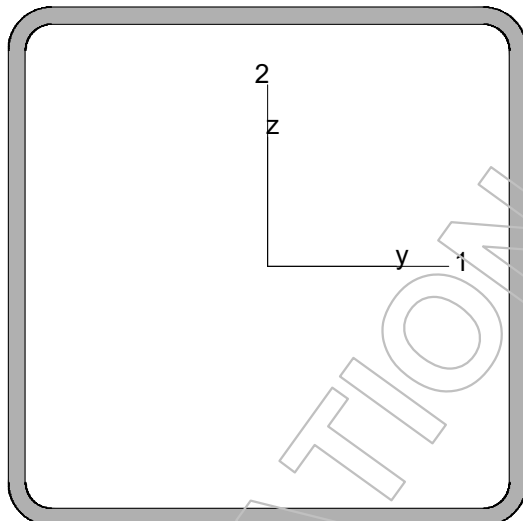
$$Y_{M1,ult} = 1.05$$

$$Y_{M1,acc/seis} = 1.00$$

$$Y_{M2,ult} = 1.25$$

$$Y_{M2,acc/seis} = 1.00$$

##### KKR 300x300x10



$$\begin{aligned} P &= 1157 \text{ mm} & f_y &= 355 \text{ N/mm}^2 \\ A &= 11257 \text{ mm}^2 & \varepsilon &= 0.81 \\ I_y &= 1.552e+08 \text{ mm}^4 & \lambda_1 &= 76.40 \\ I_z &= 1.552e+08 \text{ mm}^4 \\ I_1 &= 1.552e+08 \text{ mm}^4 \\ I_2 &= 1.552e+08 \text{ mm}^4 \\ W_{pl,1} &= 1.211e+06 \text{ mm}^3 \\ W_{pl,2} &= 1.211e+06 \text{ mm}^3 \\ W_{el,min,1} &= 1.035e+06 \text{ mm}^3 \\ W_{el,min,2} &= 1.035e+06 \text{ mm}^3 \\ i_1 &= 117 \text{ mm} \\ i_2 &= 117 \text{ mm} \\ I_t &= 2.500e+08 \text{ mm}^4 \\ I_w &= 1.542e+09 \text{ mm}^6 \end{aligned}$$

**Shear resistance, 1-1 - Part 1-1: 6.2.6, 6.2.8**LC: 'Bruddgrense 1 Evg',  $x = 0$  mmClass<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$V_{1,pl,Rd} = \frac{A_{1,v} \cdot f_y}{\sqrt{3} \cdot Y_{M0}} = \frac{5628 \cdot 355}{\sqrt{3} \cdot 1.05} = 1098.64 \text{ kN} \quad (6.18)$$

$$V_{1,pl,T,Rd} = 1 - \frac{T_{t,Ed}}{(f_y / \sqrt{3}) / Y_{M0}} \cdot V_{1,pl,Rd} =$$

$$= 1 - \frac{0.00}{(355 / \sqrt{3}) / 1.05} \cdot 1098.64 = 1098.64 \text{ kN} \quad (6.28)$$

$$\frac{V_{1,Ed}}{V_{1,pl,T,Rd}} = \frac{0.00}{1098.64} = 0.00 \leq 1.00 \quad (6.25) - \text{OK}$$

**Shear resistance, 2-2 - Part 1-1: 6.2.6, 6.2.8**LC: 'Bruddgrense 1 Evg',  $x = 0$  mmClass<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$V_{2,pl,Rd} = \frac{A_{2,v} \cdot f_y}{\sqrt{3} \cdot Y_{M0}} = \frac{5628 \cdot 355}{\sqrt{3} \cdot 1.05} = 1098.64 \text{ kN} \quad (6.18)$$

$$V_{2,pl,T,Rd} = 1 - \frac{T_{t,Ed}}{(f_y / \sqrt{3}) / Y_{M0}} \cdot V_{2,pl,Rd} =$$

$$= 1 - \frac{0.00}{(355 / \sqrt{3}) / 1.05} \cdot 1098.64 = 1098.64 \text{ kN} \quad (6.28)$$

$$\frac{V_{2,Ed}}{V_{2,pl,T,Rd}} = \frac{0.00}{1098.64} = 0.00 \leq 1.00 \quad (6.25) - \text{OK}$$

**Torsional resistance - Part 1-1: 6.2.7**LC: 'Bruddgrense 1 Evg',  $x = 0$  mmClass<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$T_{\max, \text{unit}} = 0.74 \frac{\text{N/mm}^2}{\text{kN m}} \text{ is calculated by FEM analysis.}$$

$$T_{Rd} = \frac{f_y}{\sqrt{3} \cdot T_{\max, \text{unit}} \cdot Y_{M0}} = \frac{355}{\sqrt{3} \cdot 0.74 \cdot 1.05} = 264.98 \text{ kN m}$$

$$\frac{T_{Ed}}{T_{Rd}} = \frac{0.00}{264.98} = 0.00 \leq 1.00 \quad (6.23) - \text{OK}$$

### Shear stress - Part 1-1: 6.2.6

Not relevant

### Normal stress - Part 1-1: 6.2.1

Not relevant

### Normal capacity - Part 1-1: 6.2

LC: 'Bruddgrense 3 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$V_{1,Ed} = 0.00 \text{ kN} \leq 0.5 \cdot V_{1,pl,T,Rd} = 0.5 \cdot 1098.64 = 549.32 \text{ kN} \rightarrow \rho_1 = 0.00$$

$$V_{2,Ed} = 0.00 \text{ kN} \leq 0.5 \cdot V_{2,pl,T,Rd} = 0.5 \cdot 1098.64 = 549.32 \text{ kN} \rightarrow \rho_1 = 0.00$$

$$\frac{N_{Ed}}{N_{Rd}} + \frac{M_{1,Ed}}{M_{1,Rd}} + \frac{M_{2,Ed}}{M_{2,Rd}} = \frac{3240.07}{3805.82} + \frac{0.00}{409.40} + \frac{0.00}{409.40} = 0.85 \leq 1.00 \quad (6.2) - \text{OK}$$

### Flexural buckling, 1-1 - Part 1-1: 6.3.1

LC: 'Bruddgrense 3 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$\bar{\lambda}_1 = \frac{L_{cr,1}}{i_1 \cdot \lambda_1} = \frac{3000}{117 \cdot 76.40} = 0.33 \quad (6.50)$$

$$\alpha_1 = 0.49 \quad (\text{Buckling curve: c})$$

$$\begin{aligned} \varphi_1 &= 0.5 \left[ 1 + \alpha_1 \cdot (\bar{\lambda}_1 - 0.2) + \bar{\lambda}_1^2 \right] = \\ &= 0.5 \left[ 1 + 0.49 \cdot (0.33 - 0.2) + 0.33^2 \right] = 0.59 \end{aligned}$$

$$\begin{aligned} \chi_1 &= \min \left( \frac{1}{\varphi_1 + \sqrt{\varphi_1^2 - \bar{\lambda}_1^2}}, 1.0 \right) = \\ &= \min \left( \frac{1}{0.59 + \sqrt{0.59^2 - 0.33^2}}, 1.0 \right) = 0.93 \quad (6.49) \end{aligned}$$

$$N_{b,Rd,1} = \frac{\chi_1 \cdot A \cdot f_y}{\gamma_{M1}} = \frac{0.93 \cdot 11257 \cdot 355}{1.05} = 3545.14 \text{ kN} \quad (6.47)$$

$$\frac{N_{Ed}}{N_{b,Rd,1}} = \frac{3240.07}{3545.14} = 0.91 \leq 1.00 \quad (6.46) - \text{OK}$$

### Flexural buckling, 2-2 - Part 1-1: 6.3.1

LC: 'Bruddgrense 3 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$\bar{\lambda}_2 = \frac{L_{cr,2}}{i_2 \cdot \lambda_1} = \frac{3000}{117 \cdot 76.40} = 0.33 \quad (6.50)$$

$\alpha_2 = 0.49$  (Buckling curve: c)

$$\begin{aligned} \varphi_2 &= 0.5 \left[ 1 + \alpha_2 \cdot (\bar{\lambda}_2 - 0.2) + \bar{\lambda}_2^2 \right] = \\ &= 0.5 \left[ 1 + 0.49 \cdot (0.33 - 0.2) + 0.33^2 \right] = 0.59 \end{aligned}$$

$$\begin{aligned} \chi_2 &= \min \left( \frac{1}{\varphi_2 + \sqrt{\varphi_2^2 - \bar{\lambda}_2^2}}, 1.0 \right) = \\ &= \min \left( \frac{1}{0.59 + \sqrt{0.59^2 - 0.33^2}}, 1.0 \right) = 0.93 \quad (6.49) \end{aligned}$$

$$N_{b,Rd,2} = \frac{\chi_2 \cdot A \cdot f_y}{\gamma_{M1}} = \frac{0.93 \cdot 11257 \cdot 355}{1.05} = 3545.14 \text{ kN} \quad (6.47)$$

$$\frac{N_{Ed}}{N_{b,Rd,2}} = \frac{3240.07}{3545.14} = 0.91 \leq 1.00 \quad (6.46) \quad \text{- OK}$$

### Torsional-flexural buckling - Part 1-1: 6.3.1

LC: 'Bruddgrense 3 Nytte',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$i_0 = \sqrt{i_1^2 + i_2^2 + y_0^2 + z_0^2} = \sqrt{117^2 + 117^2 + 0^2 + 0^2} = 166 \text{ mm}$$

$$N_{cr,1} = \frac{\pi^2 \cdot E \cdot I_1}{L_{cr,1}^2} = \frac{\pi^2 \cdot 210000 \cdot 155193808}{3000^2} = 35739.70 \text{ kN}$$

$$N_{cr,2} = \frac{\pi^2 \cdot E \cdot I_2}{L_{cr,2}^2} = \frac{\pi^2 \cdot 210000 \cdot 155193808}{3000^2} = 35739.70 \text{ kN}$$

$$N_{cr,T} = \frac{1}{i_0^2} \left( G \cdot I_t + \frac{\pi^2 \cdot E \cdot I_w}{L_t^2} \right) =$$

$$= \frac{1}{166^2} \left( 80769 \cdot 2.500e+08 + \frac{\pi^2 \cdot 210000 \cdot 1.542e+09}{3000^2} \right) = 732403.32 \text{ kN}$$

$$i_0^2 (N - N_{cr,1}) (N - N_{cr,2}) (N - N_{cr,T}) - N^2 y_0^2 (N - N_{cr,2}) - N^2 z_0^2 (N - N_{cr,1}) =$$

$$= 166^2 (N - 35739.70) (N - 35739.70) (N - 732403.32) - N^2 0^2 (N - 35739.70) - N^2 0^2 (N - 732403.32) = 0$$

Smallest root of the above equation related to the torsional-flexural buckling:

$$N_{cr,TF} = 732403.32 \text{ kN}$$

$$N_{cr} = \min(N_{cr,T}, N_{cr,TF}) = \min(732403.32, 732403.32) = 732403.32 \text{ kN}$$

$$\bar{\lambda}_T = \sqrt{\frac{A \cdot f_y}{N_{cr}}} = \sqrt{\frac{11257 \cdot 355}{732403.32}} = 0.07 \quad (6.53)$$

$$\alpha_T = 0.49 \quad (\text{Buckling curve: c})$$

$$\varphi_T = 0.5 \left[ 1 + \alpha_T (\bar{\lambda}_T - 0.2) + \bar{\lambda}_T^2 \right] =$$

$$= 0.5 \left[ 1 + 0.49 \cdot (0.07 - 0.2) + 0.07^2 \right] = 0.47$$

$$\chi_T = \min \left( \frac{1}{\varphi_T + \sqrt{\varphi_T^2 - \bar{\lambda}_T^2}}, 1.0 \right) =$$

$$= \min \left( \frac{1}{0.47 + \sqrt{0.47^2 - 0.07^2}}, 1.0 \right) = 1.00 \quad (6.49)$$

$$N_{b,Rd,T} = \frac{\chi_T \cdot A \cdot f_y}{Y_{M1}} = \frac{1.00 \cdot 11257 \cdot 355}{1.05} = 3805.82 \text{ kN} \quad (6.47)$$

$$\frac{N_{Ed}}{N_{b,Rd,T}} = \frac{3240.07}{3805.82} = 0.85 \leq 1.00 - \text{OK}$$

### Lateral torsional buckling, top flange - Part 1-1: 6.3.2.2

LC: 'Bruddgrense 1 Evg',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$N_{cr,LT} = \frac{\pi^2 \cdot E \cdot I_z}{(k_z \cdot L_{cr})^2} = \frac{\pi^2 \cdot 2.100e+05 \cdot 1.552e+08}{(1.00 \cdot 3000)^2} = 35739.70 \text{ kN}$$

Loaded on top edge.

$$Z = (C_2 \cdot z_g - C_3 \cdot z_j) = (0.45 \cdot -150 - 0.49 \cdot 0) = -67.50 \text{ mm}$$

$$\begin{aligned} M_{cr} &= C_1 \cdot N_{cr,LT} \cdot \left\{ \left[ \left( \frac{k_z}{k_w} \right)^2 \cdot \frac{I_w}{I_z} + \frac{G \cdot I_t}{N_{cr,LT}} + Z^2 \right]^{0.5} - Z \right\} \\ &= 1.13 \cdot 3.574e+07 \cdot \left\{ \left[ \left( \frac{1.00}{1.00} \right)^2 \cdot \frac{1.542e+09}{1.552e+08} + \frac{8.077e+04 \cdot 2.500e+08}{3.574e+07} + (-67.50)^2 \right]^{0.5} - (-67.50) \right\} \\ &= 33206.45 \text{ kN m} \end{aligned}$$

$$\bar{\lambda}_{LT} = \sqrt{\frac{W_y \cdot f_y}{M_{cr}}} = \sqrt{\frac{1210902 \cdot 355}{3.321e+10}} = 0.11$$

$\alpha_{LT} = 0.76$  (Buckling curve: d)

$$\begin{aligned} \varphi_{LT} &= 0.5 \left[ 1 + \alpha_{LT} \cdot (\bar{\lambda}_{LT} - 0.2) + \bar{\lambda}_{LT}^2 \right] = \\ &= 0.5 \left[ 1 + 0.76 \cdot (0.11 - 0.2) + 0.11^2 \right] = 0.47 \end{aligned}$$

$$\begin{aligned} X_{LT} &= \min \left( \frac{1}{\varphi_{LT} + \sqrt{\varphi_{LT}^2 - \bar{\lambda}_{LT}^2}}, 1.0 \right) = \\ &= \min \left( \frac{1}{0.47 + \sqrt{0.47^2 - 0.11^2}}, 1.0 \right) = 1.00 \quad (6.56) \end{aligned}$$

$$M_{y,b,Rd} = \frac{X_{LT} \cdot W_y \cdot f_y}{\gamma_{M1}} = \frac{1.00 \cdot 1210902 \cdot 355}{1.05} = 409.40 \text{ kN m} \quad (6.55)$$

$$\frac{M_{1,Ed}}{M_{y,b,Rd}} = \frac{0.00}{409.40} = 0.00 \leq 1.00 \quad (6.54) - \text{OK}$$



### Lateral torsional buckling, bottom flange - Part 1-1: 6.3.2.2

LC: 'Bruddgrense 1 Evg',  $x = 0$  mm

Class<sub>N</sub> = 1, Class<sub>M1</sub> = 1, Class<sub>M2</sub> = 1

$$N_{cr,LT} = \frac{\pi^2 \cdot E \cdot I_z}{(k_z \cdot L_{cr})^2} = \frac{\pi^2 \cdot 2.100e+05 \cdot 1.552e+08}{(1.00 \cdot 3000)^2} = 35739.70 \text{ kN}$$

Loaded on top edge.

$$Z = (C_2 \cdot z_g - C_3 \cdot z_j) = (0.45 \cdot -150 - 0.49 \cdot 0) = -67.50 \text{ mm}$$

$$M_{cr} = C_1 \cdot N_{cr,LT} \cdot \left\{ \left[ \left( \frac{k_z}{k_w} \right)^2 \cdot \frac{I_w}{I_z} + \frac{G \cdot I_t}{N_{cr,LT}} + Z^2 \right]^{0.5} - Z \right\} =$$

$$= 1.13 \cdot 3.574e+07 \cdot \left\{ \left[ \left( \frac{1.00}{1.00} \right)^2 \cdot \frac{1.542e+09}{1.552e+08} + \frac{8.077e+04 \cdot 2.500e+08}{3.574e+07} + (-67.50)^2 \right]^{0.5} - (-67.50) \right\}$$

$$= 33206.45 \text{ kN m}$$

$$\bar{\lambda}_{LT} = \sqrt{\frac{W_y \cdot f_y}{M_{cr}}} = \sqrt{\frac{1210902 \cdot 355}{3.321e+10}} = 0.11$$

$\alpha_{LT} = 0.76$  (Buckling curve: d)

$$\varphi_{LT} = 0.5 \left[ 1 + \alpha_{LT} \cdot (\bar{\lambda}_{LT} - 0.2) + \bar{\lambda}_{LT}^2 \right] =$$

$$= 0.5 \left[ 1 + 0.76 \cdot (0.11 - 0.2) + 0.11^2 \right] = 0.47$$

$$X_{LT} = \min \left( \frac{1}{\varphi_{LT} + \sqrt{\varphi_{LT}^2 - \bar{\lambda}_{LT}^2}}, 1.0 \right) =$$

$$= \min \left( \frac{1}{0.47 + \sqrt{0.47^2 - 0.11^2}}, 1.0 \right) = 1.00 \quad (6.56)$$

$$M_{y,b,Rd} = \frac{X_{LT} \cdot W_y \cdot f_y}{\gamma_{M1}} = \frac{1.00 \cdot 1210902 \cdot 355}{1.05} = 409.40 \text{ kN m} \quad (6.55)$$

$$\frac{M_{1,Ed}}{M_{y,b,Rd}} = \frac{0.00}{409.40} = 0.00 \leq 1.00 \quad (6.54) \text{ - OK}$$

### Interaction between normal force and bending 1. - Part 1-1: 6.3.3

Not relevant

### Interaction between normal force and bending 2. - Part 1-1: 6.3.3

Not relevant

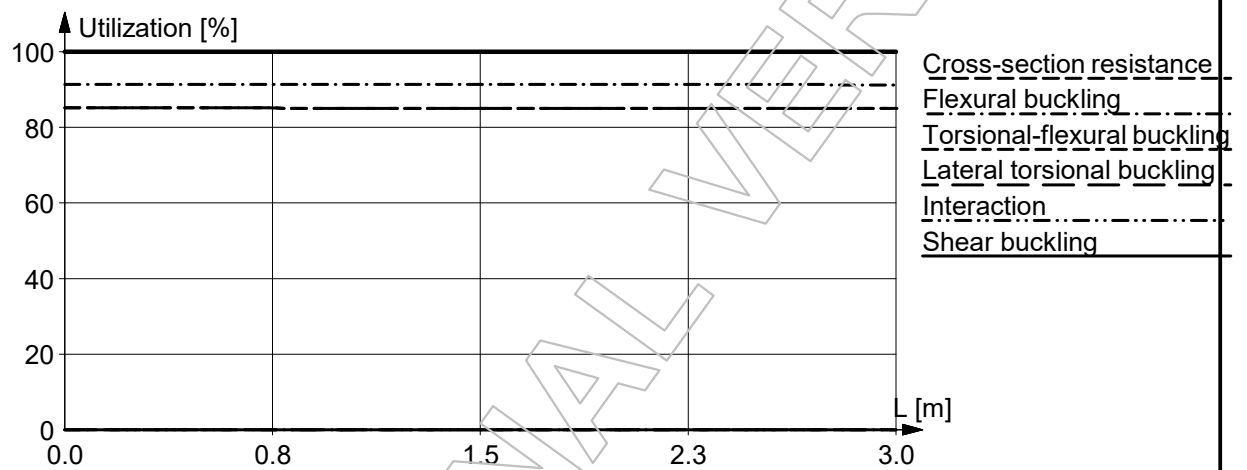
### Interaction between normal force and bending, 2nd order - Part 1-1: 6.3.3

Not relevant

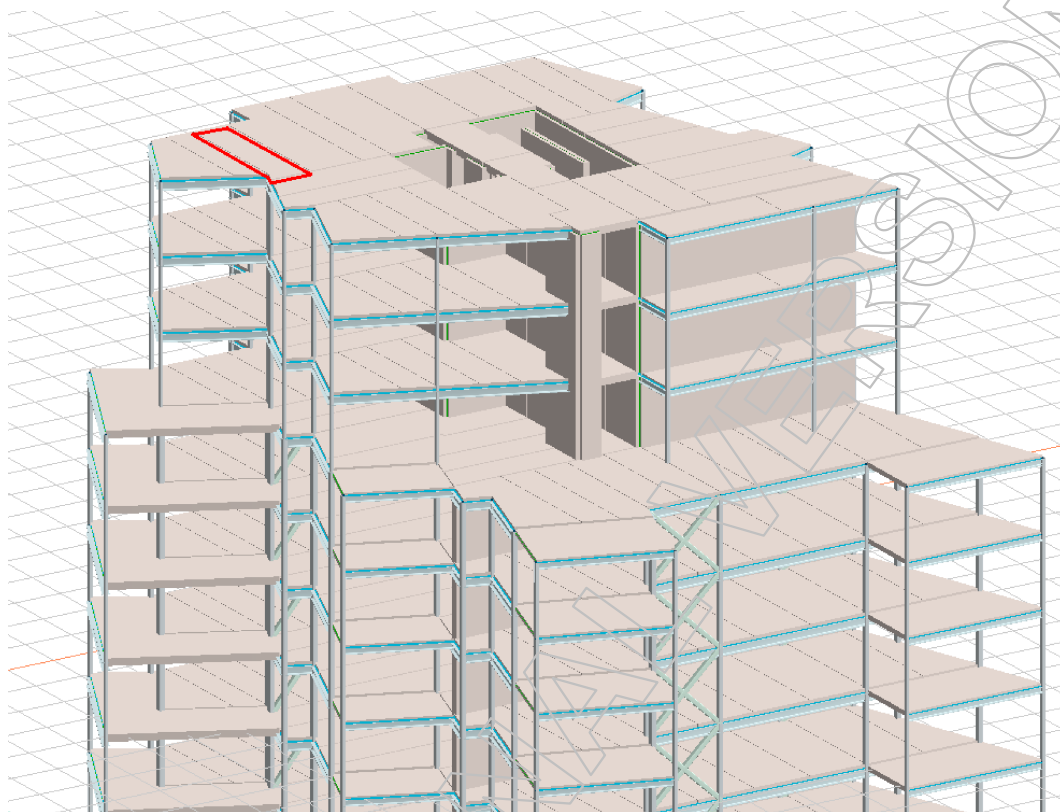
### Shear buckling - Part 1-5: 5

$$\frac{h_w}{t} = \frac{280}{10} = 28.0 \leq \frac{72}{\eta} \cdot \varepsilon = \frac{72}{1.20} \cdot 0.81 = 48.8 \rightarrow \text{Not relevant}$$

### Summary



### 2.3.3 Mest belastet CLT-dekke



Mest belastet CLT-dekke er markert i rødt, og ligger i etasje 14.

Utnyttelsesgrad

## TP.738

### Maximum of load combinations

#### CLT 300 L8s-2

Service class: 1,  $Y_{M,ult.} = 1.30$ ,  $Y_{M,acc./seis.} = 1.00$ ,  $k_{sys} = 1.00$

$t$	$=$	300 mm	$f_{m,0,k}$	$=$	22.02 N/mm <sup>2</sup>
$E_{0,mean}$	$=$	11467.00 N/mm <sup>2</sup>	$f_{m,90,k}$	$=$	4.25 N/mm <sup>2</sup>
$E_{90,mean}$	$=$	1033.00 N/mm <sup>2</sup>	$f_{t,0,k}$	$=$	11.20 N/mm <sup>2</sup>
$E_{0,t}$	$=$	10000.00 N/mm <sup>2</sup>	$f_{t,90,k}$	$=$	2.80 N/mm <sup>2</sup>
$E_{90,t}$	$=$	2500.00 N/mm <sup>2</sup>	$f_{c,0,k}$	$=$	16.80 N/mm <sup>2</sup>
$E_{0,c}$	$=$	10000.00 N/mm <sup>2</sup>	$f_{c,90,k}$	$=$	4.20 N/mm <sup>2</sup>
$E_{90,c}$	$=$	2500.00 N/mm <sup>2</sup>	$f_{v,k}$	$=$	1.35 N/mm <sup>2</sup>
$G_0$	$=$	155.00 N/mm <sup>2</sup>	$f_{r,0,k}$	$=$	1.35 N/mm <sup>2</sup>
$G_{90}$	$=$	155.00 N/mm <sup>2</sup>	$f_{r,90,k}$	$=$	0.65 N/mm <sup>2</sup>

#### Tension and bending, x - 6.2.3

Panel: 'TP.738.1', LC: 'Bruddgrense 3 Nytte',

$k_{mod} = 0.90$ , Coordinates [m]:{ 8.51; 14.03; 42.00}

$$\frac{|\sigma_{t,0,d}|}{f_{td,x}} + \frac{|\sigma_{m,x}|}{f_{md,x}} = \frac{|0.01|}{7.75} + \frac{|-3.81|}{15.24} = 0.25 \leq 1.00 \quad (6.17) - \text{OK}$$

#### Tension and bending, y - 6.2.3

Panel: 'TP.738.1', LC: 'Bruddgrense 2 Evg',

$k_{mod} = 0.90$ , Coordinates [m]:{ 8.62; 14.43; 42.00}

$$\frac{|\sigma_{t,90,d}|}{f_{td,y}} + \frac{|\sigma_{m,y}|}{f_{md,y}} = \frac{|0.04|}{1.94} + \frac{|0.35|}{2.94} = 0.14 \leq 1.00 \quad (6.17) - \text{OK}$$

#### Compression and bending, x - 6.1.4, 6.2.4

Panel: 'TP.738.1', LC: 'Bruddgrense 1 Evg',

$k_{mod} = 0.90$ , Coordinates [m]:{ 6.68; 15.53; 42.00}

$$\frac{\sigma_{c,0,d}}{f_{cd,x}} = \frac{0.00}{11.63} = 0.00 \leq 1.00 \quad (6.2) - \text{OK}$$

$$\left( \frac{\sigma_{c,0,d}}{f_{cd,x}} \right)^2 + \frac{\sigma_{m,x}}{f_{md,x}} = \left( \frac{0.00}{11.63} \right)^2 + \frac{3.60}{15.24} = 0.24 \leq 1.00 \quad (6.19) - \text{OK}$$

### Compression and bending, y - 6.1.4, 6.2.4

Panel: 'TP.738.1', LC: 'Bruddgrense 1 Evg',

$k_{mod} = 0.90$ , Coordinates [m]:{ 8.62; 14.43; 42.00}

$$\frac{\sigma_{c,90,d}}{f_{cd,y}} = \frac{0.03}{2.91} = 0.01 \leq 1.00 \quad (6.2) - \text{OK}$$

$$\left( \frac{\sigma_{c,90,d}}{f_{cd,y}} \right)^2 + \frac{\sigma_{m,y}}{f_{md,y}} = \left( \frac{0.03}{2.91} \right)^2 + \frac{0.52}{2.94} = 0.18 \leq 1.00 \quad (6.19) - \text{OK}$$

### Shear, xy - 6.1.7

Panel: 'TP.738.1', LC: 'Bruddgrense 3 Nytte',

$k_{mod} = 0.90$ , Coordinates [m]:{ 8.80; 13.97; 42.00}

$$\frac{T_{xy}}{1000 \text{ mm} \cdot t \cdot f_{v,d}} = \frac{133892.03}{1000 \text{ mm} \cdot 300 \cdot 0.93} = 0.48 \leq 1.00 \quad (6.13) - \text{OK}$$

### Shear, xz - 6.1.7

Panel: 'TP.738.1', LC: 'Bruddgrense 3 Nytte',

$k_{mod} = 0.90$ , Coordinates [m]:{ 8.80; 14.04; 42.00}

$$\frac{1.50 \cdot T_{xz}}{1000 \text{ mm} \cdot t \cdot f_{r,d,x}} = \frac{1.50 \cdot 170446.63}{1000 \text{ mm} \cdot 300 \cdot 0.93} = 0.91 \leq 1.00 \quad (6.13) - \text{OK}$$

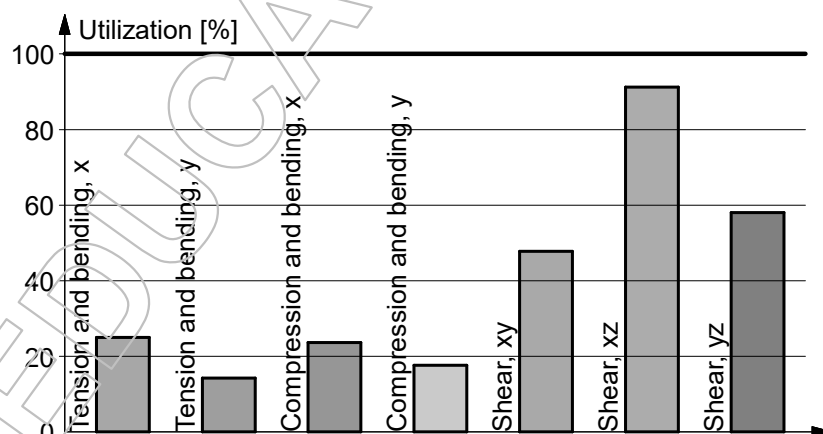
### Shear, yz - 6.1.7

Panel: 'TP.738.1', LC: 'Bruddgrense 1 Evg',

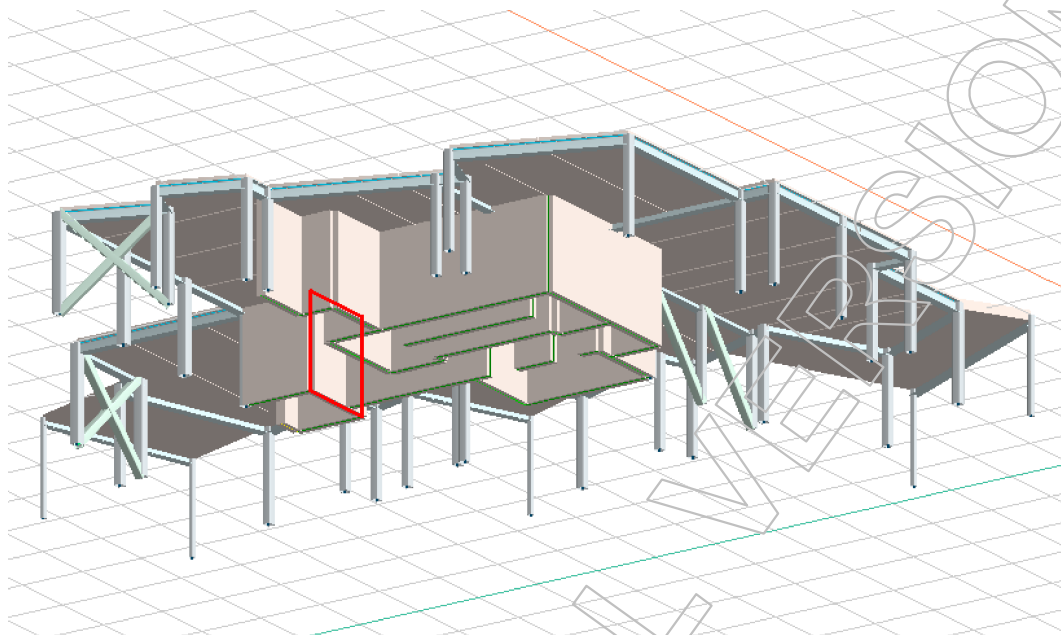
$k_{mod} = 0.90$ , Coordinates [m]:{ 8.51; 14.03; 42.00}

$$\frac{1.50 \cdot T_{yz}}{1000 \text{ mm} \cdot t \cdot f_{r,d,y}} = \frac{1.50 \cdot 52284.87}{1000 \text{ mm} \cdot 300 \cdot 0.45} = 0.58 \leq 1.00 \quad (6.13) - \text{OK}$$

### Summary



### 2.3.4 Mest belastet CLT-vegg



Mest belastet CLT-vegg er markert i rødt. Den aktuelle veggen ligger i etasje 1. Bildet er tatt fra undersiden av etasje 1.

Utnyttelsesgrad

## TP.8

### Maximum of load combinations

#### CLT 300 L8s-2

Service class: 1,  $Y_{M,ult.} = 1.30$ ,  $Y_{M,acc./seis.} = 1.00$ ,  $k_{sys} = 1.00$

$t$	$=$	300 mm	$f_{m,0,k}$	$=$	22.02 N/mm <sup>2</sup>
$E_{0,mean}$	$=$	11467.00 N/mm <sup>2</sup>	$f_{m,90,k}$	$=$	4.25 N/mm <sup>2</sup>
$E_{90,mean}$	$=$	1033.00 N/mm <sup>2</sup>	$f_{t,0,k}$	$=$	11.20 N/mm <sup>2</sup>
$E_{0,t}$	$=$	10000.00 N/mm <sup>2</sup>	$f_{t,90,k}$	$=$	2.80 N/mm <sup>2</sup>
$E_{90,t}$	$=$	2500.00 N/mm <sup>2</sup>	$f_{c,0,k}$	$=$	16.80 N/mm <sup>2</sup>
$E_{0,c}$	$=$	10000.00 N/mm <sup>2</sup>	$f_{c,90,k}$	$=$	4.20 N/mm <sup>2</sup>
$E_{90,c}$	$=$	2500.00 N/mm <sup>2</sup>	$f_{v,k}$	$=$	1.35 N/mm <sup>2</sup>
$G_0$	$=$	155.00 N/mm <sup>2</sup>	$f_{r,0,k}$	$=$	1.35 N/mm <sup>2</sup>
$G_{90}$	$=$	155.00 N/mm <sup>2</sup>	$f_{r,90,k}$	$=$	0.65 N/mm <sup>2</sup>

#### Tension and bending, x - 6.2.3

Panel: 'TP.8.1', LC: 'Vind +',  $k_{mod} = 0.90$ , Coordinates [m]:{ 17.77; 20.63; -0.00}

$$\frac{|\sigma_{t,0,d}|}{f_{td,x}} + \frac{|\sigma_{m,x}|}{f_{md,x}} = \frac{2.44}{7.75} + \frac{0.00}{15.24} = 0.31 \leq 1.00 \quad (6.17) - \text{OK}$$

#### Tension and bending, y - 6.2.3

Panel: 'TP.8.1', LC: 'Bruddgrense 4 Nytte',  $k_{mod} = 0.90$ , Coordinates [m]:{ 17.77; 20.63; 3.00}

$$\frac{|\sigma_{t,90,d}|}{f_{td,y}} + \frac{|\sigma_{m,y}|}{f_{md,y}} = \frac{0.50}{1.94} + \frac{0.00}{2.94} = 0.26 \leq 1.00 \quad (6.17) - \text{OK}$$

#### Compression and bending, x - 6.1.4, 6.2.4

Panel: 'TP.8.1', LC: 'Bruddgrense 4 Nytte',  $k_{mod} = 0.90$ , Coordinates [m]:{ 17.77; 20.63; -0.00}

$$\frac{\sigma_{c,0,d}}{f_{cd,x}} = \frac{5.26}{11.63} = 0.45 \leq 1.00 \quad (6.2) - \text{OK}$$

$$\left( \frac{\sigma_{c,0,d}}{f_{cd,x}} \right)^2 + \frac{\sigma_{m,x}}{f_{md,x}} = \left( \frac{5.26}{11.63} \right)^2 + \frac{0.00}{15.24} = 0.20 \leq 1.00 \quad (6.19) - \text{OK}$$

### Compression and bending, y - 6.1.4, 6.2.4

Panel: 'TP.8.1', LC: 'Vind +',  $k_{mod} = 0.90$ , Coordinates [m]:{ 17.77; 20.63; 3.00}

$$\frac{\sigma_{c,90,d}}{f_{cd,y}} = \frac{0.57}{2.91} = 0.20 \leq 1.00 \quad (6.2) - \text{OK}$$

$$\left( \frac{\sigma_{c,90,d}}{f_{cd,y}} \right)^2 + \frac{\sigma_{m,y}}{f_{md,y}} = \left( \frac{0.57}{2.91} \right)^2 + \frac{0.00}{2.94} = 0.04 \leq 1.00 \quad (6.19) - \text{OK}$$

### Shear, xy - 6.1.7

Panel: 'TP.8.1', LC: 'Bruddgrense 4 Nytte',  $k_{mod} = 0.90$ , Coordinates [m]:{ 17.77; 23.23; 3.00}

$$\frac{T_{xy}}{1000 \text{ mm} \cdot t \cdot f_{v,d}} = \frac{264504.44}{1000 \text{ mm} \cdot 300 \cdot 0.93} = 0.94 \leq 1.00 \quad (6.13) - \text{OK}$$

### Shear, xz - 6.1.7

Panel: 'TP.8.1', LC: 'Bruddgrense 4 Nytte',  $k_{mod} = 0.90$ , Coordinates [m]:{ 17.77; 21.48; 3.00}

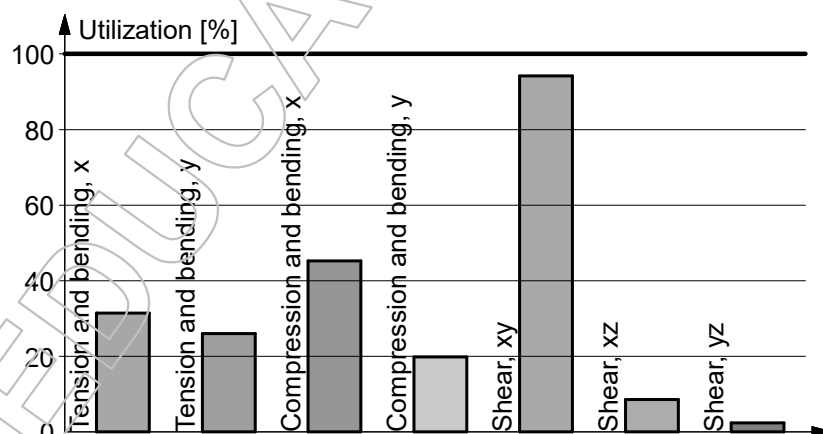
$$\frac{1.50 \cdot T_{xz}}{1000 \text{ mm} \cdot t \cdot f_{r,d,x}} = \frac{1.50 \cdot 16115.42}{1000 \text{ mm} \cdot 300 \cdot 0.93} = 0.09 \leq 1.00 \quad (6.13) - \text{OK}$$

### Shear, yz - 6.1.7

Panel: 'TP.8.1', LC: 'Bruddgrense 4 Nytte',  $k_{mod} = 0.90$ , Coordinates [m]:{ 17.77; 21.48; 3.00}

$$\frac{1.50 \cdot T_{yz}}{1000 \text{ mm} \cdot t \cdot f_{r,d,y}} = \frac{1.50 \cdot 2144.29}{1000 \text{ mm} \cdot 300 \cdot 0.45} = 0.02 \leq 1.00 \quad (6.13) - \text{OK}$$

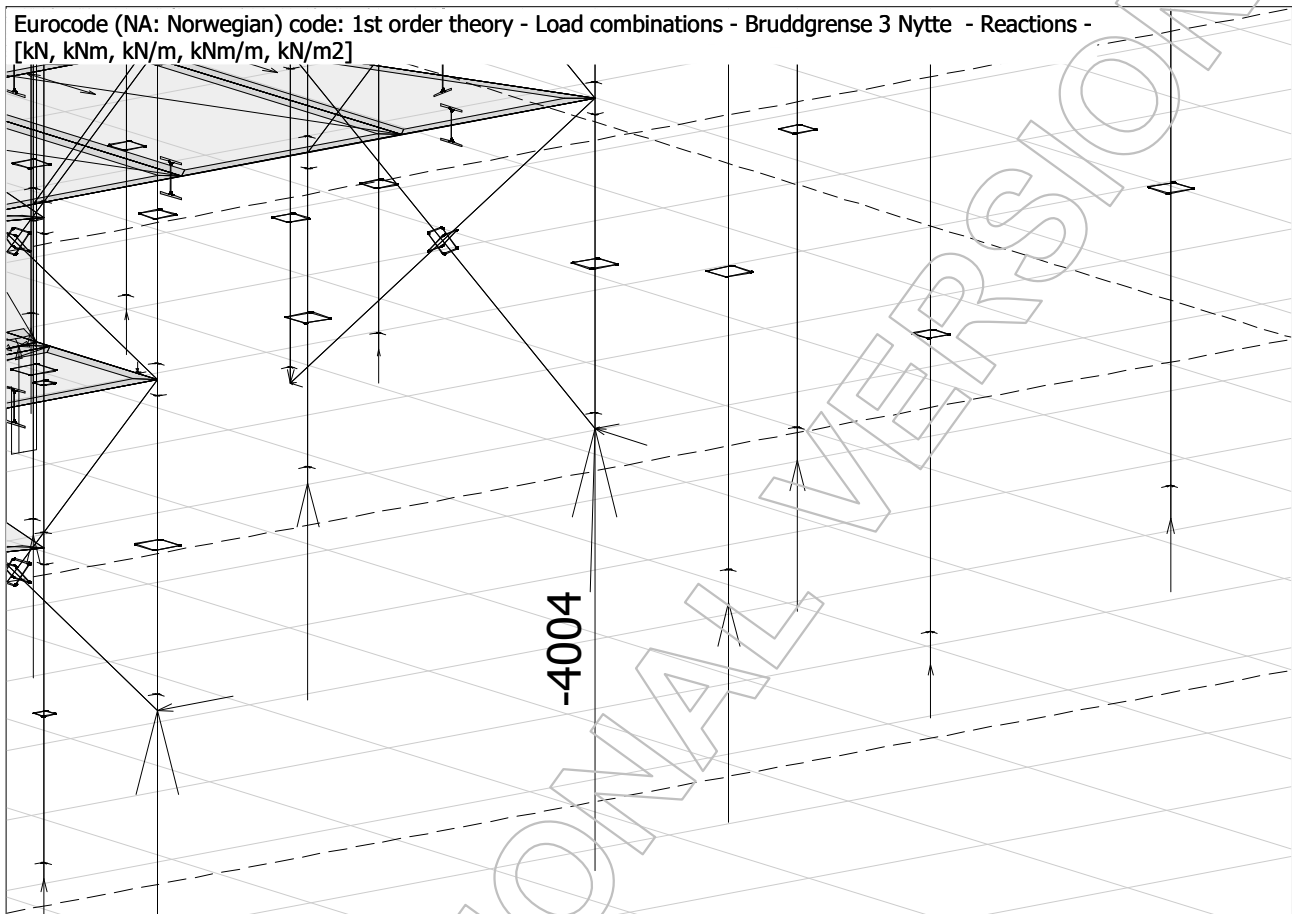
### Summary





### 2.3.5 Trykkraft i fundament

Eurocode (NA: Norwegian) code: 1st order theory - Load combinations - Bruddgrense 3 Nytte - Reactions -  
[kN, kNm, kN/m, kNm/m, kN/m<sup>2</sup>]

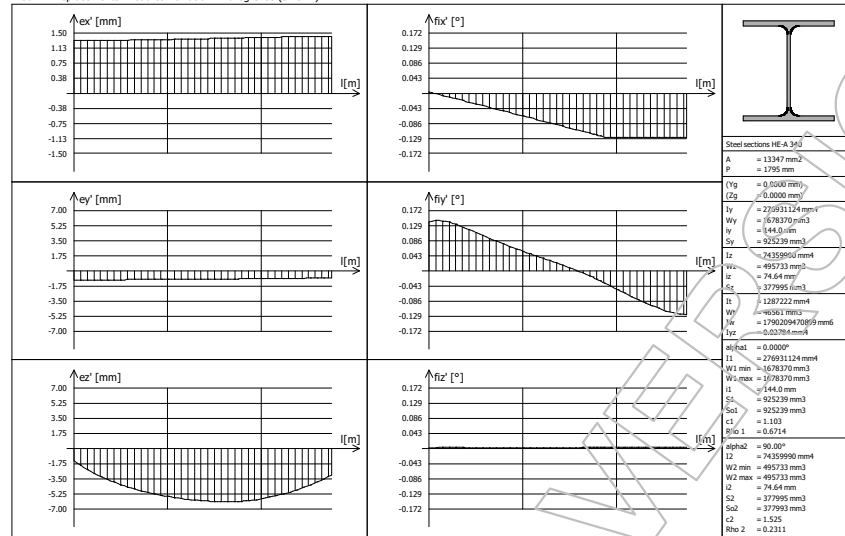


### 2.4 Bruksgrensetilstand

#### 2.4.1 Mest belastet bjelke

Nedbøyning

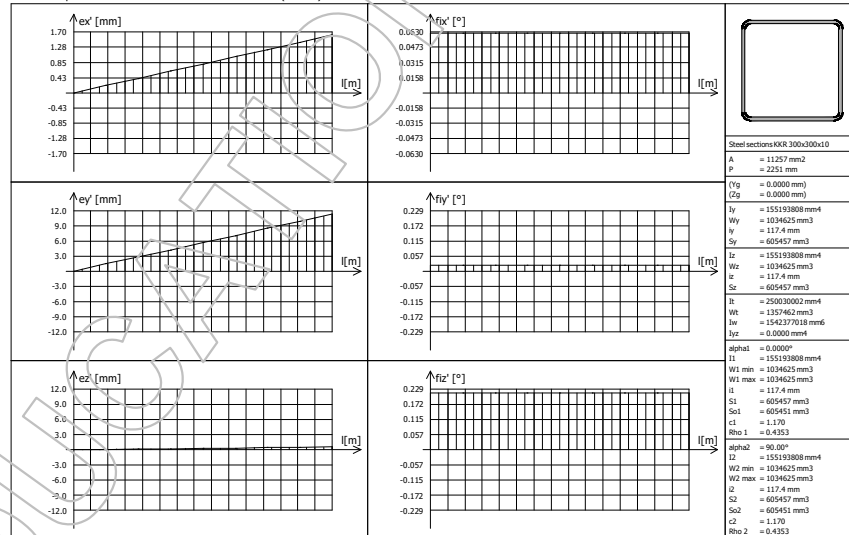
B.58.1 - Displacements - Load combination: Bruksgrense (5.49 m)



## 2.4.2 Mest belastet søyle

### Utbøyning

C.30.1 - Displacements - Max. of load combinations: U - (3.00 m)



## 2.5 Check for utnyttelse

### 2.5.1 Check Steel Design

Max. of load combinations, Bar, Utilization

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.1.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.2.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.3.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.4.1	HE-A 340	Real	12	Bruddgrens...	12	1
B.5.1	HE-A 340	Real	6	Vind +	6	1
B.6.1	HE-A 340	Real	8	Bruddgrens...	7	1
B.7.1	HE-A 340	Real	9	Bruddgrens...	8	1
B.8.1	HE-A 340	Real	17	Vind +	17	3
B.9.1	HE-A 340	Real	17	Vind +	17	2
B.10.1	HE-A 340	Real	19	Bruddgrens...	15	3
B.11.1	HE-A 340	Real	17	Bruddgrens...	17	-
B.12.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.13.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.14.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.15.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.16.1	HE-A 340	Real	10	Vind +	10	2
B.17.1	HE-A 340	Real	22	Bruddgrens...	22	3
B.18.1	HE-A 340	Real	14	Bruddgrens...	13	0
B.19.1	HE-A 340	Real	6	Vind +	6	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	12	9	-	12
1	0	0	-	6
1	7	0	-	8
1	8	0	-	9
3	0	0	-	11
2	8	0	-	17
3	17	0	-	19
-	1	0	-	9
0	8	0	-	8
0	5	4	-	5
0	3	4	-	4
0	0	5	-	6
2	0	0	-	10
3	21	0	-	22
0	14	0	-	14
0	1	0	-	6

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.20.1	HE-A 340	Real	8	Bruddgrens...	8	2
B.21.1	HE-A 340	Real	12	Bruddgrens...	12	4
B.22.1	HE-A 340	Real	7	Vind +	7	1
B.23.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.24.1	HE-A 340	Real	5	Vind +	5	0
B.25.1	HE-A 340	Real	18	Bruddgrens...	18	-
B.26.1	HE-A 340	Real	40	Bruddgrens...	40	2
B.27.1	HE-A 340	Real	20	Bruddgrens...	20	3
B.28.1	HE-A 340	Real	51	Bruddgrens...	51	1
B.29.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.30.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.31.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.32.1	HE-A 340	Real	7	Vind +	7	1
B.33.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.34.1	HE-A 340	Real	9	Bruddgrens...	8	1
B.35.1	HE-A 340	Real	10	Vind +	10	1
B.36.1	HE-A 340	Real	10	Vind +	10	1
B.37.1	HE-A 340	Real	24	Bruddgrens...	23	2
B.38.1	HE-A 340	Real	27	Bruddgrens...	27	-
B.39.1	HE-A 340	Real	8	Bruddgrens...	8	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
2	-	5	-	6
4	5	5	-	10
1	0	0	-	7
0	1	0	-	3
0	0	0	-	5
-	1	0	-	5
2	6	17	-	21
3	6	0	-	16
1	19	0	-	20
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	0	0	-	7
1	7	0	-	8
1	8	0	-	9
1	0	0	-	10
1	1	0	-	10
2	22	0	-	24
-	6	18	-	19
0	8	0	-	8

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.40.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.41.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.42.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.43.1	HE-A 340	Real	15	Vind +	15	2
B.44.1	HE-A 340	Real	5	Bruddgrens...	4	1
B.45.1	HE-A 340	Real	3	Vind +	3	0
B.46.1	HE-A 340	Real	6	Bruddgrens...	6	2
B.47.1	HE-A 340	Real	10	Bruddgrens...	10	2
B.48.1	HE-A 340	Real	5	Vind +	5	1
B.49.1	HE-A 340	Real	4	Vind +	4	0
B.50.1	HE-A 340	Real	8	Vind +	8	1
B.51.1	HE-A 340	Real	35	Bruddgrens...	35	-
B.52.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.53.1	HE-A 340	Real	13	Vind +	13	1
B.54.1	HE-A 340	Real	26	Bruddgrens...	26	6
B.55.1	HE-A 340	Real	19	Bruddgrens...	19	2
B.56.1	HE-A 340	Real	36	Vind +	36	3
B.57.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.58.1	HE-A 340	Real	70	Bruddgrens...	70	1
B.59.1	HE-A 340	Real	2	Bruddgrens...	2	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	6	2	-	6
0	4	2	-	4
0	0	0	-	1
2	0	0	-	14
0	4	0	-	5
0	1	0	-	3
2	3	1	-	5
2	8	1	-	9
1	0	0	-	5
0	3	0	-	4
1	1	0	-	8
-	22	21	-	23
1	5	0	-	6
1	-	3	-	12
6	12	18	-	22
2	12	17	-	18
3	21	20	-	32
1	3	7	-	7
1	18	14	-	20
0	0	0	-	1

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.60.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.61.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.62.1	HE-A 340	Real	16	Bruddgrens...	16	1
B.63.1	HE-A 340	Real	6	Vind +	6	1
B.64.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.65.1	HE-A 340	Real	9	Bruddgrens...	8	1
B.66.1	HE-A 340	Real	5	Vind +	5	1
B.67.1	HE-A 340	Real	4	Bruddgrens...	4	1
B.68.1	HE-A 340	Real	23	Bruddgrens...	22	1
B.69.1	HE-A 340	Real	27	Bruddgrens...	27	-
B.70.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.71.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.72.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.73.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.74.1	HE-A 340	Real	12	Bruddgrens...	12	2
B.75.1	HE-A 340	Real	4	Bruddgrens...	4	1
B.76.1	HE-A 340	Real	2	Vind +	2	0
B.77.1	HE-A 340	Real	6	Bruddgrens...	6	1
B.78.1	HE-A 340	Real	10	Bruddgrens...	10	1
B.79.1	HE-A 340	Real	3	Bruddgrens...	3	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	6	0	-	7
0	6	0	-	7
1	15	12	-	15
1	0	0	-	4
1	7	0	-	7
1	8	0	-	9
1	0	0	-	5
1	1	0	-	4
1	22	0	-	23
-	6	19	-	20
0	8	0	-	8
0	6	1	-	6
0	5	1	-	5
0	0	-	-	0
2	0	0	-	11
0	4	0	-	4
0	1	0	-	2
1	4	2	-	4
1	9	2	-	9
0	0	0	-	3

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.80.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.81.1	HE-A 340	Real	6	Vind +	6	1
B.82.1	HE-A 340	Real	38	Bruddgrens...	38	-
B.83.1	HE-A 340	Real	15	Bruddgrens...	15	1
B.84.1	HE-A 340	Real	16	Bruddgrens...	16	1
B.85.1	HE-A 340	Real	23	Bruddgrens...	23	3
B.86.1	HE-A 340	Real	16	Bruddgrens...	16	1
B.87.1	HE-A 340	Real	29	Vind +	29	2
B.88.1	HE-A 340	Real	9	Bruddgrens...	9	1
B.89.1	HE-A 340	Real	15	Bruddgrens...	15	1
B.90.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.91.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.92.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.93.1	HE-A 340	Real	16	Bruddgrens...	16	1
B.94.1	HE-A 340	Real	6	Vind +	6	1
B.95.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.96.1	HE-A 340	Real	9	Bruddgrens...	7	1
B.97.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.98.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.99.1	HE-A 340	Real	23	Bruddgrens...	22	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	3	0	-	4
1	1	0	-	6
-	26	24	-	28
1	14	0	-	14
1	13	0	-	15
3	13	19	-	19
1	13	16	-	16
2	26	23	-	27
1	3	9	-	9
1	14	11	-	15
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	15	12	-	15
1	0	0	-	4
1	7	0	-	7
1	8	0	-	9
0	0	0	-	2
0	1	0	-	2
1	22	0	-	23

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.100.1	HE-A 340	Real	27	Bruddgrens...	27	-
B.101.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.102.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.103.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.104.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.105.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.106.1	HE-A 340	Real	12	Bruddgrens...	12	1
B.107.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.108.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.109.1	HE-A 340	Real	5	Vind +	5	1
B.110.1	HE-A 340	Real	9	Bruddgrens...	9	1
B.111.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.112.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.113.1	HE-A 340	Real	4	Vind +	4	1
B.114.1	HE-A 340	Real	41	Bruddgrens...	41	-
B.115.1	HE-A 340	Real	15	Bruddgrens...	15	0
B.116.1	HE-A 340	Real	15	Bruddgrens...	15	0
B.117.1	HE-A 340	Real	20	Bruddgrens...	20	1
B.118.1	HE-A 340	Real	14	Bruddgrens...	14	0
B.119.1	HE-A 340	Real	33	Vind +	33	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
-	5	20	-	20
0	8	0	-	8
0	7	0	-	7
0	6	0	-	6
0	0	-	-	1
0	13	0	-	13
1	0	0	-	9
0	4	0	-	4
0	1	0	-	2
1	4	3	-	4
1	8	3	-	9
0	0	0	-	2
0	3	0	-	3
1	1	0	-	4
-	28	25	-	32
0	14	0	-	15
0	14	0	-	14
1	13	20	-	17
0	14	14	-	14
1	28	24	-	31



Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.120.1	HE-A 340	Real	9	Bruddgrens...	9	1
B.121.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.122.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.123.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.124.1	HE-A 340	Real	15	Bruddgrens...	15	1
B.125.1	HE-A 340	Real	6	Vind +	6	1
B.126.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.127.1	HE-A 340	Real	8	Bruddgrens...	7	1
B.128.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.129.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.130.1	HE-A 340	Real	23	Bruddgrens...	22	1
B.131.1	HE-A 340	Real	26	Bruddgrens...	26	-
B.132.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.133.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.134.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.135.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.136.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.137.1	HE-A 340	Real	11	Bruddgrens...	11	1
B.138.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.139.1	HE-A 340	Real	2	Bruddgrens...	2	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
1	2	9	-	9
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	14	11	-	15
1	0	0	-	4
1	7	0	-	8
1	8	0	-	8
0	0	0	-	1
0	1	0	-	1
1	22	0	-	23
-	4	19	-	19
0	8	0	-	8
0	8	0	-	8
0	6	0	-	7
0	0	-	-	2
0	13	0	-	13
1	0	0	-	8
0	4	0	-	4
0	1	0	-	2

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.140.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.141.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.142.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.143.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.144.1	HE-A 340	Real	4	Vind +	4	0
B.145.1	HE-A 340	Real	42	Bruddgrens...	42	-
B.146.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.147.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.148.1	HE-A 340	Real	20	Bruddgrens...	20	1
B.149.1	HE-A 340	Real	14	Bruddgrens...	14	1
B.150.1	HE-A 340	Real	36	Vind +	36	1
B.151.1	HE-A 340	Real	9	Bruddgrens...	9	1
B.152.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.153.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.154.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.155.1	HE-A 340	Real	14	Bruddgrens...	14	1
B.156.1	HE-A 340	Real	5	Vind +	5	1
B.157.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.158.1	HE-A 340	Real	8	Bruddgrens...	7	1
B.159.1	HE-A 340	Real	5	Bruddgrens...	5	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	3	4	-	4
0	8	4	-	8
0	0	0	-	1
0	3	0	-	3
0	1	0	-	3
-	29	24	-	33
0	13	0	-	13
0	13	0	-	10
1	12	19	-	19
1	14	12	-	14
1	28	24	-	33
1	1	8	-	9
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	13	10	-	14
1	0	0	-	4
1	7	0	-	7
1	8	0	-	8
0	0	0	-	1

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.160.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.161.1	HE-A 340	Real	22	Bruddgrens...	22	1
B.162.1	HE-A 340	Real	25	Bruddgrens...	25	-
B.163.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.164.1	HE-A 340	Real	9	Bruddgrens...	9	0
B.165.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.166.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.167.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.168.1	HE-A 340	Real	11	Bruddgrens...	11	1
B.169.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.170.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.171.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.172.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.173.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.174.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.175.1	HE-A 340	Real	4	Vind +	4	0
B.176.1	HE-A 340	Real	40	Bruddgrens...	40	-
B.177.1	HE-A 340	Real	12	Bruddgrens...	12	0
B.178.1	HE-A 340	Real	12	Bruddgrens...	12	0
B.179.1	HE-A 340	Real	20	Bruddgrens...	20	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	1	0	-	1
1	22	0	-	22
-	3	19	-	19
0	8	0	-	8
0	8	0	-	9
0	7	0	-	7
0	0	-	-	2
0	13	0	-	13
1	0	0	-	7
0	4	0	-	4
0	1	0	-	1
0	2	4	-	4
0	7	4	-	7
0	0	0	-	1
0	3	0	-	3
0	1	0	-	2
-	28	22	-	33
0	12	1	-	12
0	11	1	-	9
1	12	19	-	19

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.180.1	HE-A 340	Real	15	Bruddgrens...	15	1
B.181.1	HE-A 340	Real	36	Vind +	36	1
B.182.1	HE-A 340	Real	9	Bruddgrens...	9	1
B.183.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.184.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.185.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.186.1	HE-A 340	Real	13	Bruddgrens...	13	1
B.187.1	HE-A 340	Real	5	Vind +	5	1
B.188.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.189.1	HE-A 340	Real	8	Bruddgrens...	7	1
B.190.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.191.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.192.1	HE-A 340	Real	22	Bruddgrens...	22	1
B.193.1	HE-A 340	Real	24	Bruddgrens...	24	-
B.194.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.195.1	HE-A 340	Real	9	Bruddgrens...	9	0
B.196.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.197.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.198.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.199.1	HE-A 340	Real	11	Bruddgrens...	11	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
1	15	10	-	15
1	27	22	-	33
1	0	8	-	8
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	12	9	-	13
1	0	0	-	4
1	7	0	-	7
1	8	0	-	8
0	0	0	-	1
0	1	0	-	1
1	22	0	-	22
-	3	18	-	19
0	8	0	-	8
0	9	0	-	9
0	7	0	-	8
0	0	-	-	2
0	13	0	-	13
1	0	0	-	7

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.200.1	HE-A 340	Real	4	Bruddgrens...	3	0
B.201.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.202.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.203.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.204.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.205.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.206.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.207.1	HE-A 340	Real	38	Bruddgrens...	38	-
B.208.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.209.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.210.1	HE-A 340	Real	20	Bruddgrens...	20	1
B.211.1	HE-A 340	Real	15	Bruddgrens...	15	1
B.212.1	HE-A 340	Real	34	Vind +	34	1
B.213.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.214.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.215.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.216.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.217.1	HE-A 340	Real	13	Bruddgrens...	13	1
B.218.1	HE-A 340	Real	5	Vind +	5	1
B.219.1	HE-A 340	Real	8	Bruddgrens...	8	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	4	0	-	4
0	1	0	-	1
0	2	5	-	4
1	7	5	-	7
0	0	0	-	3
0	3	0	-	3
0	1	0	-	1
-	26	20	-	31
0	10	1	-	10
0	9	1	-	8
1	12	18	-	19
1	15	8	-	15
1	26	20	-	31
1	0	7	-	7
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	12	8	-	12
1	0	0	-	4
1	7	0	-	7

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.220.1	HE-A 340	Real	8	Bruddgrens...	7	1
B.221.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.222.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.223.1	HE-A 340	Real	22	Bruddgrens...	22	1
B.224.1	HE-A 340	Real	23	Bruddgrens...	23	-
B.225.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.226.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.227.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.228.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.229.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.230.1	HE-A 340	Real	10	Bruddgrens...	10	1
B.231.1	HE-A 340	Real	4	Bruddgrens...	3	0
B.232.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.233.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.234.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.235.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.236.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.237.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.238.1	HE-A 340	Real	35	Bruddgrens...	35	-
B.239.1	HE-A 340	Real	8	Bruddgrens...	8	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
1	8	0	-	8
0	0	0	-	1
0	1	0	-	1
1	22	0	-	22
-	2	18	-	18
0	8	0	-	8
0	9	0	-	9
0	8	0	-	8
0	0	-	-	2
0	13	0	-	13
1	0	0	-	7
0	4	0	-	4
0	1	0	-	2
0	1	5	-	4
1	7	5	-	7
0	0	0	-	3
0	3	0	-	3
0	1	0	-	1
-	25	17	-	29
0	8	1	-	8

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.240.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.241.1	HE-A 340	Real	20	Bruddgrens...	20	1
B.242.1	HE-A 340	Real	16	Bruddgrens...	15	1
B.243.1	HE-A 340	Real	32	Vind +	32	1
B.244.1	HE-A 340	Real	8	Bruddgrens...	7	1
B.245.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.246.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.247.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.248.1	HE-A 340	Real	12	Bruddgrens...	12	1
B.249.1	HE-A 340	Real	5	Vind +	5	1
B.250.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.251.1	HE-A 340	Real	9	Bruddgrens...	7	1
B.252.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.253.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.254.1	HE-A 340	Real	22	Bruddgrens...	22	1
B.255.1	HE-A 340	Real	22	Bruddgrens...	22	0
B.256.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.257.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.258.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.259.1	HE-A 340	Real	5	Bruddgrens...	5	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	8	1	-	6
1	12	18	-	18
1	15	7	-	16
1	24	17	-	29
1	-	6	-	8
0	0	0	-	2
0	6	0	-	7
0	6	0	-	7
1	11	6	-	11
1	0	0	-	4
1	7	0	-	7
1	8	0	-	9
0	0	0	-	0
0	1	0	-	1
1	22	0	-	22
0	2	18	-	18
0	8	0	-	8
0	10	0	-	10
0	8	0	-	8
0	0	-	-	2

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.260.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.261.1	HE-A 340	Real	10	Bruddgrens...	10	1
B.262.1	HE-A 340	Real	4	Bruddgrens...	3	0
B.263.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.264.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.265.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.266.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.267.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.268.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.269.1	HE-A 340	Real	32	Bruddgrens...	32	-
B.270.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.271.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.272.1	HE-A 340	Real	19	Bruddgrens...	19	1
B.273.1	HE-A 340	Real	16	Bruddgrens...	16	1
B.274.1	HE-A 340	Real	29	Vind +	29	1
B.275.1	HE-A 340	Real	9	Bruddgrens...	9	1
B.276.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.277.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.278.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.279.1	HE-A 340	Real	11	Bruddgrens...	11	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	13	0	-	13
1	0	0	-	5
0	4	0	-	4
0	1	0	-	2
0	1	5	-	4
1	6	5	-	6
0	0	0	-	3
0	3	0	-	3
0	1	0	-	1
-	23	14	-	26
0	6	1	-	7
0	6	1	-	5
1	12	18	-	18
1	15	6	-	16
1	22	14	-	27
1	0	8	-	9
0	0	0	-	3
0	6	0	-	7
1	6	0	-	7
1	10	5	-	10



Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.280.1	HE-A 340	Real	5	Vind +	5	1
B.281.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.282.1	HE-A 340	Real	9	Bruddgrens...	8	1
B.283.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.284.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.285.1	HE-A 340	Real	22	Bruddgrens...	21	1
B.286.1	HE-A 340	Real	21	Bruddgrens...	21	1
B.287.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.288.1	HE-A 340	Real	11	Bruddgrens...	11	0
B.289.1	HE-A 340	Real	9	Bruddgrens...	9	0
B.290.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.291.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.292.1	HE-A 340	Real	10	Bruddgrens...	10	1
B.293.1	HE-A 340	Real	4	Bruddgrens...	3	0
B.294.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.295.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.296.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.297.1	HE-A 340	Real	4	Vind +	4	0
B.298.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.299.1	HE-A 340	Real	3	Bruddgrens...	3	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
1	0	0	-	5
1	7	0	-	7
1	8	0	-	9
0	0	0	-	0
0	1	0	-	1
1	22	0	-	22
1	1	17	-	18
0	8	0	-	8
0	10	0	-	10
0	8	0	-	9
0	0	-	-	2
0	13	0	-	13
1	0	0	-	5
0	4	0	-	4
0	1	0	-	2
0	0	5	-	4
1	6	5	-	6
0	0	0	-	3
0	3	0	-	4
0	1	0	-	1

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.300.1	HE-A 340	Real	29	Bruddgrens...	29	-
B.301.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.302.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.303.1	HE-A 340	Real	19	Bruddgrens...	19	2
B.304.1	HE-A 340	Real	16	Bruddgrens...	16	1
B.305.1	HE-A 340	Real	28	Bruddgrens...	28	1
B.306.1	HE-A 340	Real	11	Bruddgrens...	10	1
B.307.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.308.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.309.1	HE-A 340	Real	7	Bruddgrens...	6	1
B.310.1	HE-A 340	Real	10	Bruddgrens...	10	1
B.311.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.312.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.313.1	HE-A 340	Real	7	Bruddgrens...	6	1
B.314.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.315.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.316.1	HE-A 340	Real	26	Bruddgrens...	26	0
B.317.1	HE-A 340	Real	23	Bruddgrens...	23	2
B.318.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.319.1	HE-A 340	Real	11	Bruddgrens...	11	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
-	22	11	-	25
0	5	2	-	5
0	4	2	-	4
2	12	17	-	18
1	15	5	-	16
1	21	11	-	26
1	1	10	-	11
0	0	0	-	3
0	5	0	-	5
1	6	0	-	7
1	8	3	-	9
0	0	0	-	4
1	7	0	-	7
1	6	0	-	7
0	0	0	-	2
0	1	0	-	2
0	26	0	-	26
2	2	21	-	21
0	8	0	-	8
0	10	0	-	10

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.320.1	HE-A 340	Real	9	Bruddgrens...	9	0
B.321.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.322.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.323.1	HE-A 340	Real	11	Bruddgrens...	11	1
B.324.1	HE-A 340	Real	4	Bruddgrens...	3	0
B.325.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.326.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.327.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.328.1	HE-A 340	Real	4	Vind +	4	0
B.329.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.330.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.331.1	HE-A 340	Real	27	Bruddgrens...	27	-
B.332.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.333.1	HE-A 340	Real	23	Bruddgrens...	23	3
B.334.1	HE-A 340	Real	18	Bruddgrens...	17	1
B.335.1	HE-A 340	Real	18	Bruddgrens...	18	1
B.336.1	HE-A 340	Real	28	Bruddgrens...	27	0
B.337.1	HE-A 340	Real	39	Bruddgrens...	37	0
B.338.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.339.1	HE-A 340	Real	3	Bruddgrens...	2	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	9	0	-	9
0	0	-	-	3
0	13	0	-	13
1	0	0	-	5
0	4	0	-	4
0	1	0	-	2
0	0	5	-	4
1	6	5	-	6
0	0	0	-	3
0	3	0	-	3
0	1	0	-	1
-	21	8	-	24
0	9	0	-	12
3	16	21	-	22
1	17	10	-	18
1	17	0	-	18
0	28	0	-	28
0	39	0	-	39
0	0	0	-	1
0	3	0	-	3

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.340.1	HE-A 340	Real	6	Bruddgrens...	6	1
B.341.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.342.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.343.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.344.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.345.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.346.1	HE-A 340	Real	11	Bruddgrens...	11	0
B.347.1	HE-A 340	Real	9	Bruddgrens...	9	0
B.348.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.349.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.350.1	HE-A 340	Real	4	Bruddgrens...	3	0
B.351.1	HE-A 340	Real	3	Vind +	3	0
B.352.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.353.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.354.1	HE-A 340	Real	3	Vind +	3	0
B.355.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.356.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.357.1	HE-A 340	Real	13	Bruddgrens...	13	-
B.358.1	HE-A 260	Real	24	Bruddgrens...	11	0
B.359.1	HE-A 260	Real	7	Bruddgrens...	6	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
1	5	0	-	6
0	5	1	-	6
0	4	0	-	3
0	3	0	-	3
1	7	3	-	7
0	8	0	-	8
0	10	0	-	10
0	9	0	-	9
0	0	-	-	2
0	13	0	-	13
0	4	0	-	4
0	1	0	-	3
0	-	4	-	5
0	6	4	-	6
0	0	0	-	3
0	3	0	-	3
0	1	0	-	1
-	11	4	-	11
0	24	0	-	24
0	7	0	-	7

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.360.1	HE-A 260	Real	2	Bruddgrens...	2	0
B.361.1	HE-A 340	Real	5	Bruddgrens...	4	0
B.362.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.363.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.364.1	HE-A 340	Real	13	Bruddgrens...	13	1
B.365.1	HE-A 340	Real	14	Bruddgrens...	14	1
B.366.1	HE-A 260	Real	24	Bruddgrens...	13	0
B.367.1	HE-A 340	Real	28	Bruddgrens...	28	1
B.368.1	HE-A 340	Real	13	Bruddgrens...	12	1
B.369.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.370.1	HE-A 340	Real	3	Bruddgrens...	2	0
B.371.1	HE-A 340	Real	6	Bruddgrens...	6	1
B.372.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.373.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.374.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.375.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.376.1	HE-A 340	Real	8	Bruddgrens...	8	0
B.377.1	HE-A 340	Real	11	Bruddgrens...	11	0
B.378.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.379.1	HE-A 340	Real	6	Bruddgrens...	6	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	1	0	-	2
0	5	0	-	5
0	13	0	-	13
0	13	0	-	13
1	12	3	-	12
1	14	0	-	14
0	23	9	-	24
1	20	11	-	26
1	1	12	-	13
0	0	0	-	2
0	3	0	-	3
1	5	0	-	6
0	5	1	-	5
0	4	0	-	4
0	3	0	-	3
1	7	3	-	7
0	8	0	-	8
0	11	0	-	11
0	9	0	-	10
0	0	-	-	2

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.380.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.381.1	HE-A 340	Real	4	Bruddgrens...	3	0
B.382.1	HE-A 340	Real	3	Vind +	3	0
B.383.1	HE-A 340	Real	5	Bruddgrens...	5	0
B.384.1	HE-A 340	Real	6	Bruddgrens...	6	1
B.385.1	HE-A 340	Real	4	Bruddgrens...	4	1
B.386.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.387.1	HE-A 340	Real	2	Bruddgrens...	2	0
B.388.1	HE-A 340	Real	11	Bruddgrens...	11	-
B.389.1	HE-A 260	Real	25	Bruddgrens...	11	0
B.390.1	HE-A 260	Real	7	Bruddgrens...	6	0
B.391.1	HE-A 260	Real	2	Bruddgrens...	2	0
B.392.1	HE-A 340	Real	14	Bruddgrens...	14	1
B.393.1	HE-A 340	Real	14	Bruddgrens...	14	1
B.394.1	HE-A 260	Real	22	Bruddgrens...	12	0
B.395.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.396.1	HE-A 340	Real	4	Bruddgrens...	4	0
B.397.1	HE-A 340	Real	9	Bruddgrens...	8	1
B.398.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.399.1	HE-A 340	Real	4	Bruddgrens...	4	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	13	0	-	13
0	4	0	-	4
0	1	0	-	3
0	-	4	-	4
1	6	4	-	6
1	0	0	-	4
0	3	0	-	4
0	1	0	-	1
-	10	3	-	11
0	24	0	-	25
0	7	0	-	7
0	1	0	-	2
1	12	3	-	13
1	14	0	-	14
0	22	7	-	22
0	1	0	-	2
0	4	0	-	4
1	8	0	-	9
0	7	1	-	7
0	2	2	-	3

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.400.1	HE-A 340	Real	3	Bruddgrens...	3	0
B.401.1	HE-A 340	Real	8	Bruddgrens...	8	1
B.402.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.403.1	HE-A 340	Real	13	Bruddgrens...	13	0
B.404.1	HE-A 340	Real	11	Bruddgrens...	11	0
B.405.1	HE-A 340	Real	7	Bruddgrens...	7	0
B.406.1	HE-A 340	Real	21	Bruddgrens...	21	0
B.407.1	HE-A 340	Real	7	Bruddgrens...	6	0
B.408.1	HE-A 340	Real	4	Bruddgrens...	4	1
B.409.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.410.1	HE-A 340	Real	11	Bruddgrens...	11	2
B.411.1	HE-A 340	Real	9	Bruddgrens...	9	1
B.412.1	HE-A 340	Real	7	Bruddgrens...	7	1
B.413.1	HE-A 340	Real	6	Bruddgrens...	6	1
B.414.1	HE-A 340	Real	12	Bruddgrens...	12	1
B.415.1	HE-A 260	Real	28	Bruddgrens...	13	0
B.416.1	HE-A 260	Real	8	Bruddgrens...	8	0
B.417.1	HE-A 260	Real	4	Bruddgrens...	2	0
B.418.1	HE-A 340	Real	18	Bruddgrens...	18	1
B.419.1	HE-A 340	Real	23	Bruddgrens...	22	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	3	1	-	3
1	8	5	-	8
0	13	0	-	13
0	13	0	-	13
0	10	0	-	11
0	0	-	-	3
0	21	0	-	21
0	6	0	-	7
1	2	0	-	3
1	-	4	-	5
2	10	4	-	10
1	0	0	-	9
1	5	0	-	7
1	1	0	-	6
1	11	4	-	12
0	27	4	-	28
0	7	4	-	7
0	2	0	-	4
1	16	5	-	17
1	22	0	-	23

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.420.1	HE-A 260	Real	21	Bruddgrens...	11	0
B.421.1	HE-A 260	Real	36	Bruddgrens...	14	1
B.422.1	HE-A 260	Real	33	Bruddgrens...	14	0
B.423.1	HE-A 260	Real	32	Bruddgrens...	14	0
B.424.1	HE-A 260	Real	32	Bruddgrens...	14	0
B.425.1	HE-A 260	Real	33	Bruddgrens...	14	0
B.426.1	HE-A 260	Real	33	Bruddgrens...	14	0
B.427.1	HE-A 260	Real	33	Bruddgrens...	14	0
B.428.1	HE-A 260	Real	32	Bruddgrens...	14	0
B.429.1	HE-A 260	Real	33	Bruddgrens...	14	0
B.430.1	HE-A 260	Real	33	Bruddgrens...	14	0
B.431.1	HE-A 260	Real	29	Bruddgrens...	14	0
B.432.1	HE-A 260	Real	30	Bruddgrens...	14	0
B.433.1	HE-A 260	Real	28	Bruddgrens...	14	0
B.434.1	HE-A 260	Real	28	Bruddgrens...	14	0
B.435.1	HE-A 260	Real	28	Bruddgrens...	14	0
B.436.1	HE-A 260	Real	28	Bruddgrens...	14	0
B.437.1	HE-A 260	Real	28	Bruddgrens...	14	0
B.438.1	HE-A 260	Real	28	Bruddgrens...	14	0
B.439.1	HE-A 260	Real	28	Bruddgrens...	14	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	19	9	-	21
1	32	0	-	36
0	32	0	-	33
0	32	0	-	32
0	32	0	-	32
0	32	0	-	33
0	32	0	-	33
0	32	0	-	33
0	32	0	-	33
0	31	0	-	32
0	31	0	-	33
0	31	0	-	33
0	28	0	-	29
0	28	0	-	30
0	28	0	-	28
0	28	0	-	28
0	28	0	-	28
0	28	0	-	28
0	28	0	-	28
0	28	0	-	28
0	28	0	-	28



Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.440.1	HE-A 260	Real	28	Bruddgrens...	14	0
B.441.1	HE-A 260	Real	28	Bruddgrens...	15	0
B.442.1	HE-A 260	Real	22	Vind +	9	3
B.443.1	HE-A 260	Real	46	Bruddgrens...	18	2
B.444.1	HE-A 260	Real	13	Bruddgrens...	9	2
B.445.1	HE-A 260	Real	13	Bruddgrens...	9	1
B.446.1	HE-A 260	Real	12	Bruddgrens...	9	1
B.447.1	HE-A 260	Real	12	Bruddgrens...	9	1
B.448.1	HE-A 260	Real	12	Bruddgrens...	9	1
B.449.1	HE-A 260	Real	12	Bruddgrens...	9	1
B.450.1	HE-A 260	Real	12	Bruddgrens...	9	1
B.451.1	HE-A 260	Real	12	Bruddgrens...	9	1
B.452.1	HE-A 260	Real	9	Bruddgrens...	6	1
B.453.1	HE-A 340	Real	20	Bruddgrens...	14	0
B.454.1	HE-A 340	Real	21	Bruddgrens...	14	0
B.455.1	HE-A 340	Real	21	Bruddgrens...	14	0
B.456.1	HE-A 340	Real	21	Bruddgrens...	14	0
B.457.1	HE-A 340	Real	21	Bruddgrens...	14	0
B.458.1	HE-A 340	Real	21	Bruddgrens...	14	0
B.459.1	HE-A 340	Real	21	Bruddgrens...	14	0

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	28	0	-	28
0	28	0	-	28
2	12	0	-	22
2	2	30	-	46
1	12	0	-	13
1	12	0	-	13
1	12	0	-	12
1	12	0	-	12
1	12	0	-	12
1	12	0	-	12
1	12	0	-	12
1	12	0	-	12
1	12	0	-	12
1	9	0	-	9
0	20	0	-	20
0	20	0	-	21
0	21	0	-	21
0	21	0	-	21
0	21	0	-	21
0	21	0	-	21
0	21	0	-	21

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.460.1	HE-A 340	Real	21	Bruddgrens...	14	0
B.461.1	HE-A 340	Real	21	Bruddgrens...	14	0
B.462.1	HE-A 340	Real	21	Bruddgrens...	15	0
B.463.1	HE-A 340	Real	17	Bruddgrens...	12	0
B.464.1	HE-A 340	Real	11	Bruddgrens...	11	10
B.465.1	HE-A 340	Real	9	Bruddgrens...	9	4
B.466.1	HE-A 340	Real	11	Bruddgrens...	11	0
B.467.1	HE-A 340	Real	6	Bruddgrens...	6	0
B.468.1	HE-A 340	Real	8	Bruddgrens...	8	4
B.469.1	HE-A 340	Real	5	Bruddgrens...	5	2
B.470.1	HE-A 340	Real	20	Bruddgrens...	20	0
B.471.1	HE-A 340	Real	15	Bruddgrens...	15	0
B.472.1	HE-A 340	Real	15	Bruddgrens...	15	0
B.473.1	HE-A 340	Real	10	Bruddgrens...	10	0
B.474.1	HE-A 340	Real	20	Bruddgrens...	20	1
B.475.1	HE-A 340	Real	11	Bruddgrens...	11	9
B.476.1	HE-A 340	Real	11	Bruddgrens...	11	8
B.477.1	HE-A 340	Real	11	Bruddgrens...	11	7
B.478.1	HE-A 340	Real	10	Bruddgrens...	10	6
B.479.1	HE-A 340	Real	9	Bruddgrens...	9	5

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
0	21	0	-	21
0	21	0	-	21
0	21	0	-	21
0	16	0	-	17
10	3	4	-	10
4	2	6	-	9
0	5	6	-	10
0	3	4	-	4
4	2	4	-	7
2	2	3	-	5
0	20	3	-	20
0	15	0	-	15
0	14	0	-	14
0	10	6	-	10
1	19	0	-	20
9	3	4	-	10
8	3	4	-	9
7	3	4	-	8
6	3	4	-	7
5	3	4	-	6

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.480.1	HE-A 340	Real	9	Bruddgrens...	9	4
B.481.1	HE-A 340	Real	8	Bruddgrens...	8	2
B.482.1	HE-A 340	Real	7	Bruddgrens...	7	2
B.483.1	HE-A 340	Real	20	Bruddgrens...	20	2
B.484.1	HE-A 340	Real	10	Bruddgrens...	10	5
B.485.1	HE-A 340	Real	10	Bruddgrens...	10	6
B.486.1	HE-A 340	Real	10	Bruddgrens...	10	6
B.487.1	HE-A 340	Real	9	Bruddgrens...	9	5
B.488.1	HE-A 340	Real	9	Bruddgrens...	9	5
B.489.1	HE-A 340	Real	8	Bruddgrens...	8	4
B.490.1	HE-A 340	Real	7	Bruddgrens...	7	3
B.491.1	HE-A 340	Real	7	Bruddgrens...	7	2
B.492.1	HE-A 340	Real	21	Bruddgrens...	21	3
B.493.1	HE-A 340	Real	8	Bruddgrens...	8	2
B.494.1	HE-A 340	Real	8	Bruddgrens...	8	4
B.495.1	HE-A 340	Real	9	Bruddgrens...	9	4
B.496.1	HE-A 340	Real	9	Bruddgrens...	9	5
B.497.1	HE-A 340	Real	9	Bruddgrens...	9	5
B.498.1	HE-A 340	Real	9	Bruddgrens...	9	5
B.499.1	HE-A 340	Real	9	Bruddgrens...	9	4

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
4	3	4	-	5
2	3	4	-	4
2	3	3	-	4
2	6	9	-	10
5	2	6	-	10
6	2	6	-	10
6	2	6	-	10
5	2	5	-	9
5	2	5	-	9
4	2	5	-	8
3	2	5	-	7
2	2	4	-	5
3	4	11	-	12
2	5	6	-	7
4	5	6	-	8
4	5	6	-	8
5	5	5	-	9
5	5	5	-	9
5	5	5	-	9
4	5	5	-	9

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.500.1	HE-A 340	Real	9	Bruddgrens...	9	4
B.501.1	HE-A 340	Real	30	Bruddgrens...	30	4
B.502.1	HE-A 340	Real	20	Bruddgrens...	19	0
B.503.1	HE-A 340	Real	20	Bruddgrens...	19	0
B.504.1	HE-A 340	Real	21	Bruddgrens...	20	0
B.505.1	HE-A 340	Real	20	Bruddgrens...	19	0
B.506.1	HE-A 340	Real	19	Bruddgrens...	19	0
B.507.1	HE-A 340	Real	19	Bruddgrens...	19	0
B.508.1	HE-A 340	Real	19	Bruddgrens...	19	0
B.509.1	HE-A 340	Real	19	Bruddgrens...	19	0
B.510.1	HE-A 340	Real	19	Bruddgrens...	19	0
B.511.1	HE-A 340	Real	6	Bruddgrens...	6	3
B.512.1	HE-A 340	Real	7	Bruddgrens...	7	5
B.513.1	HE-A 340	Real	8	Bruddgrens...	8	5
B.514.1	HE-A 340	Real	8	Bruddgrens...	8	6
B.515.1	HE-A 340	Real	9	Bruddgrens...	9	6
B.516.1	HE-A 340	Real	9	Bruddgrens...	9	7
B.517.1	HE-A 340	Real	9	Bruddgrens...	9	7
B.518.1	HE-A 340	Real	10	Bruddgrens...	10	8
B.519.1	HE-A 340	Real	12	Bruddgrens...	12	8

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
4	5	4	-	8
4	7	11	-	10
0	19	0	-	20
0	19	0	-	20
0	21	0	-	21
0	19	0	-	20
0	19	0	-	19
0	19	0	-	19
0	19	0	-	19
0	19	0	-	19
0	19	0	-	19
3	3	5	-	5
5	3	4	-	7
5	3	4	-	8
6	3	4	-	8
6	3	4	-	9
7	3	4	-	9
7	3	5	-	9
8	3	5	-	9
8	3	5	-	10

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
B.520.1	HE-A 340	Real	12	Bruddgrens...	12	9
B.521.1	HE-A 340	Real	14	Bruddgrens...	14	8
B.522.1	HE-A 340	Real	11	Bruddgrens...	11	1
B.523.1	HE-A 340	Real	16	Bruddgrens...	16	2
C.1.1	KKR 250x2...	Real	41	Bruddgrens...	37	41
C.2.1	KKR 250x2...	Real	21	Bruddgrens...	19	21
C.3.1	KKR 250x2...	Real	23	Bruddgrens...	20	23
C.4.1	KKR 250x2...	Real	41	Bruddgrens...	37	41
C.5.1	KKR 250x2...	Real	40	Bruddgrens...	36	40
C.6.1	KKR 250x2...	Real	44	Bruddgrens...	40	44
C.7.1	KKR 250x2...	Real	60	Bruddgrens...	53	60
C.8.1	KKR 250x2...	Real	34	Bruddgrens...	31	34
C.9.1	KKR 250x2...	Real	33	Bruddgrens...	30	33
C.10.1	KKR 250x2...	Real	38	Bruddgrens...	34	38
C.11.1	KKR 250x2...	Real	34	Bruddgrens...	31	34
C.12.1	KKR 250x2...	Real	29	Bruddgrens...	26	29
C.13.1	KKR 250x2...	Real	15	Bruddgrens...	14	15
C.14.1	KKR 250x2...	Real	20	Bruddgrens...	18	20
C.15.1	KKR 250x2...	Real	38	Bruddgrens...	34	38
C.16.1	KKR 250x2...	Real	40	Bruddgrens...	35	40

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
9	3	5	-	10
8	3	5	-	9
1	10	0	-	11
2	12	0	-	14
37	0	0	-	-
19	0	0	-	-
20	0	0	-	-
37	0	0	-	-
36	0	0	-	-
40	0	0	-	-
53	0	0	-	-
31	0	0	-	-
30	0	0	-	-
34	0	0	-	-
31	0	0	-	-
26	0	0	-	-
14	0	0	-	-
18	0	0	-	-
34	0	0	-	-
35	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.17.1	KKR 300x3...	Real	71	Bruddgrens...	66	71
C.18.1	KKR 300x3...	Real	85	Bruddgrens...	79	85
C.19.1	KKR 250x2...	Real	81	Bruddgrens...	72	81
C.20.1	KKR 250x2...	Real	11	Bruddgrens...	10	11
C.21.1	KKR 250x2...	Real	27	Bruddgrens...	24	27
C.22.1	KKR 250x2...	Real	14	Bruddgrens...	13	14
C.23.1	KKR 250x2...	Real	36	Bruddgrens...	33	36
C.24.1	KKR 250x2...	Real	41	Bruddgrens...	37	41
C.25.1	KKR 250x2...	Real	12	Bruddgrens...	10	12
C.26.1	KKR 250x2...	Real	20	Bruddgrens...	18	20
C.27.1	KKR 300x3...	Real	27	Bruddgrens...	20	27
C.28.1	KKR 300x3...	Real	71	Bruddgrens...	52	71
C.29.1	KKR 250x2...	Real	67	Bruddgrens...	44	67
C.30.1	KKR 300x3...	Real	91	Bruddgrens...	85	91
C.31.1	KKR 250x2...	Real	22	Bruddgrens...	19	22
C.32.1	KKR 250x2...	Real	38	Bruddgrens...	34	38
C.33.1	KKR 250x2...	Real	21	Bruddgrens...	19	21
C.34.1	KKR 250x2...	Real	22	Bruddgrens...	19	22
C.35.1	KKR 250x2...	Real	38	Bruddgrens...	34	38
C.36.1	KKR 250x2...	Real	37	Bruddgrens...	33	37

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
66	0	0	-	-
79	0	0	-	-
72	0	0	-	-
10	0	0	-	-
24	0	0	-	-
13	0	0	-	-
33	0	0	-	-
37	0	0	-	-
10	0	0	-	-
18	0	0	-	-
20	0	0	-	-
52	0	0	-	-
44	0	0	-	-
85	0	0	-	-
19	0	0	-	-
34	0	0	-	-
19	0	0	-	-
19	0	0	-	-
34	0	0	-	-
33	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.37.1	KKR 250x2...	Real	41	Bruddgrens...	36	41
C.38.1	KKR 250x2...	Real	32	Bruddgrens...	29	32
C.39.1	KKR 250x2...	Real	31	Bruddgrens...	28	31
C.40.1	KKR 250x2...	Real	35	Bruddgrens...	32	35
C.41.1	KKR 250x2...	Real	45	Bruddgrens...	40	45
C.42.1	KKR 250x2...	Real	30	Bruddgrens...	27	30
C.43.1	KKR 250x2...	Real	14	Bruddgrens...	13	14
C.44.1	KKR 250x2...	Real	17	Bruddgrens...	15	17
C.45.1	KKR 250x2...	Real	34	Bruddgrens...	31	34
C.46.1	KKR 250x2...	Real	38	Bruddgrens...	34	38
C.47.1	KKR 250x2...	Real	51	Bruddgrens...	46	51
C.48.1	KKR 250x2...	Real	67	Bruddgrens...	60	67
C.49.1	KKR 250x2...	Real	54	Bruddgrens...	48	54
C.50.1	KKR 250x2...	Real	11	Bruddgrens...	10	11
C.51.1	KKR 250x2...	Real	26	Bruddgrens...	24	26
C.52.1	KKR 250x2...	Real	14	Bruddgrens...	12	14
C.53.1	KKR 250x2...	Real	32	Bruddgrens...	29	32
C.54.1	KKR 250x2...	Real	10	Bruddgrens...	9	10
C.55.1	KKR 250x2...	Real	20	Bruddgrens...	18	20
C.56.1	KKR 250x2...	Real	83	Bruddgrens...	75	83

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
36	0	0	-	-
29	0	0	-	-
28	0	0	-	-
32	0	0	-	-
40	0	0	-	-
27	0	0	-	-
13	0	0	-	-
15	0	0	-	-
31	0	0	-	-
34	0	0	-	-
46	0	0	-	-
60	0	0	-	-
48	0	0	-	-
10	0	0	-	-
24	0	0	-	-
12	0	0	-	-
29	0	0	-	-
9	0	0	-	-
18	0	0	-	-
75	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.57.1	KKR 250x2...	Real	38	Bruddgrens...	34	38
C.58.1	KKR 250x2...	Real	34	Bruddgrens...	30	34
C.59.1	KKR 250x2...	Real	20	Bruddgrens...	18	20
C.60.1	KKR 250x2...	Real	21	Bruddgrens...	19	21
C.61.1	KKR 250x2...	Real	35	Bruddgrens...	31	35
C.62.1	KKR 250x2...	Real	34	Bruddgrens...	30	34
C.63.1	KKR 250x2...	Real	37	Bruddgrens...	33	37
C.64.1	KKR 250x2...	Real	49	Bruddgrens...	44	49
C.65.1	KKR 250x2...	Real	29	Bruddgrens...	26	29
C.66.1	KKR 250x2...	Real	28	Bruddgrens...	25	28
C.67.1	KKR 250x2...	Real	32	Bruddgrens...	29	32
C.68.1	KKR 250x2...	Real	42	Bruddgrens...	37	42
C.69.1	KKR 250x2...	Real	14	Bruddgrens...	13	14
C.70.1	KKR 250x2...	Real	15	Bruddgrens...	14	15
C.71.1	KKR 250x2...	Real	31	Bruddgrens...	28	31
C.72.1	KKR 250x2...	Real	34	Bruddgrens...	30	34
C.73.1	KKR 250x2...	Real	27	Bruddgrens...	24	27
C.74.1	KKR 250x2...	Real	40	Bruddgrens...	35	40
C.75.1	KKR 250x2...	Real	33	Bruddgrens...	29	33
C.76.1	KKR 250x2...	Real	11	Bruddgrens...	9	11

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
34	0	0	-	-
30	0	0	-	-
18	0	0	-	-
19	0	0	-	-
31	0	0	-	-
30	0	0	-	-
33	0	0	-	-
44	0	0	-	-
26	0	0	-	-
25	0	0	-	-
29	0	0	-	-
37	0	0	-	-
13	0	0	-	-
14	0	0	-	-
28	0	0	-	-
30	0	0	-	-
24	0	0	-	-
35	0	0	-	-
29	0	0	-	-
9	0	0	-	-



Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.77.1	KKR 250x2...	Real	24	Bruddgrens...	21	24
C.78.1	KKR 250x2...	Real	13	Bruddgrens...	12	13
C.79.1	KKR 250x2...	Real	30	Bruddgrens...	27	30
C.80.1	KKR 250x2...	Real	9	Bruddgrens...	8	9
C.81.1	KKR 250x2...	Real	18	Bruddgrens...	16	18
C.82.1	KKR 250x2...	Real	36	Bruddgrens...	32	36
C.83.1	KKR 250x2...	Real	64	Bruddgrens...	57	64
C.84.1	KKR 250x2...	Real	24	Bruddgrens...	22	24
C.85.1	KKR 250x2...	Real	55	Bruddgrens...	49	55
C.86.1	KKR 200x2...	Real	42	Bruddgrens...	35	42
C.87.1	KKR 200x2...	Real	26	Bruddgrens...	21	26
C.88.1	KKR 200x2...	Real	27	Bruddgrens...	22	27
C.89.1	KKR 200x2...	Real	44	Bruddgrens...	37	44
C.90.1	KKR 200x2...	Real	42	Bruddgrens...	35	42
C.91.1	KKR 250x2...	Real	33	Bruddgrens...	30	33
C.92.1	KKR 200x2...	Real	58	Bruddgrens...	49	58
C.93.1	KKR 200x2...	Real	37	Bruddgrens...	31	37
C.94.1	KKR 200x2...	Real	34	Bruddgrens...	29	34
C.95.1	KKR 200x2...	Real	40	Bruddgrens...	33	40
C.96.1	KKR 200x2...	Real	52	Bruddgrens...	43	52

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
21	0	0	-	-
12	0	0	-	-
27	0	0	-	-
8	0	0	-	-
16	0	0	-	-
32	0	0	-	-
57	0	0	-	-
22	0	0	-	-
49	0	0	-	-
35	0	0	-	-
21	0	0	-	-
22	0	0	-	-
37	0	0	-	-
35	0	0	-	-
30	0	0	-	-
49	0	0	-	-
31	0	0	-	-
29	0	0	-	-
33	0	0	-	-
43	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.97.1	KKR 200x2...	Real	17	Bruddgrens...	14	17
C.98.1	KKR 200x2...	Real	19	Bruddgrens...	16	19
C.99.1	KKR 200x2...	Real	38	Bruddgrens...	31	38
C.100.1	KKR 200x2...	Real	41	Bruddgrens...	34	41
C.101.1	KKR 200x2...	Real	31	Bruddgrens...	26	31
C.102.1	KKR 200x2...	Real	43	Bruddgrens...	36	43
C.103.1	KKR 200x2...	Real	55	Bruddgrens...	46	55
C.104.1	KKR 200x2...	Real	14	Bruddgrens...	12	14
C.105.1	KKR 200x2...	Real	29	Bruddgrens...	25	29
C.106.1	KKR 200x2...	Real	17	Bruddgrens...	14	17
C.107.1	KKR 200x2...	Real	37	Bruddgrens...	31	37
C.108.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.109.1	KKR 200x2...	Real	21	Bruddgrens...	18	21
C.110.1	KKR 200x2...	Real	45	Bruddgrens...	37	45
C.111.1	KKR 200x2...	Real	77	Bruddgrens...	64	77
C.112.1	KKR 200x2...	Real	29	Bruddgrens...	24	29
C.113.1	KKR 200x2...	Real	38	Bruddgrens...	31	38
C.114.1	KKR 200x2...	Real	24	Bruddgrens...	20	24
C.115.1	KKR 200x2...	Real	25	Bruddgrens...	21	25
C.116.1	KKR 200x2...	Real	40	Bruddgrens...	33	40

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
14	0	0	-	-
16	0	0	-	-
31	0	0	-	-
34	0	0	-	-
26	0	0	-	-
36	0	0	-	-
46	0	0	-	-
12	0	0	-	-
25	0	0	-	-
14	0	0	-	-
31	0	0	-	-
9	0	0	-	-
18	0	0	-	-
37	0	0	-	-
64	0	0	-	-
24	0	0	-	-
31	0	0	-	-
20	0	0	-	-
21	0	0	-	-
33	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.117.1	KKR 200x2...	Real	38	Bruddgrens...	32	38
C.118.1	KKR 250x2...	Real	30	Bruddgrens...	26	30
C.119.1	KKR 200x2...	Real	50	Bruddgrens...	42	50
C.120.1	KKR 200x2...	Real	34	Bruddgrens...	28	34
C.121.1	KKR 200x2...	Real	31	Bruddgrens...	26	31
C.122.1	KKR 200x2...	Real	35	Bruddgrens...	30	35
C.123.1	KKR 200x2...	Real	46	Bruddgrens...	39	46
C.124.1	KKR 200x2...	Real	14	Bruddgrens...	11	14
C.125.1	KKR 200x2...	Real	17	Bruddgrens...	14	17
C.126.1	KKR 200x2...	Real	33	Bruddgrens...	28	33
C.127.1	KKR 200x2...	Real	36	Bruddgrens...	30	36
C.128.1	KKR 200x2...	Real	34	Bruddgrens...	28	34
C.129.1	KKR 200x2...	Real	42	Bruddgrens...	35	42
C.130.1	KKR 200x2...	Real	58	Bruddgrens...	49	58
C.131.1	KKR 200x2...	Real	13	Bruddgrens...	11	13
C.132.1	KKR 200x2...	Real	26	Bruddgrens...	22	26
C.133.1	KKR 200x2...	Real	15	Bruddgrens...	13	15
C.134.1	KKR 200x2...	Real	33	Bruddgrens...	28	33
C.135.1	KKR 200x2...	Real	10	Bruddgrens...	8	10
C.136.1	KKR 200x2...	Real	18	Bruddgrens...	15	18

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
32	0	0	-	-
26	0	0	-	-
42	0	0	-	-
28	0	0	-	-
26	0	0	-	-
30	0	0	-	-
39	0	0	-	-
11	0	0	-	-
14	0	0	-	-
28	0	0	-	-
30	0	0	-	-
28	0	0	-	-
35	0	0	-	-
49	0	0	-	-
11	0	0	-	-
22	0	0	-	-
13	0	0	-	-
28	0	0	-	-
8	0	0	-	-
15	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.137.1	KKR 200x2...	Real	41	Bruddgrens...	34	41
C.138.1	KKR 200x2...	Real	67	Bruddgrens...	56	67
C.139.1	KKR 200x2...	Real	25	Bruddgrens...	21	25
C.140.1	KKR 200x2...	Real	34	Bruddgrens...	28	34
C.141.1	KKR 200x2...	Real	22	Bruddgrens...	18	22
C.142.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.143.1	KKR 200x2...	Real	36	Bruddgrens...	30	36
C.144.1	KKR 200x2...	Real	34	Bruddgrens...	28	34
C.145.1	KKR 250x2...	Real	26	Bruddgrens...	23	26
C.146.1	KKR 200x2...	Real	42	Bruddgrens...	35	42
C.147.1	KKR 200x2...	Real	31	Bruddgrens...	26	31
C.148.1	KKR 200x2...	Real	27	Bruddgrens...	22	27
C.149.1	KKR 200x2...	Real	31	Bruddgrens...	26	31
C.150.1	KKR 200x2...	Real	41	Bruddgrens...	35	41
C.151.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.152.1	KKR 200x2...	Real	14	Bruddgrens...	12	14
C.153.1	KKR 200x2...	Real	28	Bruddgrens...	24	28
C.154.1	KKR 200x2...	Real	31	Bruddgrens...	26	31
C.155.1	KKR 200x2...	Real	32	Bruddgrens...	27	32
C.156.1	KKR 200x2...	Real	38	Bruddgrens...	32	38

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
34	0	0	-	-
56	0	0	-	-
21	0	0	-	-
28	0	0	-	-
18	0	0	-	-
19	0	0	-	-
30	0	0	-	-
28	0	0	-	-
23	0	0	-	-
35	0	0	-	-
26	0	0	-	-
22	0	0	-	-
26	0	0	-	-
35	0	0	-	-
9	0	0	-	-
12	0	0	-	-
24	0	0	-	-
26	0	0	-	-
27	0	0	-	-
32	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.157.1	KKR 200x2...	Real	56	Bruddgrens...	47	56
C.158.1	KKR 200x2...	Real	12	Bruddgrens...	10	12
C.159.1	KKR 200x2...	Real	23	Bruddgrens...	20	23
C.160.1	KKR 200x2...	Real	14	Bruddgrens...	12	14
C.161.1	KKR 200x2...	Real	30	Bruddgrens...	25	30
C.162.1	KKR 200x2...	Real	9	Bruddgrens...	8	9
C.163.1	KKR 200x2...	Real	15	Bruddgrens...	13	15
C.164.1	KKR 200x2...	Real	37	Bruddgrens...	31	37
C.165.1	KKR 200x2...	Real	58	Bruddgrens...	48	58
C.166.1	KKR 200x2...	Real	21	Bruddgrens...	18	21
C.167.1	KKR 200x2...	Real	30	Bruddgrens...	25	30
C.168.1	KKR 200x2...	Real	20	Bruddgrens...	17	20
C.169.1	KKR 200x2...	Real	21	Bruddgrens...	17	21
C.170.1	KKR 200x2...	Real	32	Bruddgrens...	27	32
C.171.1	KKR 200x2...	Real	30	Bruddgrens...	25	30
C.172.1	KKR 250x2...	Real	22	Bruddgrens...	20	22
C.173.1	KKR 200x2...	Real	34	Bruddgrens...	29	34
C.174.1	KKR 200x2...	Real	27	Bruddgrens...	23	27
C.175.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.176.1	KKR 200x2...	Real	27	Bruddgrens...	22	27

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
47	0	0	-	-
10	0	0	-	-
20	0	0	-	-
12	0	0	-	-
25	0	0	-	-
8	0	0	-	-
13	0	0	-	-
31	0	0	-	-
48	0	0	-	-
18	0	0	-	-
25	0	0	-	-
17	0	0	-	-
17	0	0	-	-
27	0	0	-	-
25	0	0	-	-
20	0	0	-	-
29	0	0	-	-
23	0	0	-	-
19	0	0	-	-
22	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.177.1	KKR 200x2...	Real	37	Bruddgrens...	31	37
C.178.1	KKR 200x2...	Real	8	Bruddgrens...	7	8
C.179.1	KKR 200x2...	Real	12	Bruddgrens...	10	12
C.180.1	KKR 200x2...	Real	24	Bruddgrens...	20	24
C.181.1	KKR 200x2...	Real	26	Bruddgrens...	22	26
C.182.1	KKR 200x2...	Real	28	Bruddgrens...	23	28
C.183.1	KKR 200x2...	Real	33	Bruddgrens...	28	33
C.184.1	KKR 200x2...	Real	52	Bruddgrens...	43	52
C.185.1	KKR 200x2...	Real	11	Bruddgrens...	10	11
C.186.1	KKR 200x2...	Real	21	Bruddgrens...	17	21
C.187.1	KKR 200x2...	Real	13	Bruddgrens...	10	13
C.188.1	KKR 200x2...	Real	27	Bruddgrens...	22	27
C.189.1	KKR 200x2...	Real	8	Bruddgrens...	7	8
C.190.1	KKR 200x2...	Real	13	Bruddgrens...	11	13
C.191.1	KKR 200x2...	Real	33	Bruddgrens...	28	33
C.192.1	KKR 200x2...	Real	49	Bruddgrens...	41	49
C.193.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.194.1	KKR 200x2...	Real	26	Bruddgrens...	22	26
C.195.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.196.1	KKR 200x2...	Real	18	Bruddgrens...	15	18

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
31	0	0	-	-
7	0	0	-	-
10	0	0	-	-
20	0	0	-	-
22	0	0	-	-
23	0	0	-	-
28	0	0	-	-
43	0	0	-	-
10	0	0	-	-
17	0	0	-	-
10	0	0	-	-
22	0	0	-	-
7	0	0	-	-
11	0	0	-	-
28	0	0	-	-
41	0	0	-	-
15	0	0	-	-
22	0	0	-	-
15	0	0	-	-
15	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.197.1	KKR 200x2...	Real	28	Bruddgrens...	23	28
C.198.1	KKR 200x2...	Real	26	Bruddgrens...	22	26
C.199.1	KKR 250x2...	Real	18	Bruddgrens...	16	18
C.200.1	KKR 200x2...	Real	28	Bruddgrens...	23	28
C.201.1	KKR 200x2...	Real	24	Bruddgrens...	20	24
C.202.1	KKR 200x2...	Real	20	Bruddgrens...	16	20
C.203.1	KKR 200x2...	Real	22	Bruddgrens...	19	22
C.204.1	KKR 200x2...	Real	32	Bruddgrens...	27	32
C.205.1	KKR 200x2...	Real	6	Bruddgrens...	5	6
C.206.1	KKR 200x2...	Real	10	Bruddgrens...	8	10
C.207.1	KKR 200x2...	Real	19	Bruddgrens...	16	19
C.208.1	KKR 200x2...	Real	21	Bruddgrens...	17	21
C.209.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.210.1	KKR 200x2...	Real	28	Bruddgrens...	23	28
C.211.1	KKR 200x2...	Real	46	Bruddgrens...	38	46
C.212.1	KKR 200x2...	Real	10	Bruddgrens...	9	10
C.213.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.214.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.215.1	KKR 200x2...	Real	24	Bruddgrens...	20	24
C.216.1	KKR 200x2...	Real	7	Bruddgrens...	6	7

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
23	0	0	-	-
22	0	0	-	-
16	0	0	-	-
23	0	0	-	-
20	0	0	-	-
16	0	0	-	-
19	0	0	-	-
27	0	0	-	-
5	0	0	-	-
8	0	0	-	-
16	0	0	-	-
17	0	0	-	-
19	0	0	-	-
23	0	0	-	-
38	0	0	-	-
9	0	0	-	-
15	0	0	-	-
9	0	0	-	-
20	0	0	-	-
6	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.217.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.218.1	KKR 200x2...	Real	29	Bruddgrens...	24	29
C.219.1	KKR 200x2...	Real	40	Bruddgrens...	33	40
C.220.1	KKR 200x2...	Real	15	Bruddgrens...	12	15
C.221.1	KKR 200x2...	Real	22	Bruddgrens...	19	22
C.222.1	KKR 200x2...	Real	15	Bruddgrens...	13	15
C.223.1	KKR 200x2...	Real	16	Bruddgrens...	13	16
C.224.1	KKR 200x2...	Real	24	Bruddgrens...	20	24
C.225.1	KKR 200x2...	Real	22	Bruddgrens...	18	22
C.226.1	KKR 250x2...	Real	14	Bruddgrens...	13	14
C.227.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.228.1	KKR 200x2...	Real	21	Bruddgrens...	18	21
C.229.1	KKR 200x2...	Real	16	Bruddgrens...	14	16
C.230.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.231.1	KKR 200x2...	Real	29	Bruddgrens...	24	29
C.232.1	KKR 200x2...	Real	4	Bruddgrens...	3	4
C.233.1	KKR 200x2...	Real	7	Bruddgrens...	6	7
C.234.1	KKR 200x2...	Real	15	Bruddgrens...	12	15
C.235.1	KKR 200x2...	Real	16	Bruddgrens...	13	16
C.236.1	KKR 200x2...	Real	17	Bruddgrens...	14	17

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
9	0	0	-	-
24	0	0	-	-
33	0	0	-	-
12	0	0	-	-
19	0	0	-	-
13	0	0	-	-
13	0	0	-	-
20	0	0	-	-
18	0	0	-	-
13	0	0	-	-
19	0	0	-	-
18	0	0	-	-
14	0	0	-	-
15	0	0	-	-
24	0	0	-	-
3	0	0	-	-
6	0	0	-	-
12	0	0	-	-
13	0	0	-	-
14	0	0	-	-



Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.237.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.238.1	KKR 200x2...	Real	39	Bruddgrens...	32	39
C.239.1	KKR 200x2...	Real	9	Bruddgrens...	8	9
C.240.1	KKR 200x2...	Real	15	Bruddgrens...	13	15
C.241.1	KKR 200x2...	Real	10	Bruddgrens...	8	10
C.242.1	KKR 200x2...	Real	20	Bruddgrens...	17	20
C.243.1	KKR 200x2...	Real	6	Bruddgrens...	5	6
C.244.1	KKR 200x2...	Real	9	Bruddgrens...	8	9
C.245.1	KKR 200x2...	Real	25	Bruddgrens...	21	25
C.246.1	KKR 200x2...	Real	31	Bruddgrens...	26	31
C.247.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.248.1	KKR 200x2...	Real	19	Bruddgrens...	16	19
C.249.1	KKR 200x2...	Real	13	Bruddgrens...	11	13
C.250.1	KKR 200x2...	Real	14	Bruddgrens...	11	14
C.251.1	KKR 200x2...	Real	21	Bruddgrens...	17	21
C.252.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.253.1	KKR 250x2...	Real	11	Bruddgrens...	10	11
C.254.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.255.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.256.1	KKR 200x2...	Real	13	Bruddgrens...	11	13

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
19	0	0	-	-
32	0	0	-	-
8	0	0	-	-
13	0	0	-	-
8	0	0	-	-
17	0	0	-	-
5	0	0	-	-
8	0	0	-	-
21	0	0	-	-
26	0	0	-	-
9	0	0	-	-
16	0	0	-	-
11	0	0	-	-
11	0	0	-	-
17	0	0	-	-
15	0	0	-	-
10	0	0	-	-
15	0	0	-	-
15	0	0	-	-
11	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.257.1	KKR 200x2...	Real	14	Bruddgrens...	11	14
C.258.1	KKR 200x2...	Real	25	Bruddgrens...	21	25
C.259.1	KKR 200x2...	Real	3	Bruddgrens...	2	3
C.260.1	KKR 200x2...	Real	5	Bruddgrens...	4	5
C.261.1	KKR 200x2...	Real	10	Bruddgrens...	8	10
C.262.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.263.1	KKR 200x2...	Real	10	Bruddgrens...	9	10
C.264.1	KKR 200x2...	Real	17	Bruddgrens...	14	17
C.265.1	KKR 200x2...	Real	30	Bruddgrens...	25	30
C.266.1	KKR 200x2...	Real	8	Bruddgrens...	7	8
C.267.1	KKR 200x2...	Real	13	Bruddgrens...	11	13
C.268.1	KKR 200x2...	Real	8	Bruddgrens...	7	8
C.269.1	KKR 200x2...	Real	17	Bruddgrens...	14	17
C.270.1	KKR 200x2...	Real	5	Bruddgrens...	4	5
C.271.1	KKR 200x2...	Real	7	Bruddgrens...	6	7
C.272.1	KKR 200x2...	Real	21	Bruddgrens...	18	21
C.273.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.274.1	KKR 200x2...	Real	8	Bruddgrens...	6	8
C.275.1	KKR 200x2...	Real	16	Bruddgrens...	13	16
C.276.1	KKR 200x2...	Real	11	Bruddgrens...	9	11

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
11	0	0	-	-
21	0	0	-	-
2	0	0	-	-
4	0	0	-	-
8	0	0	-	-
9	0	0	-	-
9	0	0	-	-
14	0	0	-	-
25	0	0	-	-
7	0	0	-	-
11	0	0	-	-
7	0	0	-	-
14	0	0	-	-
4	0	0	-	-
6	0	0	-	-
18	0	0	-	-
19	0	0	-	-
6	0	0	-	-
13	0	0	-	-
9	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.277.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.278.1	KKR 200x2...	Real	17	Bruddgrens...	14	17
C.279.1	KKR 200x2...	Real	14	Bruddgrens...	12	14
C.280.1	KKR 250x2...	Real	7	Bruddgrens...	6	7
C.281.1	KKR 200x2...	Real	15	Bruddgrens...	13	15
C.282.1	KKR 200x2...	Real	15	Bruddgrens...	13	15
C.283.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.284.1	KKR 200x2...	Real	9	Bruddgrens...	8	9
C.285.1	KKR 200x2...	Real	22	Bruddgrens...	18	22
C.286.1	KKR 200x2...	Real	2	Bruddgrens...	1	2
C.287.1	KKR 200x2...	Real	3	Bruddgrens...	2	3
C.288.1	KKR 200x2...	Real	5	Bruddgrens...	4	5
C.289.1	KKR 200x2...	Real	6	Bruddgrens...	5	6
C.290.1	KKR 200x2...	Real	4	Bruddgrens...	3	4
C.291.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.292.1	KKR 200x2...	Real	22	Bruddgrens...	18	22
C.293.1	KKR 200x2...	Real	7	Bruddgrens...	6	7
C.294.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.295.1	KKR 200x2...	Real	7	Bruddgrens...	6	7
C.296.1	KKR 200x2...	Real	14	Bruddgrens...	12	14

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
9	0	0	-	-
14	0	0	-	-
12	0	0	-	-
6	0	0	-	-
13	0	0	-	-
13	0	0	-	-
9	0	0	-	-
8	0	0	-	-
18	0	0	-	-
1	0	0	-	-
2	0	0	-	-
4	0	0	-	-
5	0	0	-	-
3	0	0	-	-
9	0	0	-	-
18	0	0	-	-
6	0	0	-	-
9	0	0	-	-
6	0	0	-	-
12	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.297.1	KKR 200x2...	Real	4	Bruddgrens...	4	4
C.298.1	KKR 200x2...	Real	6	Bruddgrens...	5	6
C.299.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.300.1	KKR 200x2...	Real	14	Bruddgrens...	12	14
C.301.1	KKR 200x2...	Real	4	Bruddgrens...	3	4
C.302.1	KKR 150x1...	Real	20	Bruddgrens...	14	20
C.303.1	KKR 150x1...	Real	13	Bruddgrens...	9	13
C.304.1	KKR 150x1...	Real	13	Bruddgrens...	10	13
C.305.1	KKR 150x1...	Real	21	Bruddgrens...	16	21
C.306.1	KKR 150x1...	Real	16	Bruddgrens...	12	16
C.307.1	KKR 150x1...	Real	9	Bruddgrens...	6	9
C.308.1	KKR 150x1...	Real	19	Bruddgrens...	14	19
C.309.1	KKR 150x1...	Real	20	Bruddgrens...	14	20
C.310.1	KKR 150x1...	Real	13	Bruddgrens...	9	13
C.311.1	KKR 150x1...	Real	9	Bruddgrens...	7	9
C.312.1	KKR 150x1...	Real	26	Bruddgrens...	19	26
C.313.1	KKR 150x1...	Real	9	Bruddgrens...	7	9
C.314.1	KKR 150x1...	Real	24	Bruddgrens...	18	24
C.315.1	KKR 150x1...	Real	9	Bruddgrens...	6	9
C.316.1	KKR 150x1...	Real	13	Bruddgrens...	10	13

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
4	0	0	-	-
5	0	0	-	-
15	0	0	-	-
12	0	0	-	-
3	0	0	-	-
14	0	0	-	-
9	0	0	-	-
10	0	0	-	-
16	0	0	-	-
12	0	0	-	-
6	0	0	-	-
14	0	0	-	-
14	0	0	-	-
9	0	0	-	-
7	0	0	-	-
19	0	0	-	-
7	0	0	-	-
18	0	0	-	-
6	0	0	-	-
10	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.317.1	KKR 150x1...	Real	8	Bruddgrens...	6	8
C.318.1	KKR 150x1...	Real	18	Bruddgrens...	13	18
C.319.1	KKR 150x1...	Real	5	Bruddgrens...	4	5
C.320.1	KKR 150x1...	Real	7	Bruddgrens...	5	7
C.321.1	KKR 150x1...	Real	22	Bruddgrens...	16	22
C.322.1	KKR 150x1...	Real	14	Bruddgrens...	10	14
C.323.1	KKR 150x1...	Real	19	Bruddgrens...	14	19
C.324.1	KKR 250x2...	Real	45	Bruddgrens...	40	45
C.325.1	KKR 200x2...	Real	55	Bruddgrens...	46	55
C.326.1	KKR 200x2...	Real	48	Bruddgrens...	40	48
C.327.1	KKR 200x2...	Real	42	Bruddgrens...	35	42
C.328.1	KKR 200x2...	Real	35	Bruddgrens...	29	35
C.329.1	KKR 200x2...	Real	29	Bruddgrens...	24	29
C.330.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.331.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.332.1	KKR 200x2...	Real	13	Bruddgrens...	10	13
C.333.1	KKR 150x1...	Real	12	Bruddgrens...	8	12
C.334.1	KKR 150x1...	Real	15	Bruddgrens...	11	15
C.335.1	KKR 150x1...	Real	9	Bruddgrens...	7	9
C.336.1	KKR 150x1...	Real	9	Bruddgrens...	7	9

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
6	0	0	-	-
13	0	0	-	-
4	0	0	-	-
5	0	0	-	-
16	0	0	-	-
10	0	0	-	-
14	0	0	-	-
40	0	0	-	-
46	0	0	-	-
40	0	0	-	-
35	0	0	-	-
29	0	0	-	-
24	0	0	-	-
19	0	0	-	-
15	0	0	-	-
10	0	0	-	-
8	0	0	-	-
11	0	0	-	-
7	0	0	-	-
7	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.337.1	KKR 150x1...	Real	16	Bruddgrens...	11	16
C.338.1	KKR 150x1...	Real	12	Bruddgrens...	9	12
C.339.1	KKR 150x1...	Real	6	Bruddgrens...	4	6
C.340.1	KKR 150x1...	Real	13	Bruddgrens...	10	13
C.341.1	KKR 150x1...	Real	15	Bruddgrens...	11	15
C.342.1	KKR 150x1...	Real	9	Bruddgrens...	6	9
C.343.1	KKR 150x1...	Real	6	Bruddgrens...	5	6
C.344.1	KKR 150x1...	Real	19	Bruddgrens...	14	19
C.345.1	KKR 150x1...	Real	6	Bruddgrens...	5	6
C.346.1	KKR 150x1...	Real	16	Bruddgrens...	11	16
C.347.1	KKR 150x1...	Real	6	Bruddgrens...	5	6
C.348.1	KKR 150x1...	Real	10	Bruddgrens...	7	10
C.349.1	KKR 150x1...	Real	6	Bruddgrens...	4	6
C.350.1	KKR 150x1...	Real	13	Bruddgrens...	9	13
C.351.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.352.1	KKR 150x1...	Real	5	Bruddgrens...	4	5
C.353.1	KKR 150x1...	Real	16	Bruddgrens...	11	16
C.354.1	KKR 150x1...	Real	10	Bruddgrens...	7	10
C.355.1	KKR 150x1...	Real	14	Bruddgrens...	10	14
C.356.1	KKR 150x1...	Real	8	Bruddgrens...	5	8

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
11	0	0	-	-
9	0	0	-	-
4	0	0	-	-
10	0	0	-	-
11	0	0	-	-
6	0	0	-	-
5	0	0	-	-
14	0	0	-	-
5	0	0	-	-
11	0	0	-	-
5	0	0	-	-
7	0	0	-	-
4	0	0	-	-
9	0	0	-	-
3	0	0	-	-
4	0	0	-	-
11	0	0	-	-
7	0	0	-	-
10	0	0	-	-
5	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.357.1	KKR 150x1...	Real	10	Bruddgrens...	7	10
C.358.1	KKR 150x1...	Real	5	Bruddgrens...	4	5
C.359.1	KKR 150x1...	Real	5	Bruddgrens...	4	5
C.360.1	KKR 150x1...	Real	10	Bruddgrens...	7	10
C.361.1	KKR 150x1...	Real	7	Bruddgrens...	5	7
C.362.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.363.1	KKR 150x1...	Real	8	Bruddgrens...	6	8
C.364.1	KKR 150x1...	Real	11	Bruddgrens...	8	11
C.365.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.366.1	KKR 150x1...	Real	3	Bruddgrens...	3	3
C.367.1	KKR 150x1...	Real	12	Bruddgrens...	9	12
C.368.1	KKR 150x1...	Real	3	Bruddgrens...	2	3
C.369.1	KKR 150x1...	Real	7	Bruddgrens...	5	7
C.370.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.371.1	KKR 150x1...	Real	6	Bruddgrens...	5	6
C.372.1	KKR 150x1...	Real	3	Bruddgrens...	2	3
C.373.1	KKR 150x1...	Real	8	Bruddgrens...	6	8
C.374.1	KKR 150x1...	Real	2	Bruddgrens...	2	2
C.375.1	KKR 150x1...	Real	3	Bruddgrens...	2	3
C.376.1	KKR 150x1...	Real	10	Bruddgrens...	7	10

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
7	0	0	-	-
4	0	0	-	-
4	0	0	-	-
7	0	0	-	-
5	0	0	-	-
3	0	0	-	-
6	0	0	-	-
8	0	0	-	-
3	0	0	-	-
3	0	0	-	-
9	0	0	-	-
2	0	0	-	-
5	0	0	-	-
3	0	0	-	-
5	0	0	-	-
2	0	0	-	-
6	0	0	-	-
2	0	0	-	-
2	0	0	-	-
7	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.377.1	KKR 150x1...	Real	6	Bruddgrens...	4	6
C.378.1	KKR 150x1...	Real	9	Bruddgrens...	7	9
C.379.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.380.1	KKR 250x2...	Real	21	Bruddgrens...	14	21
C.381.1	KKR 250x2...	Real	24	Bruddgrens...	15	24
C.382.1	KKR 150x1...	Real	30	Bruddgrens...	22	30
C.383.1	KKR 150x1...	Real	34	Bruddgrens...	24	34
C.384.1	KKR 150x1...	Real	27	Bruddgrens...	20	27
C.385.1	KKR 150x1...	Real	30	Bruddgrens...	22	30
C.386.1	KKR 150x1...	Real	24	Bruddgrens...	17	24
C.387.1	KKR 150x1...	Real	26	Bruddgrens...	19	26
C.388.1	KKR 150x1...	Real	20	Bruddgrens...	15	20
C.389.1	KKR 150x1...	Real	22	Bruddgrens...	16	22
C.390.1	KKR 150x1...	Real	17	Bruddgrens...	12	17
C.391.1	KKR 150x1...	Real	19	Bruddgrens...	14	19
C.392.1	KKR 150x1...	Real	13	Bruddgrens...	10	13
C.393.1	KKR 150x1...	Real	15	Bruddgrens...	11	15
C.394.1	KKR 150x1...	Real	10	Bruddgrens...	7	10
C.395.1	KKR 150x1...	Real	11	Bruddgrens...	8	11
C.396.1	KKR 150x1...	Real	7	Bruddgrens...	5	7

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
4	0	0	-	-
7	0	0	-	-
3	0	0	-	-
14	0	0	-	-
15	0	0	-	-
22	0	0	-	-
24	0	0	-	-
20	0	0	-	-
22	0	0	-	-
17	0	0	-	-
19	0	0	-	-
15	0	0	-	-
16	0	0	-	-
12	0	0	-	-
14	0	0	-	-
10	0	0	-	-
11	0	0	-	-
7	0	0	-	-
8	0	0	-	-
5	0	0	-	-



Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.397.1	KKR 150x1...	Real	7	Bruddgrens...	5	7
C.398.1	KKR 150x1...	Real	3	Bruddgrens...	2	3
C.399.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.400.1	KKR 150x1...	Real	40	Bruddgrens...	29	40
C.401.1	KKR 150x1...	Real	40	Bruddgrens...	29	40
C.402.1	KKR 150x1...	Real	44	Bruddgrens...	32	44
C.403.1	KKR 150x1...	Real	44	Bruddgrens...	32	44
C.404.1	KKR 150x1...	Real	36	Bruddgrens...	26	36
C.405.1	KKR 150x1...	Real	36	Bruddgrens...	26	36
C.406.1	KKR 150x1...	Real	32	Bruddgrens...	23	32
C.407.1	KKR 150x1...	Real	32	Bruddgrens...	23	32
C.408.1	KKR 150x1...	Real	28	Bruddgrens...	20	28
C.409.1	KKR 150x1...	Real	28	Bruddgrens...	20	28
C.410.1	KKR 150x1...	Real	24	Bruddgrens...	17	24
C.411.1	KKR 150x1...	Real	24	Bruddgrens...	17	24
C.412.1	KKR 150x1...	Real	20	Bruddgrens...	14	20
C.413.1	KKR 150x1...	Real	20	Bruddgrens...	14	20
C.414.1	KKR 150x1...	Real	16	Bruddgrens...	12	16
C.415.1	KKR 150x1...	Real	16	Bruddgrens...	12	16
C.416.1	KKR 150x1...	Real	12	Bruddgrens...	9	12

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
5	0	0	-	-
2	0	0	-	-
3	0	0	-	-
29	0	0	-	-
29	0	0	-	-
32	0	0	-	-
32	0	0	-	-
26	0	0	-	-
26	0	0	-	-
23	0	0	-	-
23	0	0	-	-
20	0	0	-	-
20	0	0	-	-
17	0	0	-	-
17	0	0	-	-
14	0	0	-	-
14	0	0	-	-
12	0	0	-	-
12	0	0	-	-
9	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.417.1	KKR 150x1...	Real	12	Bruddgrens...	9	12
C.418.1	KKR 150x1...	Real	8	Bruddgrens...	6	8
C.419.1	KKR 150x1...	Real	8	Bruddgrens...	6	8
C.420.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.421.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.422.1	KKR 150x1...	Real	24	Bruddgrens...	18	24
C.423.1	KKR 150x1...	Real	21	Bruddgrens...	15	21
C.424.1	KKR 150x1...	Real	18	Bruddgrens...	13	18
C.425.1	KKR 150x1...	Real	16	Bruddgrens...	12	16
C.426.1	KKR 150x1...	Real	14	Bruddgrens...	10	14
C.427.1	KKR 150x1...	Real	11	Bruddgrens...	8	11
C.428.1	KKR 150x1...	Real	9	Bruddgrens...	6	9
C.429.1	KKR 150x1...	Real	6	Bruddgrens...	5	6
C.430.1	KKR 150x1...	Real	22	Bruddgrens...	16	22
C.431.1	KKR 150x1...	Real	4	Bruddgrens...	3	4
C.432.1	KKR 150x1...	Real	2	Bruddgrens...	1	2
C.433.1	KKR 150x1...	Real	63	Bruddgrens...	45	63
C.434.1	KKR 150x1...	Real	42	Bruddgrens...	30	42
C.435.1	KKR 150x1...	Real	57	Bruddgrens...	41	57
C.436.1	KKR 150x1...	Real	38	Bruddgrens...	28	38

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
9	0	0	-	-
6	0	0	-	-
6	0	0	-	-
3	0	0	-	-
3	0	0	-	-
18	0	0	-	-
15	0	0	-	-
13	0	0	-	-
12	0	0	-	-
10	0	0	-	-
8	0	0	-	-
6	0	0	-	-
5	0	0	-	-
16	0	0	-	-
3	0	0	-	-
1	0	0	-	-
45	0	0	-	-
30	0	0	-	-
41	0	0	-	-
28	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.437.1	KKR 150x1...	Real	51	Bruddgrens...	37	51
C.438.1	KKR 150x1...	Real	34	Bruddgrens...	25	34
C.439.1	KKR 150x1...	Real	45	Bruddgrens...	33	45
C.440.1	KKR 150x1...	Real	30	Bruddgrens...	22	30
C.441.1	KKR 150x1...	Real	39	Bruddgrens...	29	39
C.442.1	KKR 150x1...	Real	26	Bruddgrens...	19	26
C.443.1	KKR 150x1...	Real	34	Bruddgrens...	24	34
C.444.1	KKR 150x1...	Real	23	Bruddgrens...	16	23
C.445.1	KKR 150x1...	Real	28	Bruddgrens...	20	28
C.446.1	KKR 150x1...	Real	19	Bruddgrens...	13	19
C.447.1	KKR 150x1...	Real	22	Bruddgrens...	16	22
C.448.1	KKR 150x1...	Real	15	Bruddgrens...	11	15
C.449.1	KKR 150x1...	Real	16	Bruddgrens...	12	16
C.450.1	KKR 150x1...	Real	11	Bruddgrens...	8	11
C.451.1	KKR 150x1...	Real	10	Bruddgrens...	7	10
C.452.1	KKR 150x1...	Real	7	Bruddgrens...	5	7
C.453.1	KKR 150x1...	Real	5	Bruddgrens...	3	5
C.454.1	KKR 150x1...	Real	3	Bruddgrens...	2	3
C.455.1	KKR 250x2...	Real	49	Bruddgrens...	44	49
C.456.1	KKR 250x2...	Real	64	Bruddgrens...	57	64

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
37	0	0	-	-
25	0	0	-	-
33	0	0	-	-
22	0	0	-	-
29	0	0	-	-
19	0	0	-	-
24	0	0	-	-
16	0	0	-	-
20	0	0	-	-
13	0	0	-	-
16	0	0	-	-
11	0	0	-	-
12	0	0	-	-
8	0	0	-	-
7	0	0	-	-
5	0	0	-	-
3	0	0	-	-
2	0	0	-	-
44	0	0	-	-
57	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.457.1	KKR 300x3...	Real	55	Bruddgrens...	52	55
C.458.1	KKR 300x3...	Real	37	Bruddgrens...	34	37
C.459.1	KKR 250x2...	Real	39	Bruddgrens...	35	39
C.460.1	KKR 250x2...	Real	43	Bruddgrens...	38	43
C.461.1	KKR 200x2...	Real	50	Bruddgrens...	42	50
C.462.1	KKR 250x2...	Real	56	Bruddgrens...	50	56
C.463.1	KKR 200x2...	Real	63	Bruddgrens...	53	63
C.464.1	KKR 250x2...	Real	35	Bruddgrens...	31	35
C.465.1	KKR 250x2...	Real	36	Bruddgrens...	32	36
C.466.1	KKR 250x2...	Real	35	Bruddgrens...	31	35
C.467.1	KKR 250x2...	Real	32	Bruddgrens...	29	32
C.468.1	KKR 250x2...	Real	29	Bruddgrens...	26	29
C.469.1	KKR 250x2...	Real	26	Bruddgrens...	23	26
C.470.1	KKR 250x2...	Real	22	Bruddgrens...	20	22
C.471.1	KKR 250x2...	Real	17	Bruddgrens...	15	17
C.472.1	KKR 250x2...	Real	12	Bruddgrens...	11	12
C.473.1	KKR 250x2...	Real	65	Bruddgrens...	58	65
C.474.1	KKR 200x2...	Real	70	Bruddgrens...	58	70
C.475.1	KKR 200x2...	Real	56	Bruddgrens...	47	56
C.476.1	KKR 200x2...	Real	45	Bruddgrens...	38	45

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
52	0	0	-	-
34	0	0	-	-
35	1	2	-	38
38	0	0	-	-
42	0	0	-	-
50	0	0	-	-
53	0	0	-	-
31	1	1	-	33
32	0	0	-	33
31	0	0	-	33
29	0	1	-	31
26	0	1	-	28
23	0	1	-	25
20	0	1	-	21
15	0	1	-	17
10	1	1	-	12
58	0	0	-	-
58	0	0	-	-
47	0	0	-	-
38	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.477.1	KKR 200x2...	Real	36	Bruddgrens...	30	36
C.478.1	KKR 200x2...	Real	36	Bruddgrens...	30	36
C.479.1	KKR 200x2...	Real	44	Bruddgrens...	37	44
C.480.1	KKR 200x2...	Real	53	Bruddgrens...	44	53
C.481.1	KKR 200x2...	Real	43	Bruddgrens...	36	43
C.482.1	KKR 200x2...	Real	37	Bruddgrens...	31	37
C.483.1	KKR 200x2...	Real	32	Bruddgrens...	27	32
C.484.1	KKR 200x2...	Real	28	Bruddgrens...	24	28
C.485.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.486.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.487.1	KKR 200x2...	Real	22	Bruddgrens...	18	22
C.488.1	KKR 200x2...	Real	25	Bruddgrens...	21	25
C.489.1	KKR 200x2...	Real	30	Bruddgrens...	25	30
C.490.1	KKR 200x2...	Real	28	Bruddgrens...	23	28
C.491.1	KKR 200x2...	Real	24	Bruddgrens...	20	24
C.492.1	KKR 200x2...	Real	22	Bruddgrens...	19	22
C.493.1	KKR 200x2...	Real	21	Bruddgrens...	18	21
C.494.1	KKR 200x2...	Real	21	Bruddgrens...	18	21
C.495.1	KKR 200x2...	Real	17	Bruddgrens...	14	17
C.496.1	KKR 250x2...	Real	48	Bruddgrens...	43	48

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
30	0	0	-	-
30	0	0	-	-
37	0	0	-	-
44	0	0	-	-
36	0	0	-	-
31	0	0	-	-
27	0	0	-	-
24	0	0	-	-
19	0	0	-	-
19	0	0	-	-
18	0	0	-	-
21	0	0	-	-
25	0	0	-	-
23	0	0	-	-
20	0	0	-	-
19	0	0	-	-
18	0	0	-	-
18	0	0	-	-
14	0	0	-	-
43	1	1	-	46

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.497.1	KKR 200x2...	Real	9	Bruddgrens...	8	9
C.498.1	KKR 200x2...	Real	11	Bruddgrens...	9	11
C.499.1	KKR 200x2...	Real	16	Bruddgrens...	14	16
C.500.1	KKR 200x2...	Real	12	Bruddgrens...	10	12
C.501.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.502.1	KKR 200x2...	Real	16	Bruddgrens...	14	16
C.503.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.504.1	KKR 200x2...	Real	21	Bruddgrens...	17	21
C.505.1	KKR 200x2...	Real	23	Bruddgrens...	19	23
C.506.1	KKR 200x2...	Real	25	Bruddgrens...	21	25
C.507.1	KKR 200x2...	Real	29	Bruddgrens...	24	29
C.508.1	KKR 200x2...	Real	30	Bruddgrens...	25	30
C.509.1	KKR 200x2...	Real	36	Bruddgrens...	30	36
C.510.1	KKR 200x2...	Real	35	Bruddgrens...	29	35
C.511.1	KKR 200x2...	Real	44	Bruddgrens...	37	44
C.512.1	KKR 200x2...	Real	40	Bruddgrens...	34	40
C.513.1	KKR 200x2...	Real	54	Bruddgrens...	45	54
C.514.1	KKR 250x2...	Real	34	Bruddgrens...	30	34
C.515.1	KKR 250x2...	Real	49	Bruddgrens...	44	49
C.516.1	KKR 250x2...	Real	37	Bruddgrens...	33	37

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
8	0	0	-	-
9	1	1	-	10
14	0	0	-	-
10	0	0	-	-
15	0	0	-	-
14	0	0	-	-
15	0	0	-	-
17	0	0	-	-
19	0	0	-	-
21	0	0	-	-
24	0	0	-	-
25	0	0	-	-
30	0	0	-	-
29	0	0	-	-
37	0	0	-	-
34	0	0	-	-
45	0	0	-	-
30	0	0	-	-
44	0	0	-	-
33	0	0	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
C.517.1	KKR 250x2...	Real	60	Bruddgrens...	54	60
C.518.1	KKR 250x2...	Real	33	Bruddgrens...	29	33
C.519.1	KKR 250x2...	Real	77	Bruddgrens...	69	77
C.520.1	KKR 200x2...	Real	15	Bruddgrens...	12	15
C.521.1	KKR 200x2...	Real	18	Bruddgrens...	15	18
C.522.1	KKR 200x2...	Real	21	Bruddgrens...	18	21
C.523.1	KKR 200x2...	Real	24	Bruddgrens...	20	24
C.524.1	KKR 200x2...	Real	27	Bruddgrens...	23	27
C.525.1	KKR 200x2...	Real	30	Bruddgrens...	25	30
C.526.1	KKR 200x2...	Real	32	Bruddgrens...	27	32
C.527.1	KKR 250x2...	Real	24	Bruddgrens...	22	24
C.528.1	KKR 250x2...	Real	23	Bruddgrens...	21	23
C.529.1	KKR 250x2...	Real	25	Bruddgrens...	22	25
C.530.1	KKR 250x2...	Real	16	Bruddgrens...	14	16
C.531.1	KKR 150x1...	Real	23	Bruddgrens...	16	23
C.532.1	KKR 150x1...	Real	13	Bruddgrens...	9	13
C.533.1	KKR 150x1...	Real	7	Bruddgrens...	5	7
T.1.1	KKR 250x2...	Real	25	Bruddgrens...	20	25
T.2.1	KKR 250x2...	Real	13	Bruddgrens...	10	13
T.3.1	KKR 250x2...	Real	7	Vind +	5	7

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
54	0	0	-	-
29	0	0	-	-
69	0	0	-	-
12	1	1	-	14
15	1	0	-	17
18	1	0	-	20
20	1	0	-	22
23	1	0	-	24
25	0	0	-	27
27	1	0	-	29
22	0	0	-	22
21	0	0	-	21
22	0	0	-	23
14	0	0	-	-
16	0	0	-	21
9	0	0	-	12
5	0	0	-	6
20	-	-	-	-
10	-	-	-	-
5	-	-	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
T.4.1	KKR 250x2...	Real	27	Bruddgrens...	22	27
T.5.1	KKR 200x2...	Real	38	Bruddgrens...	27	38
T.6.1	KKR 200x2...	Real	35	Bruddgrens...	25	35
T.7.1	KKR 200x2...	Real	32	Bruddgrens...	22	32
T.8.1	KKR 200x2...	Real	27	Bruddgrens...	19	27
T.9.1	KKR 200x2...	Real	24	Bruddgrens...	17	24
T.10.1	KKR 200x2...	Real	20	Bruddgrens...	14	20
T.11.1	KKR 200x2...	Real	17	Bruddgrens...	12	17
T.12.1	KKR 200x2...	Real	13	Bruddgrens...	9	13
T.13.1	KKR 250x2...	Real	22	Bruddgrens...	18	22
T.14.1	KKR 200x2...	Real	34	Bruddgrens...	24	34
T.15.1	KKR 200x2...	Real	32	Bruddgrens...	23	32
T.16.1	KKR 200x2...	Real	29	Bruddgrens...	21	29
T.17.1	KKR 200x2...	Real	25	Bruddgrens...	18	25
T.18.1	KKR 200x2...	Real	21	Bruddgrens...	15	21
T.19.1	KKR 200x2...	Real	17	Bruddgrens...	12	17
T.20.1	KKR 200x2...	Real	14	Bruddgrens...	10	14
T.21.1	KKR 200x2...	Real	10	Bruddgrens...	7	10
T.22.1	KKR 250x2...	Real	5	Bruddgrens...	4	5
T.23.1	KKR 200x2...	Real	18	Bruddgrens...	12	18

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
22	-	-	-	-
27	-	-	-	-
25	-	-	-	-
22	-	-	-	-
19	-	-	-	-
17	-	-	-	-
14	-	-	-	-
12	-	-	-	-
9	-	-	-	-
18	-	-	-	-
24	-	-	-	-
22	-	-	-	-
20	-	-	-	-
17	-	-	-	-
15	-	-	-	-
12	-	-	-	-
10	-	-	-	-
7	-	-	-	-
4	-	-	-	-
12	-	-	-	-



Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
T.24.1	KKR 200x2...	Real	20	Bruddgrens...	16	20
T.25.1	KKR 200x2...	Real	20	Bruddgrens...	17	20
T.26.1	KKR 200x2...	Real	17	Bruddgrens...	17	17
T.27.1	KKR 200x2...	Real	16	Bruddgrens...	16	15
T.28.1	KKR 200x2...	Real	15	Bruddgrens...	15	12
T.29.1	KKR 200x2...	Real	15	Bruddgrens...	15	8
T.30.1	KKR 200x2...	Real	15	Bruddgrens...	15	5
T.31.1	KKR 200x2...	Real	12	Bruddgrens...	12	4
T.32.1	KKR 200x2...	Real	5	Bruddgrens...	5	-
T.33.1	KKR 200x2...	Real	14	Bruddgrens...	14	6
T.34.1	KKR 200x2...	Real	8	Bruddgrens...	8	3
T.35.1	KKR 200x2...	Real	15	Bruddgrens...	15	9
T.36.1	KKR 200x2...	Real	10	Bruddgrens...	10	7
T.37.1	KKR 200x2...	Real	17	Bruddgrens...	17	13
T.38.1	KKR 200x2...	Real	11	Bruddgrens...	11	10
T.39.1	KKR 200x2...	Real	18	Bruddgrens...	18	16
T.40.1	KKR 200x2...	Real	13	Bruddgrens...	12	13
T.41.1	KKR 200x2...	Real	20	Bruddgrens...	19	20
T.42.1	KKR 200x2...	Real	16	Bruddgrens...	14	16
T.43.1	KKR 200x2...	Real	24	Bruddgrens...	21	24

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
14	-	-	-	-
14	-	-	-	-
12	-	-	-	-
10	-	-	-	-
8	-	-	-	-
6	-	-	-	-
3	-	-	-	-
3	-	-	-	-
-	-	-	-	-
5	-	-	-	-
2	-	-	-	-
7	-	-	-	-
5	-	-	-	-
9	-	-	-	-
7	-	-	-	-
12	-	-	-	-
10	-	-	-	-
15	-	-	-	-
12	-	-	-	-
18	-	-	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
T.44.1	KKR 200x2...	Real	20	Bruddgrens...	15	20
T.45.1	KKR 200x2...	Real	28	Bruddgrens...	23	28
T.46.1	KKR 200x2...	Real	24	Bruddgrens...	18	24
T.47.1	KKR 250x2...	Real	24	Bruddgrens...	20	24
T.48.1	KKR 250x2...	Real	19	Bruddgrens...	16	19
T.49.1	KKR 250x2...	Real	27	Bruddgrens...	22	27
T.50.1	KKR 250x2...	Real	25	Bruddgrens...	20	25
T.51.1	KKR 250x2...	Real	23	Bruddgrens...	19	23
T.52.1	KKR 250x2...	Real	38	Bruddgrens...	31	38
T.53.1	KKR 250x2...	Real	44	Bruddgrens...	35	44
T.54.1	KKR 250x2...	Real	33	Bruddgrens...	26	33
T.55.1	KKR 250x2...	Real	42	Bruddgrens...	33	42
T.56.1	KKR 250x2...	Real	29	Bruddgrens...	23	29
T.57.1	KKR 250x2...	Real	32	Bruddgrens...	25	32
T.58.1	KKR 250x2...	Real	18	Bruddgrens...	14	18
T.59.1	KKR 200x2...	Real	37	Bruddgrens...	26	37
T.60.1	KKR 200x2...	Real	15	Bruddgrens...	11	15
T.61.1	KKR 200x2...	Real	29	Bruddgrens...	20	29
T.62.1	KKR 200x2...	Real	18	Bruddgrens...	12	18
T.63.1	KKR 200x2...	Real	23	Bruddgrens...	16	23

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
15	-	-	-	-
21	-	-	-	-
18	-	-	-	-
20	-	-	-	-
16	-	-	-	-
22	-	-	-	-
20	-	-	-	-
19	-	-	-	-
31	-	-	-	-
35	-	-	-	-
26	-	-	-	-
33	-	-	-	-
23	-	-	-	-
25	-	-	-	-
14	-	-	-	-
26	-	-	-	-
11	-	-	-	-
20	-	-	-	-
12	-	-	-	-
16	-	-	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
T.64.1	KKR 200x2...	Real	19	Bruddgrens...	13	19
T.65.1	KKR 200x2...	Real	18	Bruddgrens...	13	18
T.66.1	KKR 200x2...	Real	18	Bruddgrens...	12	18
T.67.1	KKR 200x2...	Real	14	Bruddgrens...	10	14
T.68.1	KKR 200x2...	Real	16	Bruddgrens...	11	16
T.69.1	KKR 200x2...	Real	10	Bruddgrens...	7	10
T.70.1	KKR 200x2...	Real	14	Bruddgrens...	10	14
T.71.1	KKR 200x2...	Real	7	Bruddgrens...	5	7
T.72.1	KKR 200x2...	Real	12	Bruddgrens...	9	12
T.73.1	KKR 200x2...	Real	7	Bruddgrens...	5	7
T.74.1	KKR 200x2...	Real	10	Bruddgrens...	7	10
T.75.1	KKR 150x1...	Real	11	Bruddgrens...	6	11
T.76.1	KKR 150x1...	Real	8	Bruddgrens...	4	8
T.77.1	KKR 150x1...	Real	10	Bruddgrens...	5	10
T.78.1	KKR 150x1...	Real	5	Bruddgrens...	3	5
T.79.1	KKR 150x1...	Real	8	Bruddgrens...	4	8
T.80.1	KKR 150x1...	Real	3	Vind +	2	3
T.81.1	KKR 250x2...	Real	45	Bruddgrens...	36	45
T.82.1	KKR 250x2...	Real	47	Bruddgrens...	37	47
T.83.1	KKR 250x2...	Real	37	Bruddgrens...	29	37

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
13	-	-	-	-
13	-	-	-	-
12	-	-	-	-
10	-	-	-	-
11	-	-	-	-
7	-	-	-	-
10	-	-	-	-
5	-	-	-	-
9	-	-	-	-
5	-	-	-	-
7	-	-	-	-
6	-	-	-	-
4	-	-	-	-
5	-	-	-	-
3	-	-	-	-
4	-	-	-	-
2	-	-	-	-
36	-	-	-	-
37	-	-	-	-
29	-	-	-	-

Member	Section	Status	Maximum	Combination	RCS	FB
[-]	[-]	[-]	[%]	[-]	[%]	[%]
T.84.1	KKR 250x2...	Real	38	Bruddgrens...	30	38
T.85.1	KKR 250x2...	Real	22	Bruddgrens...	18	22
T.86.1	KKR 250x2...	Real	22	Bruddgrens...	18	22
T.87.1	KKR 200x2...	Real	21	Bruddgrens...	15	21
T.88.1	KKR 200x2...	Real	21	Bruddgrens...	15	21
T.89.1	KKR 200x2...	Real	15	Bruddgrens...	10	15
T.90.1	KKR 200x2...	Real	14	Bruddgrens...	10	14
T.91.1	KKR 200x2...	Real	12	Bruddgrens...	8	12
T.92.1	KKR 200x2...	Real	10	Bruddgrens...	7	10
T.93.1	KKR 200x2...	Real	11	Bruddgrens...	8	11
T.94.1	KKR 200x2...	Real	7	Bruddgrens...	5	7
T.95.1	KKR 200x2...	Real	5	Bruddgrens...	3	5
T.96.1	KKR 200x2...	Real	11	Bruddgrens...	7	11
T.97.1	KKR 200x2...	Real	3	Bruddgrens...	2	3
T.98.1	KKR 200x2...	Real	10	Bruddgrens...	7	10
T.99.1	KKR 200x2...	Real	9	Bruddgrens...	6	9
T.100.1	KKR 200x2...	Real	2	Bruddgrens...	1	2
T.101.1	KKR 200x2...	Real	7	Bruddgrens...	5	7
T.102.1	KKR 200x2...	Real	1	Bruddgrens...	1	1

TFB	LTB,t	LTB,b	SB	IA
[%]	[%]	[%]	[%]	[%]
30	-	-	-	-
18	-	-	-	-
18	-	-	-	-
15	-	-	-	-
15	-	-	-	-
10	-	-	-	-
10	-	-	-	-
8	-	-	-	-
7	-	-	-	-
8	-	-	-	-
5	-	-	-	-
3	-	-	-	-
7	-	-	-	-
2	-	-	-	-
7	-	-	-	-
6	-	-	-	-
1	-	-	-	-
5	-	-	-	-
1	-	-	-	-

## 2.5.2 Check Timber Design

Max. of load combinations, Panel, Utilization

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.1.1	47	Vind +	47	6	45	3
TP.2.1	22	Bruddgrens...	5	10	22	11
TP.3.1	48	Bruddgrens...	42	2	48	1
TP.4.1	47	Bruddgrens...	-	14	33	14
TP.5.1	46	Vind +	46	6	43	4
TP.6.1	42	Bruddgrens...	-	6	32	4
TP.7.1	54	Vind +	54	11	50	11
TP.8.1	94	Bruddgrens...	31	26	45	20
TP.9.1	59	Bruddgrens...	-	24	50	16
TP.10.1	56	Bruddgrens...	32	8	56	6
TP.11.1	85	Bruddgrens...	38	11	85	8
TP.12.1	71	Bruddgrens...	27	34	34	29
TP.13.1	31	Bruddgrens...	28	3	31	1
TP.14.1	24	Vind +	14	2	21	1
TP.15.1	34	Bruddgrens...	32	4	34	2
TP.16.1	32	Vind +	16	4	28	3
TP.17.1	52	Bruddgrens...	37	34	52	23
TP.18.1	52	Bruddgrens...	37	14	52	4
TP.19.1	46	Bruddgrens...	3	6	14	3

Txy	Tx	Ty
[%]	[%]	[%]
30	3	3
20	7	5
23	9	4
47	4	7
25	1	1
42	10	3
39	4	2
94	9	2
59	9	22
35	14	5
37	8	2
71	21	9
17	19	10
24	4	2
30	4	2
32	8	4
50	25	14
34	4	6
46	3	2

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.20.1	20	Bruddgrens...	4	5	4	3
TP.21.1	20	Bruddgrens...	16	6	15	3
TP.22.1	41	Bruddgrens...	13	14	7	9
TP.23.1	13	Bruddgrens...	8	3	8	2
TP.24.1	31	Bruddgrens...	18	12	12	13
TP.25.1	38	Bruddgrens...	19	24	15	18
TP.26.1	38	Bruddgrens...	14	15	16	17
TP.27.1	49	Bruddgrens...	26	25	18	18
TP.28.1	51	Bruddgrens...	23	16	24	24
TP.29.1	16	Bruddgrens...	10	2	9	2
TP.30.1	27	Bruddgrens...	23	4	22	3
TP.31.1	77	Bruddgrens...	55	18	36	16
TP.32.1	65	Bruddgrens...	26	50	22	33
TP.33.1	83	Bruddgrens...	17	35	8	24
TP.34.1	24	Bruddgrens...	15	19	15	13
TP.35.1	46	Bruddgrens...	29	13	27	8
TP.36.1	84	Vind +	84	23	58	19
TP.37.1	21	Bruddgrens...	9	4	6	2
TP.38.1	27	Bruddgrens...	9	18	8	11
TP.39.1	26	Bruddgrens...	23	6	26	3

Txy	Tx	Ty
[%]	[%]	[%]
20	3	2
20	3	1
14	41	27
8	13	2
20	31	26
38	32	30
38	34	34
47	49	31
51	46	51
5	16	5
9	27	4
55	77	37
55	49	65
22	83	45
11	24	22
18	46	10
38	48	59
9	21	14
16	27	15
21	3	3

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.40.1	22	Bruddgrens...	-	11	18	13
TP.41.1	24	Bruddgrens...	6	1	24	1
TP.42.1	45	Vind +	-	11	28	12
TP.43.1	17	Bruddgrens...	6	5	17	4
TP.44.1	43	Bruddgrens...	-	4	29	3
TP.45.1	33	Bruddgrens...	8	15	33	14
TP.46.1	75	Bruddgrens...	5	31	40	26
TP.47.1	88	Bruddgrens...	-	6	88	4
TP.48.1	88	Bruddgrens...	-	10	88	7
TP.49.1	42	Bruddgrens...	-	40	24	34
TP.50.1	26	Vind +	-	2	11	1
TP.51.1	27	Vind +	3	4	13	2
TP.52.1	27	Vind +	16	3	23	1
TP.53.1	31	Vind +	4	4	13	3
TP.54.1	35	Bruddgrens...	15	35	32	22
TP.55.1	32	Bruddgrens...	15	12	32	4
TP.56.1	2	Bruddgrens...	-	0	2	0
TP.57.1	56	Bruddgrens...	23	3	27	26
TP.58.1	15	Bruddgrens...	10	2	9	2
TP.59.1	27	Bruddgrens...	23	4	22	3

Txy	Tx	Ty
[%]	[%]	[%]
22	2	5
13	11	4
45	2	7
11	0	0
43	9	3
31	7	2
75	18	22
64	13	3
76	8	3
42	18	8
26	24	12
27	2	1
27	1	2
31	1	1
25	9	12
32	5	5
0	0	0
55	48	56
5	15	5
9	27	4

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.60.1	47	Bruddgrens...	25	18	19	11
TP.61.1	42	Bruddgrens...	7	16	6	10
TP.62.1	24	Bruddgrens...	16	19	15	12
TP.63.1	63	Bruddgrens...	5	33	26	29
TP.64.1	67	Bruddgrens...	3	4	67	2
TP.65.1	26	Bruddgrens...	22	6	26	5
TP.66.1	34	Bruddgrens...	2	27	32	19
TP.67.1	21	Bruddgrens...	13	9	12	8
TP.68.1	32	Bruddgrens...	10	4	9	5
TP.69.1	50	Bruddgrens...	17	9	17	10
TP.70.1	42	Bruddgrens...	38	21	35	11
TP.71.1	69	Bruddgrens...	38	32	36	33
TP.72.1	47	Bruddgrens...	14	15	14	14
TP.73.1	11	Bruddgrens...	6	2	6	1
TP.74.1	11	Bruddgrens...	6	3	6	2
TP.75.1	41	Bruddgrens...	18	8	18	7
TP.76.1	27	Bruddgrens...	12	4	10	4
TP.77.1	25	Bruddgrens...	17	19	13	18
TP.78.1	37	Bruddgrens...	17	6	17	5
TP.79.1	53	Bruddgrens...	17	22	17	20

Txy	Tx	Ty
[%]	[%]	[%]
30	47	28
9	42	23
11	24	21
63	8	6
32	1	1
20	4	3
34	6	5
6	21	18
4	32	7
21	37	50
27	42	24
57	55	69
14	47	18
2	11	3
4	11	8
33	41	20
6	27	8
25	25	24
11	37	8
31	41	53



Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.80.1	46	Bruddgrens...	17	10	16	11
TP.81.1	23	Bruddgrens...	15	18	15	9
TP.82.1	17	Bruddgrens...	14	5	14	2
TP.83.1	15	Bruddgrens...	15	3	14	2
TP.84.1	24	Bruddgrens...	17	2	14	2
TP.85.1	40	Bruddgrens...	5	16	5	20
TP.86.1	21	Bruddgrens...	16	2	21	1
TP.87.1	27	Bruddgrens...	-	10	15	12
TP.88.1	19	Bruddgrens...	1	1	19	1
TP.89.1	46	Vind +	-	12	24	12
TP.90.1	14	Bruddgrens...	2	1	14	1
TP.91.1	44	Bruddgrens...	-	4	25	4
TP.92.1	42	Vind +	5	12	37	9
TP.93.1	51	Vind +	-	9	23	6
TP.94.1	56	Bruddgrens...	-	6	41	1
TP.95.1	73	Bruddgrens...	-	2	52	3
TP.96.1	39	Bruddgrens...	-	6	12	4
TP.97.1	28	Bruddgrens...	-	2	11	1
TP.98.1	28	Vind +	3	3	12	1
TP.99.1	28	Vind +	13	3	20	2

Txy	Tx	Ty
[%]	[%]	[%]
40	46	21
22	23	21
14	17	4
13	15	4
13	24	3
12	40	32
16	3	3
27	1	2
11	10	3
46	3	7
6	0	0
44	9	3
42	3	1
51	4	9
56	3	3
73	2	1
39	4	3
28	2	2
28	2	1
28	1	2

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.100.1	31	Vind +	3	2	12	1
TP.101.1	25	Bruddgrens...	9	6	25	6
TP.102.1	32	Bruddgrens...	9	4	25	2
TP.103.1	2	Bruddgrens...	-	0	2	0
TP.104.1	59	Bruddgrens...	23	19	30	27
TP.105.1	16	Bruddgrens...	10	2	9	2
TP.106.1	28	Bruddgrens...	23	4	22	3
TP.107.1	57	Bruddgrens...	24	10	11	10
TP.108.1	45	Bruddgrens...	8	14	6	11
TP.109.1	24	Bruddgrens...	16	19	15	11
TP.110.1	28	Bruddgrens...	17	2	19	1
TP.111.1	23	Vind +	16	5	21	6
TP.112.1	36	Bruddgrens...	3	3	36	2
TP.113.1	21	Bruddgrens...	13	8	12	10
TP.114.1	32	Bruddgrens...	10	3	9	3
TP.115.1	53	Bruddgrens...	17	9	17	10
TP.116.1	43	Bruddgrens...	38	21	35	11
TP.117.1	71	Bruddgrens...	38	33	36	33
TP.118.1	48	Bruddgrens...	14	13	14	14
TP.119.1	11	Bruddgrens...	6	2	6	2

Txy	Tx	Ty
[%]	[%]	[%]
31	1	1
16	2	2
32	5	5
0	0	0
58	50	59
5	16	5
9	28	4
19	51	57
8	45	25
11	24	20
28	1	1
23	2	2
20	6	2
7	21	18
3	32	8
21	36	53
27	43	25
56	53	71
12	48	18
2	11	3

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.120.1	17	Bruddgrens...	6	2	6	1
TP.121.1	43	Bruddgrens...	18	8	18	7
TP.122.1	28	Bruddgrens...	11	4	10	4
TP.123.1	25	Bruddgrens...	15	19	13	17
TP.124.1	38	Bruddgrens...	17	4	17	3
TP.125.1	57	Bruddgrens...	17	14	17	21
TP.126.1	54	Bruddgrens...	16	7	14	13
TP.127.1	21	Bruddgrens...	15	16	16	10
TP.128.1	17	Bruddgrens...	14	4	14	2
TP.129.1	16	Bruddgrens...	15	3	14	2
TP.130.1	24	Bruddgrens...	16	2	14	2
TP.131.1	44	Bruddgrens...	5	16	5	22
TP.132.1	33	Bruddgrens...	15	5	13	5
TP.133.1	32	Bruddgrens...	14	5	13	5
TP.134.1	78	Bruddgrens...	3	4	78	3
TP.135.1	17	Bruddgrens...	11	2	17	1
TP.136.1	31	Bruddgrens...	1	10	17	10
TP.137.1	15	Bruddgrens...	-	1	15	1
TP.138.1	45	Bruddgrens...	-	9	22	8
TP.139.1	11	Bruddgrens...	-	1	11	1

Txy	Tx	Ty
[%]	[%]	[%]
4	17	8
32	43	22
5	28	8
24	25	23
8	38	8
26	45	57
28	54	21
14	21	12
7	17	4
7	16	5
7	24	4
12	44	36
24	33	15
21	32	16
64	1	1
13	2	2
31	1	2
9	6	2
45	5	6
6	0	0

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.140.1	48	Bruddgrens...	-	8	22	7
TP.141.1	33	Vind +	-	2	23	2
TP.142.1	51	Vind +	-	4	23	3
TP.143.1	27	Bruddgrens...	-	2	25	1
TP.144.1	34	Bruddgrens...	-	2	34	1
TP.145.1	37	Bruddgrens...	-	3	11	3
TP.146.1	28	Bruddgrens...	-	2	10	1
TP.147.1	29	Vind +	4	2	12	2
TP.148.1	29	Vind +	9	4	17	4
TP.149.1	32	Vind +	2	2	11	1
TP.150.1	21	Bruddgrens...	6	2	21	3
TP.151.1	31	Bruddgrens...	6	3	21	3
TP.152.1	2	Bruddgrens...	-	0	2	0
TP.153.1	62	Bruddgrens...	23	3	32	28
TP.154.1	16	Bruddgrens...	10	2	9	2
TP.155.1	27	Bruddgrens...	23	3	22	2
TP.156.1	60	Bruddgrens...	22	10	12	10
TP.157.1	45	Bruddgrens...	8	13	6	11
TP.158.1	23	Bruddgrens...	16	20	15	11
TP.159.1	20	Bruddgrens...	11	2	14	1

Txy	Tx	Ty
[%]	[%]	[%]
48	6	2
33	3	1
51	3	7
27	2	1
25	1	1
37	3	2
28	1	1
29	3	2
29	1	1
32	1	1
13	1	1
31	4	4
0	0	0
61	51	62
5	16	5
8	27	4
15	53	60
9	45	25
13	23	19
20	1	1

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.160.1	23	Vind +	11	5	17	5
TP.161.1	23	Bruddgrens...	-	2	23	1
TP.162.1	22	Bruddgrens...	14	8	12	9
TP.163.1	33	Bruddgrens...	10	3	9	3
TP.164.1	56	Bruddgrens...	17	9	17	11
TP.165.1	43	Bruddgrens...	38	21	35	9
TP.166.1	84	Bruddgrens...	38	37	36	36
TP.167.1	49	Bruddgrens...	15	10	15	13
TP.168.1	11	Bruddgrens...	6	2	6	1
TP.169.1	20	Bruddgrens...	6	2	6	1
TP.170.1	35	Bruddgrens...	18	8	18	7
TP.171.1	28	Bruddgrens...	11	3	10	3
TP.172.1	34	Bruddgrens...	15	18	13	16
TP.173.1	39	Bruddgrens...	17	4	17	3
TP.174.1	63	Bruddgrens...	17	12	17	21
TP.175.1	47	Bruddgrens...	16	10	14	13
TP.176.1	22	Bruddgrens...	16	16	14	11
TP.177.1	18	Bruddgrens...	14	5	14	2
TP.178.1	16	Bruddgrens...	14	3	14	2
TP.179.1	25	Bruddgrens...	15	3	14	1

Txy	Tx	Ty
[%]	[%]	[%]
23	3	2
20	1	0
8	22	18
3	33	8
21	36	56
26	43	25
55	50	84
10	49	18
2	11	3
5	20	8
30	35	24
5	28	8
25	34	29
7	39	8
22	52	63
20	47	21
11	22	13
4	18	4
4	16	7
3	25	4

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.180.1	45	Bruddgrens...	6	16	5	23
TP.181.1	33	Bruddgrens...	13	6	13	5
TP.182.1	43	Bruddgrens...	8	3	38	2
TP.183.1	14	Bruddgrens...	7	2	14	1
TP.184.1	25	Bruddgrens...	1	6	16	8
TP.185.1	11	Bruddgrens...	-	1	11	1
TP.186.1	44	Bruddgrens...	1	9	21	7
TP.187.1	11	Bruddgrens...	-	1	11	1
TP.188.1	49	Bruddgrens...	-	9	21	9
TP.189.1	32	Vind +	-	3	19	1
TP.190.1	47	Vind +	-	4	23	2
TP.191.1	24	Bruddgrens...	-	2	20	1
TP.192.1	24	Bruddgrens...	-	1	24	1
TP.193.1	35	Bruddgrens...	-	2	9	2
TP.194.1	27	Vind +	-	3	8	2
TP.195.1	29	Vind +	4	3	11	2
TP.196.1	29	Vind +	6	7	14	5
TP.197.1	31	Vind +	1	2	10	1
TP.198.1	16	Bruddgrens...	2	1	16	3
TP.199.1	30	Bruddgrens...	3	3	16	3

Txy	Tx	Ty
[%]	[%]	[%]
12	45	38
22	33	18
43	1	1
10	2	2
25	1	2
8	4	1
44	6	6
6	0	0
49	5	2
32	2	1
47	2	6
24	1	1
18	1	0
35	2	2
27	1	0
29	4	2
29	1	1
31	1	1
11	1	1
30	3	3

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.200.1	2	Bruddgrens...	-	0	2	0
TP.201.1	64	Bruddgrens...	23	5	33	29
TP.202.1	16	Bruddgrens...	10	2	9	2
TP.203.1	27	Bruddgrens...	23	3	22	2
TP.204.1	61	Bruddgrens...	20	9	12	10
TP.205.1	44	Bruddgrens...	8	13	6	11
TP.206.1	23	Bruddgrens...	16	20	15	10
TP.207.1	23	Bruddgrens...	14	1	16	1
TP.208.1	23	Bruddgrens...	7	3	14	3
TP.209.1	20	Bruddgrens...	-	2	19	1
TP.210.1	22	Bruddgrens...	14	8	12	9
TP.211.1	34	Bruddgrens...	10	3	9	3
TP.212.1	59	Bruddgrens...	17	8	17	11
TP.213.1	43	Bruddgrens...	38	20	35	7
TP.214.1	77	Bruddgrens...	38	35	36	34
TP.215.1	49	Bruddgrens...	15	8	15	11
TP.216.1	12	Bruddgrens...	6	2	6	1
TP.217.1	22	Bruddgrens...	6	3	6	1
TP.218.1	35	Bruddgrens...	18	8	18	7
TP.219.1	29	Bruddgrens...	10	3	10	3

Txy	Tx	Ty
[%]	[%]	[%]
0	0	0
62	52	64
5	16	5
8	27	4
13	53	61
10	44	25
13	23	18
23	1	1
23	4	2
20	1	0
8	22	18
3	34	8
21	36	59
26	43	26
49	46	77
9	49	16
3	12	3
6	22	9
29	35	26
5	29	8

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.220.1	34	Bruddgrens...	15	18	15	15
TP.221.1	38	Bruddgrens...	17	4	17	2
TP.222.1	63	Bruddgrens...	17	12	17	21
TP.223.1	48	Bruddgrens...	16	14	14	5
TP.224.1	22	Bruddgrens...	17	15	14	11
TP.225.1	18	Bruddgrens...	14	5	14	3
TP.226.1	17	Bruddgrens...	15	3	14	2
TP.227.1	26	Bruddgrens...	15	3	15	2
TP.228.1	46	Bruddgrens...	6	15	5	23
TP.229.1	34	Bruddgrens...	13	7	13	6
TP.230.1	31	Bruddgrens...	7	4	27	2
TP.231.1	11	Bruddgrens...	4	1	11	1
TP.232.1	22	Bruddgrens...	1	5	15	6
TP.233.1	11	Bruddgrens...	1	1	11	1
TP.234.1	40	Vind +	1	9	21	6
TP.235.1	11	Bruddgrens...	0	1	11	1
TP.236.1	49	Bruddgrens...	-	10	20	9
TP.237.1	30	Vind +	-	3	15	1
TP.238.1	42	Vind +	-	5	22	3
TP.239.1	22	Bruddgrens...	-	2	18	1

Txy	Tx	Ty
[%]	[%]	[%]
25	34	29
7	38	8
20	51	63
16	48	21
9	22	14
3	18	4
4	17	7
4	26	4
12	46	38
25	34	19
31	1	1
9	2	2
22	1	2
6	3	1
40	7	5
6	0	0
49	4	1
30	1	1
42	2	5
22	1	1



Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.240.1	18	Bruddgrens...	-	2	18	1
TP.241.1	32	Bruddgrens...	-	2	9	2
TP.242.1	26	Vind +	-	3	7	2
TP.243.1	27	Vind +	3	3	10	2
TP.244.1	29	Vind +	3	8	11	6
TP.245.1	29	Vind +	1	2	8	1
TP.246.1	13	Bruddgrens...	-	1	13	2
TP.247.1	29	Bruddgrens...	1	3	13	2
TP.248.1	2	Bruddgrens...	-	0	2	0
TP.249.1	65	Bruddgrens...	23	5	34	30
TP.250.1	16	Bruddgrens...	10	2	9	2
TP.251.1	27	Bruddgrens...	23	3	22	2
TP.252.1	61	Bruddgrens...	18	9	13	10
TP.253.1	42	Bruddgrens...	8	13	6	11
TP.254.1	22	Bruddgrens...	16	19	15	9
TP.255.1	25	Bruddgrens...	16	1	17	1
TP.256.1	24	Bruddgrens...	4	2	12	2
TP.257.1	19	Bruddgrens...	-	2	18	1
TP.258.1	21	Bruddgrens...	14	8	12	9
TP.259.1	34	Bruddgrens...	10	3	9	3

Txy	Tx	Ty
[%]	[%]	[%]
13	1	0
32	2	1
26	1	1
27	5	3
29	1	1
29	1	1
11	1	1
29	2	2
0	0	0
64	53	65
5	16	5
8	27	4
12	53	61
10	42	23
13	22	17
25	1	1
24	5	2
19	1	0
8	21	18
4	34	9

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.260.1	61	Bruddgrens...	17	3	18	12
TP.261.1	43	Bruddgrens...	37	19	35	6
TP.262.1	74	Bruddgrens...	37	32	36	31
TP.263.1	49	Bruddgrens...	15	6	15	10
TP.264.1	12	Bruddgrens...	6	2	6	1
TP.265.1	24	Bruddgrens...	6	3	6	2
TP.266.1	35	Bruddgrens...	18	8	18	7
TP.267.1	29	Bruddgrens...	10	3	10	3
TP.268.1	35	Bruddgrens...	15	17	16	15
TP.269.1	38	Bruddgrens...	17	4	17	2
TP.270.1	61	Bruddgrens...	17	13	17	20
TP.271.1	48	Bruddgrens...	16	14	15	7
TP.272.1	22	Bruddgrens...	17	14	14	12
TP.273.1	18	Bruddgrens...	14	4	14	3
TP.274.1	17	Bruddgrens...	15	3	14	2
TP.275.1	27	Bruddgrens...	15	3	15	2
TP.276.1	45	Bruddgrens...	6	14	5	23
TP.277.1	35	Bruddgrens...	13	8	13	6
TP.278.1	25	Bruddgrens...	6	4	20	3
TP.279.1	11	Bruddgrens...	1	1	10	1

Txy	Tx	Ty
[%]	[%]	[%]
22	37	61
25	43	26
44	44	74
9	49	15
3	12	3
7	24	9
30	35	27
5	29	8
25	35	29
7	38	8
18	50	61
13	48	21
8	22	14
4	18	4
4	17	6
5	27	4
12	45	38
26	35	20
25	1	1
11	2	2

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.280.1	20	Bruddgrens...	1	3	14	4
TP.281.1	11	Bruddgrens...	3	1	11	1
TP.282.1	37	Bruddgrens...	1	9	20	6
TP.283.1	10	Bruddgrens...	1	2	10	1
TP.284.1	48	Bruddgrens...	1	10	19	10
TP.285.1	28	Bruddgrens...	-	3	13	1
TP.286.1	37	Bruddgrens...	-	5	20	3
TP.287.1	20	Bruddgrens...	-	1	16	1
TP.288.1	13	Bruddgrens...	-	2	13	1
TP.289.1	29	Bruddgrens...	-	3	9	3
TP.290.1	24	Vind +	-	3	7	2
TP.291.1	25	Vind +	3	3	9	2
TP.292.1	27	Vind +	2	9	9	7
TP.293.1	26	Vind +	-	2	7	1
TP.294.1	10	Bruddgrens...	-	1	10	1
TP.295.1	26	Bruddgrens...	-	3	10	2
TP.296.1	1	Bruddgrens...	-	0	1	0
TP.297.1	65	Bruddgrens...	23	8	35	30
TP.298.1	16	Bruddgrens...	10	2	9	2
TP.299.1	26	Bruddgrens...	23	2	22	2

Txy	Tx	Ty
[%]	[%]	[%]
20	1	2
5	4	1
37	7	5
6	0	0
48	4	1
28	1	1
37	1	4
20	1	1
10	0	0
29	2	1
24	1	1
25	6	3
27	1	1
26	1	1
10	1	1
26	2	1
0	0	0
64	54	65
5	16	5
7	26	4

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.300.1	60	Bruddgrens...	15	9	16	10
TP.301.1	40	Bruddgrens...	8	13	5	10
TP.302.1	22	Bruddgrens...	16	18	15	9
TP.303.1	26	Bruddgrens...	17	2	18	1
TP.304.1	23	Bruddgrens...	2	2	10	2
TP.305.1	17	Bruddgrens...	-	2	16	1
TP.306.1	21	Bruddgrens...	13	8	12	8
TP.307.1	34	Bruddgrens...	10	3	9	3
TP.308.1	62	Bruddgrens...	17	2	19	12
TP.309.1	43	Bruddgrens...	37	18	36	7
TP.310.1	74	Bruddgrens...	37	30	36	28
TP.311.1	49	Bruddgrens...	15	10	15	9
TP.312.1	12	Bruddgrens...	6	2	6	1
TP.313.1	25	Bruddgrens...	6	3	6	2
TP.314.1	36	Bruddgrens...	18	8	18	7
TP.315.1	29	Bruddgrens...	10	2	10	3
TP.316.1	35	Bruddgrens...	15	17	16	14
TP.317.1	37	Bruddgrens...	17	4	17	2
TP.318.1	60	Bruddgrens...	17	14	17	20
TP.319.1	47	Bruddgrens...	16	14	15	7

Txy	Tx	Ty
[%]	[%]	[%]
12	52	60
10	40	22
12	22	16
26	1	1
23	5	1
17	1	1
8	21	18
4	34	9
23	37	62
25	43	26
40	42	74
8	49	14
4	12	3
7	25	9
32	36	28
5	29	8
25	35	29
7	37	8
18	48	60
12	47	21

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.320.1	22	Bruddgrens...	17	13	14	12
TP.321.1	18	Bruddgrens...	14	4	14	3
TP.322.1	17	Bruddgrens...	15	3	14	2
TP.323.1	27	Bruddgrens...	15	3	15	2
TP.324.1	43	Bruddgrens...	5	14	5	22
TP.325.1	37	Bruddgrens...	13	8	13	5
TP.326.1	20	Bruddgrens...	6	4	15	3
TP.327.1	13	Bruddgrens...	1	1	10	1
TP.328.1	17	Bruddgrens...	2	3	12	4
TP.329.1	11	Bruddgrens...	5	1	11	1
TP.330.1	34	Bruddgrens...	2	9	19	6
TP.331.1	10	Bruddgrens...	2	2	10	1
TP.332.1	47	Bruddgrens...	3	10	18	9
TP.333.1	26	Bruddgrens...	-	2	11	1
TP.334.1	32	Bruddgrens...	-	5	18	3
TP.335.1	17	Bruddgrens...	-	1	15	1
TP.336.1	12	Bruddgrens...	-	2	12	1
TP.337.1	26	Bruddgrens...	-	3	8	3
TP.338.1	22	Vind +	-	2	7	2
TP.339.1	23	Vind +	2	3	8	2

Txy	Tx	Ty
[%]	[%]	[%]
8	22	13
4	18	4
5	17	6
5	27	5
12	43	37
27	37	21
20	1	1
13	2	2
17	2	2
4	4	1
34	7	5
6	0	0
47	3	1
26	1	1
32	1	3
17	2	1
8	1	0
26	2	1
22	1	1
23	6	3

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.340.1	25	Vind +	2	10	8	7
TP.341.1	23	Vind +	-	1	6	1
TP.342.1	9	Bruddgrens...	-	1	8	1
TP.343.1	24	Bruddgrens...	-	3	8	2
TP.344.1	1	Bruddgrens...	-	0	1	0
TP.345.1	65	Bruddgrens...	23	14	35	30
TP.346.1	16	Bruddgrens...	10	2	9	2
TP.347.1	26	Bruddgrens...	23	2	22	2
TP.348.1	59	Bruddgrens...	14	9	16	10
TP.349.1	37	Bruddgrens...	8	12	5	9
TP.350.1	22	Bruddgrens...	16	18	15	8
TP.351.1	27	Bruddgrens...	18	2	19	1
TP.352.1	22	Bruddgrens...	1	2	10	2
TP.353.1	15	Bruddgrens...	-	2	15	1
TP.354.1	21	Bruddgrens...	13	8	13	8
TP.355.1	34	Bruddgrens...	10	3	9	3
TP.356.1	63	Bruddgrens...	17	12	19	12
TP.357.1	43	Bruddgrens...	37	17	36	8
TP.358.1	73	Bruddgrens...	37	27	36	18
TP.359.1	48	Bruddgrens...	15	9	15	8

Txy	Tx	Ty
[%]	[%]	[%]
25	1	1
23	1	1
9	1	1
24	2	1
0	0	0
64	54	65
6	16	5
7	26	4
11	51	59
9	37	20
12	22	15
27	1	1
22	5	1
15	1	1
8	21	17
4	34	9
24	37	63
25	43	26
36	42	73
8	48	13

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.360.1	12	Bruddgrens...	6	2	7	1
TP.361.1	26	Bruddgrens...	6	4	6	2
TP.362.1	38	Bruddgrens...	18	8	18	8
TP.363.1	30	Bruddgrens...	10	3	10	3
TP.364.1	35	Bruddgrens...	15	17	16	14
TP.365.1	37	Bruddgrens...	17	4	17	2
TP.366.1	58	Bruddgrens...	17	15	17	19
TP.367.1	47	Bruddgrens...	16	14	15	7
TP.368.1	22	Bruddgrens...	17	5	14	12
TP.369.1	18	Bruddgrens...	14	3	14	3
TP.370.1	18	Bruddgrens...	15	2	14	2
TP.371.1	28	Bruddgrens...	15	3	15	2
TP.372.1	41	Bruddgrens...	5	13	5	21
TP.373.1	38	Bruddgrens...	13	8	13	5
TP.374.1	16	Bruddgrens...	6	4	12	3
TP.375.1	15	Bruddgrens...	1	1	9	1
TP.376.1	15	Bruddgrens...	2	3	11	4
TP.377.1	10	Bruddgrens...	6	1	10	1
TP.378.1	31	Bruddgrens...	4	8	17	6
TP.379.1	9	Bruddgrens...	3	2	9	1

Txy	Tx	Ty
[%]	[%]	[%]
4	12	3
8	26	10
33	38	29
5	30	8
25	35	29
7	37	8
17	47	58
12	47	20
7	22	13
4	18	4
5	18	6
5	28	5
11	41	35
28	38	22
16	1	1
15	2	2
15	2	2
3	4	1
31	6	4
6	0	0

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.380.1	44	Bruddgrens...	6	9	16	9
TP.381.1	24	Bruddgrens...	0	2	10	2
TP.382.1	29	Bruddgrens...	-	5	15	3
TP.383.1	15	Bruddgrens...	-	1	13	1
TP.384.1	11	Bruddgrens...	1	2	11	1
TP.385.1	23	Bruddgrens...	-	4	8	3
TP.386.1	19	Vind +	-	2	6	1
TP.387.1	20	Bruddgrens...	2	3	7	2
TP.388.1	23	Vind +	1	10	7	8
TP.389.1	20	Vind +	-	1	5	1
TP.390.1	9	Bruddgrens...	-	2	8	1
TP.391.1	21	Bruddgrens...	-	2	8	2
TP.392.1	1	Bruddgrens...	-	0	1	0
TP.393.1	65	Bruddgrens...	23	15	35	30
TP.394.1	16	Bruddgrens...	10	2	9	2
TP.395.1	26	Bruddgrens...	23	2	22	2
TP.396.1	57	Bruddgrens...	13	9	16	9
TP.397.1	34	Bruddgrens...	7	12	4	8
TP.398.1	22	Bruddgrens...	16	17	15	8
TP.399.1	27	Bruddgrens...	18	2	19	1

Txy	Tx	Ty
[%]	[%]	[%]
44	3	1
24	1	1
29	1	3
15	2	1
8	1	0
23	2	1
19	2	1
20	7	4
23	1	1
20	1	1
9	2	1
21	2	2
0	0	0
64	54	65
6	16	5
7	26	4
11	50	57
9	34	18
11	22	14
27	1	1



Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.400.1	21	Bruddgrens...	-	3	9	3
TP.401.1	13	Bruddgrens...	-	1	12	1
TP.402.1	20	Bruddgrens...	13	8	13	8
TP.403.1	34	Bruddgrens...	9	3	9	3
TP.404.1	64	Bruddgrens...	17	13	19	9
TP.405.1	43	Bruddgrens...	37	17	36	8
TP.406.1	72	Bruddgrens...	37	25	37	16
TP.407.1	48	Bruddgrens...	16	9	15	6
TP.408.1	12	Bruddgrens...	6	2	7	1
TP.409.1	27	Bruddgrens...	6	4	6	2
TP.410.1	39	Bruddgrens...	18	9	18	8
TP.411.1	30	Bruddgrens...	10	3	10	3
TP.412.1	35	Bruddgrens...	16	17	16	13
TP.413.1	37	Bruddgrens...	17	3	17	2
TP.414.1	57	Bruddgrens...	17	16	17	19
TP.415.1	46	Bruddgrens...	16	14	15	6
TP.416.1	21	Bruddgrens...	17	5	14	11
TP.417.1	18	Bruddgrens...	14	3	14	3
TP.418.1	18	Bruddgrens...	14	2	15	2
TP.419.1	28	Bruddgrens...	15	3	15	2

Txy	Tx	Ty
[%]	[%]	[%]
21	6	1
13	1	1
8	20	17
4	34	9
25	37	64
24	43	26
33	42	72
8	48	12
4	12	3
8	27	10
34	39	29
5	30	8
25	35	29
7	37	8
17	46	57
11	46	20
7	21	13
4	18	4
4	18	6
5	28	5

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.420.1	39	Bruddgrens...	6	12	5	19
TP.421.1	39	Bruddgrens...	13	7	13	5
TP.422.1	16	Bruddgrens...	7	4	12	3
TP.423.1	16	Bruddgrens...	2	2	9	1
TP.424.1	13	Bruddgrens...	3	4	9	4
TP.425.1	9	Bruddgrens...	6	1	9	1
TP.426.1	28	Bruddgrens...	6	8	14	7
TP.427.1	9	Bruddgrens...	4	2	9	1
TP.428.1	41	Bruddgrens...	8	9	14	8
TP.429.1	22	Bruddgrens...	2	2	10	2
TP.430.1	26	Bruddgrens...	2	5	12	3
TP.431.1	12	Bruddgrens...	-	1	11	1
TP.432.1	9	Bruddgrens...	2	2	9	2
TP.433.1	20	Bruddgrens...	0	6	10	3
TP.434.1	16	Vind +	-	2	5	1
TP.435.1	17	Bruddgrens...	2	2	6	2
TP.436.1	21	Bruddgrens...	1	11	6	8
TP.437.1	17	Vind +	0	1	5	1
TP.438.1	10	Bruddgrens...	1	4	10	4
TP.439.1	19	Bruddgrens...	-	2	8	1

Txy	Tx	Ty
[%]	[%]	[%]
11	39	33
29	39	23
16	1	1
16	2	2
13	2	2
3	3	1
28	6	4
6	0	0
41	2	1
22	2	1
26	2	2
12	2	2
8	1	0
20	3	1
16	2	1
17	7	4
21	1	1
17	1	1
10	2	1
19	2	2

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.440.1	1	Bruddgrens...	-	0	1	-
TP.441.1	65	Bruddgrens...	23	30	34	20
TP.442.1	16	Bruddgrens...	10	3	9	2
TP.443.1	28	Bruddgrens...	23	1	22	2
TP.444.1	56	Bruddgrens...	12	9	15	9
TP.445.1	32	Bruddgrens...	5	11	3	7
TP.446.1	22	Bruddgrens...	16	17	15	8
TP.447.1	27	Bruddgrens...	18	2	19	1
TP.448.1	20	Bruddgrens...	-	4	9	3
TP.449.1	11	Bruddgrens...	-	1	11	1
TP.450.1	20	Bruddgrens...	14	8	13	8
TP.451.1	34	Bruddgrens...	9	3	9	3
TP.452.1	64	Bruddgrens...	17	14	20	9
TP.453.1	43	Bruddgrens...	37	16	36	9
TP.454.1	71	Bruddgrens...	37	23	37	16
TP.455.1	47	Bruddgrens...	16	9	16	5
TP.456.1	12	Bruddgrens...	6	2	7	1
TP.457.1	26	Bruddgrens...	6	4	6	3
TP.458.1	40	Bruddgrens...	18	9	18	7
TP.459.1	30	Bruddgrens...	10	4	10	3

Txy	Tx	Ty
[%]	[%]	[%]
0	0	0
64	53	65
6	16	5
7	28	4
11	49	56
7	32	16
11	22	14
27	1	1
20	6	1
11	1	1
8	20	17
4	34	9
26	37	64
24	43	26
31	42	71
8	47	12
4	12	3
8	26	10
35	40	30
5	30	8

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.460.1	35	Bruddgrens...	16	17	16	13
TP.461.1	37	Bruddgrens...	17	3	17	2
TP.462.1	57	Bruddgrens...	17	17	17	19
TP.463.1	45	Bruddgrens...	16	14	15	5
TP.464.1	21	Bruddgrens...	17	5	14	11
TP.465.1	18	Bruddgrens...	14	3	14	3
TP.466.1	18	Bruddgrens...	14	2	15	2
TP.467.1	29	Bruddgrens...	14	3	15	2
TP.468.1	36	Bruddgrens...	6	12	4	18
TP.469.1	40	Bruddgrens...	13	7	13	5
TP.470.1	19	Bruddgrens...	7	4	11	3
TP.471.1	17	Bruddgrens...	2	2	7	2
TP.472.1	45	Bruddgrens...	5	45	9	1
TP.473.1	11	Bruddgrens...	6	1	8	1
TP.474.1	29	Bruddgrens...	9	15	13	12
TP.475.1	8	Bruddgrens...	4	2	8	1
TP.476.1	32	Bruddgrens...	10	9	13	6
TP.477.1	10	Bruddgrens...	2	2	10	1
TP.478.1	9	Bruddgrens...	3	6	6	2
TP.479.1	16	Bruddgrens...	1	5	8	2

Txy	Tx	Ty
[%]	[%]	[%]
25	35	29
7	37	8
16	45	57
9	45	20
8	21	12
4	18	4
4	18	6
6	29	5
11	36	31
29	40	24
19	1	1
17	7	7
25	2	3
2	11	4
29	5	3
6	0	0
32	8	2
8	2	2
9	0	0
16	1	2

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.480.1	14	Vind +	-	2	4	1
TP.481.1	15	Bruddgrens...	2	2	5	1
TP.482.1	19	Bruddgrens...	2	10	4	7
TP.483.1	16	Bruddgrens...	-	1	4	1
TP.484.1	9	Bruddgrens...	0	5	9	5
TP.485.1	16	Bruddgrens...	0	2	7	2
TP.486.1	1	Bruddgrens...	-	0	1	-
TP.487.1	66	Bruddgrens...	23	44	34	3
TP.488.1	17	Bruddgrens...	10	3	9	2
TP.489.1	30	Bruddgrens...	23	16	22	1
TP.490.1	26	Bruddgrens...	17	2	19	1
TP.491.1	18	Bruddgrens...	-	11	7	2
TP.492.1	10	Bruddgrens...	1	1	10	1
TP.493.1	20	Bruddgrens...	14	9	13	8
TP.494.1	33	Bruddgrens...	9	3	9	3
TP.495.1	63	Bruddgrens...	17	14	20	9
TP.496.1	41	Bruddgrens...	18	9	18	6
TP.497.1	31	Bruddgrens...	10	4	10	3
TP.498.1	33	Bruddgrens...	6	10	4	16
TP.499.1	51	Bruddgrens...	18	8	18	6

Txy	Tx	Ty
[%]	[%]	[%]
14	2	1
15	9	5
19	1	1
16	1	1
7	2	2
16	3	2
0	0	0
66	53	64
6	17	5
13	30	4
26	1	1
18	6	1
10	1	1
7	20	16
4	33	9
27	37	63
35	41	29
6	31	8
11	33	28
35	51	29

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.500.1	19	Bruddgrens...	1	2	9	2
TP.501.1	26	Bruddgrens...	2	5	6	4
TP.502.1	12	Bruddgrens...	2	2	8	1
TP.503.1	25	Bruddgrens...	0	12	8	6
TP.504.1	37	Bruddgrens...	21	3	21	3
TP.505.1	24	Bruddgrens...	21	3	21	2
TP.506.1	24	Bruddgrens...	20	3	20	3
TP.507.1	23	Bruddgrens...	20	2	20	2
TP.508.1	42	Bruddgrens...	37	15	36	10
TP.509.1	70	Bruddgrens...	37	23	37	16
TP.510.1	46	Bruddgrens...	16	9	16	5
TP.511.1	12	Bruddgrens...	6	2	7	1
TP.512.1	26	Bruddgrens...	6	4	6	3
TP.513.1	29	Bruddgrens...	6	9	3	6
TP.514.1	57	Bruddgrens...	19	12	16	10
TP.515.1	21	Bruddgrens...	11	4	11	3
TP.516.1	23	Bruddgrens...	14	10	13	3
TP.517.1	41	Bruddgrens...	16	7	15	5
TP.518.1	19	Bruddgrens...	16	5	14	7
TP.519.1	16	Bruddgrens...	8	5	7	3

Txy	Tx	Ty
[%]	[%]	[%]
19	1	1
26	1	0
12	2	2
25	1	2
7	37	7
8	24	7
7	24	5
9	23	4
25	42	26
31	42	70
8	46	12
4	12	3
8	26	10
7	29	15
14	48	57
6	21	8
7	23	7
7	41	16
11	19	10
10	16	8

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.520.1	15	Bruddgrens...	11	5	9	3
TP.521.1	18	Bruddgrens...	3	2	8	2
TP.522.1	44	Bruddgrens...	31	31	21	16
TP.523.1	10	Bruddgrens...	5	2	6	1
TP.524.1	30	Vind +	30	14	22	10
TP.525.1	6	Bruddgrens...	3	2	6	1
TP.526.1	36	Bruddgrens...	16	5	5	5
TP.527.1	7	Bruddgrens...	4	5	7	2
TP.528.1	10	Bruddgrens...	8	4	3	1
TP.529.1	13	Bruddgrens...	0	4	4	2
TP.530.1	11	Bruddgrens...	1	1	4	1
TP.531.1	16	Bruddgrens...	4	2	5	2
TP.532.1	19	Bruddgrens...	3	11	3	8
TP.533.1	14	Bruddgrens...	2	1	4	1
TP.534.1	7	Bruddgrens...	0	5	7	1
TP.535.1	13	Bruddgrens...	0	4	7	3
TP.536.1	1	Bruddgrens...	-	0	1	-
TP.537.1	64	Bruddgrens...	34	27	26	30
TP.538.1	16	Bruddgrens...	10	3	9	2
TP.539.1	36	Bruddgrens...	23	10	23	6

Txy	Tx	Ty
[%]	[%]	[%]
5	15	7
18	6	7
44	5	4
3	10	3
19	13	6
5	0	0
36	6	2
7	5	2
10	1	0
13	1	2
11	1	0
16	9	5
19	1	2
14	1	1
6	3	2
13	2	2
0	0	0
62	52	64
8	16	7
10	36	16

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.540.1	26	Bruddgrens...	16	2	19	1
TP.541.1	22	Vind +	2	12	9	5
TP.542.1	7	Bruddgrens...	1	1	7	1
TP.543.1	19	Bruddgrens...	14	8	13	8
TP.544.1	33	Bruddgrens...	9	3	9	3
TP.545.1	63	Bruddgrens...	17	15	20	9
TP.546.1	53	Bruddgrens...	18	12	18	9
TP.547.1	34	Bruddgrens...	10	4	10	4
TP.548.1	30	Bruddgrens...	6	11	4	14
TP.549.1	17	Bruddgrens...	5	4	13	3
TP.550.1	16	Bruddgrens...	1	1	6	2
TP.551.1	14	Vind +	0	3	4	1
TP.552.1	9	Bruddgrens...	1	2	5	1
TP.553.1	22	Bruddgrens...	-	7	12	3
TP.554.1	42	Bruddgrens...	37	13	36	9
TP.555.1	69	Bruddgrens...	37	22	37	19
TP.556.1	46	Bruddgrens...	16	7	16	6
TP.557.1	12	Bruddgrens...	6	2	7	1
TP.558.1	25	Bruddgrens...	6	4	6	3
TP.559.1	27	Bruddgrens...	4	9	3	5

Txy	Tx	Ty
[%]	[%]	[%]
26	1	1
22	6	1
7	1	1
7	19	16
4	33	9
25	37	63
31	53	36
5	34	10
9	30	26
17	4	1
16	2	1
14	1	0
9	2	1
22	2	2
25	42	25
33	42	69
8	46	12
5	12	3
8	25	10
6	27	14



Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.560.1	37	Bruddgrens...	13	5	9	7
TP.561.1	22	Bruddgrens...	15	4	15	4
TP.562.1	18	Bruddgrens...	15	5	15	3
TP.563.1	19	Bruddgrens...	11	6	11	4
TP.564.1	20	Bruddgrens...	11	8	11	9
TP.565.1	17	Bruddgrens...	4	2	8	1
TP.566.1	31	Bruddgrens...	9	20	16	15
TP.567.1	9	Vind +	4	2	4	1
TP.568.1	20	Bruddgrens...	8	6	15	5
TP.569.1	5	Bruddgrens...	2	2	5	1
TP.570.1	23	Bruddgrens...	2	6	4	6
TP.571.1	8	Bruddgrens...	3	5	6	2
TP.572.1	4	Vind +	4	0	3	0
TP.573.1	10	Bruddgrens...	1	4	3	2
TP.574.1	9	Bruddgrens...	2	1	3	0
TP.575.1	11	Bruddgrens...	1	2	3	2
TP.576.1	16	Bruddgrens...	0	14	3	10
TP.577.1	10	Bruddgrens...	3	2	2	1
TP.578.1	7	Bruddgrens...	1	3	7	2
TP.579.1	10	Bruddgrens...	1	7	7	4

Txy	Tx	Ty
[%]	[%]	[%]
13	25	37
6	22	7
5	18	10
7	19	16
6	20	10
17	7	5
31	5	2
3	9	3
20	14	5
5	0	0
23	1	1
8	6	2
2	1	0
10	1	1
9	1	1
11	8	4
16	1	2
10	1	1
6	5	4
10	3	3

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.580.1	0	Bruddgrens...	-	0	0	-
TP.581.1	63	Bruddgrens...	34	30	26	29
TP.582.1	17	Bruddgrens...	10	3	9	2
TP.583.1	35	Bruddgrens...	23	10	23	6
TP.584.1	25	Bruddgrens...	15	2	18	1
TP.585.1	22	Vind +	3	10	8	6
TP.586.1	7	Bruddgrens...	2	1	6	0
TP.587.1	19	Bruddgrens...	14	8	13	8
TP.588.1	33	Bruddgrens...	9	5	9	3
TP.589.1	62	Bruddgrens...	17	16	19	9
TP.590.1	54	Bruddgrens...	18	12	18	9
TP.591.1	35	Bruddgrens...	10	4	10	4
TP.592.1	28	Bruddgrens...	6	14	4	13
TP.593.1	11	Bruddgrens...	4	4	7	2
TP.594.1	14	Bruddgrens...	1	2	5	1
TP.595.1	11	Vind +	-	3	3	2
TP.596.1	8	Bruddgrens...	2	1	4	1
TP.597.1	20	Bruddgrens...	0	3	4	2
TP.598.1	42	Bruddgrens...	34	13	37	13
TP.599.1	67	Bruddgrens...	36	21	37	19

Txy	Tx	Ty
[%]	[%]	[%]
0	0	0
62	51	63
8	17	7
9	35	15
25	1	1
22	7	1
7	1	0
8	19	16
4	33	9
25	37	62
33	54	36
5	35	10
8	28	24
11	1	0
14	2	0
11	1	0
8	1	0
20	2	2
25	42	25
36	42	67

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.600.1	45	Bruddgrens...	16	7	16	6
TP.601.1	12	Bruddgrens...	6	3	7	1
TP.602.1	25	Bruddgrens...	6	5	6	3
TP.603.1	26	Bruddgrens...	3	10	3	4
TP.604.1	36	Bruddgrens...	14	6	9	7
TP.605.1	21	Bruddgrens...	15	4	15	4
TP.606.1	18	Bruddgrens...	15	5	15	3
TP.607.1	19	Bruddgrens...	11	6	11	4
TP.608.1	21	Bruddgrens...	11	8	11	9
TP.609.1	24	Bruddgrens...	4	9	10	5
TP.610.1	62	Bruddgrens...	10	39	32	24
TP.611.1	20	Bruddgrens...	3	10	3	4
TP.612.1	50	Bruddgrens...	8	18	28	17
TP.613.1	10	Bruddgrens...	1	10	5	4
TP.614.1	29	Bruddgrens...	0	29	5	18
TP.615.1	12	Bruddgrens...	7	6	12	3
TP.616.1	4	Bruddgrens...	4	2	4	1
TP.617.1	17	Bruddgrens...	1	16	2	3
TP.618.1	14	Bruddgrens...	2	3	2	1
TP.619.1	19	Bruddgrens...	2	3	2	3

Txy	Tx	Ty
[%]	[%]	[%]
8	45	12
5	12	3
9	25	10
6	26	13
12	23	36
6	21	7
5	18	9
7	19	15
6	21	10
24	18	10
62	16	6
7	20	6
50	16	12
8	0	0
29	3	2
12	7	3
4	1	0
17	7	4
8	14	7
8	19	9

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.620.1	23	Bruddgrens...	1	23	2	21
TP.621.1	9	Bruddgrens...	1	9	2	3
TP.622.1	35	Bruddgrens...	6	33	21	18
TP.623.1	41	Bruddgrens...	5	34	21	20
TP.624.1	0	Bruddgrens...	0	0	0	0
TP.625.1	87	Bruddgrens...	50	47	36	41
TP.626.1	26	Bruddgrens...	16	5	16	3
TP.627.1	48	Bruddgrens...	38	8	37	9
TP.628.1	50	Bruddgrens...	12	2	30	4
TP.629.1	25	Bruddgrens...	3	23	10	13
TP.630.1	9	Bruddgrens...	2	2	6	1
TP.631.1	33	Bruddgrens...	21	14	20	15
TP.632.1	48	Bruddgrens...	15	17	14	7
TP.633.1	84	Bruddgrens...	29	25	28	14
TP.634.1	71	Bruddgrens...	30	16	30	10
TP.635.1	52	Bruddgrens...	17	8	16	6
TP.636.1	35	Bruddgrens...	7	22	5	14
TP.637.1	16	Bruddgrens...	8	15	16	5
TP.638.1	12	Bruddgrens...	1	9	3	4
TP.639.1	14	Vind +	0	14	1	7

Txy	Tx	Ty
[%]	[%]	[%]
22	4	3
7	1	2
35	25	9
41	16	10
0	0	0
83	73	87
12	26	10
15	48	19
50	2	2
25	16	4
9	3	1
13	33	28
6	48	13
38	57	84
44	71	53
10	52	14
12	35	27
15	1	1
12	11	2
10	2	2

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.640.1	7	Bruddgrens...	1	5	2	0
TP.641.1	16	Bruddgrens...	1	7	2	3
TP.642.1	29	Bruddgrens...	25	21	23	12
TP.643.1	19	Bruddgrens...	10	4	10	2
TP.644.1	60	Bruddgrens...	10	9	10	4
TP.645.1	30	Bruddgrens...	7	17	4	5
TP.646.1	39	Bruddgrens...	22	8	8	8
TP.647.1	39	Bruddgrens...	24	7	24	7
TP.648.1	30	Bruddgrens...	25	13	25	11
TP.649.1	21	Bruddgrens...	13	7	11	5
TP.650.1	22	Bruddgrens...	13	14	11	10
TP.651.1	32	Bruddgrens...	27	11	27	10
TP.652.1	39	Bruddgrens...	29	10	27	10
TP.653.1	42	Bruddgrens...	31	10	27	10
TP.654.1	42	Bruddgrens...	32	10	27	10
TP.655.1	43	Bruddgrens...	32	10	27	10
TP.656.1	43	Bruddgrens...	32	10	27	10
TP.657.1	43	Bruddgrens...	32	10	27	10
TP.658.1	43	Bruddgrens...	32	10	27	10
TP.659.1	43	Bruddgrens...	33	10	27	10

Txy	Tx	Ty
[%]	[%]	[%]
7	3	2
16	12	9
18	29	20
8	19	5
14	60	22
10	30	19
17	23	39
11	39	14
8	30	29
8	21	17
7	22	11
15	32	13
15	39	13
15	42	14
15	42	14
15	43	14
15	43	14
15	43	14
15	43	14
15	43	14

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.660.1	44	Bruddgrens...	34	10	28	9
TP.661.1	41	Bruddgrens...	41	10	34	10
TP.662.1	39	Bruddgrens...	39	10	33	10
TP.663.1	39	Bruddgrens...	39	10	34	10
TP.664.1	38	Bruddgrens...	38	10	34	10
TP.665.1	37	Bruddgrens...	37	10	34	10
TP.666.1	37	Bruddgrens...	37	10	34	10
TP.667.1	37	Bruddgrens...	37	10	34	10
TP.668.1	37	Bruddgrens...	37	10	34	10
TP.669.1	37	Bruddgrens...	37	10	34	10
TP.670.1	37	Bruddgrens...	37	10	34	10
TP.671.1	38	Bruddgrens...	38	10	35	10
TP.672.1	22	Bruddgrens...	20	8	19	7
TP.673.1	19	Bruddgrens...	19	5	17	4
TP.674.1	21	Bruddgrens...	20	6	19	6
TP.675.1	22	Bruddgrens...	20	6	19	6
TP.676.1	22	Bruddgrens...	20	6	19	6
TP.677.1	22	Bruddgrens...	20	6	19	6
TP.678.1	22	Bruddgrens...	20	6	19	6
TP.679.1	22	Bruddgrens...	20	7	19	6

Txy	Tx	Ty
[%]	[%]	[%]
15	44	14
12	30	7
10	29	7
10	30	7
9	30	7
9	30	7
9	30	7
9	30	7
9	30	7
9	30	7
9	30	7
9	30	7
9	30	7
8	22	12
7	19	10
8	21	8
8	22	8
8	22	8
8	22	8
8	22	8
8	22	9

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.680.1	21	Bruddgrens...	20	7	19	6
TP.681.1	21	Bruddgrens...	20	7	19	6
TP.682.1	14	Bruddgrens...	14	5	13	4
TP.683.1	52	Bruddgrens...	30	26	29	26
TP.684.1	54	Bruddgrens...	31	25	29	26
TP.685.1	55	Bruddgrens...	31	25	29	26
TP.686.1	55	Bruddgrens...	31	25	29	27
TP.687.1	54	Bruddgrens...	31	25	29	27
TP.688.1	54	Bruddgrens...	31	25	29	28
TP.689.1	53	Bruddgrens...	31	25	29	28
TP.690.1	52	Bruddgrens...	31	26	29	28
TP.691.1	52	Bruddgrens...	31	26	29	28
TP.692.1	51	Bruddgrens...	30	26	29	28
TP.693.1	57	Bruddgrens...	23	21	21	22
TP.694.1	26	Bruddgrens...	15	5	15	4
TP.695.1	58	Bruddgrens...	21	20	19	22
TP.696.1	37	Bruddgrens...	13	13	12	17
TP.697.1	17	Bruddgrens...	9	4	9	2
TP.698.1	17	Bruddgrens...	9	4	9	2
TP.699.1	37	Bruddgrens...	13	13	12	17

Txy	Tx	Ty
[%]	[%]	[%]
8	21	9
8	21	9
3	14	5
30	52	37
29	54	37
30	55	38
30	55	34
30	54	34
30	54	35
30	53	35
30	52	35
30	52	35
30	51	35
23	57	32
7	26	9
30	58	39
24	37	28
5	17	5
5	17	5
25	37	29

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.700.1	43	Bruddgrens...	11	10	6	12
TP.701.1	11	Bruddgrens...	10	8	4	4
TP.702.1	41	Bruddgrens...	18	22	18	17
TP.703.1	47	Bruddgrens...	24	4	24	2
TP.704.1	65	Bruddgrens...	23	24	23	29
TP.705.1	57	Bruddgrens...	21	13	21	3
TP.706.1	36	Bruddgrens...	20	14	19	9
TP.707.1	41	Bruddgrens...	15	11	14	14
TP.708.1	80	Bruddgrens...	13	15	11	13
TP.709.1	45	Vind +	45	5	44	4
TP.710.1	19	Bruddgrens...	14	5	15	4
TP.711.1	19	Bruddgrens...	14	5	15	4
TP.712.1	19	Bruddgrens...	14	5	15	4
TP.713.1	19	Bruddgrens...	14	5	14	3
TP.714.1	20	Bruddgrens...	15	5	14	3
TP.715.1	20	Bruddgrens...	15	5	14	3
TP.716.1	21	Bruddgrens...	15	5	14	3
TP.717.1	22	Bruddgrens...	15	5	14	3
TP.718.1	22	Bruddgrens...	14	6	14	3
TP.719.1	22	Bruddgrens...	14	7	14	3

Txy	Tx	Ty
[%]	[%]	[%]
15	24	43
11	1	1
30	41	35
8	47	9
22	54	65
8	57	27
10	30	36
24	41	37
19	50	80
21	6	3
11	19	8
11	19	8
12	19	8
12	19	8
13	20	8
14	20	8
16	21	8
17	22	8
19	22	8
17	22	8



Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.720.1	16	Bruddgrens...	14	4	13	4
TP.721.1	31	Bruddgrens...	22	4	22	3
TP.722.1	34	Bruddgrens...	22	8	22	8
TP.723.1	24	Bruddgrens...	18	2	18	2
TP.724.1	27	Bruddgrens...	19	19	18	10
TP.725.1	25	Bruddgrens...	20	11	19	5
TP.726.1	32	Bruddgrens...	25	9	23	11
TP.727.1	35	Bruddgrens...	25	10	25	4
TP.728.1	47	Bruddgrens...	23	7	23	7
TP.729.1	41	Bruddgrens...	25	2	24	3
TP.730.1	80	Bruddgrens...	25	19	24	16
TP.731.1	26	Bruddgrens...	15	2	15	2
TP.732.1	52	Bruddgrens...	15	13	14	10
TP.733.1	16	Bruddgrens...	11	1	11	1
TP.734.1	26	Bruddgrens...	15	2	15	1
TP.735.1	52	Bruddgrens...	15	12	14	10
TP.736.1	16	Bruddgrens...	11	1	11	1
TP.737.1	56	Bruddgrens...	21	4	19	4
TP.738.1	91	Bruddgrens...	25	14	24	18
TP.739.1	56	Bruddgrens...	32	29	32	30

Txy	Tx	Ty
[%]	[%]	[%]
7	16	13
10	31	8
14	34	34
5	24	6
17	27	8
11	25	24
15	32	18
17	35	10
19	47	23
11	41	10
23	55	80
8	26	7
15	29	52
3	16	5
8	26	7
15	29	52
3	16	5
7	56	11
48	91	58
24	56	55

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.740.1	68	Bruddgrens...	15	8	19	12
TP.741.1	27	Bruddgrens...	20	14	20	15
TP.742.1	37	Bruddgrens...	13	3	12	3
TP.743.1	37	Bruddgrens...	13	3	12	3
TP.744.1	68	Bruddgrens...	15	8	19	12
TP.745.1	28	Bruddgrens...	20	16	20	15
TP.746.1	39	Bruddgrens...	13	3	11	2
TP.747.1	35	Bruddgrens...	18	7	15	10
TP.748.1	24	Bruddgrens...	20	16	20	16
TP.749.1	39	Bruddgrens...	13	2	12	2
TP.750.1	37	Bruddgrens...	14	5	14	10
TP.751.1	24	Bruddgrens...	20	16	20	16
TP.752.1	38	Bruddgrens...	13	2	12	2
TP.753.1	36	Bruddgrens...	14	6	14	10
TP.754.1	25	Bruddgrens...	20	16	20	17
TP.755.1	38	Bruddgrens...	13	3	12	2
TP.756.1	34	Bruddgrens...	14	7	14	10
TP.757.1	26	Bruddgrens...	20	17	20	17
TP.758.1	37	Bruddgrens...	13	3	12	2
TP.759.1	33	Bruddgrens...	14	7	14	10

Txy	Tx	Ty
[%]	[%]	[%]
35	68	41
12	27	25
5	37	8
5	37	8
35	68	41
12	28	26
6	39	9
35	33	30
10	24	21
6	39	9
27	37	29
9	24	22
6	38	8
25	36	28
10	25	23
6	38	8
24	34	28
10	26	24
6	37	8
23	33	27

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.760.1	26	Bruddgrens...	20	17	20	18
TP.761.1	36	Bruddgrens...	13	3	12	2
TP.762.1	31	Bruddgrens...	14	8	14	9
TP.763.1	27	Bruddgrens...	20	18	20	18
TP.764.1	35	Bruddgrens...	13	3	12	2
TP.765.1	30	Bruddgrens...	14	9	14	9
TP.766.1	29	Bruddgrens...	20	19	20	19
TP.767.1	34	Bruddgrens...	13	4	12	2
TP.768.1	27	Bruddgrens...	14	9	14	8
TP.769.1	30	Bruddgrens...	19	19	19	20
TP.770.1	30	Bruddgrens...	13	4	12	2
TP.771.1	22	Bruddgrens...	14	11	14	8
TP.772.1	29	Bruddgrens...	19	20	19	20
TP.773.1	29	Bruddgrens...	13	4	12	2
TP.774.1	21	Bruddgrens...	14	10	14	7
TP.775.1	35	Bruddgrens...	19	20	19	20
TP.776.1	30	Bruddgrens...	13	4	12	2
TP.777.1	22	Bruddgrens...	14	12	14	7
TP.778.1	32	Bruddgrens...	19	21	19	21
TP.779.1	40	Bruddgrens...	18	3	18	3

Txy	Tx	Ty
[%]	[%]	[%]
11	26	25
5	36	8
22	31	26
11	27	27
5	35	7
21	30	25
12	28	29
5	34	7
19	27	23
13	29	30
5	30	10
14	21	22
14	29	29
5	29	8
14	21	21
16	35	30
5	30	10
14	21	22
17	31	32
8	40	13

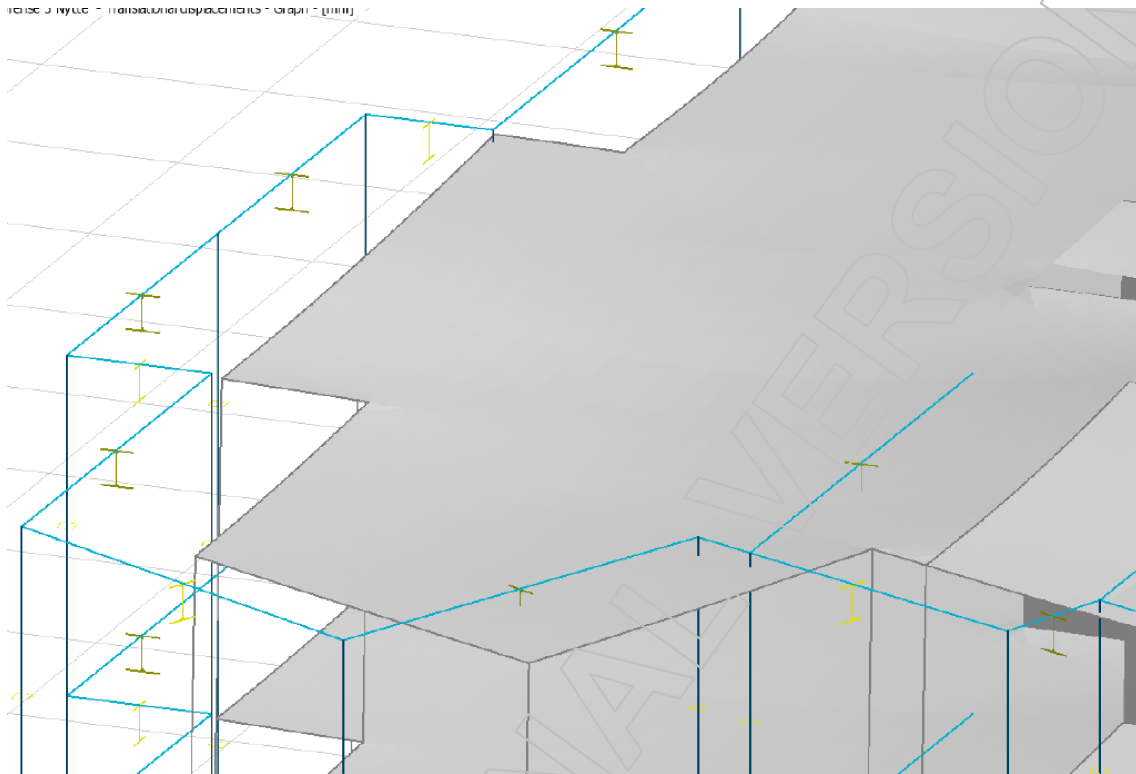
Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.780.1	29	Bruddgrens...	17	8	17	8
TP.781.1	20	Bruddgrens...	6	5	5	4
TP.782.1	40	Bruddgrens...	18	3	18	3
TP.783.1	29	Bruddgrens...	17	9	17	8
TP.784.1	38	Bruddgrens...	18	3	18	3
TP.785.1	30	Bruddgrens...	16	9	17	8
TP.786.1	39	Bruddgrens...	18	3	18	3
TP.787.1	29	Bruddgrens...	17	10	17	8
TP.788.1	39	Bruddgrens...	18	3	18	3
TP.789.1	29	Bruddgrens...	17	11	17	10
TP.790.1	40	Bruddgrens...	18	3	18	3
TP.791.1	30	Bruddgrens...	17	12	17	11
TP.792.1	16	Bruddgrens...	5	5	5	4
TP.793.1	13	Bruddgrens...	5	5	5	4
TP.794.1	12	Bruddgrens...	5	5	4	4
TP.795.1	14	Bruddgrens...	5	5	4	4
TP.796.1	18	Bruddgrens...	5	5	4	4
TP.797.1	41	Bruddgrens...	18	4	18	3
TP.798.1	30	Bruddgrens...	17	12	17	13
TP.799.1	42	Bruddgrens...	18	4	18	3

Txy	Tx	Ty
[%]	[%]	[%]
15	29	20
5	20	7
9	40	13
15	29	25
9	38	13
17	30	18
9	39	13
17	29	19
9	39	13
18	29	22
9	40	13
19	30	25
5	16	6
6	13	9
6	12	10
6	14	11
7	18	13
10	41	14
19	30	29
10	42	14

Panel	Max.	Combination	Sx+	Sy+	Sx-	Sy-
[-]	[%]	[-]	[%]	[%]	[%]	[%]
TP.800.1	76	Bruddgrens...	17	14	17	14
TP.801.1	42	Bruddgrens...	18	4	19	3
TP.802.1	31	Bruddgrens...	17	17	17	14
TP.803.1	21	Bruddgrens...	5	6	4	4
TP.804.1	48	Bruddgrens...	5	6	5	4
TP.805.1	26	Bruddgrens...	10	5	4	4
TP.806.1	40	Bruddgrens...	13	12	13	21
TP.807.1	42	Bruddgrens...	13	11	14	22
TP.808.1	50	Bruddgrens...	16	13	15	26
TP.809.1	46	Bruddgrens...	16	10	15	25
TP.810.1	48	Bruddgrens...	17	10	15	27
TP.811.1	49	Bruddgrens...	12	10	17	28
TP.812.1	51	Bruddgrens...	12	10	18	29
TP.813.1	51	Bruddgrens...	12	11	18	30
TP.814.1	79	Bruddgrens...	13	15	17	30
TP.815.1	3	Bruddgrens...	-	0	3	0
TP.816.1	40	Bruddgrens...	20	6	15	3
TP.817.1	39	Bruddgrens...	18	4	18	3
TP.818.1	25	Bruddgrens...	17	14	17	8
TP.819.1	20	Bruddgrens...	8	12	8	8

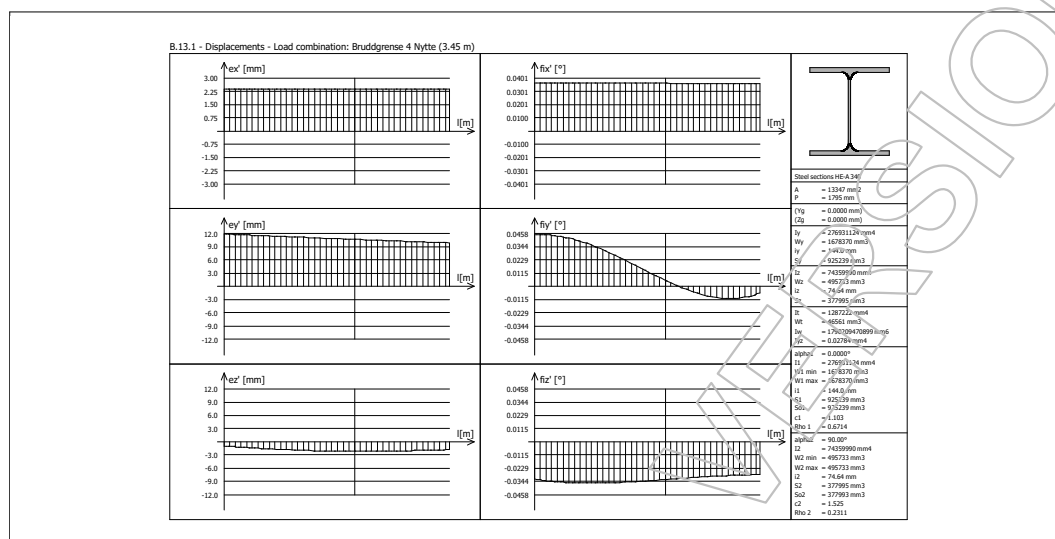
Txy	Tx	Ty
[%]	[%]	[%]
19	30	76
10	42	14
23	31	31
7	21	15
6	48	14
5	26	14
29	40	31
31	42	32
35	50	39
34	46	35
36	48	36
37	49	37
38	51	38
38	51	37
37	79	36
0	0	0
14	40	13
7	39	13
16	25	20
13	20	11

## 2.6 Stabilitet fra vindlast



Figuren viser forskyvning av konstruksjonen i øverste etasjen. Skalering gjør at forskyvninger virker større enn de faktisk er. Dette blir gjort for å lettere se og forstå forskyvningene. Denne er beregnet i bruddgrensetilstand.

## Forskyvning i 1. etasje



## Forskyvning i takplan

