# Effects of oxide additives on the hydrotalcite derived Ni catalysts for CO<sub>2</sub> reforming of methane

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Abstract: Here we provide new mechanistic and kinetic insights into the functions of oxides on Ni catalysts in methane dry reforming combining kinetic studies with density functional theory (DFT) calculations. Hydrotalcite derived Ni catalysts with a small amount of oxide additive (CeO<sub>2</sub>, ZrO<sub>2</sub>, ZnO) as promoters are synthesized and characterized by different techniques, X-ray diffraction (XRD), X-ray fluorescence (XRF), N<sub>2</sub> physisorption, H<sub>2</sub> chemisorption, transmission electron microscopy (TEM), scanning electron microscopy (SEM) and thermogravimetric analysis combined with mass spectrometry (TGA-MS). Regarding H<sub>2</sub>/CO ratio, the CeO<sub>2</sub>-Ni shows the highest the values along all the temperatures. Moreover, the CeO<sub>2</sub>-Ni catalyst has the best stability among the four catalysts, while ZnO-Ni experiences the most severe deactivation. Kinetic studies in terms of reaction orders and activation energies are performed and compared to the DFT investigations, to assess the functions of oxide promoters. The CeO<sub>2</sub>-Ni catalyst shows the lowest apparent activation energy for CO<sub>2</sub> activation, and it is also found that forward turnover rate is independent of CO<sub>2</sub> partial pressure for all the samples. In DFT calculations, CO<sub>2</sub> is more favorable to be activated on the support and the TOF obtained from G plot is in perfect agreement with our experiment value. In addition, it is also found that basicity and electron affinity of different oxide additives can be well correlated to the activation of CO<sub>2</sub> and catalyst deactivation. In general, both the increased basicity of oxide and electron affinity of metal help to promote the CO<sub>2</sub> activation and enhance the catalyst's stability. We propose that the CeO<sub>2</sub>-Ni catalyst has best performance for CO<sub>2</sub> activation, thus leading to a higher surface oxygen concentration to oxidize the carbon on the catalysts, which prolongs the catalyst's life.

Keywords: Methane dry reforming; Oxide additive; Catalytic performance; Kinetic study; Basicity

#### 1. Introduction

In recent decades, CO<sub>2</sub> utilization has become increasingly important because of escalating global warming phenomenon [1]. It is of great importance to reduce the emissions of greenhouse gases and also to further utilize processes capable of consuming these gases in both scientific research and industrial application [2,3]. Conversion of CO<sub>2</sub> to syngas via dry reforming of methane (DRM) has received considerable attention and prominent research interest [4,5]. Above all, this process provides a pathway to reduce and recycle greenhouse gases (CH<sub>4</sub> and CO<sub>2</sub>) and convert them into syngas (H<sub>2</sub> and CO) [6]. In addition, the generation of syngas via methane is one of the most technically advanced routs for natural gas utilization [7]. On the other hand, the DRM reaction is seen as an attractive alternative for steam reforming of methane (SRM) because it can directly utilize raw natural gas and does not require subsequent gas separation and purification to remove CO<sub>2</sub> [8]. Furthermore, the produced syngas from DRM has a lower H<sub>2</sub>/CO ratio than that from SRM, which is more suitable for further usage in the Fischer-Tropsch synthesis of long-chain hydrocarbons [9]. Moreover, dry reforming of methane is regarded as the basis for upgrading the calorific value of hydrocarbons for the solar reforming of natural gas process [10].

DRM is a highly endothermic reaction and requires a high operating temperature to attain high equilibrium conversion of CO<sub>2</sub> and CH<sub>4</sub> into H<sub>2</sub> and CO, and to minimize the thermodynamic driving force for coke formation [11]. Ni-based catalysts are considered as a promising candidate for this reaction owing to their low cost and high activity [12,13]. However, dry reforming of methane is inevitablely accompanied by catalysts deactivation due to carbon deposition through CO disproportionation ( $2CO \rightarrow C + CO_2$ ) and methane decomposition ( $CH_4 \rightarrow C + 2H_2$ ) [14,15]. The deactivation of catalyst due to coke formation is a major obstacle for the commercialization of methane dry reforming over the Ni catalysts. In addition, at high reaction temperatures, the sintering of Ni particles could also cause

catalyst deactivation [16–18]. Moreover, due to the occurrence of the reverse water gas shift reaction (rWGS:  $H_2 + CO_2 \rightarrow CO + H_2O$ ), it would lead to the H<sub>2</sub>/CO ratio lower than 1 [19,20]. Thus, single component Ni catalysts are not able to meet the stability and selectivity requirements [21]. There is an urgently need to develop a cost-effective, thermally stable and highly selective Ni catalyst without decreasing the initial activity.

In addition, during the DRM, CO<sub>2</sub> is activated and reduced into CO, it was reported that this process proceeds on the support instead of active metal alone [11,22,23]. Van Keulen et al. [24] found that the amount of adsorbed CO<sub>2</sub> molecules on ZrO<sub>2</sub> support was much greater than that of Pt atoms on the catalyst surface, suggesting that the ZrO<sub>2</sub> support, could adsorb and activate CO<sub>2</sub>.

Ni-based catalysts with a small amount of oxide additive as promoter, have received increasing attention in recent years, both for their technological impact and scientific importance [25–28]. Oxide additive could improve Ni catalyst's resistance against deactivation, enhance H<sub>2</sub>/CO ratio, and meanwhile, maintain their catalytic activity in DRM, thus providing an opportunity to design new catalysts with improved selectivity and stability without decreasing the initial activity. Koo et al. [25] reported that ceria promoted Ni/Al<sub>2</sub>O<sub>3</sub> catalysts could markedly suppress the coke formation for combined steam and CO<sub>2</sub> reforming of methane through improving the Ni dispersion on the support. Similar results have been reported by Tsubaki [26]. They proved that joint promoter La<sub>2</sub>O<sub>3</sub>/CeO<sub>2</sub> could help to control the size of the Ni particle in methane dry reforming over Ni/Al<sub>2</sub>O<sub>3</sub>, thus improving coke resistance ability. In addition, Corthals et al. [27] used MgAl<sub>2</sub>O<sub>4</sub> spinel powder as the support to prevent sintering of Ni for methane dry reforming. They observed that both CeO<sub>2</sub> and ZrO<sub>2</sub> promoted Ni/MgAl<sub>2</sub>O<sub>4</sub> catalysts are promising for DRM. Moreover, CaO provides good performance for keeping catalysts from sintering [28], while with the Ca loading increasing, both the conversion of CH<sub>4</sub> and CO<sub>2</sub> decreased, which might be attributed to the increase in

Ni electron density.

Ni-containing hydrotalcite-derived catalysts have received increasing attention and been considered as promising catalysts for DRM [29-31]. It has been reported that after the calcination of such double-layered hydroxides, it results in a homogeneous mixture of well dispersed oxides having interesting physical-chemical properties and high thermal stability [32–35]. In addition, hydrotalcite-derived catalysts have basic properties resulting in higher strength of CO<sub>2</sub> adsorption, which is beneficial for the DRM reaction [30,31]. Experimental approaches have been exploited to gain deeper insight into the effect of oxide additives on Ni hydrotalcite-derived catalysts in DRM. Debek et al. [36] found that incorporation of Ce into Ni-containing hydrotalcite-derived catalysts enhanced reducibility of nickel species, and meanwhile resulted in the formation of new strong basic sites, which improved catalytic stability in long-term reaction. Literature also reported that ceria has a high oxygen storage capacity (OSC) which is useful for the reaction in enhancing the reducibility within the fluorite lattice [37]. In addition, Debek et al. [38] also investigated the Zr-promoted Ni hydrotalcite-derived catalysts in DRM. The presence of Zr could inhibit carbon nanofibers formation from CH<sub>4</sub> decomposition, and the ability of the Zr-containing catalysts to adsorb CO<sub>2</sub> on weak basic sites resulted in the formation of active carbonate species that were able to react with CH4 through the DMR route. Although Zr promotion decreased activity, it strongly increased the stability and selectivity of the catalysts [39]. Moreover, ZrO<sub>2</sub> may increase the content of oxygen vacancies on the catalysts surface, which plays an important role for the dissociative adsorption of  $CO_2$  [40,41]. In spite of well reported promotional effects of oxides in the methane dry reforming, a better fundamental understanding of the promotional effects is highly required.

Here we provide new mechanistic and kinetic insights into the functions of oxides on Ni catalysts in methane dry reforming combining reaction kinetics with DFT study. Hydrotalcite

derived Ni catalysts with a small amount of oxide additive (CeO<sub>2</sub>, ZrO<sub>2</sub>, ZnO) as promoters are synthesized and characterized by different techniques. Kinetic study in terms of reaction orders and activation energies are performed and compared to the DFT investigations, to assess the functions of oxide additives.

#### 2. Experiment

#### 2.1 Catalyst preparation

#### 2.1.1 12wt% Ni catalyst

Monometallic 12wt% Ni derived from hydrotalcite-like precursor has been prepared by co-precipitation using metal nitrites component, the details is shown in Table S1 in the supporting information. An aqueous solution of NaOH and Na<sub>2</sub>CO<sub>3</sub> (400 ml) was added at a constant rate into a reactor containing an aqueous mixtures of nitrates Ni(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, Mg(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O and Al(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O (400 ml) in a period of 2 h [33–35]. After the addition was finished, the pH of mixture solution was adjusted to between 8 and 9. Then the reactor containing mixture solution was kept in the oil bath for 16 h at 80 °C. The resultant hydrotalcite was cooled, then filtered and washed with deionized water several times. The hydrotalcite was then dried at 100 °C for 12 h (denoted as NiO-HT). And the prepared catalyst was calcined in the air at 600 °C for 6 h, which destroyed the hydrotalcite structure and formed mixed oxides NiO/Mg(Al)O. The catalyst was crashed into powder and sieved to particle size between 75–125 µm.

#### Table 1 move to supporting information

Chemicals for	: 12 wt% Ni	preparation.
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	Ni(NO <sub>3</sub> ) <sub>2</sub> ·6H <sub>2</sub> O	Mg(NO <sub>3</sub> ) <sub>2</sub> ·6H2O	$Al(NO_3)_3 \cdot 9H_2O$	NaOH	Na <sub>2</sub> CO <sub>3</sub>
Molar Ratio	0.37	2.63	1	8	0.5
Molar (mol)	0.02775	0.1972	0.0750	0.6000	0.0375
Mass (g)	8.070	50.575	28.135	24.000	5.962

#### 2.1.2 Oxide additive (CeO<sub>2</sub>, ZrO<sub>2</sub>, ZnO) loading

In this paper, we prepared the promoted Ni-based catalysts through incipient wetness, impregnating the calcined hydrotalcite-derived Ni catalysts with additive precursor  $[Ce(NO_3)_3.6H_2O, ZrO(NO_3)_2.aq$  and  $Zn(NO_3)_2.6H_2O]$ . The loading of promoter is fixed at about 3wt%. We checked the pore volume of Ni catalysts after calcination from N<sub>2</sub> physisorption. According to the pore volume, we determined the amount of the deionized water with calculated precursor salt used in the impregnation. The promoter catalysts firstly were dried at ambient temperature overnight, and then were re-calcined in air at 600 °C for 6 h, resulting in oxides. Finally, the catalysts were crashed into powder and sieved to particle size between 75–125 µm. The neat Ni catalyst, CeO<sub>2</sub>, ZrO<sub>2</sub> and ZnO promoted Ni catalysts are named as Ni, CeO<sub>2</sub>-Ni, ZrO<sub>2</sub>-Ni and ZnO-Ni, respectively.

# 2.2 Catalyst characterization

*XRD*. XRD experiments were performed at ambient temperature on a Bruker D8 Advance DaVinci and diffractometer equipped with the Cu K $\alpha$  radiation ( $\lambda = 1.54056$  Å) Xray source. XRD patterns were examined with 2 $\theta$  values ranging from 20° to 80° at a scanning speed of 1°/min.

 $N_2$  physisorption. Brunauer-Emmett-Teller (BET) surface area of the catalyst was measured by N<sub>2</sub> physical adsorption at liquid nitrogen temperature (Micromeritics, TriStar II 3020). All samples (100 mg) needed to be degassed under vacuum at 200 °C overnight prior to the test. The BET method was applied to calculate the specific surface area based on the N<sub>2</sub> isotherms. And the total pore volume was obtained at single point adsorption of pores less than 850.946 Å diameter at P/Po = 0.976709541 and the average pore size were acquired by BET model on the basis of the N<sub>2</sub> isotherms curve.

 $H_2$  chemisorption. Metal dispersion was determined by hydrogen chemisorption performed at 40 °C (Micromeritics, ASAP 2020S). Calcined catalysts (100 mg) were loaded in tubular quartz reactor, evacuated at 40 °C for 1h and reduced in H<sub>2</sub> flow at 670 °C for 16 h. After the reduction, the sample was evacuated for 0.5 h at 670°C and subsequently for 1 h at 40 °C. Then after the leak test pass, the sample was continuously evacuated for 0.5 at 40 °C, at this temperature, an adsorption isotherm was recorded and the metal dispersion was determined based on the quantity of hydrogen uptake.

*XRF*. Metal oxides proportion was confirmed by XRF analysis (Rigaku, Supermini200). Calcined samples (100 mg) were mixed homogeneously with boric acid (around 2.5 g) and then pressed into pellets for test. The pellets were put into special sample holders and the test was completed in vacuum.

*TGA-MS*. Coke formation on spent catalysts was investigated by a TGA-MS (TGA: Netzsch STA 449C Jupiter, MS: Netzsch Aërlos QMS 403C) system under an air atmosphere. The experiments were conducted under an air stream (50ml/min), heating from ambient temperature to 1000 °C, at a ramping rate of 10 °C/min, and dwelling for half hour at this temperature. The amount of coke deposition was estimated by the mass loss in TGA analysis, confirming by MS results.

*TEM.* TEM images were taken and analyzed using a JEOL-2010F, with an accelerating voltage of 200 kV. The samples were prepared by ultrasonic dispersion of the reduced catalysts in ethanol. Drops of samples were put on a copper grid supported with a carbon film.

SEM. The morphology of spent catalysts were analyzed by SEM (FEI, APREO) to observe more details on coke formation and sintering of different samples, operated at 2.00 kV.

#### 2.3 Catalytic test

Catalytic activity test was performed in a quartz fixed-bed tubular reactor (internal diameter: 10 mm) at atmospheric pressure. The catalyst bed consisted of 10 mg of the Ni or promoted Ni catalysts (75–125 $\mu$ m) diluted with inert 250 mg  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> (75–125 $\mu$ m). Before testing, the catalysts were reduced at 670 °C for 16 h in a mixture of 1/1 H<sub>2</sub>/Ar (total flow

100 mL/min). A series of mass flow controllers (Bronkhorst) allowed to feed reactant gas of 200 ml/min (CH4:CO<sub>2</sub>:Ar = 30:30:140, with a gas hourly space velocity (GHSV) of 1,200,000 mL·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup>), and the GHSV is calculated from total flow. The Ar was used as balance and internal standard gas for CH4 and CO<sub>2</sub> conversion calculations. A gas chromatograph (GC6890N, Agilent) using helium as the carrier gas was applied to analyze different gas species online including CH4, CO<sub>2</sub>, H<sub>2</sub>, CO and Ar. The GC was equipped with a thermal conductivity detector (TCD), and water was removed prior to GC analysis. In activity test as well as selectivity test, the reaction temperature increased from 450 °C to 800 °C with an interval of 50 °C, and the output data from GC was collected under steady-state for around 60 min at every temperature. In addition, stability test was performed at 700 °C for 30 h, CH4:CO<sub>2</sub>:Ar = 60:60:30 ml/min. And coke formation was investigated after 30 h stability test.

CH<sub>4</sub> and CO<sub>2</sub> conversions ( $X_{CH4}$  and  $X_{CO2}$ ), H<sub>2</sub> and CO selectivity ( $S_{H2}$  and  $S_{CO}$ ) as well as the H<sub>2</sub>/CO ratio, were calculated as follows:

$$X_{CH4} = \frac{F_{CH4,in} - F_{CH4,out}}{F_{CH4,in}}$$
(1)

$$X_{CO2} = \frac{F_{CO2,in} - F_{CO2,out}}{F_{CO2,in}}$$
(2)

$$S_{H2} = \frac{F_{H2,\text{out}}}{2 \times (F_{CH4,\text{in}} - F_{CH4,\text{out}})}$$
(3)

$$S_{CO} = \frac{F_{CO,out}}{(F_{CH4,in} - F_{CH4,out}) + (F_{CO2,in} - F_{CO2,out})}$$
(4)

$$H_2 / CO = \frac{F_{\text{H2,out}}}{F_{CO,\text{out}}}$$
(5)

where  $F_{i,in/out}$  is the molar flow rate of each species for feed gas (in) and effluent gas (out).

CH<sub>4</sub> and CO<sub>2</sub> average reaction rate ( $r_{CH4}$  and  $r_{CO2}$ ) and average turnover frequency

(*TOF*<sub>CH4</sub> and *TOF*<sub>CO2</sub>) were calculated as follows at differential conditions:

$$r = \frac{X \cdot F}{W} = \frac{X \cdot F}{W \cdot 22414 \cdot 60} \cdot \frac{273.15}{298.15} (\text{mol} \cdot \text{s}^{-1} \cdot g_{cat}^{-1})$$
(6)

$$TOF = \frac{r \cdot Mi}{fi \cdot D} = \frac{r \cdot M_{Ni}}{f_{Ni} \cdot D} (s^{-1})$$
(7)

where X is the conversion, F is the gas flow rate, W is the catalysts weight,  $M_{Ni}$  is the molecular weight of Ni and  $f_{Ni}$  is the metal Ni weight fraction in catalysts. The dispersion D was estimated based on the Ni surface area of catalyst measured by hydrogen chemisorption.

For kinetic study, preliminary experiments were performed to eliminate external and internal mass and heat limitation. A high GHSV = 2,400,000 mL·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup> with a catalyst weight of 5 mg was applied to control all the methane conversion level less than 15% at a differential condition. The catalyst was diluted with inert 250 mg  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> to minimize the temperature gradients and ensure the plug flow in the catalyst bed. The kinetic study was performed at temperatures from 450 °C to 550 °C with an interval of 25 °C. The apparent activation energy for each sample from both CO<sub>2</sub> and CH<sub>4</sub> conversion were calculated according to the Arrhenius equation. In addition, CO<sub>2</sub> reaction order test was performed at the same GHSV applied in the activity test, at the temperature of 550 °C, keeping the CH<sub>4</sub> partial pressure constant, adjusting the partial pressure of CO<sub>2</sub> and Ar.

#### **2.4 DFT calculations**

All the DFT calculations were conducted with a periodic slab model using the Vienna ab initio simulation program (VASP) [42,43]. Calculations were conducted with the generalized gradient approximation (GGA) and the BEEF-vdW exchange correlation functional [44]. Projector augmented wave (PAW) method was used to describe the electrons-ion interaction [45]. Five atomic layers Ni(111) surface were modeled, the bottom two layers were fixed at their equilibrium bulk positions, and the top three layers and the adsorbates were allowed to relax. And the plane wave cutoff energy of 400 eV was applied in the calculation of the compact convergence. Additionally, a  $p(3 \times 3)$  supercell was applied to neglect the surrounding adsorbate interactions in this work. DFT calculations considered spin-polarized electrons for Ni(111), due to the magnetic moment of Ni. A 15 Å vacuum region was used to ensure the intermolecular interaction between the slabs was negligible. In addition, a Fermi smearing of 0.2 eV was applied in present work. Brillouin zone integration was approximated by a sum over special k-points chosen using the Monkhorst–Pack method [46]. The meshes of  $5 \times 5 \times 1$  k-points for the Ni(111) surface. Moreover, transition states were searched through dimer method [47]. All the transition states were verified by frequency analysis, and only one imaginary frequency was identified for each transition state.

#### 3. Results and discussion

#### 3.1 Characterization of catalysts before reaction

#### 3.1.1 XRD

X-ray diffraction patterns of the prepared hydrotalcite-like precursors and calcined samples with different oxide additive are shown in Fig. 1. Fresh hydrotalcite-like samples exhibit typical reflections at  $2\theta = 23.5^{\circ}$ ,  $35^{\circ}$ ,  $60.5^{\circ}$  and  $61.9^{\circ}$ , corresponding to the (006), (009), (110) and (113) planes in the multilayer hydrotalcite structure [33,35]. No additional phases are observed, pointing to the successful incorporation of Ni into the hydrotalcite structure. The patterns acquired for the calcined samples show three main reflections at  $2\theta = 36^{\circ}$ ,  $43.5^{\circ}$  and  $63^{\circ}$ , which could be assigned to the periclase-like structure of Ni-Mg-Al mixed oxides generated from the thermal decomposition of hydrotalcite samples [33,35]. The peak for CeO<sub>2</sub> [48], ZrO<sub>2</sub> [49,50] and ZnO [51] are weak, due to a small amount of oxide adding, the details are provided in Fig. 1.



Fig. 1. XRD patterns of hydrotalcite-like precusors and calcined samples with different oxide additives.
♣ Hydrotalcite-like precusors; ♦ Mixed Oxide NiO-Mg(Al)O; ● CeO<sub>2</sub>; ♥ ZrO<sub>2</sub> and ■ ZnO.

#### 3.1.2 N<sub>2</sub> physisorption

Fig. 2 shows the nitrogen adsorption/desorption isotherms and pore size distribution of Ni catalysts with different oxide additives. The nitrogen adsorption/desorption isotherms of calcined samples can be categorized as type IV isotherms, typical of mesoporous materials [52,53]. The values of BET surface area for all samples range between 180 to 200 m<sup>2</sup>/g<sub>cat</sub>. And the total pore volume show a slight decrease with the adding of promoter, dropping from 0.42 to 0.35 cm<sup>3</sup>/g. The similar trend is observed for average pore size, decreasing from 9.46 to 7.67 nm. Table 2 presents the BET surface area, pore volume and average pore diameter calculated from the N<sub>2</sub> adsorption/desorption isotherms.



Fig. 2. Nitrogen adsorption/desorption isotherms and pore size distribution of Ni catalysts with different oxide additives.

# Table 2

BET surface area, pore volume and average pore diameter calculated from  $N_2$  adsorption/desorption isotherms.

Catalyst	BET Surface Area [m <sup>2</sup> /g <sub>cat</sub> ]	Pore Volume [cm <sup>3</sup> /g]	Average Pore Diameter [nm]
Ni	182.52	0.42	9.14
CeO <sub>2</sub> -Ni	195.23	0.38	7.68
ZrO <sub>2</sub> -Ni	198.27	0.38	7.68
ZnO-Ni	179.06	0.35	7.67

# Ni loading ICP

# 3.1.3 H<sub>2</sub> chemisorption and TEM

The active surface area of Ni and promoted Ni catalysts was calculated from the quantity of hydrogen uptake, according to the assumption that the stoichiometry of H/Ni<sub>s</sub> (surface nickel atom) is 1 [4,33]. Compared with pure Ni catalysts, the sample of Ni catalysts promoted by CeO<sub>2</sub> and ZrO<sub>2</sub> show a slight decrease in metallic surface area and total dispersion. In addition, similar trend is observed for ZnO promoted Ni catalys, the details are provided in Table 3.

#### Table 2

Catalyst	Ni Loading [wt%]	Metallic Surface Area [m <sup>2</sup> /g <sub>cat</sub> ]	Total Dispersion [%]
Ni	12.0	9.44	11.82
CeO <sub>2</sub> -Ni	12.0	9.13	11.43
ZrO <sub>2</sub> -Ni	12.0	9.33	11.68
ZnO-Ni	12.0	9.08	11.40

Metallic surface area and total dispersion of calcined samples.

Fig. 3 shows the TEM images of Ni catalysts. Specifically, Fig 3a and 3b indicate that the average particle size of Ni catalysts is around 8.10 nm, the dispersion calculated by 1/d (d is the average particle size) is 12.34 %, which is in good agreement with the result from H<sub>2</sub> chemisorption (11.82 %). In addition, fringes of 0.20 nm of metallic Ni<sup>0</sup> was attributed to (111) planes [54] of Ni catalysts, as depicted in Fig. 3c.



Fig. 3. TEM images of 12Ni catalysts (a) fresh sample, (b) reduced sample, and (c) surface lattice distance.3.1.4 XRF

Table 4 provides the component of each sample after calcination. The XRF results showed that the loading of different oxide additives in Ni catalysts is 2.84 wt% for CeO<sub>2</sub>, 2.76 wt% for ZrO<sub>2</sub> and 2.58 wt% for ZnO, respectively, which are all close to the nominal loading of 3.0 wt%, indicating that we have successfully synthesized the Ni catalysts with various oxide additives as promoter.

#### Table 4

Component (%)	Ni	CeO <sub>2</sub> -Ni	ZrO <sub>2</sub> -Ni	ZnO-Ni
MgO	58.30	56.07	59.03	56.47
Al <sub>2</sub> O <sub>3</sub>	24.21	22.48	24.17	22.89
NiO	16.81	15.5	12.99	14.94
Oxide additive		2.84	2.76	2.58

Component of each sample after calcination.

#### 3.2 Activity and selectivity test

Fig. 4a and 4b shows the CH<sub>4</sub> and CO<sub>2</sub> conversion with the increase of temperature for Ni catalysts with different oxide additives. In order to see the intrinsic activity for different catalysts, we keep the conversion of reactants away from the equilibrium. The results indicates that the conversion of reactants increases with the temperature increasing. In addition, all of the promoted Ni catalysts presents slight lower activity compared with Ni catalyst. Specifically, at low temperature, the CeO<sub>2</sub>-Ni, ZrO<sub>2</sub>-Ni and ZnO-Ni have the similar conversion of CH<sub>4</sub> and CO<sub>2</sub>, while at high temperature, the activity follows the trend: CeO<sub>2</sub>-Ni > ZrO<sub>2</sub>-Ni > ZnO-Ni. Moreover, due to the occurrence of reverse water gas shift reaction, the conversion of CO<sub>2</sub> is higher than that of CH<sub>4</sub> [55,56].

Fig. 4c and 4d provides the H<sub>2</sub> selectivity and CO selectivity, respectively. The CeO<sub>2</sub>-Ni has the best performance for H<sub>2</sub> selectivity, it is higher than the other three in the whole process, and reaches 1 at 650 °C. Regarding the CO selectivity, ZrO<sub>2</sub>-Ni stands out among four samples, it is up to 1 at 550 °C, while for ZnO-Ni, it neither enhances the H<sub>2</sub> selectivity nor the CO selectivity, even it is worse than the Ni catalyst. Furthermore, Fig. 4e depicts the H<sub>2</sub>/CO ratio with the increase of temperature for different samples. The CeO<sub>2</sub>-Ni shows the highest value along all the temperatures, and also firstly reaches 1 at 650 °C, which indicates that it could suppress the rWGS reaction, thus CeO<sub>2</sub>-Ni is considered as a promising candidate for this reaction in terms of selectivity.



Fig. 4. Activity and selectivity test of catalysts for DRM: (a) CH<sub>4</sub> conversion; (b) CO<sub>2</sub> conversion; (c) H<sub>2</sub> selectivity; (d) CO selectivity and (e) H<sub>2</sub>/CO ratio. Reaction conditions: CO<sub>2</sub>/CH<sub>4</sub>/Ar = 30/30/140 mL/min, GHSV = 1,200,000 mL·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup>, 1 atm.

# **3.3 Rate and TOF remove??**

In order to compare activity for different samples, we have calculated the average reaction rate and TOF from both CH<sub>4</sub> and CO<sub>2</sub> sides at all temperatures. Table 5 and 6 give

the average reaction rate of CH<sub>4</sub> and CO<sub>2</sub>, respectively. It is found that average reaction rate increases with the temperature increasing. Generally, the average reaction rate follows the order: Ni > CeO<sub>2</sub>-Ni > ZrO<sub>2</sub>-Ni > ZnO-Ni. Additionally, the average reaction rate of CO<sub>2</sub> is slightly higher than the CH<sub>4</sub> average reaction rate, due to the occurrence of rWGS reaction. In addition, Fig. 5 presents the TOF for different samples with the increasing temperature, similar trend is observed with average reaction rate. There is a slight decrease in activity (TOF) for CeO<sub>2</sub>-Ni and ZrO<sub>2</sub>-Ni, compared with Ni.

#### Table 5

CH<sub>4</sub> average reaction rate at different temperatures. Reaction conditions:  $CO_2/CH_4/Ar = 30/30/140$  mL/min, GHSV = 1,200,000 mL·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup>, 1 atm.

Temperature	CH <sub>4</sub> average reaction rate (mmol·s <sup>-1</sup> ·g <sub>cat</sub> -1)				
(°C)	<mark>Ni</mark>	CeO <sub>2</sub> -Ni	ZrO2-Ni	<mark>ZnO-Ni</mark>	
<mark>450</mark>	<mark>0.129</mark>	<mark>0.086</mark>	<mark>0.061</mark>	<mark>0.061</mark>	
<mark>500</mark>	<mark>0.243</mark>	<mark>0.170</mark>	<mark>0.137</mark>	<mark>0.133</mark>	
<mark>550</mark>	<mark>0.409</mark>	<mark>0.311</mark>	<mark>0.278</mark>	<mark>0.255</mark>	
<mark>600</mark>	<mark>0.623</mark>	<mark>0.517</mark>	<mark>0.476</mark>	<mark>0.437</mark>	
<mark>650</mark>	<mark>0.889</mark>	<mark>0.783</mark>	<mark>0.738</mark>	<mark>0.676</mark>	
<mark>700</mark>	<b>1.200</b>	1.079	1.032	<mark>0.960</mark>	
<mark>750</mark>	<mark>1.482</mark>	1.371	<mark>1.339</mark>	1.243	
<mark>800</mark>	<mark>1.741</mark>	<mark>1.627</mark>	<mark>1.608</mark>	<mark>1.494</mark>	

#### Table 6

CO<sub>2</sub> average reaction rate at different temperatures. Reaction conditions: CO<sub>2</sub>/CH<sub>4</sub>/Ar = 30/30/140

|--|

<b>Temperature</b>	$CO_2$ average reaction rate (mmol·s <sup>-1</sup> ·g <sub>cat</sub> <sup>-1</sup> )				
(°C)	<mark>Ni</mark>	CeO <sub>2</sub> -Ni	ZrO2-Ni	ZnO-Ni	
<mark>450</mark>	<mark>0.194</mark>	<mark>0.112</mark>	<mark>0.090</mark>	<mark>0.112</mark>	
<mark>500</mark>	<mark>0.351</mark>	<mark>0.243</mark>	<mark>0.215</mark>	<mark>0.231</mark>	
<mark>550</mark>	<mark>0.572</mark>	<mark>0.441</mark>	<mark>0.403</mark>	<mark>0.399</mark>	
<mark>600</mark>	<mark>0.817</mark>	<mark>0.701</mark>	<mark>0.656</mark>	<mark>0.634</mark>	
<mark>650</mark>	1.104	<mark>0.993</mark>	<mark>0.944</mark>	<mark>0.903</mark>	
<mark>700</mark>	<mark>1.379</mark>	1.277	1.236	<mark>1.185</mark>	
<mark>750</mark>	<mark>1.615</mark>	1.529	<mark>1.498</mark>	<mark>1.432</mark>	
<mark>800</mark>	<mark>1.800</mark>	1.721	1.702	<mark>1.631</mark>	



**Fig. 5.** TOF for different samples with the increasing temperature from (a) CH<sub>4</sub> and (b) CO<sub>2</sub> conversion. Reaction conditions: CO<sub>2</sub>/CH<sub>4</sub>/Ar = 30/30/140 mL/min, GHSV = 1,200,000 mL·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup>, 1 atm.

#### 3.4 Stability test

Stability tests are performed at 700°C after 30 h running. As seen from Fig. 6a, the Ni and ZnO-Ni present a larger decrease of CO<sub>2</sub> conversion compared with the sample of CeO<sub>2</sub>-Ni and ZrO<sub>2</sub>-Ni. To clearly show the degree of deactivation for all samples, we normalize it by dividing the initial conversion for each catalyst, as shown in Fig. 6b. Compared with the Ni catalyst, the ZrO<sub>2</sub>-Ni catalyst shows a similar deactivation behavior, and the stability is slightly better than Ni sample. In addition, CeO<sub>2</sub>-Ni has the best stability among the four samples, while ZnO-Ni experiences the most severe deactivation. As a consequence, the stability follows the order: CeO<sub>2</sub>-Ni > ZrO<sub>2</sub>-Ni > Ni > ZnO-Ni. Moreover, we define the deactivation factor as follows:

$$\alpha = 1 - X(20) / X(0) \tag{8}$$

where  $\alpha$  is the deactivation factor, X(20) and X(0) represent the conversion of CO<sub>2</sub> after 20 h and initial value, respectively.

The deactivation factor  $\alpha$  is according to the following sequence: 0.06 [CeO<sub>2</sub>-Ni] < 0.09 [ZrO<sub>2</sub>-Ni] < 0.10 [Ni] < 0.15 [ZnO-Ni], the bigger value of  $\alpha$ , the worse the stability is.

Therefore, we conclude that the stability of Ni catalyst can be significantly improved by adding CeO<sub>2</sub>.



Fig. 6. Stability test of catalysts for DRM: (a)  $X_{CO2}$ ; (b) X(t)/X(0). Reaction conditions: CO<sub>2</sub>/CH<sub>4</sub>/Ar = 60/60/30 mL/min, 700 °C, 1 atm, 30 h.

#### 3.5 Role of oxide additive in the stability of the catalysts

Coke formation and sintering are the two dominant reasons for causing the catalysts deactivation. In the following sections, we present the TGA plot of spent samples after stability test to check the amount of coke formation, as well as generated CO<sub>2</sub> signal by MS. In addition, for the morphology of spent catalysts have been inspected by SEM, providing more information on coke formation and sintering.

#### **3.5.1 TGA–MS analysis**

The temperature programmed oxidation (TPO) was conducted under an air stream (50ml/min), heating from ambient temperature to 1000 °C, at a ramping rate of 10 °C/min, and dwelling for half hour at this temperature. The amount of coke deposition was estimated by the mass loss in TGA analysis, confirming by MS results, as seen from Fig. 7. Generally, the mass loss curves can be divided into three major ranges. From ambient temperature to 220 °C, the mass loss mainly due to the moisture removal. The second range is from 220 °C to 350 °C, the oxidation of reduced Ni causes a small increase in weight. The most important range is from 350 °C to 800 °C, the deposited carbon oxidation and elimination leads to the

mass loss, which could be confirmed by CO<sub>2</sub> signal from MS. It is demonstrated that adding a small amount of oxide additive into Ni catalysts could markedly suppress the carbon formation. In addition, CO<sub>2</sub> peaks (Fig. 7b) of TPO of carbon formed on oxide promoted Ni catalysts shifted to lower temperatures compared to the Ni catalyst, indicating that the carbon deposited on the oxide promoted catalysts is softer and less crystallized than one on Ni catalyst.



Fig. 7. (a) TGA analysis after stability test; (b) CO<sub>2</sub> signal from MS.

#### 3.5.2 SEM analysis

SEM images of spent catalysts with different oxide additives after 30 h running are shown in Fig. 8. As seen from the figures, significant amount of filamentous carbon was observed over the spent Ni, while the promoted Ni with oxide additives showed much less filamentous carbon formation. Especially for ZrO<sub>2</sub>-Ni and ZnO-Ni, the filamentous carbon was hardly observed on these samples. Literature [52] reported that carbon whisker almost does not paly the dominate role in causing the deactivation, therefore, although a small amount of filamentous carbon was formed on the CeO<sub>2</sub>-Ni catalysts, it can still keep the best stability among four catalysts. In addition, according to the stability test, the ZnO-Ni experienced the most severe deactivation. However, very little filamentous carbon was observed on this sample after stability test, combined with the TGA-MS analysis, carbon oxidation leads to the mass loss, so we infer that the encapsulated carbon dominates the coke deposition on this catalyst, which could block the active sites of metal surface and bring about the deactivation of catalysts [14].



Fig. 8. SEM images after stability test: (a) Ni; (b) CeO<sub>2</sub>-Ni; (c) ZrO<sub>2</sub>-Ni; and (d) ZnO-Ni.

# 3.6 Kinetic study

# 3.6.1 Apparent activation energy

In order to control the reaction at the differential condition, the experiments of kinetic

study was performed at the methane flow based GHSV of 720,000 mL •h-1 • gcat-1 from 450 °C to 550 °C with an interval of 25 °C. The reaction rates of CH<sub>4</sub> and CO<sub>2</sub> based on the catalyst and Ni weight are presented in Table S2 and S3, respectively in the supporting information. Fig. 9 displays the Arrhenius plot for TOF of CH<sub>4</sub> and CO<sub>2</sub> on each catalyst with 25 K temperature increment, from 723 to 823 K. Generally, the apparent activation energy for CH<sub>4</sub> conversion of promoted samples are all higher than that on Ni catalyst. The values of activation energy on CeO<sub>2</sub>-Ni and ZnO-Ni are 78.69 kJ/mol and 78.21 kJ/mol, respectively, higher than that of 70.69 kJ/mol on ZrO<sub>2</sub>-Ni. In addition, regarding the CO<sub>2</sub> conversion, both CeO<sub>2</sub>-Ni and ZrO<sub>2</sub>-Ni show a little bit lower activation energy compared with Ni, while ZnO presents a higher activation barrier. It is suggested that the oxide additive CeO<sub>2</sub>-Ni and ZrO<sub>2</sub>-Ni could lower the energy for CO<sub>2</sub> activation, thus promoting the CO<sub>2</sub> dissociation into CO and O. Furthermore, the produced O species play the key role for CH<sub>x</sub> and surface carbon oxidation, which affects the H<sub>2</sub>/CO ratio and the formed surface carbon amount.



Fig. 9. Arrhenius plot for TOF of CH<sub>4</sub> and CO<sub>2</sub> on each catalyst with 25 K temperature increment: (a) Ni; (b) CeO<sub>2</sub>-Ni; (c) ZrO<sub>2</sub>-Ni; and (d) ZnO-Ni. Reaction conditions: CO<sub>2</sub>/CH<sub>4</sub>/Ar = 30/30/140 mL/min, GHSV = 2,400,000 mL·h<sup>-1</sup>·g<sub>cat</sub><sup>-1</sup>, 1 atm.

#### 3.6.2 CO<sub>2</sub> Reaction order

Effect of CO<sub>2</sub> partial pressure on forward TOF of CH<sub>4</sub> has been shown in Fig. 10. It can be clearly seen that CH<sub>4</sub> forward turnover rate is not influenced by CO<sub>2</sub> partial pressure, which has been reported in Wei and Iglesia study [57], the CO<sub>2</sub> reaction order is approaching to 0. However, CO<sub>2</sub> reaction order of 1 was found by in Özkara-Aydınoglu and Aksoylu [58]. It is worth noting that the support is MgO of Wei and Iglesia study, while later one is Al<sub>2</sub>O<sub>3</sub>. In this paper, the ratio of Mg:Al is approximately close to 2.63:1, so MgO dominates the main properties of the support. The generated Mg(Al)O mixed oxides from calcination of hydrotalcite is basic [31,32]. Thus, CO<sub>2</sub> reaction order found in this paper is similar to the one in Wei and Iglesia's study.



Fig. 10. Effect of  $CO_2$  partial pressure on forward TOF of  $CH_4$  (balance Ar, total pressure = 100 kPa).

Zero order of  $CO_2$  reaction suggests that the  $CH_x$  (1-4) dissociation is the ratedetermining step (RDS), in good agreement with Wei and Iglesia's [57] work. Obviously, the reaction mechanism and kinetics could depend on the support properties, which will be discussed in a more detail in the next section.

#### 3.7 DFT calculations for CH<sub>4</sub>/CO<sub>2</sub> reforming reaction on Ni

DFT calculation of adsorption of intermediates and free energy of reaction pathway of CH<sub>4</sub>/CO<sub>2</sub> reforming is performed to gain a better kinetic insight of effects of catalyst properties. The elementary steps involved in the mechanism is presented in Fig. 11. All the thermodynamic properties were calculated at a temperature of 1023 K. The standard molar Gibbs free energy for each species in methane dry reforming follows [12]:

$$G^{0} = E_{\text{total}} + E_{ZPE} + \gamma RT (1 + In \frac{P}{P^{0}}) + U^{0} - TS^{0}$$
(9)

where  $E_{total}$  is the total energy obtained from DFT calculations, and  $E_{ZPE}$ ,  $U^0$  and  $S^0$  are the correction energy from zero-point energy (ZPE), thermal energy and entropy, respectively. *R* is the gas constant, *P* is the partial pressure of the gas-phase molecule,  $\gamma$  is 0 for the surface adsorbed species and 1 for gaseous molecule.

We plot the Gibbs free energy for methane dry reforming on Ni catalyst, both CO<sub>2</sub> activation on the metal surface and support have been considered, as depicted in Fig. 11. Although it might be a small free energy for activation of CO<sub>2</sub> on support and surface diffusion to metal, here we simplify and treat it as an extreme case of zero entropy change of CO<sub>2</sub> activation on Ni surface.



Fig. 11 Free energy landscape in DRM on Ni surface:  $CO_2$  activation on the metal surface (in black) and on the support (in red). Reaction conditions:  $P_{CH4} = 0.15$  bar,  $P_{CO2} = 0.15$  bar,  $P_{Ar} = 0.70$  bar, T = 1023 K. Transition states on Ni surface: (a) CH<sub>4</sub>--CH<sub>3</sub>+H; (b) CH<sub>3</sub>--CH<sub>2</sub>+H; (c) CH<sub>2</sub>--CH+H; (d) CO<sub>2</sub>--CO+O; (e)

#### CH+O--CHO; and (f) CHO--CO+H.

It can be clearly seen from Fig. 11 that the rate-determining step depends significantly on the CO<sub>2</sub> activation mechanism due to the large  $\Delta G$  of the CO<sub>2</sub> activation step on the Ni surface. When the CO<sub>2</sub> activates at the Ni surface, CO<sub>2</sub> activation and CH\*+O\* step have similar free energy with the highest free energy in the  $\Delta G$  profile. These two steps are kinetic relevant steps for DRM which is contradict with the experimental observation CH<sub>x</sub> (1-4) that dissociation is the rate-determining step. When CO<sub>2</sub> activates on the oxides lowered significantly the total energy, the CH<sub>x</sub> (x = 2-4) dissociation steps have similar free energy with the highest free energy in the  $\Delta G$  profile. The CH<sub>x</sub> (x = 2-4) dissociation steps are kinetic relevant steps, in good agreement with the experimental observation. The turn over frequency (TOF) could also be calculated as follows based on the highest point of G plot:

$$TOF_{DFT} = \frac{k_b T}{h} \exp(\frac{-\Delta G}{RT}) P_{CH4} P_{H2}^n$$
(10)

where  $k_b$  is the Boltzmann constant, T is the reaction temperature, h is the Planck constant,  $\Delta G$  is the highest point of G plot, R is the gas constant,  $P_{CH4}$  is the partial pressure of CH4, and  $P_{H2}$  is the partial pressure of H<sub>2</sub>, due to the second C–H bond activation is regarded as the *RDS*, here reaction order for H<sub>2</sub> n = - 0.5.

The highest Gibbs free energy is around 240 kJ/mol, TOF<sub>DFT</sub> is 5.92 s<sup>-1</sup> at 1023 K accordingly, which is very close to our experiment value TOF<sub>EXP</sub> 6.13 s<sup>-1</sup> at 1023 K. For the CO<sub>2</sub> activation on Ni surface, the highest Gibbs free energy is around 360 kJ/mol, which corresponds to a TOF of  $4.42 \times 10^{-6}$  s<sup>-1</sup>, far lower than the experimental one. Therefore, based on both the kinetic and DFT results, it can be concluded that CO<sub>2</sub> activation on oxides plays a significant role in DRM reaction.

#### 3.8 Functions of oxide additive

CO<sub>2</sub> is a mildly acidic molecule and it is normally attracted by the basic sites of solid surfaces. However, the nature of the CO<sub>2</sub> molecule is regarded amphoteric due to the electron-deficient C atom and the electron-rich O atom. The activation of CO<sub>2</sub> on the solid surface depends on its basicity. Generally metal oxides are acid-base materials which can be categorized into basic (e.g. MgO), acidic (e.g.  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>), amphoteric (e.g. CeO<sub>2</sub>, ZrO<sub>2</sub>and ZnO) and neutral (SiO<sub>2</sub>) materials. The metal cations (M<sup>n+</sup>) interact with the electron-rich O atom in CO<sub>2</sub> as Lewis acid, while the O<sup>2-</sup> chemically interacts with the electron deficient basic C atom in CO<sub>2</sub> molecule as Lewis base. CO<sub>2</sub> activates over surface M<sup>n+</sup>-O<sup>2-</sup> pairs on the boundaries of metals and supports or supports, followed by its subsequent dissociation into CO and O, as well as surface diffusion. Electronegativity is the tendency to attract electrons, or to stabilize negative charges. An oxygen bound to a less-electronegative metal atom will be a stronger base (add refs). We plotted Eaco<sub>2</sub> and deactivation factor as a function of electronegativity of cations in the oxides [64], as a descriptor in Fig. 12. In general, both Eaco<sub>2</sub> and decrease with decreasing electronegativity of cations in the oxides. As shown in

Figure 12, the basicity of oxide additives increases in an order:  $CeO_2 > ZrO_2 > ZnO$  [60–63], (refs) with decreasing electronegativity of cations, in a good agreement of with the literature. Ce in CeO<sub>2</sub> with the lower electronegativity and O<sup>2-</sup> with strong Lewis basicity interact more strongly with CO<sub>2</sub> molecule which destabilize the transition state structure thus enhance the activation via dissociation of CO<sup>2\*</sup> to CO\* and O\*, and lower the activation energy of CO<sub>2</sub> activation.

The Ni surface areas of promoted catalysts is only slightly lower than the neat Ni catalyst (Table 2). In addition, no obvious peaks corresponding to the oxide additives in the XRD patents were observed. These results suggest that the oxides are most likely well dispersed on the support. However, it is difficult to estimate the dispersion of oxide additives. Anyhow, a well dispersed oxides with high activity of CO<sub>2</sub> adsorption and dissociation, located nearby the metal particles and a fast surface diffusion are highly desired. It has been reported that the metal and oxide interface is the active sites for CO<sub>2</sub> dissociation (ACS Catal. 2016, 6, 4501–4505). The insights provided here could rationalize the literature observations. Van Keulen et al. [24] also observed that conversion of CO<sub>2</sub> was greater for Pt/ZrO<sub>2</sub> compared to Pt/Al<sub>2</sub>O<sub>3</sub> at the same Pt loading. This varying activity towards CO<sub>2</sub> activation could be attributed to the greater basicity of the ZrO<sub>2</sub> support and the presence of O deficiencies. In contrast, Mark et al. [59] found that Al<sub>2</sub>O<sub>3</sub>, which is acidic in nature, does not help to activate the mildly acidic CO<sub>2</sub>.

The fact that the apparent activation energy of CO<sub>2</sub> activation depends on the electronegativity of cations in the oxide additives suggests the activation on the added oxides is domination for CO<sub>2</sub> activation while the surface diffusion is relatively fast and not kinetically relevant. Figure 12b clearly illustrates the deactivation function is a function of electronegativity of cations of the oxides. The lower deactivation function, indicating a lower deactivation rate and better catalyst stability, was obtained at a lower electronegativity. The

enhanced CO<sub>2</sub> activation at lower electronegativity promoted generation of O\*. Through diffusion of O\* into Ni surfaces, it enhanced the surface reaction steps of CHx with O\* and thus reduced the coke formation and stabilized the catalysts.

In addition, it should be noted that the Al-Mg mixed oxide obtained from calcination of hydrotalcite like materials is also basic. The exact electronegativity of the support without oxide promotion is unknown. We try to apply the relationship in Fig. 12a to unknown catalysts. Based on the activation energy of CO<sub>2</sub>, the electronegativity for Ni catalyst without promoter can be predicted to be approximately **??** kJ/mol. Plotting the predicted electron affinity and experimental deactivation factor in Fig. 12b, it fits well the tendency of the deactivation factor as a function of electron affinity. It proves an applicability of these two plots in catalyst design. Both the increased basicity of oxide and electron affinity of metal help to promote the CO<sub>2</sub> activation and enhance the catalyst's stability. We propose that CeO<sub>2</sub>-Ni has best performance for CO<sub>2</sub> activation, thus leading to a higher concentration of surface oxygen to oxidize the carbon on the catalysts, which prolongs the catalyst's life.



Fig. 12. (a) Ea<sub>CO2</sub> and (b) deactivation factor as a function of electron affinity of metal in the oxides.

The plot in Fig. 12 provides a principle for catalyst design for DRM to achieve better stability. Oxides consisting of cations with lower electronegativity such as Bi (91), Sb (101),

Sn (107) etc [64] are predicted to be good candidates for promoters of Ni catalysts, which will be investigated in future.

#### 4. Conclusions

Through impregnating oxide additives (CeO<sub>2</sub>, ZrO<sub>2</sub> and ZnO) into the 12 wt% Ni hydrotalcite-derived catalysts, we synthesized thermally stable and highly selective promoted Ni catalyst for methane dry reforming reaction. All the promoted Ni catalysts presented slightly lower activity compared to the Ni catalyst. CeO2-Ni catalyst exhibited the highest H<sub>2</sub>/CO ratio along all the temperatures and the best stability. DFT calculation assisted kinetic analysis and experimental kinetic study reveal the dependence of the rate-determining step on the CO<sub>2</sub> activation. For the fast oxide assisted CO<sub>2</sub> activation process, the methane activation became the rate-determining step. Promotion of Ni catalyst by oxides such as CeO2, ZrO2 and ZnO enhanced CO<sub>2</sub> activation. The activation energy decreased and stability increased with decreasing electronegativity of cations of oxide additives and CeO<sub>2</sub>-Ni catalyst has the lowest apparent activation energy for CO<sub>2</sub> activation and the best stability. The enhanced CO<sub>2</sub> activation increased the surface oxygen concentration, which promoted oxidation of the surface carbon species, thus reduced carbon formation and improved the catalyst stability. This work presents new mechanistic and kinetic insights into the functions of oxides on Ni catalysts in methane dry reforming combing kinetic studies and DFT calculations, identified electronegativity of the cations of the oxide additive as a descriptor, which could provide principles for catalysts design to improve stability and selectivity of Ni based catalysts.

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