

Fast Economic Model Predictive Control for a Gas Lifted Well Network ^{*}

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Abstract: This paper considers the optimal operation of an oil and gas production network by formulating it as an economic nonlinear model predictive control (NMPC) problem. Solving the associated nonlinear program (NLP) can be computationally expensive and time consuming. To avoid a long delay between obtaining updated measurement information and injecting the new inputs in the plant, we apply a sensitivity-based predictor-corrector path-following algorithm in an advanced-step NMPC framework. We demonstrate the proposed method on a gas-lift optimization case study, and compare the performance of the path-following economic NMPC to a standard economic NMPC formulation.

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1. INTRODUCTION

Operation of an oil and gas production network involves making daily control decisions in order to maximize the revenue while satisfying process and operating constraints. This is known as short-term production optimization or daily production optimization (DPO). Mathematical tools are increasingly used in production optimization to compute the optimal decision variables based on a digital representation of the system. The use of mathematical optimization for daily production optimization has enabled production increases in the range of 1-4% (Stenhouse et al., 2010). A comprehensive survey of optimization tools used for production optimization can be found in Bieker et al. (2007). DPO problems may be formulated as either static optimization problems or dynamic optimization problems. Useful discussions on the static and dynamic formulations for DPO are provided in Foss et al. (2017), where the authors note that DPO applications may benefit from dynamic formulations in some cases, particularly when the profit is strongly affected by short-term control decisions.

In this paper, we consider such a dynamic production optimization problem, where the control and optimization layers are tightly integrated. In this case, the production optimization problem is formulated as an economic nonlinear model predictive control (ENMPC) problem. The key idea in ENMPC is to use a single dynamic optimization problem to control the process, and to optimize the economic performance simultaneously. By doing so, the economic cost is optimized also during transient operation of the system. In the face of volatile oil prices and competitive markets, optimizing the transients to maximize profits has become more and more desirable.

For large-scale production networks, the economic NMPC problem formulation may become rather large with several hundred decision variables. For example, the production optimization of the Troll oil field in the Norwegian continental shelf includes more than one hundred subsea wells (Hauge et al., 2005). This leads to optimization problems that are computationally very intensive. Moreover, nonlinear models are typically used for economic optimization, which further adds to the computational complexity. Computational cost has been a prohibitive factor for the widespread implementation of dynamic optimization in the oil and gas industry, despite being a promising approach, as noted in Forbes et al. (2015). Solving the large-scale nonlinear programming (NLP) problem may take a significant amount of time and this computational delay can lead to performance degradation or even to closed-loop instabilities (Findeisen and Allgöwer, 2004). Hence there is a clear need for numerical methods that make it possible to obtain updated solutions to the large-scale NLP in very short time.

In this paper we address this issue by applying a sensitivity-based path-following algorithm in an advanced-step NMPC framework (Suwartadi et al., 2017) to a gas-lift optimization problem. The algorithm has the advantage that it can handle large parameter changes, and still give an accurate approximation of the solution. Several sensitivity-based approaches have been proposed to address the issue of computation time. See e.g. Diehl et al. (2005), Zavala and Biegler (2009), Jäschke et al. (2014). A review article on fast NMPC schemes is given by Wolf and Marquardt (2016).

At each sample time, the NMPC optimization problems are identical, except for one time varying parameter, namely, the initial state. All the fast sensitivity approaches capitalize on this property. When new measurements of the states become available, these approaches use the

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sensitivity of the optimal solution that was computed at a previous time step to obtain fast approximate solutions to the new resulting nonlinear optimization problem. Such approximations enable fast implementation of the optimal input in the plant in a minimal delay.

The remainder of the paper is organized as follows. The daily production optimization problem for a gas lifted well network is introduced in Section 2. The sensitivity-based economic NMPC with the path-following approach is presented in Section 3. Simulation results from a gas-lift optimization case study are presented in Section 4, before concluding the paper in Section 5.

2. PROBLEM FORMULATION

An offshore oil and gas production network typically consists of several wells that produce to a common processing facility. The reservoir fluid enters through the well bore of each well and is produced to a topside processing facility via a common production manifold as shown in Fig.1. In some wells, the reservoir pressure may not be sufficient to lift the fluids to the surface. In such cases, artificial lift methods are employed to boost the production from the wells. In this paper, we consider the gas lift method, which is a commonly used artificial lift technology. In gas lifted wells, compressed gas is injected into the well tubing via the annulus to reduce the mixture density. This results in reduced hydrostatic pressure, and hence boosted production. However, higher gas injection rates also increase the frictional pressure drop. The oil production starts to decline if the effect of the frictional pressure drop is dominant over the effect of the hydrostatic pressure drop.

Production from a cluster of $\mathcal{N} = \{1, \dots, n_w\}$ gas lifted wells can be modelled as a semi-explicit index-1 DAE system of the form,

$$\dot{\mathbf{x}} = f(\mathbf{x}, \mathbf{z}, \mathbf{u}), \quad (1a)$$

$$0 = g(\mathbf{x}, \mathbf{z}, \mathbf{u}), \quad (1b)$$

where $f(\mathbf{x}, \mathbf{z}, \mathbf{u})$ is the set of differential equations and $g(\mathbf{x}, \mathbf{z}, \mathbf{u})$ is the set of algebraic equations. The dynamics arise in the model due to the mass balances for oil and gas phases in each well and the riser. Algebraic equations are used to describe the densities, pressures and flow rates for each well and the riser, as described in detail by Krishnamoorthy et al. (2016).

The inlet separator in the topside processing facility sets the downstream boundary conditions which are typically kept at a constant pressure by tight regulatory control. The upstream boundary conditions are set by the reservoir inflow conditions. The DPO problem is concerned with the production network exposed to these upstream and downstream conditions, and hence the reservoir model and topside processing facilities are not included in the production optimization problem.

Gas lifted wells are often controlled by adjusting the gas lift injection rate of each well. The production network is also subject to process and operating constraints. For example, the total gas processing capacity in the topside facilities may be constrained, or the rate of compressed gas injection may be limited. The optimization problem then involves computing the optimal gas lift injection rates

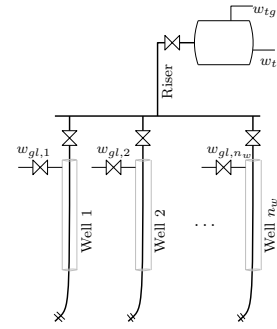


Fig. 1. Schematic representation of a gas lifted production network with n_w wells producing to a common topside processing facility.

for each well such that the operating profits are maximized subject to the network processing and operating constraints.

Before this can be formulated as an economic NMPC problem, the infinite dimensional problem is discretized into finite horizon optimal control problem using direct collocation method. The discretized system dynamics at any time instant l can be expressed as,

$$\mathbf{F}(\boldsymbol{\chi}_{l+1}, \boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) = 0. \quad (2)$$

A detailed explanation on how the system is discretized into a nonlinear programming problem using direct collocation can be found in Krishnamoorthy et al. (2016).

The economic NMPC problem can then be formulated as

$$\begin{aligned} \mathcal{P}_N(\mathbf{x}_k) : \min_{\boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l} & \Psi(\boldsymbol{\chi}_{k+N}, \boldsymbol{\zeta}_{k+N}) + \sum_{l=k}^{k+N-1} \psi(\boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) \\ \text{s.t. } & \mathbf{F}(\boldsymbol{\chi}_{l+1}, \boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) = 0, \quad \forall l \in \mathcal{N} \\ & \mathbf{G}(\boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) \leq 0, \quad \forall l \in \mathcal{N} \\ & (\boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) \in \mathcal{Z}, \quad \forall l \in \mathcal{N} \\ & (\boldsymbol{\chi}_{k+N}, \boldsymbol{\zeta}_{k+N}) \in \mathcal{X}_f \\ & \boldsymbol{\chi}_0 = \mathbf{x}_k. \end{aligned} \quad (3)$$

Here $\boldsymbol{\chi}_l \in \mathbb{R}^{n_x}$, $\boldsymbol{\nu}_l \in \mathbb{R}^{n_\nu}$, and $\boldsymbol{\zeta}_l \in \mathbb{R}^{n_c}$ represent the predicted state, control input, and algebraic at time instance l , respectively for all l belonging to $\mathcal{N} = \{k, \dots, k+N\}$. The constraints include the system dynamics as equality constraint, nonlinear inequality constraints \mathbf{G} , and the equality constraint of the initial predicted state $\boldsymbol{\chi}_0$ equal to the actual state $\mathbf{x}_k \in \mathbb{R}^{n_x}$ obtained from measurement data. The path constraint confines the predicted state, algebraic, and control inside the set \mathcal{Z} , and the final state and algebraic variables $(\boldsymbol{\chi}_{k+N}, \boldsymbol{\zeta}_{k+N})$ are constrained to lie in the set \mathcal{X}_f . The objective function comprises the final cost $\Psi(\boldsymbol{\chi}_{k+N}, \boldsymbol{\zeta}_{k+N}) \in \mathcal{C}^2 : \mathbb{R}^{n_x} \times \mathbb{R}^{n_c} \rightarrow \mathbb{R}$ and the stage cost $\psi(\boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) \in \mathcal{C}^2 : \mathbb{R}^{n_x} \times \mathbb{R}^{n_c} \times \mathbb{R}^{n_\nu} \rightarrow \mathbb{R}$.

In the gas lifted well problem, the stage cost is defined as

$$\psi(\boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) := \sum_{i=1}^{n_w} (-r_o w_{po,i} + r_{gl} w_{gl,i}), \quad (4)$$

where r_o is the oil price, r_{gl} is the cost for gas lift injection, and n_w denotes the number of production wells. The nonlinear inequality constraints enforce the total gas capacity constraints,

$$\mathbf{G}(\boldsymbol{\chi}_l, \boldsymbol{\zeta}_l, \boldsymbol{\nu}_l) := \sum_{i=1}^{n_w} (w_{pg,i} - w_g^{max}). \quad (5)$$

The path constraints are in the form of bound constraints for the state, control inputs as well as the algebraic variables

$$\begin{pmatrix} \underline{\boldsymbol{\chi}} \\ \underline{\boldsymbol{\zeta}} \\ \underline{\boldsymbol{\nu}} \end{pmatrix} \leq \begin{pmatrix} \boldsymbol{\chi}_l \\ \boldsymbol{\zeta}_l \\ \boldsymbol{\nu}_l \end{pmatrix} \leq \begin{pmatrix} \overline{\boldsymbol{\chi}} \\ \overline{\boldsymbol{\zeta}} \\ \overline{\boldsymbol{\nu}} \end{pmatrix}. \quad (6)$$

The notations $\overline{\cdot}$ and $\underline{\cdot}$ represent the upper and lower bound for the corresponding variable. It is easily possible to limit the state variables with the bound constraints since the system dynamics are transcribed using direct collocation, in which the state, algebraic, and control are treated as optimization variables.

Once the economic NMPC problem is formulated, it can be solved in a receding horizon fashion. At each sample time k , the state measurement or estimate \mathbf{x}_k is assigned as the initial state for the optimization problem (3). The optimization problem is solved to compute the optimal input trajectory $\boldsymbol{\nu}_{[l,l+N]}^*$ over the prediction horizon. The first step of the optimal control sequence is implemented in the plant, i.e. $\mathbf{u}_k^* = \boldsymbol{\nu}_1^*$. At the next time step $k+1$, new measurements of the state \mathbf{x}_{k+1} are obtained and the optimization procedure is repeated, hence enabling closed-loop implementation.

We consider a full-state feedback control structure. The measurements from the plant are used for estimating the states. The estimated states are then used for full state feedback for the economic NMPC, which computes the optimal inputs for the plant. The state estimation is performed online by an extended Kalman filter (EKF). The EKF is implemented in discrete time as described in Krishnamoorthy et al. (2017). Commonly available measurements such as annulus pressure, wellhead pressure and down hole pressure for each well along with the riser head pressure, manifold pressure and total oil and gas production rates are used as measurements for the EKF.

In an ideal case, the optimization problem (3) would be solved instantly and the optimal input would be implemented in the plant without time delay. In practice, however, there is always some delay between the state measurement/estimation and the implementation of the optimal control input. This is mainly because of the computational time required to solve the optimization problem (3). For many linear MPC applications, the computational delay is rather small and can be neglected. However, for large-scale nonlinear systems, as the number of optimization variable increases, solving the optimization problem requires more time, and the computational delay may no longer be neglected.

3. FAST ECONOMIC NMPC

To address the issue of computational delay, fast sensitivity-based NMPC approaches have been developed. One such approach is the advanced-step NMPC (asNMPC) introduced by Zavala and Biegler (2009), where at time k , the NMPC problem is solved with the predicted state value of time $k+1$ instead of using the measured/estimated state \mathbf{x}_k . An approximation of the NLP solution is then computed using a single sensitivity step (Zavala and Biegler,

2009), or a path-following approach (Jäschke et al., 2014; Suwartadi et al., 2017) as soon as the measurement \mathbf{x}_{k+1} is available at time $k+1$. In this work we use the predictor-corrector path-following algorithm based on Suwartadi et al. (2017), described below.

Since the optimization problem (3) differs only in the initial state variable, which is denoted as the equality constraint $\boldsymbol{\chi}_0 = \mathbf{x}_k$, from one NMPC iteration to another, the problem can be cast as the following parametric NLP problem

$$\begin{aligned} \min_{\mathbf{X}} \quad & \mathcal{J}(\mathbf{X}, \mathbf{p}) \\ \text{s.t.} \quad & c_i(\mathbf{X}, \mathbf{p}) = 0, i \in \mathcal{E}, \\ & c_i(\mathbf{X}, \mathbf{p}) \leq 0, i \in \mathcal{I}, \end{aligned} \quad (7)$$

where $\mathbf{X} \in \mathbb{R}^{n_x}$ is the primal variable, $\mathbf{p} \in \mathbb{R}^{n_p}$ is the parameter, and the objective function $\mathcal{J} : \mathbb{R}^{n_x} \times \mathbb{R}^{n_p} \rightarrow \mathbb{R}$. The equality and inequality constraints $c : \mathbb{R}^{n_x} \times \mathbb{R}^{n_p} \rightarrow \mathbb{R}^{n_c}$ are represented by the sets $\mathcal{E} = \{1, \dots, m\}$ and $\mathcal{I} = \{m+1, \dots, n_c\}$, respectively.

We define Lagrangian of the problem (7) as

$$\mathcal{L}(\mathbf{X}, \boldsymbol{\lambda}, \mathbf{p}) := \mathcal{J}(\mathbf{X}, \mathbf{p}) + \boldsymbol{\lambda}^T c(\mathbf{X}, \mathbf{p}), \quad (8)$$

where $\boldsymbol{\lambda}$ is the dual variable or Lagrange multiplier. The first-order optimality (*Karush-Kuhn-Tucker (KKT)*) conditions are

$$\begin{aligned} \nabla_{\mathbf{X}} \mathcal{L}(\mathbf{X}, \boldsymbol{\lambda}, \mathbf{p}) &= 0, \\ c_i(\mathbf{X}, \mathbf{p}) &= 0, i \in \mathcal{E}, \\ c_i(\mathbf{X}, \mathbf{p}) &\leq 0, i \in \mathcal{I}, \\ \boldsymbol{\lambda}_i^T c_i(\mathbf{X}, \mathbf{p}) &= 0, i \in \mathcal{I}, \\ \boldsymbol{\lambda}_i &\geq 0, i \in \mathcal{I}. \end{aligned} \quad (9)$$

Active inequality constraints are denoted by the set $\mathcal{A}(\mathbf{X}, \mathbf{p}) = \{c_i(\mathbf{X}, \mathbf{p}) = 0, i \in \mathcal{I}\}$. For a given multiplier $\boldsymbol{\lambda}$ and \mathbf{X} that satisfies the KKT conditions (9), the active inequality set $\mathcal{A}(\mathbf{X}, \mathbf{p})$ has two subsets, which are a weakly active set $\mathcal{A}_0(\mathbf{X}, \boldsymbol{\lambda}, \mathbf{p}) = \{i \in \mathcal{A}(\mathbf{X}, \mathbf{p}) \mid \boldsymbol{\lambda}_i = 0\}$ and a strong active set $\mathcal{A}_+(\mathbf{X}, \boldsymbol{\lambda}, \mathbf{p}) = \{i \in \mathcal{A}(\mathbf{X}, \mathbf{p}) \mid \boldsymbol{\lambda}_i > 0\}$.

Furthermore, we define the optimality residual as

$$\eta(\mathbf{X}, \boldsymbol{\lambda}, \mathbf{p}) = \left\| \begin{pmatrix} \nabla_{\mathbf{X}} \mathcal{J}(\mathbf{X}, \mathbf{p}) + \nabla_{\mathbf{X}} c(\mathbf{X}, \mathbf{p}) \boldsymbol{\lambda} \\ c(\mathbf{X}, \mathbf{p})_{\mathcal{E}} \\ [\min(c(\mathbf{X}, \mathbf{p}), \boldsymbol{\lambda})]_{\mathcal{I}} \end{pmatrix} \right\|_{\infty}. \quad (10)$$

Here, we assume that the linear independent constraint qualification (LICQ) is satisfied at any point \mathbf{X} that satisfies the KKT conditions (9).

Definition 1. (LICQ). Given a vector \mathbf{p} and a point \mathbf{X} , the *linear independence constraint qualification* (LICQ) holds at \mathbf{X} if the set of vectors $\{\nabla_{\mathbf{X}} c_i(\mathbf{X}, \mathbf{p})\}_{i \in \mathcal{E} \cup \mathcal{A}(\mathbf{X}, \mathbf{p})}$ are linearly independent.

We also assume that the strong second order sufficient condition is also satisfied.

Definition 2. (SSOSC). The *strong second order sufficient condition* (SSOSC) holds at $(\mathbf{X}, \boldsymbol{\lambda})$ that satisfies the KKT conditions, if $\mathbf{d}^T \nabla_{\mathbf{X}}^2 \mathcal{L}(\mathbf{X}, \mathbf{p}, \boldsymbol{\lambda}) \mathbf{d} > 0$ for all $\mathbf{d} \neq 0$ such that $\nabla_{\mathbf{X}} c_i(\mathbf{X}, \mathbf{p})^T \mathbf{d} = 0$ for $i \in \mathcal{E} \cup \mathcal{A}_+(\mathbf{X}, \mathbf{p}, \boldsymbol{\lambda})$.

We are now ready to state the result for sensitivity of the NLP, where $\mathbf{X}^*(\mathbf{p})$ and $\boldsymbol{\lambda}^*(\mathbf{p})$ are the primal and dual solutions of (7), respectively.

Theorem 3. Let \mathcal{J} , c be twice continuously differentiable in \mathbf{p} and \mathbf{X} near a solution of (7) $(\mathbf{X}^*, \mathbf{p}_0)$, and let LICQ and SSOSC hold at $(\mathbf{X}^*, \mathbf{p}_0)$. Then the solution $(\mathbf{X}^*(\mathbf{p}), \boldsymbol{\lambda}^*(\mathbf{p}))$ is Lipschitz continuous in a neighborhood of $(\mathbf{X}^*, \boldsymbol{\lambda}^*, \mathbf{p}_0)$, and the solution function $(\mathbf{X}^*(\mathbf{p}), \boldsymbol{\lambda}^*(\mathbf{p}))$ is directionally differentiable. Moreover, the directional derivative uniquely solves the following quadratic problem:

$$\begin{aligned} \min_{\Delta \mathbf{X}} \quad & \frac{1}{2} \Delta \mathbf{X}^T \nabla_{\mathbf{X}\mathbf{X}}^2 \mathcal{L}(\mathbf{X}^*, \mathbf{p}_0, \boldsymbol{\lambda}^*) \Delta \mathbf{X} \\ & + \Delta \mathbf{X}^T \nabla_{\mathbf{p}\mathbf{X}} \mathcal{L}(\mathbf{X}^*, \mathbf{p}_0, \boldsymbol{\lambda}^*) \Delta \mathbf{p} \\ \text{s.t.} \quad & \\ & \nabla_{\mathbf{X}} c_i(\mathbf{X}^*, \mathbf{p}_0)^T \Delta \mathbf{X} \\ & + \nabla_{\mathbf{p}} c_i(\mathbf{X}^*, \mathbf{p}_0)^T \Delta \mathbf{p} = 0 \quad i \in \mathcal{A}_+ \cup \mathcal{E}, \\ & \nabla_{\mathbf{X}} c_j(\mathbf{X}^*, \mathbf{p}_0)^T \Delta \mathbf{X} \\ & + \nabla_{\mathbf{p}} c_j(\mathbf{X}^*, \mathbf{p}_0)^T \Delta \mathbf{p} \leq 0 \quad j \in \mathcal{A}_0. \end{aligned} \quad (11)$$

Proof. See Robinson (1980) and (Bonnans and Shapiro, 1998, Section 5.2). \square

Instead of solving a full NLP problem, one can solve a quadratic programming (QP) problem (11) to compute a first-order approximation of the solution to the optimization problem (3) in the vicinity of perturbation \mathbf{p}_0 . We refer the QP (11) to as *pure-predictor QP*. Note that there is no requirement of strict complimentary in the theorem, allowing for active-set changes.

To improve the approximation of the solution, we introduce a corrector term in the objective function, and taking into account that the parameter \mathbf{p} enters linearly in the problem, we can formulate the following QP (Suwartadi et al., 2017; Kungurtsev and Diehl, 2014)

$$\begin{aligned} \min_{\Delta \mathbf{X}} \quad & \frac{1}{2} \Delta \mathbf{X}^T \nabla_{\mathbf{X}\mathbf{X}}^2 \mathcal{L}(\mathbf{X}^*, \mathbf{p}_0 + \Delta \mathbf{p}, \boldsymbol{\lambda}^*) \Delta \mathbf{X} \\ & + \nabla_{\mathbf{X}} \mathcal{J}^T \Delta \mathbf{X} \\ \text{s.t.} \quad & \\ & c_i(\mathbf{X}^*, \mathbf{p}_0 + \Delta \mathbf{p})^T \Delta \mathbf{p} \\ & + \nabla_{\mathbf{X}} c_i(\mathbf{X}^*, \mathbf{p}_0 + \Delta \mathbf{p})^T \Delta \mathbf{X} = 0, i \in \mathcal{A}_+ \cup \mathcal{E}, \\ & c_j(\mathbf{X}^*, \mathbf{p}_0 + \Delta \mathbf{p})^T \Delta \mathbf{p} \\ & + \nabla_{\mathbf{X}} c_j(\mathbf{X}^*, \mathbf{p}_0 + \Delta \mathbf{p})^T \Delta \mathbf{X} \leq 0, j \in \mathcal{I} \setminus \mathcal{A}_+. \end{aligned} \quad (12)$$

We denote the QP above as *predictor-corrector QP*, see Algorithm 1. This QP formulation provides a reasonably good approximation of the NLP solution in a small neighborhood of \mathbf{p}_0 . To allow large perturbation (large $\Delta \mathbf{p}$), we employ a path-following approach, that is, to solve a series of QP problems. This is analogous to Euler integration scheme for ordinary differential equations. The parameter \mathbf{p} is updated according to $\mathbf{p}(t_j) = (1 - t_j) \mathbf{p}_0 + t_j \mathbf{p}_f$, where $t_0 = 0$ until it reaches $t = 1$, that is $t_0 = 0, t_1 < t_2 \dots < t_j < t_{j+1} \dots < t_{end} = 1$. The parameter \mathbf{p}_f corresponds to new measurement data. During the course of path-following iteration, the primal variable $\Delta \mathbf{X}$ and dual variable $\Delta \boldsymbol{\lambda}$ are updated for each t_j . The optimality residual condition η (10) is computed and compared against its

maximum tolerance η_{max} . If necessary, the stepsize Δt is reduced to satisfy $\eta < \eta_{max}$. The method is implemented as a subroutine in Algorithm 1, denoted as QP_PC_PF.

As described in Suwartadi et al. (2017) and Jäschke et al. (2014), we apply the path-following QP within the advanced-step NMPC (*asNMPC*) framework (see Zavala and Biegler (2009)) and refer the method to as *pf-NMPC*. The *pf-NMPC* procedure includes the following three steps.

- (1) Solve the NLP problem (3) at time k constraining the initial state value to the predicted state at $k + 1$.
- (2) When the measurement \mathbf{x}_{k+1} becomes available at time $k + 1$, compute an approximation of the NLP solution (3) using the QP (12) in a path-following manner.
- (3) Implement the optimal control input and update $k \leftarrow k + 1$ and repeat from Step 1.

A sketch of the pf-NMPC procedure is described in Algorithm 1.

4. SIMULATION RESULTS

In this section we use a gas lifted well network with $n_w = 2$ wells to demonstrate the pf-NMPC controller and compare its results against the ideal NMPC (iNMPC) controller which solves the problem (3) using an NLP solver. All simulations are done in MATLAB using CasADi version 3.2.0 as algorithmic differentiation tool (Andersson, 2013) where IPOPT (Wächter and Biegler, 2006) is included as an NLP solver. We use the QP solver from TOMLAB MINOS (Murtagh and Saunders, 1982).

First, we run a steady-state optimization with total gas production capacity constraint equals to 9.5 kg/s. The optimized steady-state control inputs, algebraic and state variables are incorporated in the stage cost regularization terms, i.e.,

$$\begin{aligned} \psi_m(\boldsymbol{\chi}_l, \boldsymbol{\nu}_l, \boldsymbol{\zeta}_l) = & \psi(\boldsymbol{\chi}_l, \boldsymbol{\nu}_l, \boldsymbol{\zeta}_l) \\ & + \alpha (\|\boldsymbol{\chi}_l - \mathbf{x}_s\|, \|\boldsymbol{\nu}_l - \mathbf{u}_s\|, \|\boldsymbol{\zeta}_l - \mathbf{z}_s\|), \end{aligned} \quad (13)$$

where \mathbf{x}_s , \mathbf{u}_s , and \mathbf{z}_s are the steady-state state variable, control input, algebraic variable respectively.

Next, we run the NMPC controllers and initiate the system with an initial condition far away from the optimal point. The NMPC controllers are implemented with sampling time of 5 minutes with a prediction horizon of 2 hours yielding 3014 optimization variables and 2966 nonlinear constraints in the NLP.

We set $\eta_{max} = 10^{-5}$ and initial $\Delta t = 1.0$ for the pf-NMPC controller. Note that we use an adaptive steplength strategy for Δt in the Algorithm 1 meaning that the steplength Δt may be reduced in case $\eta_{max} > 10^{-5}$.

4.1 Comparison of Open-loop Optimization Results

We compare the open loop solutions from the ideal NMPC and pf-NMPC controllers at time $t = 10$ minute (at second NMPC iteration). The results are shown in Figure 2 in which the total oil and gas production are depicted. The solutions from pf-NMPC accurately track those of the ideal

Algorithm 1 Economic pf-NMPC algorithm**Input:** initial state \mathbf{x}_0 , initial Δt , and η_{max} .

```

for  $k = 0, 1, 2, \dots$  do
   $[\mathbf{X}^*, \boldsymbol{\lambda}^*] \leftarrow$  solution NLP  $\mathcal{P}_N(\mathbf{x}_{k+1})$  for  $k + 1$ .
  if a measurement of  $\mathbf{x}_{k+1}$  is available then
    Set  $\mathbf{p}_0 \leftarrow \mathbf{x}_{k+1}$ .
    Set  $\mathbf{p}_f \leftarrow \mathbf{x}_{k+1}$ .
     $\mathbf{X} \leftarrow$  QP_PC_PF( $\mathbf{X}^*, \boldsymbol{\lambda}^*, \mathbf{p}_0, \mathbf{p}_f, \Delta t$ )
    Extract first input value from  $\mathbf{X}$  and inject to
    the plant as  $\mathbf{u}_k$ .
    Update initial state  $\mathbf{x}_0 \leftarrow \mathbf{x}_{k+1}$ .
    Set  $k + 1 \leftarrow k$ .
  end if
end for

```

function QP_PC_PF($\mathbf{X}, \boldsymbol{\lambda}, \mathbf{p}_0, \mathbf{p}_f, \Delta t$)

```

Define parameter  $\gamma$  satisfying  $0 < \gamma < 1$ .
Determine  $\mathcal{A}_+$ .
Set parameter  $\eta_{max}$ .
Set  $j \leftarrow 0$ .
Set  $t_j \leftarrow 0$ .
while  $t_j < 1$  do
  Compute  $\eta_j := \eta(\mathbf{X}_j, \boldsymbol{\lambda}_j, \mathbf{p}(t_j))$ .
  if QP is feasible then ▷ solve QP
    Compute  $\eta_{j+\Delta} := \eta(\mathbf{X}_j + \Delta\mathbf{X}, \Delta\boldsymbol{\lambda}, \mathbf{p}(t_j + \Delta t))$ .
    if  $\eta_{j+\Delta} > \eta_{max}$  then.
      Decrease  $\Delta t$ . ▷ reduce QP stepsize
       $j \leftarrow j + 1$ .
    else
       $\mathbf{X} \leftarrow \mathbf{X} + \Delta\mathbf{X}$ 
       $\boldsymbol{\lambda} \leftarrow \Delta\boldsymbol{\lambda}$ 
       $t_{j+1} \leftarrow t_j + \Delta t$ 
       $\mathbf{p}(t_j) = (1 - t_j)\mathbf{p}_0 + t_j\mathbf{p}_f$ 
      if  $\eta_{j+\Delta} < \eta_j^{1+\gamma}$  then ▷ very good step
        Increase  $\Delta t$ .
      end if
      Update  $\mathcal{A}_+$ . ▷ from QP's dual solution.
       $j \leftarrow j + 1$ .
    end if
  else
    Decrease  $\Delta t$ . ▷ reduce QP stepsize
     $j \leftarrow j + 1$ .
  end if
end while
return  $\mathbf{X}$ 
end function

```

Output: $\mathbf{x}_1, \mathbf{x}_2, \mathbf{x}_3, \mathbf{u}_1, \mathbf{u}_2, \mathbf{u}_3, \dots$

NMPC controller. The errors between the ideal NMPC and pf-NMPC are plotted in Figure 3.

4.2 Closed-loop Results

Next, we compare the closed-loop solution for both NMPC controllers. The solutions, control input profiles as well as total gas and oil productions, are displayed in Figure 4 and Figure 5. The total gas production capacity constraint, shown in Figure 5, is active. The solutions of pf-NMPC approximate the solutions of the ideal NMPC controllers very well. Moreover, we compare the online optimization

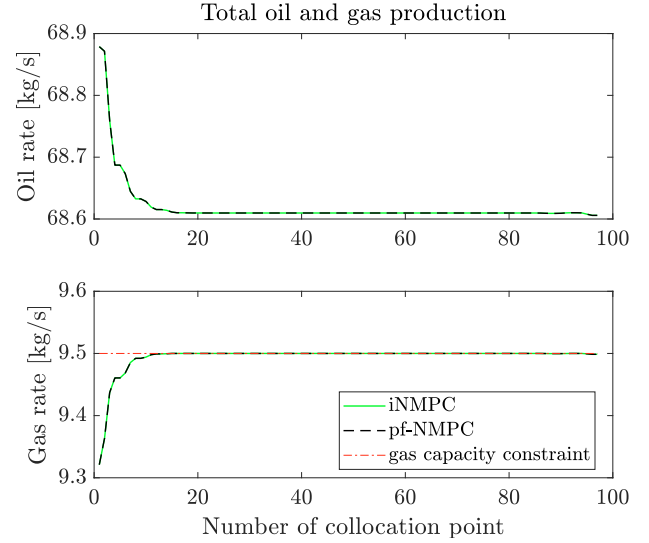


Fig. 2. Comparison of total oil and gas production for iNMPC and pf-NMPC controllers from open loop solutions at iteration number two. The solution of iNMPC is depicted in green color, which overlaps the solution of pf-NMPC denoted in black color.

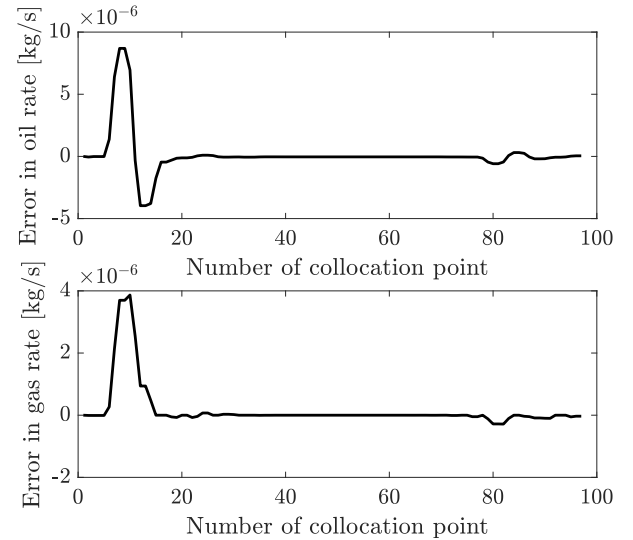


Fig. 3. Total production errors for open-loop solution at iteration number two.

	online optimization runtime (in sec.)		
	min	max	average
iNmPC	0.85	0.94	0.88
pf-NmPC	0.34	0.39	0.36

runtime for 60 NMPC iterations. It is shown that the pf-NMPC controller is able to speed up the optimization more than two times faster than those of the ideal NMPC controller. However, a rigorous comparison of runtime is very implementation dependent, and outside the scope of this paper.

5. CONCLUSION

In this paper we presented an economic nonlinear model predictive control for a gas lifted well network. To address the issue of computational delay associated with economic

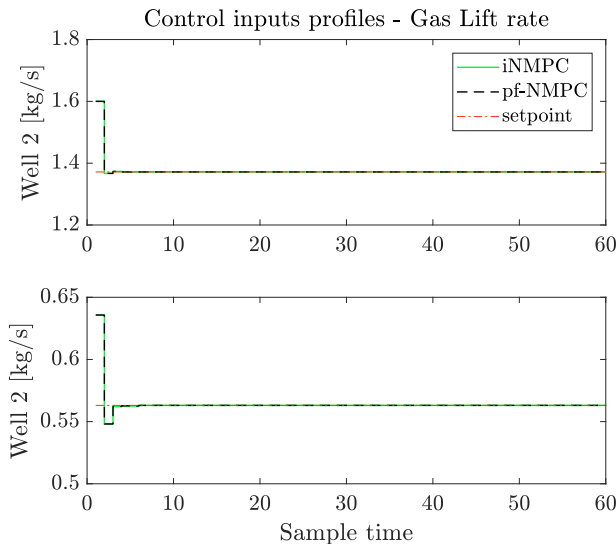


Fig. 4. Control inputs comparison of iNMPC and pf-NMPC controllers from closed-loop solutions.

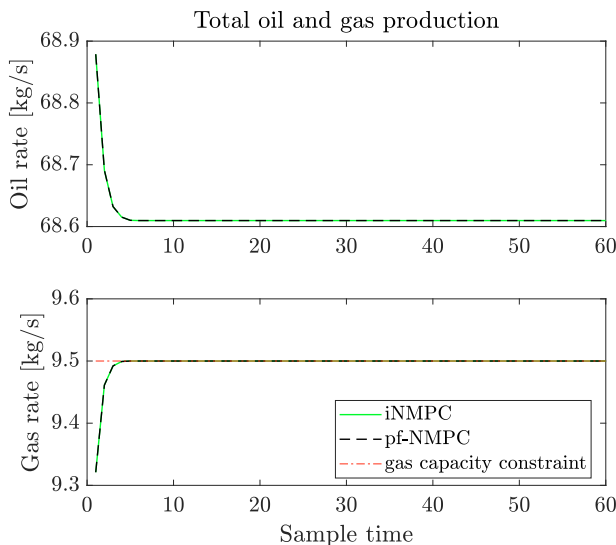


Fig. 5. Total production of oil and gas of iNMPC and pf-NMPC controllers from closed-loop solutions.

NMPC, we presented a path-following predictor-corrector approach. Using simulation results, we showed that the pf-NMPC is able to provide a fast solution, while honoring the active constraints and reasonably approximating the solutions.

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