

1 **hydrological and thermal effects of hydropeaking on early life stages of salmonids: a**
2 **modelling approach for implementing mitigation strategies**

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28 **Hydrological and thermal effects of hydropeaking on early life stages of salmonids: a**
29 **modelling approach for implementing mitigation strategies**

30

31 **Abstract**

32 Alterations in hydrological and thermal regimes can potentially affect salmonid early life stages
33 development and survival. The dewatering of salmon spawning redds due to hydropeaking can lead to
34 mortality in early life stages, with higher impact on the alevins as they have lower tolerance to
35 dewatering than the eggs. Flow-related mitigation measures can reduce early life stage mortality. We
36 present a set of modelling tools to assess impacts and mitigation options to minimise the risk of
37 mortality in early life stages in hydropeaking rivers. We successfully modelled long-term hydrological
38 and thermal alterations and consequences for development rates. We estimated the risk of early life
39 stages mortality and assessed the cost-effectiveness of implementing three release-related mitigation
40 options. The economic cost of mitigation was low and ranged between 0.7% and 2.6% of the annual
41 hydropower production. Options reducing the flow during spawning (B and C) in addition to only
42 release minimum flows during development (A) were considered more effective for egg and alevin
43 survival. Options B and C were however constrained by water availability in the system for certain
44 years, and therefore only option A was always feasible. The set of modelling tools used in this study
45 were satisfactory and their applications can be useful especially in systems where little field data is
46 available. Targeted measures built on well-informed modelling tools can be tested on their
47 effectiveness to mitigate dewatering effects vs. the hydropower system capacity to release or conserve
48 water for power production. Environmental flow releases targeting specific ecological objectives can
49 provide better cost-effective options than conventional operational rules complying with general
50 legislation.

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53 **Keywords**

54 Hydropeaking, Atlantic salmon, water temperature modelling, early life stages development and
55 survival, mitigation measures, hydropower production modelling

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59 1. Introduction

60 Atlantic salmon (*Salmo salar*, L) usually spawns in the autumn by burying their eggs in river gravels.
61 The eggs hatch in spring when a certain number of degree days has been reached. After hatching, the
62 alevins stay in the gravels until having absorbed their yolk-sac and then emerge from the substratum,
63 ready for external feeding. These early life stages are highly dependent on the physico-chemical
64 characteristics of the surrounding hyporheic water, with redds usually constructed in groundwater
65 upwelling areas [Hansen, 1975; Baxter and McPhail, 1999; Garrett et al., 1998; Saltveit and
66 Brabrand, 2013].

67 In hydropeaking rivers, changes in the hydrological and thermal regimes may influence the survival
68 and development of salmonid early life stages [Casas-Mulet et al., 2014b; Casas-Mulet et al., 2016;
69 Harnish et al., 2014]. Impacts in the flow regime may leave salmon redds exposed to dewatered
70 conditions [Young et al., 2011], inducing a limiting factor for the management of sustainable salmon
71 populations [Malcolm et al., 2012; McMichael et al., 2005]. Even if early life stages are well
72 protected in the gravel, dewatering conditions in the redds will impact both egg and alevin survival
73 [Becker et al., 1983; Neitzel and Becker, 1985]. The effects of hydropeaking on river water
74 temperatures can also be significant [Zolezzi et al., 2011]. Hydrological alterations are known to
75 significantly impact the natural thermal regime in rivers [Webb et al., 2008; Olden and Naiman 2010],
76 with major effects to aquatic organisms [McCullough, 1999; McCullough et al., 2009]. Thermal
77 alterations can cause possible bottleneck in salmonid populations by advancing or delaying the
78 development in early stages, promoting negative effects such earlier emergence from the redds or
79 shorten the growth season [Einum and Fleming, 2000; Fisk II et al., 2013].

80 The effects of redd dewatering to salmonid early life stages survival are well understood and differ
81 between egg and alevin phases [Becker and Neitzel, 1985; Becker et al., 1982; Becker et al., 1983;
82 Neitzel and Becker, 1985]. They are particularly relevant in hydropeaking rivers, where dewatering
83 events occur very frequently [Casas-Mulet et al., 2014b; Casas-Mulet et al., 2015b; Harnish et al.,
84 2014]. Eggs are more tolerant and able to survive dewatering events for weeks if they remain moist
85 and not subjected to extreme temperatures or predation [Casas-Mulet et al., 2014b; Reiser and White,
86 1983]. Conversely, after hatching, alevins are dependent on gills for respiration and mortality
87 increases significantly in relatively brief dewatering events (within 1 to 3 hours), if no surface water
88 covers the redds [Becker et al., 1982; Becker et al., 1983].

89 In order to effectively implement mitigation measures in regulated rivers, environmental flows
90 releases mimicking the natural hydrological and thermal regime are the optimal solution to mitigate

91 impacts to ecosystems [Arthington *et al.*, 2010; Olden and Naiman 2010; Poff and Zimmerman,
92 2010]. Suggested mitigation options for early life stages in regulated rivers include the active use of
93 release-related strategies below dams. They aim at either discourage salmon from spawning in
94 habitats potentially subject to dewatering [McMullin and Graham, 1981; Connor and Pflug, 2004],
95 provide minimum discharges during critical conditions for eggs and alevins [Fisk II *et al.*, 2013;
96 Harnish *et al.*, 2014; McMichael *et al.*, 2005], or reduce the difference between spawning and
97 incubation discharge [Stober and Tyler, 1982]. In addition, recent studies on two Norwegian rivers
98 emphasized the importance of considering groundwater upwelling and intragravel water quality when
99 devising mitigation measures for early life stages survival [Casas-Mulet *et al.*, 2014b; Casas-Mulet *et*
100 *al.*, 2016; Saltveit and Brabrand, 2013]. To our knowledge, integrated studies understanding the
101 combined effect of hydrological and thermal alterations of hydropeaking on early life stages are
102 currently inexistent. Such studies are key to select relevant mitigations strategies for the survival of
103 eggs and alevins during early life development, a bottleneck for salmonid populations [Enders *et al.*,
104 2007].

105 Our aim is to present a set of modelling tools for the integrated assessment of impacts and mitigation
106 options for embryo and alevin survival in hydropeaking rivers. Using the Lundesokna river (Norway)
107 as a case study, we addressed the following objectives:

- 108 - To model the alteration of natural thermal regimes and consequences for early life stages
109 development,
- 110 - To estimate the combined impact of altered hydrological and thermal regimes to egg and
111 alevin survival,
- 112 - To assess the cost-effectiveness of different release-related mitigation approaches to minimise
113 early life stages mortality.

114

115 **2. Field study in the Lundesokna River**

116 *2.1. Study sites*

117 The River Lundesokna is a major tributary to the River Gaula (Figure 1). The Gaula is the largest
118 unregulated river in Central Norway. It is listed among Norway's top three salmon rivers, with an
119 average annual catch of about 34 tons over the last 15 years. The Lundesokna is subject to daily flow
120 fluctuations as its lowermost power plant, Sokna (Figure 1), operates according to daily and weekly
121 market demand. Three reservoirs (Håen, Samsjøen and Holtsjøen) supply 145 Mm³ of water to the
122 Lundesokna hydropower system (Figure 1). Hydropeaking in the Lundesokna results in periodically
123 abrupt flow fluctuations that can change from 0.45 to 19 m³s⁻¹ in < 20 minutes (ramping rate ~3

124 $\text{cm}\cdot\text{min}^{-1}$). A minimum flow of $0.3 \text{ m}^3\text{s}^{-1}$ bypasses the power house, and the production discharge
125 ranges between $8 \text{ m}^3\text{s}^{-1}$ (minimum) and $18 \text{ m}^3\cdot\text{s}^{-1}$ (maximum). A more detailed description of the
126 Lundesokna hydropower system is found in *Casas-Mulet et al.* [2014c].

127 A total of four sites in the River Lundesokna (Figure 1) were selected for this study. They were
128 characterised for differentiated river morphologies and had been used in previous studies on fish
129 stranding potential [*Casas-Mulet et al.*, 2015c]. Additional studies were carried out in site 2 (Figure
130 1), with a focus on egg and alevin development and survival [*Casas-Mulet et al.*, 2014b; 2016].

131 *2.2. Field data collection*

132 Water levels, discharges and water temperatures were collected at the four selected sites. Two
133 piezometers containing water pressure and temperature loggers (Diver ®) were installed at each of the
134 sites (Figure 1) to monitor surface and interstitial water. One piezometer was located permanently
135 under water (W) and the other in the ramping zone (RZ). RZ are locations subject surface dewatering
136 as a consequence of fluctuating flows (Figure 2). One VEMCO water temperature logger was also
137 installed in the water column at each site. Additionally, one air pressure (for water pressure
138 compensation) and temperature logger (Baro Diver ®) was installed at Site 2. Data was collected from
139 March 2012 to June 2013 at 10 min-resolution.

140

141 **3. Modelling tool-set**

142 The following sub-sections describe the set of modelling tools we used to address each of the specific
143 objectives stated above (Figure 3). They include long-term comparisons between (i) unregulated and
144 hydropeaking scenarios to assess how hydrological and thermal alterations impact salmonid early life
145 stages development and survival; and (ii) current and alternative hydropeaking scenarios to assess the
146 feasibility of implementing release/related mitigation options.

147 *3.1. Long-term discharge and water temperature modelling*

148 In order to enable long-term comparison between hydropeaking and unregulated scenarios, the
149 following modelling strategy was devised for the period 2002-2015¹:

150 (i) Daily unregulated discharge

¹ The first available regulated discharge data in Lundesokna was 2002.

151 No records of unregulated flows and/or water temperature exist for the Lundesokna River. Therefore,
152 we used hourly Gaula discharge data to compute unregulated discharge in Lundesokna using a
153 quantile regression method described by *Hailegeorgis and Alfredsen* [2016]. We used discharge data
154 from Eggafoss gauge, in the Gaula river (Figure 1), obtained from the Norwegian Water Resources
155 Directorate (NVE). A flow duration curve was generated for Lundesokna by a separate linear
156 regression model for every 1% using catchment area as the variable, and a total of 26 measured
157 catchments in the region as basis for the transfer. The unregulated time series were then created from
158 the flow duration curve assuming that streamflow at time t has the same percentile for the gauged and
159 ungauged catchment. Daily unregulated discharge were subsequently computed. For details on model
160 fits and catchments used in the transfer, see *Hailegeorgis and Alfredsen* [2016].

161 (ii) Daily unregulated water temperature

162 We used air2stream [*Toffolon and Piccolroaz, 2015*] to estimate unregulated daily water temperature
163 in the Lundesokna River. Air2stream makes simplifications to the basic lumped energy balance model
164 resulting in a model only dependent on air temperature and discharge to simulate the changes in water
165 temperature. The model was therefore well suited for Lundesokna where observed water temperature,
166 local radiation data and river geometry upstream of the power plant outlet were missing. We
167 calibrated air2stream using 2010-12 discharge and water temperature data from the river Gaula
168 (Egafoss gauge, NVE) and air temperature from the Voll station near Trondheim (obtained from the
169 Norwegian Meteorological Institute). The calibrated air2stream model (Nash-Sutcliffe Efficiency,
170 NSE of 0.95) was then used to compute water temperature in Lundesokna based on air temperature
171 data from Voll and modelled unregulated discharge from Lundesokna.

172 (iii) Hourly hydropeaking water discharge

173 Regulated discharges in Lundesokna downstream Sokna power plant were computed by adding the
174 $0.3 \text{ m}^3 \cdot \text{s}^{-1}$ constant bypass release to Sokna production and spill data, available in hourly resolution
175 from NVE.

176 (iv) Hourly hydropeaking water temperature

177 Regulated water temperature downstream Sokna power plant was calculated by applying a simple
178 energy balance model [*Zolezzi et al., 2011*] at an hourly time-step, with the temperature after mixing
179 resulting in:

180
$$T_d = \frac{T_u Q_u + T_r Q_r}{Q_d} \quad (1)$$

181 where Q is the flow and T is the water temperature for (u) unregulated upstream reach, (r) release
182 from Sokna reservoir and (d) downstream reach. We applied modelled unregulated daily data at an
183 hourly step for Q_u and T_u calculations, and used hourly hydropeaking water discharge calculations for
184 Q_r . Based on the observed data in 2012-13, we established the following rules and relationships for T_d
185 and T_r estimations:

- 186 - If production $\leq 1 \text{ m}^3 \cdot \text{s}^{-1}$, $T_d = T_u$.
- 187 - When production was $> 1 \text{ m}^3 \cdot \text{s}^{-1}$,
 - 188 ○ $T_r \sim 0.81$, during 01.12 -28.02,
 - 189 ○ $T_r = 0.7 \times T_u + 0.5$ ($R^2=0.7$) from 1 March to 31 July,
 - 190 ○ $T_r = 0.9 \times T_u - 0.6$ ($R^2=0.7$) between 1 August and 30 November.

191 (v) Estimation of interstitial water temperature in the redds

192 We used hourly 2012-13 field data to estimate the relationship between surface and interstitial
193 temperature in the redds though linear regressions at each site (1-4) and locations (RZ and W). We
194 then applied these relationships to model 2002-15 daily surface water temperature data for both
195 unregulated and hydropeaking scenarios. For unregulated scenarios, we used W data only to be
196 applied at both locations (RZ and W), as we assumed exposure to dewatering at RZ locations was
197 minimal.

198 3.2. Estimation of critical conditions for egg and alevin stages

199 3.2.1. Development rates estimation

200 We use Crisp model [Crisp, 1988] to estimate egg and alevin development rates and the timing of
201 hatching and initial feeding or swim-up. The following formula was used to determine the time
202 intervals:

$$203 \log D = b \log(T - \alpha) + \log a \quad (2)$$

204 where D is the number of days from spawning until 50% of the eggs have developed to the next stage,
205 T is the water temperature in the redds, and b , a and α are constants established at -2.6, 5.2 and -11,
206 respectively, for salmonids [Forseth and Harby, 2014]. By using the daily average temperature in the
207 redds (interstitial water) from the peak time of spawning (1 November), daily egg development can be
208 estimated as a percentage (100/D). The cumulative sum of the development can then be used to
209 estimate the timing of hatching and swim-up; when the sum of development reaches 100% and 170%,
210 respectively. Despite no data on natural spawning timing was available for the Lundesokna River, we
211 considered spawning period to start 1 October with a peak on 1 November. Such consideration was

212 based on observations made in other parts of the Gaula catchment, and information provided from the
213 local hatchery in Lundesokna.

214 We used hourly interstitial water temperatures at locations RZ and W to compute daily average data
215 for input to the Crisp model. We then estimated egg and alevin development rates for long-term
216 unregulated vs. hydropeaking scenarios. Observations of early life stage development were made in
217 the Lundesokna River for the period 2011-12 [Casas-Mulet *et al.*, 2014b] and they were used as an
218 approximate comparison to the modelled estimations.

219 3.3. Establishment of critical conditions

220 Based on previous observations in the river Lundesokna [Casas-Mulet *et al.*, 2014b, 2016] and
221 survival thresholds from the literature, we defined a set of critical conditions that could potentially
222 lead to salmonid early life stages mortality. We used RZ locations in site 2 as a reference and
223 established the following:

224 (i) Critical conditions for eggs (pre-hatch stage) occur when discharge $\leq 0.65 \text{ m}^3 \cdot \text{s}^{-1}$ and air
225 temperatures are below $0 \text{ }^\circ\text{C}$ for periods of ≥ 3 hours.

226 Casas-Mulet *et al.* [2014b] observed total dewatering of the redds at RZ locations when discharges
227 were $\leq 0.65 \text{ m}^3 \cdot \text{s}^{-1}$ (Figure 4). Despite surface dewatering, the eggs were able to survive for long
228 periods of time given moist conditions in the gravel. Mortality risk started after 3 hours of
229 exposure to air temperatures below $0 \text{ }^\circ\text{C}$.

230 (ii) Critical conditions for alevins (hatch-to-swim-up stage) mortality occur when discharge ≤ 3.5
231 $\text{m}^3 \cdot \text{s}^{-1}$ for periods of ≥ 3 hours.

232 Alevins require surface water covering the redds for survival [Casas-Mulet *et al.*, 2016]. Potential
233 spawning areas at site 2 were totally covered in water during discharges $\sim 3.5 \text{ m}^3 \cdot \text{s}^{-1}$ [Casas-Mulet
234 *et al.*, 2014c; 2015b] (Figure 4). Alevins may tolerate dewatering within the first 1 hour of
235 dewatering exposure, but significant decreased survival within 3 hours [Becker and Neitzel, 1985;
236 Becker *et al.*, 1982; Becker *et al.*, 1983; Neitzel and Becker, 1985]. Therefore, we considered
237 mortality risk for alevins occur after 3 hours of dewatering.

238

239 Estimated hatching and swim-up dates were combined with long-term hourly hydrological and air
240 temperature data to determine whether eggs or alevins were in the redds and to identify critical
241 conditions. We did the computations for both unregulated vs. hydropeaking scenarios.

242

243

244 *3.4. Assessment of mitigation strategies implementation in the Lundesokna River*

245 Table 1 provides a representative selection of flow-related mitigation options to minimise salmonid
246 early life stages mortality in rivers subject to dewatering. *Stober and Tyler* [1982] suggested to reduce
247 the differences between spawning and incubation flows to provide eggs and embryos with greater
248 protection from dewatering in a river subject to frequent flow changes. A reduction in the area of river
249 channel subjected to dewatering was also suggested by *McMullin and Graham* [1981] and *Connor*
250 *and Pflug* [2004]. Altering the timing and magnitude of discharge fluctuations can minimize the
251 adverse effects of operating hydroelectric dams on the productivity of downstream fall salmonid
252 populations [*Fisk II et al.*, 2013; *Harnish et al.*, 2014; *McMichael et al.*, 2005].

253 In summary, a minimum flow release during critical conditions for egg and alevin stages is the
254 dominant suggested mitigation measure (Table 1). In addition, a flow reduction during the spawning
255 period is also suggested to constraint the spawning area that later can be watered securely when
256 minimum flow is released during egg and alevin development. Information gained from Table 1
257 provided the basis to select potential release-related mitigation options in the Lundesokna River.
258 Current limitation in the hydropower system also had to be considered. They include an absolute
259 minimum production discharge of $8 \text{ m}^3 \cdot \text{s}^{-1}$ for environmental flow release, as no automatic bypass
260 system is implemented Sokna power plant. *Casas-Mulet et al.* [2014c] suggested a release of $8 \text{ m}^3 \cdot \text{s}^{-1}$
261 for 1 hour every 3 hours to be the most cost-effective for egg survival studies. Based on the above, the
262 following three release-related mitigation options were established:

263 **Option A:** Minimum production discharge to be released during periods with critical conditions
264 for egg and alevins from 1 November. This option would cover most redds in water
265 but could not ensure the total protection of redds created by early spawners (before 1
266 November), neither the redds spawned during high discharges ($> 8 \text{ m}^3 \cdot \text{s}^{-1}$). We
267 consider this option would reduce the risk of mortality moderately.

268 **Option B:** Minimum production discharge to be released during periods with critical conditions
269 for egg and alevins from 1 November. In addition, a reduction in flows (maximum
270 release of $8 \text{ m}^3 \cdot \text{s}^{-1}$) between 15 and 30 October to be applied. This option would
271 ensure full protection for mid/late spawners but could not ensure total protection of
272 redds by early spawners (before 15 October). We consider this option would
273 considerably reduce the risk of mortality.

274 **Option C:** Minimum production discharge to be released during periods with critical conditions
275 for egg and alevins from 1 November. In addition, a reduction in flows (maximum 8
276 m³.s⁻¹) between 1 and 30 October to be applied. This option would ensure full
277 protection for all spawners. We consider this option would significantly reduce the
278 risk of mortality.

279 We modelled the implementation of each of the mitigation options using long-term hourly
280 hydropeaking discharge data. We forced the hydropower system to release the required flow (Option
281 A) and/or to stop/reduce the production (Options B/C) during all identified critical conditions for eggs
282 and alevins, depending on the flow requirements for each stage.

283

284 *3.5. Feasibility and cost-effectiveness assessment*

285 We assessed the feasibility in terms of water usage for each of the release-related mitigation
286 options (A, B and C) by:

287 (i) comparing the availability of water in the hydropower system for minimum flow
288 releases during critical conditions.

289 We obtained the volume of water available in the system (including the three reservoirs, Figure 1) on
290 1 November and 1 April through nMAG hydropower simulation program [Killingtveit and Sælthun,
291 1995]. The available volume was then compared to the volume of water needed to implement the
292 necessary minimum release for eggs and alevin. We assessed water availability for the
293 implementation of each option for the period 2002-15.

294 (ii) comparing the available storage in the reservoirs vs. volume of water needed to hold
295 for flow reduction during spawning (for options B and C only).

296 Data on available storage in the reservoirs was obtained from subtracting nMAG modelled reservoir
297 volumes on 1 October to the total system capacity (145 Mm³). The total water produced in October
298 each year was then compared to such storage capacity to assess if the system was able to store the
299 water needed for flow reduction during spawning.

300 The nMAG program was validated with actual reservoir data obtained from NVE and Trønderenergi
301 (hydropower company operating in Lundesokna), available for the period 2004-15.

302 (iii) calculating additional production flow needed for release during critical conditions.

303 The percentage of additional discharge needed for release was compared to the actual water used for
304 production for each year. This comparison was used to estimate the relative impact of each mitigation
305 options to long-term water usage. For options B and C, the water saved in October was discounted
306 from the water usage to release during critical conditions (half of it during pre-hatch and half during
307 hatch-to-swim-up).

308 In order to assess the economic feasibility of each option, we used long-term hourly production
309 (MWh) data obtained from NVE, and hourly energy market price (euro/MWh) from Nord Pool². We
310 estimated annual costs and revenue, including:

- 311 (i) opportunity gains from Sokna power plant additional production during critical
312 periods, assuming it was sold to actual market price;
- 313 (ii) opportunity gains from selling the water saved in October later on at an average
314 annual market price. The price estimation excluded the period for which the water
315 was saved, being 37.44 euro.MWh⁻¹ for option B and 40.68 euro.MWh⁻¹ for option C;
- 316 (iii) opportunity costs attached to Sokna power plant production during critical periods
317 instead of during higher market prices assuming to be the average of all annual prices
318 (43.56 euro.MWh⁻¹);
- 319 (iv) potential costs related to additional starts and stops of the turbines (each estimated on
320 200 euro [*Casas-Mulet et al.*, 2014c]) during critical periods.

321 A final balance was calculated to assess the relative cost-effectiveness of implementing each of the
322 options. This was then compared to the current annual revenue from Sokna power plant production.

323

324 **4. Results**

325 *4.1. Discharge and water temperature modelling*

326 Long-term discharge, surface and interstitial water temperatures were successfully modelled for
327 unregulated vs. hydropeaking scenarios. Figure 5 illustrate the outcomes for the period 2012-13, for
328 which observed hydropeaking water temperature data only was available for comparison (resulting in
329 0.8 R² via linear regression). Air2stream model validation for the year 2012-13 resulted with a NSE
330 value of 0.88.

331 Whilst unregulated water temperature changes were minimal within a season, discharge and water
332 temperatures varied greatly in hydropeaking scenarios (Figure 5). W location temperatures were

² www.nordpoolspot.com

333 generally warmer than RZ locations and surface water during both winter and spring. Only in early
334 summer, RZ became similar or even warmer than W locations and surface water.

335

336 *4.2. Egg and alevins development rates*

337 Long-term hydrological and thermal modelling were used to estimate hatch and swim-up dates at
338 locations W and RZ for unregulated vs. hydropeaking scenarios (Table 2). Egg development rates
339 (hatching dates) at site 2 were non-significantly ($p=0.89$) different between hydropeaking vs.
340 unregulated scenarios. However, hatching was significantly ($p<0.001$) delayed (12 days, in average)
341 at RZ locations in hydropeaking scenarios when compared to unregulated scenarios. At all sites,
342 during hydropeaking conditions, hatching occurred significantly ($p<0.001$) earlier at locations W than
343 in locations RZ, with up to 16 days in difference (Figure 6).

344 Estimated swim-up occurred significantly earlier in unregulated compared to hydropeaking scenarios
345 at both locations RZ ($p<0.001$) and W ($p=0.012$). Average differences were 11 and 6 days,
346 respectively. In hydropeaking scenarios, swim-up occurred 6 days (on average) earlier in W positions
347 than in RZ locations (Figure 6).

348 Observations of hatching occurrences at W locations in site 2 were made on 14 April 2011 and alevins
349 with a fully depleted yolk sack were observed on 16 June. Modelling outcomes for the same year
350 estimated hatching and swim-up dates on 28 April and 13 June, respectively (Table 2).

351

352 *4.3. Critical periods for eggs and alevins*

353 Differences in development rates between hydropeaking and unregulated scenarios were greater at
354 sites 1 and 2 in the period 2012-13 (Figure 7). In hydropeaking scenarios, higher frequency of critical
355 conditions for both eggs ($\leq 0.65\text{m}^3\cdot\text{s}^{-1}$) and alevins ($\leq 3.5\text{m}^3\cdot\text{s}^{-1}$) occurred at site 2.

356 Table 3 illustrates that for the period 2002-15, critical conditions for early life stages occurred more
357 frequently in hydropeaking scenarios than in unregulated conditions at site 2. In hydropeaking
358 scenarios, critical conditions for eggs occurred every single year, with maximum durations of 8.5
359 days; and critical conditions for alevins occurred every year, except in 2011-12, with durations up to
360 7.9 days (Table 3). In unregulated scenarios, critical conditions at site 2 occurred only in two years
361 (2002-03 and 2010-11), affecting solely egg stages. They occurred in 10 and 7 occasions, but with
362 longer durations up to 14.5 days.

363

364 *4.4. Feasibility and cost-effectiveness of mitigation options*

365 Validation of the nMAG model showed 0.6% average differences between daily simulated and
366 observed total reservoir volumes for the period 2004-15.

367 The feasibility assessment in terms of annual water usage is summarised in Table 4 for options A, B
368 and C. Water usage and additional production were the highest in option A, as water was not hold
369 during spawning. For all options, more changes in water usage were required in the system to
370 minimise alevin mortality than to reduce egg mortality. Changes included increased numbers of
371 minimum releases released for option A or increased flow reductions for options B and C.

372 The implementation of options B and C were not feasible in some the years as no sufficient storage
373 capacity was available in the reservoirs on 1 October. The reservoirs were too full at that time to hold
374 the water needed for flow reduction during spawning. Insufficient available storage (>100%, Table 4)
375 occurred in periods 2002-05 and 2007-12 for option B. For option C, insufficient available storage
376 only occurred in years 2004-05 and 2007-08.

377 The economic feasibility assessment concluded that additional costs would be incurred if any of the
378 three options were implemented in the Lundesokna system (Table 5, Figure 8). However,
379 implementation costs would be low compared to the annual production revenue from the Sokna power
380 plant. They were 1.87% (option A), 0.69% (option B) and 0.7% (option C) (Figure 8). The estimated
381 costs of implementing option A resulted from lower opportunity revenue and higher opportunity and
382 extra start costs. The differences in costs between applying options B vs. C was minimal, with
383 negligible differences in extra starts costs and slight higher opportunity costs in option B.

384

385 **5. Discussion**

386 *Self-assessment of the modelling tool-set*

387 The modelling tool-set presented in this study was overall satisfactory to assess impacts and
388 mitigation options for embryo and alevin survival in hydropeaking rivers. This modelling tool-set can
389 be particularly useful in hydropower systems where little field data is available. Several site-specific
390 limitations and considerations for its transferability are described below, but overall, the set of
391 modelling tools can be used (individually or integrally) in other hydropower systems to support the
392 assessment of defined flow-related mitigation options.

393 Hydrological and thermal modelling. Hydrological and thermal modelling were satisfactory and
394 allowed comparison between hydropeaking vs. unregulated scenarios. *Hailegeorgis and Alfredsen*
395 [2016] showed that the quantile regression model provides good simulation of discharge data in the
396 test catchments in the same region as Lundesokna. The approach to model unregulated water
397 temperature gave satisfactorily results based on calibration and validation outcomes from Egafoss.
398 The transferability of the model to Lundesokna could not be validated as unregulated data
399 observations were not available (in general, pre-regulation hydrological and thermal data are rare in
400 most catchments in Norway). However, given the proved high performance of such modelling tools in
401 other contexts, we believe these are highly reliable for the purpose of this study.

402 Interstitial water temperature modelling. Modelled interstitial water temperatures provided a reliable
403 prediction of the overall trends, but did not reflect variations in relation to surface water temperatures
404 accurately. We recognise accurate surface vs. interstitial water temperature modelling is required to
405 further advance our understanding in such important processes in the redds, particular for fine time-
406 scale studies. However, for the purpose of this study and provided we used daily averaged data for
407 input to the Crisp model, we considered this approach to be sufficient.

408 Early life stages development estimation and validation. Crisp's model application assumed all
409 spawning occurred 1 November. Although 1 November is considered the peak date for spawning, we
410 acknowledge this is a limitation not only because it assumes all spawning occurred in one day, but
411 also because any potential effects of hydropeaking on spawning timing were not considered [*Vollset*
412 *et al.*, 2016]. These investigations were outside the scope of this paper but should be taken into
413 account in future research. Although modelled vs. observed data in 2011 was a positive validation, we
414 prefer to not use these dates as strict reference for two reasons: (i) hatchery eggs were used for the
415 experiments, potentially promoting earlier dates given the unnatural exposure to warm water in pre-
416 eyed stages, and (ii) high hydrological and thermal variability due to hydropeaking occurs between
417 years, with consequences to development.

418 Establishment of critical conditions for early life stages. Thresholds used to establish critical
419 conditions for eggs and alevins were site-specific of the River Lundesokna and may not be directly
420 translated into other river systems. Moreover, the predominance of oxygenated groundwater in
421 Norway allowed for a very low flow threshold for eggs to survive (assuming groundwater influx
422 would encourage egg survival). This assumption may not be feasible in other parts of the world as the
423 effect of groundwater influx may promote embryo mortality [*Malcolm et al.*, 2009; *Soulsby et al.*,
424 2005].

425 Hydropower production simulations. Simulated reservoir volumes and available storage through
426 nMAG were satisfactory to assess water usage feasibility. Similar modelling outcomes were achieved

427 in Casas-Mulet *et al.* [2014c]. Particularly in systems where hydropower regulation data is not
428 available, the use of hydropower simulation models such as nMAG is highly valuable to evaluate
429 release-related options with variable system constraints. Hydropower simulators can also be helpful
430 during decision-making to estimate the feasibility of mitigation options before implementation.

431 Economic feasibility assessment. We recognise limitations in estimating cost and revenues to assess
432 cost-effectiveness of mitigation options. Changes would undoubtedly occur in the overall annual
433 production if any of the options were to be implemented. Therefore, such calculations should be used
434 as a relative measure only to enable comparison between options.

435

436 *Thermal regime alteration and consequences for salmonid early life stages development*

437 Changes in surface water temperatures due to hydropeaking are termed as thermopeaking [Zolezzi *et*
438 *al.*, 2011], with the highest alterations during extreme dewatering events [Casas-Mulet *et al.*, 2015b].
439 All our findings coincide in the seasonal patterns of reduced water temperature during dewatering
440 events in winter and an increase in spring follows the expected seasonal pattern [Casas-Mulet *et al.*,
441 2015b; Vanzo, 2015; Zolezzi *et al.*, 2011].

442 Both the hydrological and thermal regimes in the Lundesokna are altered by hydropeaking production
443 with resulting delays on salmon hatching and swim-up. Altered surface water temperature from
444 hydropeaking translate into changes on interstitial water temperatures [Casas-Mulet *et al.*, 2015b]. As
445 a consequence, these changes may impact embryo development. However, the greatest differences
446 were found in the ramping zone. Regular dewatering at RZ locations led to interstitial water being
447 exposed to cold air temperature in winter, delaying development in the reds. Conversely, Fisk II *et al.*
448 [2013] had observed dewatering events were likely to accelerate the development likely from
449 exposure to warmer ambient temperature in non-salmonid species.

450 *Combined impacts of thermal and hydrological alterations on salmonid early life stages survival*

451 Hydropeaking scenarios illustrated several critical periods for both eggs and alevins survival in almost
452 all years. Unregulated scenarios resulted in few but long-lasting critical conditions due to natural flow
453 fluctuations. However, they only occurred in two years and solely affected egg stages. These events
454 would not occur often, but their extended durations would most likely impact the salmonid population
455 for that year. Flows during the hatch to swim-up period are most critical for population success
456 [Harnish *et al.*, 2014]. Moreover, no critical low flows occurred between hatch to swim-up in

457 unregulated scenarios, suggesting such period should be a key focus in future environmental flows
458 management in salmonid rivers.

459 In hydropeaking scenarios, the consistent delay in hatching may provide some opportunities for
460 overall survival in some years if salmonids remain longer in egg stages, given their less-demanding
461 water needs. This assumption, however, needs to be investigated further on a specific year basis.

462 *Cost-effectiveness of mitigation approaches*

463 Minimum flow releases during critical conditions are a common mitigation recommendation to
464 minimise early life stages mortality. Although it may not avoid mortality in redds laid during the
465 highest flows, it would ensure high probability of survival in targeted areas. Additional flow reduction
466 during spawning (options B and C) would ensure higher survival rates as it would target the
467 avoidance of spawning in high potential mortality areas. Assuming that optimal spawning areas are
468 distributed equally in the riverbed (see *Casas-Mulet et al., 2014a*), this additional measure would be
469 the most effective to minimise mortality. The sooner and longer flow reduction is implemented during
470 spawning, the higher the probability that no fish would spawn in high mortality risk areas. In this
471 regard, option A was the least effective to minimise mortality risk and the most expensive. However,
472 options B and C could not always be applied due to the limited storage capacity in the reservoirs.
473 Therefore, option A was the only feasible measure many of the years.

474 Understanding the feasibility in terms of water usage in hydropower systems is therefore key. Reliable
475 information on storage and water availability in a hydropower system is needed, so realistic
476 environmental releases can be achieved. In addition, allowing flexible operations may results in win-
477 win situations for the overall system economics and environmental benefits, rather to stick to strict
478 legislative rules.

479 **6. Conclusions**

480 In this study, we successfully applied a set of modelling tools to assess impacts and mitigation options
481 to reduce early life stages mortality risk in hydropeaking rivers. We modelled long-term hydrological
482 and thermal alterations to estimate development rates; we estimated the risk of early life stages
483 mortality and assessed the cost-effectiveness and feasibility of implementing three release-related
484 mitigation options.

485 The natural hydrological and thermal regimes are affected by hydropeaking, with consequences to
486 salmon early life stages development and survival. Redd dewatering due to hydropeaking increases
487 the mortality risk for early life stages with higher impacts to alevins given their lower tolerance to

488 exposure. The implementation release-related mitigation options during identified critical conditions
489 for egg and alevins can potentially reduce the risk of mortality. The costs of the three assessed
490 mitigation options was relatively low compared to annual production revenue (A: 1.87%, B: 0.69%
491 and C: 0.7%). Options B and C were the most effective in minimising the mortality risk. However,
492 lack of available storage in the reservoirs some of the years limited their application. Therefore,
493 Option A was the only option that could be feasibly implemented every year for the period 2002-15.

494 Targeted options built on well-informed modelling approaches can provide opportunities to mitigate
495 effects of dewatering with optimal use of water in the hydropower system. They can be tested on
496 efficiency, feasibility and costs through different hydropower production scenarios before
497 implementation. Environmental flow releases targeting specific ecological objectives can provide
498 better cost-effective options than conventional operational rules complying with general legislation.
499 The outcomes of this research are particularly relevant for the future management of hydropeaking
500 rivers.

501

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506 discharge model for Lundesokna.

507

508

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622

623 **Figures captions**

624 Figure1. River Lundesokna and study sites locations.

625 Figure 2. Typical transect at each of the study sites and maximum and minimum discharge during
626 regulated conditions in 2012-2013.

627 Figure 3. Diagram of the modelling tool-set used for the assessment of three release-related mitigation
628 measures to minimise mortality in salmonid early life stages in the hydropeaking river Lundesokna
629 (Norway).

630 Figure 4. Schematic of a representative transect in Site 2, illustrating the areas with high ($>8\text{m}^3\cdot\text{s}^{-1}$),
631 reduced ($0.65\text{-}8\text{m}^3\cdot\text{s}^{-1}$) and very low risk ($0.3\text{m}^3\cdot\text{s}^{-1}$) of mortality for early life stages. according to the
632 discharge in the river at the time of spawning and whether or not mitigation measures are
633 implemented. The thresholds of critical conditions for alevin and egg survival are also illustrated.

634 Figure 5. Discharge and surface water temperature for unregulated (top central) and hydropeaking
635 (bottom central) scenarios for the period 2012-13 in the Lundesokna River. Panels above and below
636 central graphs include surface and interstitial temperatures in the permanently wet (W, dark grey
637 dashed lines) and the ramping zone (RZ, light grey dashed lines) locations during three days in winter
638 (a, unregulated; c, hydropeaking) and late spring (b, unregulated; d, hydropeaking). Note that all data
639 is modelled except for observed discharge data for the hydropeaking scenario.

640 Figure 6. Average of all sites (1-4) hatching and swim-up dates at RZ (left) and W (right) redd
641 locations during unregulated (top) and hydropeaking (bottom) scenarios for all studied year. Note
642 vertical black lines are overall period average.

643 Figure 7. Illustration of egg development model (Crisp, 1985) for location RZ during unregulated
644 (solid line) vs. hydropeaking (dotted line) for all sites in 2012-13. Periods with partial or total
645 dewatering conditions are depicted in light and dark grey, respectively. Such periods are illustrated
646 only for hydropeaking scenarios.

647 Figure 8. Economic assessment for each of the measures from all years' average including the
648 economic balance of the measure (top number in bold, all costs) from the calculation of opportunity
649 revenue and costs, and the proportion of the cost in comparison to the actual production revenue
650 (bottom number in bold and italics, in percentage).

651

652 **Tables captions**

653 Table 1. Key literature references on mitigation measures for fish gravel stages in regulated rivers.

654 Table 2. Hatching and Swim-up dates at each of the locations (W and RZ) for each site (1-4) during
655 unregulated vs. hydropeaking scenarios.

656 Table 3. Average of numbers and durations of critical periods per year occurring in Site 2, and overall
657 period average during unregulated vs. hydropeaking conditions.

658 Table 4. Annual and all years' average of feasibility in terms of water usage for each of the
659 implemented measures (A, B, C).

660 Table 5. Annual economic feasibility assessment, and average of all years, for the implementation of
661 each measure (A, B, C).

662

663