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# Numerical Simulations of Flow Around a Bluff Body, Using Multigrid and an Immersed Boundary Method 

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# MASTER THESIS IN MARINE TECHNOLOGY 

## SPRING 20017

## FOR

## STUD. TECHN.

## Numerical simulations of flow around a bluff body, using multigrid and a immersed boundary method.

In the thesis the candidate shall present his personal contribution to the resolution of problem within the scope of the thesis work.

A simplified CFD solver should be developed, based on the SOLA code. The candidate shall familiarize herself with theory and numerical approximations in the code.

The candidate shall pay special attention to calculation efficiency. It will be important that the code runs fast for simulations of large models with many grid points. Different alternatives for speeding up the code should be considered.

If time permits, the candidate should also implement an immersed boundary method. This method should be used for making the code calculate flow around complex geometries. Special care should be given to how the force on the body is implemented.

As a test case for the code, the student shall calculate flow around a circular cylinder.
Theories and conclusions should be based on mathematical derivations and/or logic reasoning identifying the various steps in the deduction.

The candidate should utilize the existing possibilities for obtaining relevant literature.
The thesis should be organized in a rational manner to give a clear exposition of results, assessments, and conclusions. The text should be brief and to the point, with a clear language. Telegraphic language should be avoided.

The thesis shall contain the following elements: A text defining the scope, preface, list of contents, summary, main body of thesis, conclusions with recommendations for further work, list of symbols and acronyms, reference and (optional) appendices. All figures, tables and equations shall be numerated.

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## Preface

This is a master thesis on CFD, which is my last contribution to my master degree at Norwegian University of Science and Technology (NTNU) as a part of the study program engineering and ICT. The work was carried out during the spring 2017 and is an extension of my project thesis "Navier Stokes Solver".

I would first like to thank my supervisor Håvard Holm for the time, valuable input and support during this semester. Furthremore I would like to thank Jon Coll Mossige for sharing his knowledge and work on the immersed boundary method.

Finally I would like to thank my family and friends for being helpful and supportive during all my five years at NTNU.

## Summary

Increase in computational efficiency is one of the most prominent factors for successful applications of large CFD models with many grid points. Consequences of the increase are reduction in CPU-time and memory usage, so better mesh refinement could be used. Hence, the CFD-solver will improve the resolution in the computational domain.

This report provides an introduction to the background theory in CFD with basis on methods used to develop a simple incompressible Navier Stokes solver. Different multigrid algorithms and an immersed boundary method are discussed, where the solver exploit the cause of increased computational efficiency, especially by using multigrid. Validation is done based on efficiency and accuracy for the multigrid algorithms compared to Gauss Seidel method and SOR method. Force calculations around a submerged bluff cylinder in a 2D flow are used to validate the immersed boundary method implemented in the solver together with a full multigrid algorithm.

By implementing a full multigrid method, the time used to solve the Poisson equation was reduced significantly and the accuracy of the resolution is kept. The validation tests of a solver combining an immersed boundary method and the full multigrid algorithm was successfully carried out except for too low coefficients at $\mathrm{Re}=100$ in the final test case. The accuracy of flow resolution was specially affected by the time refinement and the width of the computational domain.

## Sammendrag

Økning i beregnings effektivitet er en av hoved faktorene for å oppnå suksessfulle CFD applikasjoner for store modeller med mange grid-punkter. Konsekvensene av økningen er reduksjon i CPU-tid og minne bruk, så finere grid kan bli brukt og CFD-løseren kan dermed oppnå enda bedre numeriske resultater i domenet.

Denne rapporten gir en introduksjon til bakgrunnsteori til CFD basert på de metoder som blir brukt til å utvikle en enkel inkompressibel Navier Stokes løser. Forskjellige multigrid algoritmer og en immersed boundary methode er diskutert, hvor løseren utnytter den resulterende økningen av beregnings effektivitet, særlig på vegne av multigird metoden. Valideringen er basert på effektivitet og nøyaktighet for multigrid algoritmene sammenlignet med Gauss Seidel metoden og SOR metoden. Krefter rundt en nedsenket fast sylinder i en 2D strøm er beregnet og brukt til å validere immersed boundary metoden som er implementert i løseren sammen med en full multigrid metode.

Ved å implementere en full multigrid metode, er tiden brukt på å løse Poissons likning redusert betraktelig samtidig som nøyaktigheten i resultatet er beholdt. Gjennomføringen av validerings testene for en løser som kombinerer en immersed boundary methode og en full multigrid methode var vellykket, bortsett fra for lave koeffisienter i siste test ved $\mathrm{Re}=100$. Nøyaktigheten i strømningsfeltet var særlig påvirket av valget av tids-steg og bredden på domenet som ble brukt til simuleringene.

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## Chapter 1

## Introduction

### 1.1 Background

To get essential engineering data for complex problems, Computational Fluid Dynamics (CFD) is a useful tool to provide data in an inexpensive way. By numerical simulations, a CFD-solver studies the physical laws under viscous conditions by solving the governing equations numerically. At a current state, it has been developed numbers of CFD-solvers. Some are commercial, e.g. Fluent, and other are open source, e.g. OpenFoam. The solvers are build up by using different approaches based on old methods. The development of the solvers are not yet at a level where the user can work with the tool uncritically, so knowledge of numerics involved are essential.

CFD is a powerful tool and can be used to visualize complex problems outside our range of vision, like Peskin (1972) used CFD with an Immersed Boundary Method (IBM) to simulate blood-flow trough a human heart valve, figure 1.1. Different areas of the solution domain can be observed without disturbing the flow field around. Perhaps the simulations simulate a flow around an complex rigid boundaries like Lai and Peskin (2000) presented in their studies. The
results may supplement experimental tests as a qualitative tool to decide e.g. design before the tests are preformed.

Because of computational limitations, CFD applications are not at a level where it can be used for real time computations. Increase in computational power and efficiency is one of the most prominent factors. When focusing on efficiency in a Navier Stokes solver, the Poisson solver should be evaluated. The process solving the Poisson equation usually takes the vast majority of the runtime. To affect the overall performance, an efficient method should be used on the Poisson solver. At a current state, one of the most efficient methods is still the multigrid method introduced by (Brandt, 1977).


Figure 1.1: Blodflow trough a human heart valve (Peskin, 1972).

### 1.2 Objectives

The main objective of this thesis is to develop a CFD-solver with special attention paid to calculation efficiency, so the code runs fast for simulations of large models with many grid points. As a test case, flow around a cylinder is tested with spacial attention on the forces. Therefore, a method for simulations of fluid structure interactions (FSI) is developed. The main objective is future divided into:

1. Modeling the Navier Stokes equation in a proper way based on old methods.
2. Develop multigrid methods to reach convergence faster than iterative schemes.
3. Implement immersed boundary method (IBM) for simulations of fluidstructure problem.

### 1.3 Approach

The basis of the Navier Stokes solver is formed by "SOLA - Solution Algorithm for 2D incompressible laminar transient flow", an excerpt from "A Navier Stokes Solver using the Multigrid Method" by Reidar Kristoffersen and based on Hirt et al. (1975). My project thesis "Navier Stokes Solver" (Aarsnes) consists of a preliminary layout and development of the solver, and this master thesis is an extension for that.

The following limitations are used in the solver:
1 Constant density, $\rho=$ constant

2 Constant viscosity, $v=$ constant

3 Newtonian fluid

4 Laminar flow

5 Cartesian coordinates, $\left(x_{i}\right)=(x, y)^{T}$ and $\left(u_{i}\right)=(u, v)^{T}$

Hence, the governing equations to be solved simplifies to a simple two-dimensional incompressible Navier Stokes system. The temporal-derivatives are discretized by a forward Euler scheme and the spatial-derivatives are discretized by a second order central differences scheme on an equidistant staggered grid. This is known as the FTCS-scheme (Forward-Time Central-Space). For the iterativescheme used to solve the Poisson equation, Gauss Seidel, successive over-relaxation (SOR) or different multigrid methods may be chosen. In a test case with flow around a cylinder, the FSI problem is solved by IBM.

### 1.4 Outline

Chapter 2 provides an overview of the fundamental theory in a CFD-solver. The simplified governing equations, discretization methods to solve the derivatives, different way of structuring the computational nodes in the domain and some numerical methods are presented. In Chapter 3, the efficient multigrid method is described in three different algorithms. Chapter 4 presents how to solve the FSI problem with IBM. The code layout and some comments to the development are given in Chapter 5. Validation of the code and a test case of flow around a cylinder is presenter in Chapter 6, and concluded in Chapter 7 together with some recommendations for future work.

## Chapter 2

## Fundamental Theory

In this chapter some fundamental theory used for developing a Navier-Stokes solver are introduced. This is an extension from my project thesis "Navier Stokes Solver" (Aarsnes), where the relevant parts from the project are included here.

### 2.1 Navier Stokes Equation

For many viscous flow problems, it is not possible to get an accurate solution using simple equations. The solutions of the Navier-Stokes equations can display very fine details of the flow structure, such as strong viscous-inviscid interactions with large separated flow regions. The unsteady compressible NavierStokes equations are a mixed set of hyperbolic-parabolic equations in time, and the incompressible Navier-Stokes equations are a mixed set of elliptic-parabolic equations. Thus, the inviscid and viscous equations require significantly different solution strategies.

### 2.1.1 Incompressible Navier Stokes equation

When heat transfer or significant property variations are not present, the incompressible Navier-Stokes equation is the best choice. The governing equations for the two-dimensional incompressible Navier-Stokes system with a constant property flow and without body forces or external heat can be written in conservative form:

$$
\begin{gather*}
\frac{\partial u}{\partial t}+u \frac{\partial u}{\partial x}+v \frac{\partial u}{\partial y}=-\frac{1}{\rho} \frac{\partial p}{\partial x}+v\left(\frac{\partial^{2} u}{\partial x^{2}}+\frac{\partial^{2} u}{\partial y^{2}}\right)  \tag{2.1}\\
\frac{\partial v}{\partial t}+u \frac{\partial v}{\partial x}+v \frac{\partial v}{\partial y}=-\frac{1}{\rho} \frac{\partial p}{\partial y}+v\left(\frac{\partial^{2} v}{\partial x^{2}}+\frac{\partial^{2} v}{\partial y^{2}}\right)  \tag{2.2}\\
\frac{\partial u}{\partial x}+\frac{\partial v}{\partial y}=0 \tag{2.3}
\end{gather*}
$$

Here, $u$ and $v$ represents the velocity components in $x$ - and $y$-direction, respectively, $p$ is the pressure, $\rho$ is the density and $v$ is the kinematic viscosity. Equation 2.1 is the $x$-momentum equation and 2.2 is the $y$-momentum equation, which are parabolic PDEs. Equation 2.3 is the continuity equation, which is an elliptic PDE. In the momentum equations there is a convective term, $\mathbf{u} \nabla \mathbf{u}$, and a diffusive term, $v \nabla^{2} \mathbf{u}$, hence the Navier-Stokes equation belongs to the class of convection-diffusion equations.

### 2.1.2 Dimensionless approach of variables

A dimensionless approach generalize the problem and reduces the number of parameters in the equation. This is possible because it is easier to see how to treat the parameters, i.e. possibilities for neglecting or approximating them. The purpose of making Navier Stokes equation dimensionless is to reduce the number of times the equation needs to be solved numerically.

Table 2.1: Non-dimensional parameters (Richard H. Pletcher, 2013).

| Name | Reference parameter | Non-dimensional parameter |
| :---: | :---: | :---: |
| Velocity | U | $\mathbf{u}^{*}=\frac{\mathbf{u}}{U}$ |
| Length | L | $\mathbf{r}^{*}=\frac{\mathrm{U}}{L}$ |
| Time | - | $t^{*}=\frac{t U}{L}$ |
| Pressure | - | $p^{*}=\frac{p}{\rho U^{2}}$ |
| Reynolds number | - | $R e=\frac{U L}{v}$ |

For the case of flow without heat transfer, the non-dimensional equations only depend on the Reynolds number, which is a ratio between the viscous and the advective term. This means that the non-dimensional parameters will have the same value at same Reynolds number. The non-dimensional primitivevariables for a Cartesian coordinate system are introduced in table 2.1.

By substituting the non-dimensional parameters from table 2.1 into the Navier Stokes equations 2.1, 2.2 and 2.3, the non-dimensional $x$-momentum equation $2.5, \mathrm{y}$-momentum equation 2.6 and continuity equation 2.4 are obtained.

$$
\begin{gather*}
\frac{\partial u^{*}}{\partial x^{*}}+\frac{\partial v^{*}}{\partial y^{*}}=0  \tag{2.4}\\
\frac{\partial u^{*}}{\partial t^{*}}+u^{*} \frac{\partial u^{*}}{\partial x^{*}}+v^{*} \frac{\partial u^{*}}{\partial y^{*}}=-\frac{\partial p^{*}}{\partial x^{*}}+\frac{1}{R e}\left(\frac{\partial^{2} u^{*}}{\partial x^{* 2}}+\frac{\partial^{2} u^{*}}{\partial y^{* 2}}\right)  \tag{2.5}\\
\frac{\partial v^{*}}{\partial t^{*}}+u^{*} \frac{\partial v^{*}}{\partial x^{*}}+v^{*} \frac{\partial v^{*}}{\partial y^{*}}=-\frac{\partial p^{*}}{\partial y^{*}}+\frac{1}{R e}\left(\frac{\partial^{2} v^{*}}{\partial x^{* 2}}+\frac{\partial^{2} v^{*}}{\partial y^{* 2}}\right) \tag{2.6}
\end{gather*}
$$

### 2.1.3 The projection method

For an incompressible fluid, the pressure and the velocity are independent of time.

The projection method, also called the method of fractional steps, is a procedure used to decouple the pressure and velocity and was first presented by Chorin (1968) on a regular grid. The pressure gradient terms are omitted from the momentum equation (2.1 and 2.2) in the frist step and advanced in time. By using the Helmholtz decomposition, resolved into a divergence-free term and a curl-free term, equation 2.7 is preformed.

$$
\begin{equation*}
\frac{\mathbf{u}^{k+1}-\mathbf{u}^{*}}{\Delta t}+\nabla p^{k+1}=0 \tag{2.7}
\end{equation*}
$$

Where $\frac{\mathbf{u}^{k+1}-\mathbf{u}^{*}}{\Delta t}$ has zero divergence and $\nabla p^{k+1}$ has zero curl. $\mathbf{u}^{*}$ denotes the predicted velocity, $\mathbf{u}^{k+1}$ is the velocity field at the new time-step and $p^{k+1}$ is the new pressure. Now, there are two unknowns, $\mathbf{u}^{k+1}$ and $p^{k+1}$, that must be solved to find the solution. The continuity equation 2.3 can be differentiated to yield, thus the pressure field needs to satisfy the incompressibility constraint 2.8.

$$
\begin{equation*}
\nabla \cdot \mathbf{u}^{k+1}=0 \tag{2.8}
\end{equation*}
$$

Hence, the Poisson equation 2.9 will be derived with a source term equal to the divergence of the predicted velocity field and the pressure difference as an potential function .

$$
\begin{equation*}
\nabla^{2} p^{k+1}=\frac{1}{\Delta t} \nabla \mathbf{u}^{*} \tag{2.9}
\end{equation*}
$$

Then follow this solution procedure:
1 Calculate the predicted velocity $\mathbf{u}^{*}$ from momentum equation while neglecting the pressure gradient terms.

2 Solve the Poisson equation 2.9 for the corrected pressure $p^{n+1}$.
3 Calculate the corrected velocity $\mathbf{u}^{n+1}$ from 2.7.
The projection method is possible to implement on both regular and staggered grids, where explicit and implicit methods are employed. Using an explicit-first-order Euler scheme for time-derivatives and staggered grid Peyret and Taylor demonstrated that the scheme is closely related to marker and cell (MAC) method by Harlow et al. (1965).

### 2.2 Grid

Grid, also called mesh, is a necessary tool when working with computational simulations. To approximate numerical solutions to a PDE, a discretization of the equation needs to be done to find a system of algebraic differential equations. Therefor the discretization is accomplished by placing discrete nodes over the solution field, where the discrete nodes can be connected in different ways to form discrete cells. The differential equations can be represented over discrete nodes or over discrete cells. This is just a short introduction to some types of grids, for future reading see Thompson et al. (1998).


Figure 2.1: Different kinds of grids, a modification from Djeddi et al. (2013).

When coupling grid and solution processes together several choices based on underlying principles and mathematics can be made to optimize the process. For the finite difference method (FDM), the derivatives of field variables are easily expressed, thus structured grids are usually used. For the finite element method (FEM) and the finite volume method (FVM), unstructured grids are more convenient because of the flexibility these methods offers.

### 2.2.1 Staggered grid

Staggered grid is a structured grid, i.e. with uniform cell size, where the field variables are represented at different locations (Harlow et al., 1965). The pressure is represented at the center of the cell and the velocities at the cell edges in each direction, see figure 2.2. Staggered grids are more accurate than nonstaggered (collocated) grids and can therefore use coarser grids, sometimes twice as coarse grid, to obtain the same accuracy (Mccormick, 1988). For pressure calculations, like the Poisson equation, staggered grids has an advantage because of a more direct coupling between velocity and pressure, thus avoiding unphysical pressure oscillations.


Figure 2.2: Staggered grid (Djeddi et al., 2013).

### 2.2.2 Adaptive grid

When using structured grid on a flow filed, unnecessary computational effort are done in some parts of the domain. Usually, a flow field is not uniform, hence different grid treatment should be used for different areas in the domain, see figure 2.3.


Figure 2.3: Adaptive grid around a cylinder (Vanella et al., 2014)

Adaptive grids follows gradients in the physical solution, hence the areas with higher gradients, f.ex high velocity and pressure gradients, are better represented with a refined grid due to the rest of the domain. High gradients usually occurs around boundary layers and flow fields past a body is a critical area where higher resolutions are need. Structured grid will in these cases need high resolution in the whole domain to handle the high gradients around the body, which is very inefficient.

### 2.3 Discretization

As mentioned on section 2.2, the discrete operators depends on the chosen grid, but also on a discretization method. A discretization method approximates the first and second derivatives in the Navier Stokes system, equations 2.5, 2.6 and 2.4. The momentum equations are re-ranged to make the discretization easier with the temporal derivatives on the left hand side and the spatial derivatives on the right hand side. see equation 2.10. $i$ and $j$ denotes x - and y - direction, respectively, for velocity and in space.

$$
\begin{equation*}
\frac{\partial u_{i}}{\partial t}=-\frac{\partial u_{i} u_{j}}{\partial x_{j}}-\frac{\partial p}{\partial x_{i}}+\frac{1}{R e} \frac{\partial^{2} u_{i}}{\partial x_{j}} \tag{2.10}
\end{equation*}
$$

### 2.3.1 Spatial

Spatial discretization methods are used to represent and evaluate PDE's. The most common ones are the FDM, the FVM and the FEM. This subsection will give a short introduction of each.


Figure 2.4: Primary behavior of FDM, FVM and FEM

## Finite Difference Method

The FDM is working on stencils, see figure 2.4. Thus, the method is approximating the node derivatives for a problem and leads to sparse matrices. It is limited for use on uniform-structured grid and is therefore simple to implement and derive.

There are different approaches of FDM, which differ in how the stencil is built up. One approach is the central FDM, see figure 2.5, a five point stencil scheme which approximates the derivatives with the closest neighboring nodes.


Figure 2.5: 5-point stencil for central FDM.

## Finite Element Method

The FEM is working on elements, see figure 2.4. Thus, the method uses basis functions over a finite region which leads to large, banded matrices. The advantages of the method are that it can be used on unstructured grids and that it is general. Irregular geometries require more computer storage, making FEM more time consuming in these situations.

## Finite Volume Method

The FVM is working with volumes, see figure 2.4. Thus, the method is approximating integrals to find the solution. Divergence terms are converted to surface integrals using the divergence theorem and evaluated as fluxes at the surface of the finite volumes. The advantages of the method are that it can be used on unstructured grids and that it is conservative.

### 2.3.2 Temporal

In time, it is useful to consider the discretization process in two stages (LeVeque, 1992):

1. Discretize the problem in space and leave it continuous in time. Then the PDE become a system of ordinary differential equations (ODE's), also called semi discrete equations. Then the right hand side can be solved as a boundary value problem.
2. Discretize in time using a numerical method that solves a system of ODE's.

Two different explicit numerical methods for solving the system of ODE's are described briefly.

## Forward Euler

Explicit Euler scheme is named after and first introduced by Euler (1768), see equation 2.11, is first-order accurate in time, $\mathscr{O}(\Delta t)$. Hence, small time-step $\Delta t$ is decreed because on the lack of stability and accuracy.

$$
\begin{equation*}
\frac{u^{n+1}-u^{n}}{\Delta t}=R\left(u^{n}\right) \tag{2.11}
\end{equation*}
$$

$R\left(u^{n}\right)$ is the right hand side of the equation, $n$ is the current time-step and $n+1$ is the new time-step.

## Runge-Kutta

Solving the system of ODE's by a first-order method may entail high computational costs. By choosing a higher-order method like Runge-Kutta (Kutta, 1901) is recommended if high accuracy is desired. Runge-Kutta schemes can have different orders of accuracy depending on the order of the applied Runge-Kutta. For a second-order Runge-Kutta method, see equation 2.12, the order of accuracy is two, $\mathscr{O}\left(\Delta t^{2}\right)$.

$$
\begin{equation*}
u^{(1)}=u^{n}+\Delta t R\left(u^{n}\right) \quad u^{n+1}=u^{n}+\frac{\Delta t}{2}\left(R\left(u^{n}\right)+R\left(u^{(1)}\right)\right) \tag{2.12}
\end{equation*}
$$

$R\left(u^{n}\right)$ is the right hand side of the forward Euler equation 2.11, $n$ is the current time-step and $n+1$ is the new time-step.

### 2.4 Boundary Conditions

A boundary value problem is a differential equation together with some constraints, boundary conditions (BC). The technique used for implementing BC's have great influence on the stability and convergence of the numerical solution. For flow field problems, just a limited domain of the problem will be evaluated. Therefore, BC's need to be specified in a finite distance from e.g. the geometry in the flow. The two main BC's are:

- Dirichlet boundary condition, or fixed boundary condition, specifies the value at the boundary, $f(x)$, and can be expressed in a general form as

$$
u(x)=f(x) \quad \forall_{x} \in \partial \Omega, \quad \Omega \subset \mathbb{R}^{n}
$$

- Neumann boundary conditions specifies what the value of derivatives over the boundary, $f(x)$, is and can be expressed in a general form as

$$
\frac{\partial u(x)}{\partial \mathbf{n}}=f(x) \quad \forall_{x} \in \partial \Omega, \quad \Omega \subset \mathbb{R}^{n}
$$

Thus, the boundary needs to be sufficiently smooth so a derivative in the same direction exist. Neumann boundary conditions are not well defined at corners.

Where $\mathbf{n}$ denotes the normal vector to the boundary $\partial \Omega$ of the domain $\Omega$ and $u$ is the velocity of the fluid.

According to way of representing the calculation values on a staggered grid, ghost-cells outside of the domain (i.e. exterior cells) are being used to specify BC's. For a geometry, the cell right inside of the geometry-wall can be seen as ghost-cells. BC's in a staggered grid are located at the boundary of a calculation
cell. Therefore a BC at a vertical cell-wall will pass through a horizontal-velocity node and a horizontal-wall will pass trough a vertical-velocity node. Some BC's for a 2D staggered grid are future discussed.

A rigid impermeable wall may be either no-slip or free-slip, considered as a plane of symmetry (Harlow et al., 1965). The velocity nodes on the wall will vanish at all times for either wall types. Suppose a impermeable wall along the $y$-axis, see figure 2.6, then the velocities will have the constraints:

- No-slip: $u^{\prime}=0$ and $v^{\prime}=-v$
- Free-slip: $u^{\prime}=0$ and $v^{\prime}=v$

Where $u^{\prime}$ and $v^{\prime}$ are velocities in the ghost-cells and $u$ and $v$ are the velocities in the fluid. Analogous boundary conditions are applied on a wall along the $x$-axis. In general, there should be no change in pressure over a boundary if there are no body-forces, hence $p^{\prime}=p . p^{\prime}$ is the pressure in the ghost-cell and $p$ is the pressure on the fluid side.


Figure 2.6: Boundary conditions on a vertical wall

Velocity and pressure needs to have at least one Dirichlet condition, i.e. be stated at least once in the domain, otherwise the numerical system could turn out unsolvable.


Figure 2.7: How to apply periodic boundary condition

To apply periodic boundary conditions (Patankar et al., 1977) an extra source term need to be attached to the momentum equation for the stream direction. Periodic conditions are pressure driven, so the source term will be equivalent to the pressure drop per unit periodic length. The boundary conditions for velocity and pressure at inlet cells are equal to the ghost-cells at outlet face and vice versa for the outlet cells:

- Inlet: $u_{\text {inlet }}=u_{\text {outlet }}^{\prime} \quad v_{\text {inlet }}=v_{\text {outlet }}^{\prime} \quad p_{\text {inlet }}=p_{\text {outlet }}^{\prime}$
- Outlet: $u_{\text {outlet }}=u_{\text {inlet }}^{\prime} \quad v_{\text {outlet }}=v_{\text {inlet }}^{\prime} \quad p_{\text {outlet }}=p_{\text {inlet }}^{\prime}$

A visualization is given in figure 2.7.

### 2.5 Methods to Solve Linear Systems

The Poisson equation 2.9 is a linear system of equations and can be written as $A \mathbf{u}=\mathbf{b} . A$ is the coefficient matrix, $\mathbf{u}$ is a vector of unknowns and $\mathbf{b}$ is the source term. To solve it, an iterative or a direct scheme is used.

Direct schemes, e.g. Gaussian elimination, is solving the systems of equations exactly. Direct schemes are efficient on systems with a limited number
of unknowns. However, when the number of unknowns increase the computational work increases considerably too and a iterative scheme should be considered.

Iterative methods is based on relaxing the solution at each node by starting with an initial guess and modifying it until a limit of convergence is reached. Each modifying is an iteration called relaxing sweep and the final solution would become an approximation of the exact solution. Gauss Seidel and SOR are two iterative schemes that may be used. Gauss Seidel is a simple method which requires only one storage vector, hence it is easy to implement. SOR method may be a refinement of the Gauss Seidel method but provides faster convergence by choosing a optimal damping coefficient $\omega_{\text {opt }}$. As Kahan (1958) presented $\omega$ $\epsilon(0,2)$ for SOR to converge, however $\omega_{\text {opt }}$ may be hard to find. For $\omega=1$, SOR is the same as Gauss Seidel method.

In chapter 3 a more complex method for solving the Poisson equation is introduced, the multigrid method. Equations for implementation of Gauss Seidel and SOR on a 2D central FDM scheme are prescribed in section 6.1 together with a limit for convergence.

### 2.6 Stability Analysis

Stability criteria are taken into account to ensure that there will be no numerical uncertainties in the simulation. By Lax's equivalence theorem provided by Richtmyer and Morton (1967) this is true if the scheme is consistent.

Lax's equivalence theorem: Given a properly posed initial value problem and a finite-difference approximation that satisfies the consistency condition, stability is the necessary and sufficient condition for convergence.

The Navier Stokes equation is a complex non-linear PDE, therefore it is hard to apply von Neumann's analysis. The normal procedure is to linearize the equation and investigate one term at a time. In subsection 2.1, the different terms are pointed out for the Navier -Stokes equation.


Figure 2.8: Stability, CFL-condition. Left figure: stable. Right figure: unstable.

From the convection term, the Courant-Friedrichs-Lewy condition (CFL-condition)
2.13 is derived, see figure 2.8. The non-dimensional number $C$ is called the Courant number, which represent how many cell-sizes $\Delta x_{i}$ a fluid particle passes trough a time-step $\Delta t$ with velocity $u_{x_{i}}$. The condition must be consistent in all dimensions and at the whole domain at each time-step.

$$
\begin{equation*}
C_{i}=\frac{u_{x_{i}} \Delta t}{\Delta x_{i}} \leq C_{\text {max }}, \quad i=1,2,3 \tag{2.13}
\end{equation*}
$$

$C_{\max }$ is changing with the discretization method. Deciding whether the timediscretization method are implicit or explicit has a great impact. For explicit methods $C_{\text {max }}$ is usually equals to one. Implicit methods are usually less sensitive for numerical instability, so $C_{\max }$ can be larger.

From the diffusion term, a stability criteria to ensure that the viscous diffusion of momentum is limited to one cell per time-step, see equation 2.14, is derived.

$$
\begin{equation*}
\Delta t \leq \frac{R e}{2}\left(\frac{\Delta x^{2} \cdot \Delta y^{2}}{\Delta x^{2}+\Delta y^{2}}\right) \tag{2.14}
\end{equation*}
$$

The last stability criteria ensures that the stability is sustained for the computation. The equation 2.15 provides positive diffusion by stabilizing the numerically unstable convection term. The condition must be consistent in all dimensions and on the whole domain at each time-step, since it build on the CFL-condition.

$$
\begin{equation*}
\Delta t \leq \operatorname{Min}\left(\frac{2}{\operatorname{Re}\left(u_{i, j}^{n}\right)^{2}}, \frac{2}{\operatorname{Re}\left(v_{i, j}^{n}\right)^{2}}\right) \tag{2.15}
\end{equation*}
$$

Equations 2.14 and 2.15 are here given for a 2D problem and based on $C_{\max }=1$, i.e. adjusted for explicit methods. For other $C_{\max }$ they will change accordingly.

## Stability of Explicit Euler

Linear stability of explicit Euler is found from $|1+h \lambda| \leq 1$, where $\lambda$ is the eigenvalue of the linear test equation. The stability domain is given in figure 2.9, where the axes are the real and imaginary of $h \lambda$. The explicit Euler method demands small time-steps if the solution is fast decaying or have highly oscillating modes.


Figure 2.9: The stability area for a explicit Euler scheme, the axis are scaled for $h \lambda$.

## Chapter 3

## Multigrid

The multigrid method for solving elliptic PDE introduced by Brandt (1977) accelerate the convergence of an iterative method, like Jacobi method or Gauss Seidel method, from $\mathscr{O}\left(n^{2}\right)$ to $\mathscr{O}(n)$, when the PDE is discretized on $n$ grid points. This is done by combining coarse and fine grids, where the error is transferred from fine to coarser grids. By analyzing the error or difference in the iterative scheme with Fourier analysis, it can be seen that the error components have different frequencies. Iterative methods like Jacobi and Gauss Seidel are efficient for reducing high frequencies, because the new solution value is dependent on the previous one. Therefore, in a multigrid algorithm the coarse grid is used to reduce the low frequency components (which becomes high frequency components on coarse grids) of the error and the fine grid improves the accuracy by reducing the high frequencies. Hence, the coarse grids are only used to obtain correction, never to seek solutions of the original problem.

In a multigrid method, several grids which are typically increased by a factor of 2 can be used. Set the chosen difference representation on the left side of the equation and the discretized iterative scheme on the right side, then equation 3.1 represents the linear system to be solved.

$$
\begin{equation*}
A^{h} \mathbf{u}^{h}=\mathbf{f}^{h} \tag{3.1}
\end{equation*}
$$

Where $h$ is the grid spacing on the corresponding equidistant grid. See subsection 2.5 for an introduction on methods to solve the linear system of equations. The method could be applied to the linear system directly or to the error equation, which is called the residual equation.

## The residual equation

Let $\mathbf{u}^{*(k)}$ be an approximation of $\mathbf{u}$ at iteration $k$, then the error $\mathbf{e}^{(k)}=\mathbf{u}-\mathbf{u}^{*(k)}$ satisfies the residual equation 3.2.

$$
\begin{equation*}
A \mathbf{e}^{(k)}=\mathbf{f}-A \mathbf{u}^{*(k)}=: \mathbf{r}^{(k)} \tag{3.2}
\end{equation*}
$$

In multigrid methods, the residual equation is used to update the current $\mathbf{u}^{(k)}$. An approximation of $\mathbf{e}^{(k)}, \mathbf{e}^{*(k)}$, is computed and used to find the new iteration $\mathbf{u}^{(k+1)}=\mathbf{u}^{(k)}+\mathbf{e}^{*(k)}$. Close to the solution the error $\mathbf{e}^{(k)}$ is small, therefore zero is a good initial guess for 3.2.

There are two ways of constructing multigrid methods, the standard geometric multigrid (GMG) and the algebraic multigrid (AMG). GMG, which is the multigrid design used in this chapter, have some limitations regarding hierarchy of grids. Sometimes the hierarchy dependency on the underlying geometry is hard to handle, then AMG can be used. In contrast to GMG, AMG do not exploit the underlying geometry and work directly on the linear system. For future reading on AMG, see Stüben (1983) and Xu and Zikatanov (2017).

### 3.1 Grid Transfer

When grids are transferred, they are either restricted, i.e. transfer error from fine to coarse grid, or prolongated (also called interpolation), i.e. transfer initial solution from coarse to fine grid.

When transposing from a fine to a coarser grid, the error (residual) is transfered from $\Omega^{h}$ to $\Omega^{2 h}$. By a discrete Fourier analysis of the modes on different grids (Wienands and Oosterlee, 2001) can prove that the k-th Fourier mode on $\Omega^{h}$ is the k-th Fourier mode on $\Omega^{2 h}$, see equation 3.3 (Strang, 2006). A transformation from the fine to the coarse grid provides the k -th mode with higher frequency when $1<\mathrm{k}<\frac{n}{2}$.

$$
\begin{gather*}
w_{k, 2 j}^{h}=\sin \left(\frac{2 j k \pi}{n}\right)=\sin \left(\frac{j k \pi}{\frac{n}{2}}\right)=w_{k, j}^{2 h}, \quad \text { for } 1<k<\frac{n}{2}  \tag{3.3}\\
w_{k, 2 j}^{h}=-w_{n-k, j}^{2 h}, \quad \text { for } \frac{n}{2}<k<n \tag{3.4}
\end{gather*}
$$

For $\frac{n}{2}<\mathrm{k}<\mathrm{n}$ the k -th mode becomes negative, see equation 3.4, which means that the modes on $\Omega^{2 h}$ is represented as relatively smooth compared to the oscillating modes on $\Omega^{h}$. Therefore, it is necessary to reduce the oscillating error on modes on $\Omega^{h}$ before transferring (restricting) it to $\Omega^{2 h}$. Usually, 1-2 iterations
is enough for reducing the high frequency errors with an iterative scheme.
To improve the behavior of an iterative method, the initial guess is important. In a multigrid scheme, this is done by solving the problem approximately on the coarsest grid, $\Omega^{x h}$, and transferring (prolongate) the solution to the next finer grid, $\Omega^{(x+1) h}$. The transferred solution can be used as a initial guess on the fine grid since the oscillating error modes are damped on the coarsest grid.

### 3.1.1 Restriction

The transformation from fine to coarse grid is called restriction. A restriction procedure can restrict solutions or residual dependent on the multigrid algorithm. Restriction operator, $I_{h}^{2 h}$, can be preformed in different ways, in this subsection two different methods is taken into consideration, injection and weighted restriction.

$$
\begin{aligned}
I_{h}^{2 h}: \mathbb{R}^{n} \rightarrow \mathbb{R}^{n / 2} \\
\mathbf{u}^{2 h}=I_{h}^{2 h} \mathbf{u}^{h}
\end{aligned}
$$

The fine grid, $\Omega^{h}$, consists of $n$ grid cells and the coarse grid, $\Omega^{2 h}$, consists of $\frac{n}{2}$ grid cells. Node numbering $i$ and $j$ on the coarse grid corresponds to node numbering $2 i$ and $2 j$ on the fine grid.

## Injection

The simplest restriction method is restriction by injection. A injection matrix, $I_{h}^{2 h}$, for a FDM consists of only one and zeros, i.e. ignores the odd-numbered fine grid values and directly adopt the even-numbered values to the coarse grid. With this method, the error will not be corrected on the odd-numbered fine nodes. This can cause a reduction of the efficiency of the multigrid method.

## Weighted restriction

Weighted restriction uses all the nodes on the fine grid in the transformation and can be preformed in several ways, full-weighted, half-weighted etc. The injection matrix $I_{h}^{2 h}$ for full-weighted restriction has the relation to the linear interpolation matrix equals to $I_{h}^{2 h}=\frac{1}{2}\left(I_{2 h}^{h}\right)^{T}$ (Strang, 2006). In 2D, the full- weighted stencil will include nine neighboring points.

### 3.1.2 Prolongation

The transformation from coarse grid to fine grid is called prolongation (or interpolation). This is done by a prolongation matrix, $I_{2 h}^{h}$, which is defined by a local averaging for FDMs. The simplest averaging method is linear interpolation, see figure 3.1.

$$
\begin{array}{r}
I_{2 h}^{h}: \mathbb{R}^{n / 2} \rightarrow \mathbb{R}^{n} \\
\mathbf{u}^{h}=I_{2 h}^{h} \mathbf{u}^{2 h}
\end{array}
$$

The coarse grid, $\Omega^{2 d}$, consists of $\frac{n}{2}$ grid cells and the fine grid, $\Omega^{d}$, consists of $n$ grid cells. Node numbering $2 i$ and $2 j$ on the fine grid corresponds to node numbering $i$ and $j$ on the coarse grid.


Figure 3.1: Linear interpolation in 1D (Drikakis et al., 1998).

### 3.2 Different algorithms

There are many possibilities for preforming a multigrid method. In this section algorithms for a two-step, $v$-cycle and full multigrid is focused on. For future explanation or reading on other algorithms see Wesseling (1995) and Stüben and Trottenberg (1982).

The new variables in the algorithms is explained here, where $\nu_{1}$ is the presmoothing, $\nu_{2}$ is the coarse-smoothing and $\nu_{3}$ is the post-smoothing, see section 3.3 for more information on the smoothing parameters. The residual is denoted as $\mathbf{r}$ and the solution-error as $\mathbf{e}$.

It is important that the right-hand side of the linear system, $\mathbf{f}$, is constant trough the methods, i.e. $\mathbf{f}$ is equal on a downward stoke and an upward stoke for the respective grid depth.

### 3.2.1 The Two-Level Method

Two-step multigrid can be used to test the residual equation 3.2 in a multigrid method. A schematic configuration is given in figure 3.2 and the algorithm is:

1 Iterate $A^{h} \mathbf{u}^{h}=\mathbf{f}^{h}, v_{1}$-times.

2 Compute the residual $\mathbf{r}^{h}=\mathbf{f}^{h}-A^{h} \mathbf{u}^{h}$ on $\Omega^{h}$ and restrict it to $\Omega^{2 h}, \mathbf{f}^{2 h}=$ $I_{h}^{2 h} \mathbf{r}^{h}$.

3 Iterate $A^{2 h} \mathbf{e}^{2 h}=\mathbf{f}^{2 h} v_{2}$-times or solve directly. Start with the initial guess $\mathbf{e}^{2 h}=0$.

4 Prolongate $\mathbf{e}^{2 h}$ to $\Omega^{2 h}, \mathbf{e}^{h}=I_{2 h}^{h} \mathbf{e}^{2 h}$ and update the solution $\mathbf{u}^{h}=\mathbf{u}^{h}+\mathbf{e}^{h}$.

5 Iterate $A^{h} \mathbf{u}^{h}=\mathbf{f}^{h}, v_{3}$-times.
level


Figure 3.2: Schematic of two-step multigrid, modification from Strang (2006).

### 3.2.2 V-Cycle Multigrid Method

A V-cycle multigrid method starts similar as a two-step multigrid method, but the depth of the cycle can vary, see figure 3.3. The V-cycle multigrid method is the simplest one and the algorithm is:

1 Iterate $A^{h} \mathbf{u}^{h}=\mathbf{f}^{h}, v_{1}$-times. Store $\mathbf{u}^{h}$ and $\mathbf{f}^{h}$.

2 Compute the residual $\mathbf{r}^{h}=\mathbf{f}^{h}-A^{h} \mathbf{u}^{h}$ on $\Omega^{h}$ and restrict it to $\Omega^{2 h}, \mathbf{f}^{2 h}=$ $I_{h}^{2 h} \mathbf{r}^{h}$. Store $\mathbf{f}^{2 h}$.

3 Iterate $A^{2 h} \mathbf{e}^{2 h}=\mathbf{f}^{2 h} v_{2}$-times and store $\mathbf{e}^{2 h}$. Start with the initial guess $\mathbf{e}^{2 h}=0$.

4 Compute the residual $\mathbf{r}^{2 h}=\mathbf{f}^{2 h}-A^{2 h} \mathbf{u}^{2 h}$ on $\Omega^{2 h}$ and restrict it to $\Omega^{4 h}, \mathbf{f}^{4 h}=$ $I_{2 h}^{4 h} \mathbf{r}^{2 h}$. Store $\mathbf{f}^{4 h}$.

- Continue until coarsest grid is reached ...

5 Solve coarsest grid $A^{x h} \mathbf{e}^{x h}=\mathbf{f}^{x h}$ by iterating $\nu_{3}$-times or solve directly. Start with the initial guess $\mathbf{e}^{x h}=0$.

6 Prolongate $\mathbf{e}^{x h}$ to $\Omega^{(x+1) h}, \mathbf{e}^{(x+1) h}=I_{x h}^{(x+1) h} \mathbf{e}^{x h}$ and update the solution $\mathbf{e}^{(x+1) h}=\mathbf{e}_{\text {old }}^{(x+1) h}+\mathbf{e}_{\text {new }}^{(x+1) h}$.

7 Iterate $A^{(x+1) h} \mathbf{e}^{(x+1) h}=\mathbf{f}^{(x+1) h}, v_{3}$-times.

- Continue until finest grid is reached ...

8 Prolongate $\mathbf{e}^{2 h}$ to $\Omega^{h}, \mathbf{e}^{h}=I_{2 h}^{h} \mathbf{e}^{2 h}$ and update the solution $\mathbf{u}^{h}=\mathbf{u}^{h}+\mathbf{e}^{h}$.
9 Iterate $A^{h} \mathbf{u}^{h}=\mathbf{f}^{h}, v_{3}$-times.

The V-cycle algorithm can be preformed in different number of cycles, $\gamma$, by using a for-loop over step 2-9.


Figure 3.3: Schematic of V-cycle multigrid, modification from Strang (2006).

### 3.2.3 The Full Multigrid Method

The full multigrid method start at the coarsest grid and prolongate up to the next finer grid to provide a good initial guess. Then V-cycles of each depth are preformed to improve the solution until the finest grid is reached, see figure 3.4. The full multigrid algorithm is:

1 Store $\mathbf{f}^{h}$.
2 Restrict $\mathbf{f}^{h}$ to $\Omega^{2 h}, \mathbf{f}^{2 h}=I_{h}^{2 h} \mathbf{f}^{h}$ and store $\mathbf{f}^{2 h}$.

- Continue until the coarsest grid is reached ...

3 Restrict $\mathbf{f}^{(x-1) h}$ to $\Omega^{x h}, \mathbf{f}^{x h}=I_{(x-1) h}^{x h} \mathbf{f}^{(x-1) h}$.
4 Solve coarsest grid $A^{x h} \mathbf{e}^{x h}=\mathbf{f}^{x h}$ by iterating $v_{3}$-times or solve directly and store $\mathbf{e}^{x h}$. Start with the initial guess $\mathbf{e}^{x h}=0$.

5 Prolongate $\mathbf{e}^{x h}$ to $\Omega^{(x+1) h}, \mathbf{e}^{(x+1) h}=I_{x h}^{(x+1) h} \mathbf{e}^{x h}$ and store $\mathbf{e}^{(x+1) h}$.

- Run V-cycles, see subsection 3.2.2, for each depth until the finest grid is reached ...

6 Prolongate $\mathbf{e}^{2 h}$ to $\Omega^{h}, \mathbf{e}^{h}=I_{2 h}^{h} \mathbf{e}^{2 h}$ and update the solution $\mathbf{u}^{h}=\mathbf{u}^{h}+\mathbf{e}^{h}$.
7 Iterate $A^{h} \mathbf{u}^{h}=\mathbf{f}^{h}, v_{3}$-times.


Figure 3.4: Schematic of full multigrid, modification from Strang (2006).

### 3.3 Smoothening Parameters

The purpose of a multigrid method is to reach convergence more efficiently then an iterative method. For a PDE problem, the accuracy is solved to $\mathscr{O}\left(n^{2}\right)$ in 5-12 iterations (Mccormick, 1988).

During a multigrid scheme, there are stated three different values for iterations, pre-smoothing, coarse-smoothing and post-smoothing. This is done to solve the multigrid method as efficient as possible.

For pre-smoothing, which is used in a downward stoke, there only needs to be preformed a few iterations, 1-3, depending on the problem to be solved. The purpose (goal) here is not to reach convergence, but to reduce the high frequencies which an iterative scheme do quite fast, see section 3.1 for more details.

For coarse-smoothing, which is used to smooth the coarsest grids, there can be preformed a higher number of iterations. Usually, the cost and time spent on iterating on the coarsest grids is quite low compared to iterating on the finest grid. Therefore it is expedient (appropriate) to find a optimal number for coarsesmoothing so the initial guess for the next coarsest grid is good. This number will make a change in the computational work and the running time for a multigrid method.

For post-smoothing, which is used in an upward stoke, number of iterations can vary depending on the the problem to be solved. There should not be necessary to iterate to many times. Usually, it is better to change the coarse-smoothing or number of cycles instead of increasing the number of post-smoothing iterations, to reach convergence.

### 3.4 Convergence and Computational Work

It is possible to find a convergence factor $\beta$, which is the spectral radius of the overall iteration matrix, by numerical analysis Strang (2006). $\beta$ is a constant factor less than one, $\beta<1$, and independent of the grid size $h$. Hence, theoretically the number of iterations is bounded independent of the grid level on the linear system and only dependent of the accuracy.

To achieve an optimal multigrid algorithm, the number of floating point operations (flops) per multigrid cycle should behave like $\mathscr{O}(n)$, where $n$ is the number of degrees of freedom (unknowns). Number of flops for a deep v-cycle or a full multigrid is greater than for a two-step multigrid Strang (2006), the relation is given in equation 3.5.

Flops in full MG $<\frac{2^{d}}{2^{d}-1}($ Flops in $V-$ cycle $)<\left(\frac{2^{d}}{2^{d}-1}\right)^{2}($ Flops in two - step $)$
$d$ is the dimension in space and the power of 2 is related to the transpose relation between a fine and a coarse grid. Hence, the total number of flops are asymptotically optimal for multigrid methods.

Good programing is decisive to optimize the multigrid algorithm together with the chosen transposing methods. Regardless, the multigrid method is one of the most efficient iterative methods known today (Hackbusch, 1985).

## Chapter 4

## Immersed Boundary Method

The governing equations for the fluid are easily adopted to fluid-structure interaction problems. This is done by an approach to model the coupling between the structure and the fluid. Hence, the immersed boundary method (IBM) can be used to solve the coupling.

The IBM was first proposed and implemented by Peskin (1972). He inserted an immersed boundary of the flexible leaflet of a human heart valve and presented it as a method for solving the Navier-Stokes equation on a rectangular domain accomplished by replacing the boundary by a field of force defined on the mesh points of the rectangular domain. Later, the method was adopted by Lai and Peskin (2000) to simulate rigid boundaries.

In IBM, the immersed boundary points on a geometry does not need to conform with the Eulerian grid points in the computational fluid domain. The points are applied to a Lagrangian grid, but by imposing the immersed boundary conditions on the geometry the immersed boundary can be handled in the Eulerian grid by modifying the governing equations.

There are several advantages by using the IBM to apply a geometry in a fluid:

- The geometry does not need to fit the computational grid.
- It can handle moving boundaries.
- Grid complexity and quality are not significantly affected.
- The computational cost of each grid node is generally less expensive, i.e. less memory and CPU are used.
- IBM solved by explicit time stepping schemes require solvers only for the Eulerian equations (Guy et al., 2015).
- Works together with multigrid methods.


### 4.1 Imposing of Immersed Boundary Conditions

Imposing of the immersed boundary conditions is the key factor in an immersed boundary algorithm. The method used to impose these boundary conditions is what distinguishes the algorithms, i.e. how to modify the governing equations. The domain occupied by the geometry is denoted by $\Omega_{b}$ and the immersed boundary by $\Gamma_{b}$, then the immersed boundary conditions is specified as equation 4.1.

$$
\begin{equation*}
\mathbf{u}=\mathbf{u}_{\Gamma} \quad \text { and } \quad \frac{\partial p}{\partial \mathbf{x}}=0 \quad \text { on } \Gamma_{b} \tag{4.1}
\end{equation*}
$$

The governing equations (2.5, 2.6 and 2.4 ) for the domain $\Omega$ is discretized without taking the immersed boundary into account. The immersed boundary condition is imposed indirectly by modifying 2.5 and 2.6 with a forcing function $\mathbf{f}_{\mathbf{b}}$, see 4.2 , representing the effect of the immersed boundary.

$$
\begin{gather*}
\mathbf{u}_{t}+\mathbf{u} \cdot \nabla \mathbf{u}=-\nabla p+\frac{1}{R e} \nabla^{2} \mathbf{u}+\mathbf{f}_{\mathbf{b}} \quad \text { on } \Omega  \tag{4.2}\\
\nabla \cdot \mathbf{u}=0 \tag{4.3}
\end{gather*}
$$

The forcing function can be implemented in two different ways:

1. Continuous forcing method $-\mathbf{f}_{\mathbf{b}}$ is applied to the entire domain, i.e. 4.2 is solved on $\left(\Omega+\Omega_{b}\right)$.
2. Discrete forcing method - first, $\mathbf{f}_{\mathbf{b}}=0$ and 4.2 is discretized without the immersed boundary, then the cell-velocities near the immersed boundary are adjusted to account for the immersed boundary.

When a continuous forcing method is used, elastic and rigid boundaries needs different treatment. This method will not be described here, for future discussions around elastic boundaries read Peskin (1972) and for rigid boundaries read Goldstein et al. (1993).

### 4.2 Discrete Forcing Methods

Discrete forcing methods are divided into indirect and direct forcing approaches. Indirect approaches are imposing the immersed BC's indirectly on the immersed boundary. Otherwise, the direct forcing approaches are imposing the immersed BC's directly on the immersed boundary, which will be future discussed here.

### 4.2.1 Direct Forcing approach

The direct forcing approach was derived by Mohd-Yusof (1997). He provided a method where the velocity value is imposed directly on the boundary and the implementation do not require additional CPU time. To demonstrate the main
steps in the approach assume a 2D immersed boundary with the Eulerian grid points $(i, j)$. Considering the equation 4.2 discretized in time by the explicit Euler method, equation 4.4 arise.

$$
\begin{equation*}
\frac{u_{i, j}^{n+1}-u_{i, j}^{n}}{\Delta t}=R H S_{i, j}+f_{i, j} \tag{4.4}
\end{equation*}
$$

$n+1$ and $n$ are respectively the next and the present time-step, $i, j$ is the location on the Eulerian grid. For $u_{i, j}^{n+1}=U_{i, j}$, where $U_{i, j}$ is the fluid velocity next to the immersed boundary, then equation 4.5 for $f_{i, j}$ yields.

$$
\begin{equation*}
f_{i, j}=\frac{U_{i, j}-u_{i, j}^{n}}{\Delta t}-R H S_{i, j} \quad \text { near } \Gamma_{b} \tag{4.5}
\end{equation*}
$$

Since the immersed boundary does usually not coincide with the underlying grid, an interpolation procedure needs to be used to determine $U_{i, j}$ close to the intersection points.

When the projection method from subsection 2.1.3 is used to decouple the velocities and the pressure, the immersed BC's are forced on the predicted velocities, $u_{i, j}^{*}$ and $v_{i, j}^{*}$, together with the interpolation procedure. Balaras (2004) prescribe this simplification without reducing the temporal accuracy of the method.

### 4.2.2 Interpolation

Different interpolation schemes can be used to find the velocities close to the immersed boundary. Fadlun et al. (2000) presents three different schemes on a staggered grid (see figure 4.1), no interpolation, volume fraction weighting and velocity interpolation, and tested the results they provided. The velocity interpolation gave the best results and will be described here.


Figure 4.1: From Fadlun et al. (2000). (a) no interpolation,(b) volume fraction weighting, (c) linear interpolation.

The interpolation scheme presented by Fadlun et al. (2000) is different and more accurate than the interpolation scheme presented by Peskin (1972). The interpolation is done by a linear approximation of the velocities close to the immersed boundary wall. The velocity profiles are assumed to be approximately linear from the wall if the grid around the immersed boundary is fine enough.

## Chapter 5

## Code layout

A Navier Stokes solver is developed to preform case studies with multigrid and IBM. The incompressible Navier Stokes equations for a 2-dimensional flow is solved on an equidistant grid and the following sections will give a short introduction on the code layout, methods used, assumptions taken and limitations on the code. The respective code is found in Appendix B and a flow chart can be seen in figure 5.1.

The programming language used to develop the program is C with compiler gcc and flags -W and -o. Double precisions is used to ensure convergence of the simulations. A vtf-file is written in the end of each time-step (or at chosen timesteps) to visualize the result in GLview. The program is ran on Ubuntu 16.04 with 4 (64-bit, l.8GHz) CPUs.


Figure 5.1: Flow chart of the Navier Stokes solver


Figure 5.2: A staggered grid cell at position $i, j$.

### 5.1 Staggered Grid Generation

The solver uses an equidistant staggered grid in the computational domain. When refering to $u, v$ and $p$ in the computational node, the definitions given in figure 5.3, 5.4 and 5.5 are the current one. By using these definitions, halfinteger velocity adresses are not needed and a cell i defined as in figure 5.2.


Figure 5.3: The representation of u-velocity in the staggered grid.


Figure 5.4: The representation of v -velocity in the staggered grid.


Figure 5.5: The representation of the pressure in the staggered grid.

### 5.2 Finite Difference Scheme

A FDM scheme, represented by the nodes in figure 5.6, 5.7 and 5.8, is used to solve the spatially differential terms in equation 2.10 as $R H S(u, v, p)$ in 5.1. The FDM-stencil presented by Harlow and Welch (Harlow et al., 1965) is used with the following equations for the viscous terms 5.3, the advective terms 5.2 and the pressure terms 5.4. $h=\Delta x=\Delta y$ since an equidistant grid is used and $u$.

$$
\begin{equation*}
\frac{\mathbf{u}^{*}-\mathbf{u}^{n}}{\Delta t}=R H S(u, v, p) \tag{5.1}
\end{equation*}
$$

Where $\mathbf{u}=\{u, v\}$ is the velocities in 2D.

$$
\left.\begin{array}{c}
A_{x}=\frac{0.25}{h}\left(\left(u_{i+1, j}+u_{i, j}\right)^{2}-\left(u_{i, j}+u_{i-1, j}\right)^{2}\right. \\
\left.+\left(u_{i, j+1}+u_{i, j}\right)\left(v_{i+1, j}+v_{i, j}\right)-\left(u_{i, j}+u_{i, j-1}\right)\left(v_{i+1, j-1}+v_{i, j-1}\right)\right) \\
A_{y}=\frac{0.25}{h}\left(\left(u_{i, j+1}+u_{i, j}\right)\left(v_{i+1, j}+v_{i, j}\right)-\left(u_{i-1, j}+u_{i-1, j-1}\right)\left(v_{i-1, j}+v_{i, j}\right)\right. \\
\left.+\left(v_{i, j}+v_{i, j+1}\right)^{2}-\left(v_{i, j-1}+v_{i, j}\right)^{2}\right)
\end{array}\right] \begin{gathered}
V_{x}=\frac{1}{R e}\left(\frac{u_{i+1, j}+u_{i-1, j}+u_{i, j+1}+u_{i, j-1}-4 u_{i, j}}{h^{2}}\right) \\
V_{y}=\frac{1}{R e}\left(\frac{v_{i+1, j}+v_{i-1, j}+v_{i, j+1}+v_{i, j-1}-4 v_{i, j}}{h^{2}}\right) \\
P_{x}=\frac{p_{i, j}-p_{i+1, j}}{h} \\
P_{y}=\frac{p_{i, j}-p_{i, j+1}}{h} \tag{5.4}
\end{gathered}
$$



Figure 5.6: The representation of pressure and velocities used for x -direction calculations.


Figure 5.7: The representation of pressure and velocities used for Figure 5.8: Velocities y -direction calculations. used to calculate $p_{i, j}$.

### 5.3 Explicit Euler Scheme

An explicit Euler scheme 2.11 is used to solve the temporal discretization. Hence, the Navier Stokes equations will be solved for each $\Delta t$ until tmax is reached, starting from $t=0$, see 5.1. The current spatial values are used in the right-hand side solution according to the explicit Euler scheme, see equation 5.5.

$$
\begin{equation*}
\frac{\mathbf{u}^{*}-\mathbf{u}^{n}}{\Delta t}=R H S\left(u^{n}, v^{n}, p^{n+1}\right) \tag{5.5}
\end{equation*}
$$

To solve the pressure-velocity coupling by the projection method a predictor, PM-predictor, is stated from the euler scheme. The output from the PMpredictor results in the predicted velocities, equation 5.6, which are used to form the right-hand side of the Poisson equation. After the Poisson equation is solved, a projection method corrector, PM-corrector, will update the nonsolenoidal velocities with the pressure correction found in the Poisson solver, see equation 5.7.

$$
\begin{align*}
& u^{*}=u^{n}+\Delta t R H S\left(u^{n}, v^{n}, p^{n}\right) \\
& v^{*}=v^{n}+\Delta t R H S\left(u^{n}, v^{n}, p^{n}\right) \tag{5.6}
\end{align*}
$$

$$
\begin{gather*}
u^{n}=u^{*}-\Delta t \frac{\Delta p_{i+1, j}-\Delta p_{i, j}}{h}  \tag{5.7}\\
v^{n}=v^{*}-\Delta t \frac{\Delta p_{i, j+1}-\Delta p_{i, j}}{h} \\
p^{n+1}=p^{n}+\Delta p \tag{5.8}
\end{gather*}
$$

### 5.4 Poisson Solver

The Poisson equation can be solved with different equation solvers. In the present code, Gauss Seidel, SOR, two-step multigrid and V-cycle multigrid are compared. The right-hand side, $f$, is stated as the divergence of the predicted velocities, $u^{*}$ and $v^{*}$, divided by $\Delta t$.

$$
\begin{equation*}
-\Delta p=f \quad \text { in } \quad \Omega=(0,1)^{2} \tag{5.9}
\end{equation*}
$$

### 5.4.1 Gauss Seidel

Gauss Seidel method is implemented straight forward. Equation 5.10 presents the scheme to be iterated for each iteration $k$.

$$
\begin{equation*}
\Delta p_{i, j}^{k}=\frac{1}{4}\left(\Delta p_{i+1, j}^{k-1}+\Delta p_{i-1, j}^{k} \Delta p_{i, j+1}^{k-1}+\Delta p_{i, j-1}^{k}-h^{2} f_{i, j}\right) \tag{5.10}
\end{equation*}
$$

### 5.4.2 Successive Over Relaxation

For SOR method it is reasonable to find the optimal omega, $\omega_{\text {opt }}$, for the currant grid size. $\omega_{\text {opt }}$ is found by linear interpolation between the grid size and interpolation values found from experimental results. The iterative scheme solved is presented in equation 5.11 and iterated for each iteration $k$.

$$
\begin{equation*}
\Delta p_{i, j}^{k}=\left(1-\omega_{o p t}\right) \Delta p_{i, j}^{k-1}+\frac{\omega_{o p t}}{4}\left(\Delta p_{i+1, j}^{k-1}+\Delta p_{i-1, j}^{k} \Delta p_{i, j+1}^{k-1}+\Delta p_{i, j-1}^{k}-h^{2} f_{i, j}\right) \tag{5.11}
\end{equation*}
$$

### 5.4.3 Multigrid

The multigrid method is implemented to accelerate the rate of convergence of the Poisson solver. Three different multigrid algorithms are implemented, twostep multigrid (see algorithm in subsection 3.2.1), v-cycle multigrid (see algorithm in subsection 3.2.2) and full multigrid(see algorithm in subsection 3.2.3). All the algorithms are using Gauss-Seidel, presented in subsection 5.4.1, to find an approximate solution. The number of interior points in $x$ - and $y$-direction is $2^{d}$ in a $[0: 1] \mathrm{x}[0: 1]$ domain, where $d$ is the number of multigrid levels.

In 2D, the injection done by the restriction matrix $I_{h}^{2 h}$ in the present code is presented in equation 5.12. $n$ is the number of fine grid points, $h$ represents the fine grid and $2 h$ the coarse grid.

$$
\begin{equation*}
\Delta p_{i, j}^{2 h}=\Delta p_{2 i, 2 j}^{h}, \quad i=1, \ldots, \frac{n}{2} \text { and } j=1, \ldots, \frac{n}{2} \tag{5.12}
\end{equation*}
$$

The prolongation matrix $I_{2 h}^{h}$ for linear interpolation will in 2D be represented as bilinear interpolation, see figure 5.9 with corresponding equation 5.13 , where $n$ is the number of coarse grid points.

$$
\begin{align*}
& e_{2 i, 2 j}^{h}=\frac{9}{16} e_{i, j}^{2 h}+\frac{3}{16}\left(e_{i+1, j}^{2 h}+e_{i, j+1}^{2 h}\right)+\frac{1}{16} e_{i+1, j+1}^{2 h} \\
& e_{2 i+1,2 j}^{h}=\frac{9}{16} e_{i+1, j}^{2 h}+\frac{3}{16}\left(e_{i+1, j+1}^{2 h}+e_{i, j}^{2 h}\right)+\frac{1}{16} e_{i, j+1}^{2 h}, \\
& e_{2 i, 2 j+1}^{h}=\frac{9}{16} e_{i, j+1}^{2 h}+\frac{3}{16}\left(e_{i+1, j+1}^{2 h}+e_{i, j}^{2 h}\right)+\frac{1}{16} e_{i+1, j}^{2 h},  \tag{5.13}\\
& e_{2 i+1,2 j+1}^{h}=\frac{9}{16} e_{i+1, j+1}^{2 h}+\frac{3}{16}\left(e_{i+1, j}^{2 h}+e_{i, j+1}^{2 h}\right)+\frac{1}{16} e_{i, j}^{2 h}, \\
& \text { for } \quad i=0, \ldots, n \quad \text { and } \quad j=0, \ldots, n .
\end{align*}
$$

To improve the prolongation, mixed interpolation, see figure 5.10, are implemented at the boundaries on the fine grid. Mixed interpolation is prescribed under section 3.1.2 and developed in the present code as equation 5.14. boundary represents a boundary point in the fine grid for $e^{h}$ and in the coarse grid for $e^{2 h}$. $n$ is the number of coarse grid points.

$$
\begin{align*}
& e_{\text {boundar } y, 2 j}^{h}=\frac{3}{4} e_{\text {boundar } y, j}^{2 h}+\frac{1}{4} e_{\text {boundar } y, j+1}^{2 h} \\
& e_{\text {boundar } y, 2 j+1}^{h}=\frac{3}{4} e_{\text {boundar } y, j+1}^{2 h}+\frac{1}{4} e_{\text {boundar } y, j}^{2 h} \\
& e_{2 i, \text { boundar } y}^{h}=\frac{3}{4} e_{i, \text { boundar } y}^{2 h}+\frac{1}{4} e_{i+1, \text { boundar } y}^{2 h}  \tag{5.14}\\
& e_{2 i+1, \text { boundar } y}^{h}=\frac{3}{4} e_{i+1, \text { boundar } y}^{2 h}+\frac{1}{4} e_{i, \text { boundar } y}^{2 h} \\
& \text { for } \quad i=0, \ldots, n \quad \text { and } \quad j=0, \ldots, n
\end{align*}
$$



Figure 5.9: Bilinear interpolation Figure 5.10: Mixed interpolation (Drikakis et al., 1998).

### 5.5 IBM

To insert a geometry in the fluid flow, IBM is used. The IBM developed in the present code is based on Mossige (2017) and measures the force function by direct force approach, which is a discrete force method.

Coinciding with theory prescribed in chapter 4 , the velocities close to the immersed boundary should be modified. In order to find the positions relative to the underlying computational grid, the staggered grid configurations needs to be taken into consideration. To interpolate parallel to the velocity directions, which is done in the present code, a grid shifting of the velocity is accomplished. To save computational time, a domain surrounding the immersed boundary is defined, see fiure 5.11. A representation of parallel linear interpolation and the grid shift are given in figure 5.13 and 5.12.


Figure 5.11: A demonstration of the surrounding domain for an immersed boundary.


Figure 5.12: How to apply grid shift on the surrounding domain. The black grid is the original staggered grid, red is $v$-velocities and green is $u$ - velocities.


Figure 5.13: Parallel interpolation after $\frac{1}{2}$-gridshift, from Mossige (2017).

The direction into the fluid from the immersed boundary is detected for each intersection point and the two first fluid node velocities are used in the linear interpolation together with the immersed boundary velocity. The purpose of the interpolation is to modify the first fluid node with respect to the two other nodes, i.e. the effect of the boundary is stated indirectly. Since the predicted velocities, see equation 5.6, are used in the IBM, the interpolated velocities are flagged to not be corrected by the PM-corrector. Pressure boundary conditions are not imposed according to Fadlun et al. (2000) and the internal flow flied is a freely developed.

Force coefficients for lift and drag are calculated from the lift and drag forces, see equation 5.15. For each intersection point, $i$, a contribution to the forces are measured by Newton's second law and third law, see equation 5.16, where the change in velocity in $x$-direction will give a contribution to the drag force and the change in velocity in $y$-direction will give a contribution to the lift force. Hence, the forces are equal but has the opposite direction of the influence the immersed boundary has on the fluid. $u_{d}$ and $v_{d}$ denotes the difference between the interpolated and the predicted velocity, $A$ is the areal of the geometry, $u_{\infty}$ is the inflow velocity, $\rho$ is the density and $\rho h^{2}$ represents the mass.

$$
\begin{align*}
C_{D} & =2 \frac{F_{D}}{\rho u_{\infty}^{2} A}  \tag{5.15}\\
C_{L} & =2 \frac{F_{L}}{\rho u_{\infty}^{2} A}
\end{align*}
$$

$$
\begin{align*}
& F_{D}=\sum_{i}-\frac{u_{d}}{\Delta t} \rho h^{2}  \tag{5.16}\\
& F_{L}=\sum_{i}-\frac{v_{d}}{\Delta t} \rho h^{2}
\end{align*}
$$

When a fluid flows over a geometry, the geometry exerts a (pressure) force, and if a geometry surface is no-slip, the fluid exerts a share force too. Conceptually, the geometry exerts a force with opposite direction on the fluid (Goldstein et al., 1993).

### 5.5.1 Limitations on the Immersed Boundary

How to define the immersed boundary geometry has certain limitations, which needs to be taken into consideration:

- The geometry should be located $2 h$ from the boundary cells because of the choice of interpolation nodes described earlier.
- The geometry should be a closed polygon.
- Grid generation around the immersed boundary have to be fine enough to assume linear velocity profiles.
- The immersed boundary cannot be too close to another part of the immersed boundary, then an interpolated velocity can be used to interpolate a new velocity.
- The forced motion procedure on a body is not tested, hence may not be perfectly developed.

The IBM-module is not complete due to the fluid structure interaction problem. It still reminds to implement the deformation and the velocity response of the immersed boundary. At this point, the boundaries can only move by a pre-described motion as a closed rigid geometry.

### 5.6 Convergence criteria

For the Poisson solver, the convergence criteria is $10^{-6}$ due to the infinity-norm, see equation 5.17. $\Delta p_{d}$ is the change in $\Delta p$ per iteration.

$$
\begin{equation*}
\left\|\Delta p_{d}\right\|_{\infty} \leq 10^{-6} \tag{5.17}
\end{equation*}
$$

### 5.7 General Limitations

To define the domain in the refinement test, a change where made to handle rectangular domains. This includes the $\operatorname{dim} X$ and $\operatorname{dim} Y$ in the code, which are factors multiplied by the number of cells in the original domain [0:1]x[0:1]. Be aware of that $\operatorname{dim} X$ and $\operatorname{dim} Y$ needs to be equals to or larger than 1.0. To get right post-processing in GLview, $\operatorname{dim} X$ needs to be larger or equals to $\operatorname{dim} Y$, but this has no impact on the computations done before the post-processing stage. The IBM is not affected by the multiplication, hence the immersed boundary need to be placed in the domain $[0: 1] x[0: 1]$ with the same restrictions as described earlier. This modification of the code is not optimal, but are done in the late stage of the implementation process due to efficiency of the computational work.

During the implementation some changes were made in the code, which have impact on the code setup. Static allocation of memory where implemented first, but during the implementation of multigrid methods, too much memory where occupied for larger problems. Therefore, a change to dynamic allocation where made. By lack of time, just the necessary modifications for this change where implemented.

### 5.8 Post-processing

In the post processing stage, an averaging of the velocities and pressure is done to be represented in the same node as specified for visualization in GLview. The averaging is only for the visualization and will not affect the previous calculations steps. When using IBM, the interpolated velocities close to the immersed boundary are already specified, but this is not taken into consideration at this stage. This means that the visualization of velocities closest to the boundary will be affected by the velocities inside of the immersed boundary and the BC's at the wall are not achieved in the visualization. This should be taken into consideration when analyzing the figures.

## Chapter 6

## Validation

The developed solver is validated to check accuracy, efficiency and force coefficients, a final test case is done in the end to collect it all. First, the Poisson solver is validated and the most efficient method with acceptable accuracy is used in the following. Further, the chosen method is tested together with the IBM in a final case. Refinement tests are preformed before the final test case to optimize the simulations. An efficiency overview for one time-step of the final test case is presented at the end.

The fluid solver without IBM is assumed to work OK and is not validated here. The fluid solver is previously validated in my project thesis (Aarsnes), where the solver is based on the same methods as the present solver and SOR method is used to solve the Poisson equation. Some modifications are done in the code, but it is still reasonably to assume that the validations are valid.

### 6.1 Poisson Solver

In the Navier-Stokes solver, there are several possible methods defined to solve the Poisson equation 2.9. Only iterative methods has been developed according to the large model problem and memory limitations. Two simple methods, Gauss Seidel and SOR, are tested against the more complex multigrid methods. In subsection 6.1.1 the Poisson solver is run with Gauss Seidel method and SOR method, in subsection 6.1.2 it is run with different multigrid methods. First, a test problem is defined.

## Test Problem

A test problem is defined and used in all validations under this section. The domain, $\Omega=[0,1] \mathrm{x}[0,1]$, have periodic boundary conditions at $d \Omega$ and a nonzero forcing function 6.1 of the Poisson equation. The analytical solution of the problem is given in equation 6.2. Mesh resolution in the tests for the Poisson solver is $256 \times 256$ with $\mathrm{h}=\frac{1}{256}$. $x$ and $y$ refers to the position on the 2 D domain.

$$
\begin{gather*}
\mathbf{f}(x, y)=\cos (2 \pi x) \cos (2 \pi y)  \tag{6.1}\\
p_{\text {exact }}=\frac{1}{(2 \pi)^{2}} \cos (2 \pi x) \cos (2 \pi y) \tag{6.2}
\end{gather*}
$$

### 6.1.1 Gauss Seidel and SOR

Figure 6.1 and figure 6.2 shows the analytical solution, equation 6.2, plotted against the numerical solutions preformed by Gauss Seidel and SOR. The solution values lie along a line in the middle of the domain, horizontally $(y=0.5)$. In both cases, the numerical results are following the analytical solution in an acceptable way by crossing it, hence the curvature line of the difference given in figure 6.3 and figure 6.4. The difference between the analytical solution and the numerical solution turns out asymmetric with the left slope slower than the right slope. Thereby, there is a small displacement in the Poisson solver preformed by the Gauss Seidel method. This could arise from how the solver sweep trough the domain in $x$ - and $y$-direction. Here, the Gauss Seidel method sweep from the lower left corner to the upper right corner of the domain. Since $y$ is constant trough the domain, the solution passes from left to right and can permit the largest errors to accumulate at the high values of $x$ (Kahan, 1958). When this displacement occurs in the Gauss Seidel method, it will also occur in the other methods which are based on the Gauss Seidel algorithm. Figure 6.4 is a plot of the difference when using SOR method to solve the Poisson equation numerically. SOR can be seen as a method who applies a correction to the value already obtained from the Gauss Seidel method based on extrapolation from previous iterations (Richard H. Pletcher, 2013) and therefor provide a more asymmetric but accurate solution.

From Kahan (1958), SOR should smooth down the error to the convergence criteria (see subsection 5.6) faster then Gauss Seidel if the damping factor $\omega$ is optimal. Figures 6.5 and 6.6 shows how the residual, $\Delta p^{k}-\Delta p^{k-1}$, propagate during the iterations, $k$, for the two methods. The Gauss Seidel method smooths the Poisson equation properly in 3431 iterations and SOR in 571 iterations. Hence, SOR method are proven to be faster then Gauss Seidel.


Figure 6.1: Analytical solution (green) vs numerical solution (purple) by Gauss Seidel.


Figure 6.2: Analytical solution (green) vs numerical solution (purple) by SOR.


Figure 6.3: Difference between the analytical solution and Gauss Seidel.


Figure 6.4: Difference between the analytical solution and SOR.


Figure 6.5: Change in residual per iteration for Gauss Seidel method.


Figure 6.6: Change in residual per iteration for SOR.

### 6.1.2 Multigrid

A way to test whether a multigrid algorithm works properly or not, is to measure the residual before and after the algorithm goes to a coarser grid (Wesseling, 1995). A significant reduction in the residual should be found.


Figure 6.7: Change in residual per iteration for two-step MG.


Figure 6.8: Change in residual per iteration for v-cycle MG when $\mathrm{d}=3$.

Figures 6.7, 6.8, 6.9 and 6.10 consists of plots of the residual reduction before an after the algorithm goes to a coarser grid, i.e. change in residual over a vcycle. The number of iterations is measured depending on the depth in the vcycle. The results coincides with the theory presented in chapter 3.


Figure 6.9: Change in residual per iteration for v-cycle MG when $\mathrm{d}=4$.


Figure 6.10: Change in residual per iteration for full MG.

It is possible to see that the change in residual deceases faster in the beginning of the iteration scheme when the depth in the v-cycle increases. This coincides with the reduction in high frequencies error for each grid step, i.e. transfered to lower frequencies on the fine grid, and deeper v-cycles will reach the convergence limit faster.

For the full multigrid algorithm, which starts on the coarsest grid, the reduction in residual is significantly higher in the beginning then for the v-cycle, but it also starts with a higher residual. By the algorithm, the method will continuously improve the initial guess at each depth, and quickly reduce the slow low frequent components of the fine grid. Independently of when the convergence criteria is reached, the algorithm applies v-cycles at each depth until the solution is back on the fine grid.

In a multigrid algorithm, the projection and restriction are sensitive parts. If the reduction in the residual is not found, these parts are not functioning properly and should be investigated (Wesseling, 1995).

To decide the number of pre-, coarse- and post-iterations, different iteration testes are made. The optimal iteration number is stated from the run-time for a converged solution. As a default case, pre-iteration $\nu_{1}=2$, coarse-iteration $\nu_{2}=$ 50 and post-iteration $\nu_{3}=8$. Figure 6.11 is a plot of the change in residual over number of cycles when changing $\nu_{1}$. The optimal choice for $\nu_{1}$ is 2 . Figure 6.12 is a plot of the CPU-time used for different number of iterations where the optimal choice of $\nu_{3}$ is 8 . For v-cycle multigrid and full multigrid, different number of coarse-iterations are optimal. From plots on figures 6.13 and 6.14, it can be seen that $v_{2}$ for $v$-cycle multigrid should be 35 and for the full multigrid $\nu_{2}$ should be 15 , with respect to the CPU-time. These iteration values are used in all future work.


Figure 6.11: Pre-iteration test, iterations - 1:purple, 2:green, 3:blue.


Figure 6.12: Post-iteration test.


Figure 6.13: CPU-time vs number of coarse iterations, v-cycle MG.


Figure 6.14: CPU-time vs number of coarse iterations, full MG.

The multigrid methods, figure 6.17 and 6.15, are less accurate then the SOR method, but more accurate then the Gauss Seidel method. The difference from the analytical solution, equation 6.2 , to the numerical solutions are still propagating asymmetrically trough the domain, figure 6.18 and 6.16 , see the accuracy validation of the Gauss Seidel method for more details. The same way of finding solution values and difference as prescribed under 6.1.1 yields for these plots.


Figure 6.15: Analytical solution (green) vs numerical solution (purple) by v-cycle MG with $\mathrm{d}=3$.


Figure 6.16: Difference between the analytical solution and numerical solution of v -cycle MG with $\mathrm{d}=3$.


Figure 6.17: Analytical solution (green) vs numerical solution (purple) by full MG.


Figure 6.18: Difference between the analytical solution and numerical solution of full MG.

### 6.1.3 Comparison

To compare the different methods used to solve the Poisson equation, number of iterations and the speed-up factor is presented. The speed-up factor is calculated basted on the measured CPU-time for a method with respect to the measured CPU-time for the Gauss Seidel method, see equation 6.3.

$$
\begin{equation*}
S=\frac{(C P U-t i m e)_{G S}}{(C P U-t i m e)_{m e t h o d}} \tag{6.3}
\end{equation*}
$$

For a multigrid algorithm, the iterations is counted only for post-iterations on a upward stoke. This is an approximation based on the cost done to preform an iteration on a coarser grid compared to the finest grid. Since an upward stoke consists of coarser grids too, all iteration counts are merged together to count on just one stoke (upward, because it have most iterations). Therefore, the full multigrid iterations will count less then the iterations done on a v-cycle, i.e. the full multigrid has maximum 8 iterations on the finest grid per time-step. Together with the speed-up factor, this will give a good enough result of the efficiency relation between the different methods.

The plot of the speed-up factor, 6.19, and the plot of iterations, 6.20 , have coinciding but opposite (ranging of the methods) results.

The Gauss Seidel method is clearly the slowest method, as expected. SOR will generally speed up the run-time 2-3 times and the two-step multigrid approximately 5 times, independent of number of grid points in the domain. Vcycle multigrid with depth more then two and the full multigrid method are dependent on number of grid points in the domain. On very coarse grids, they are not working optimal, therefore $h>\frac{1}{64}$ when using multigrid. The speed-up factor for the v-cycle algorithm will stagnate at approximately 15 for depth equals to three and 33 for depth equals to four. In a v-cycle it is not adequate to go
deeper then four depths. Therefor, in this solver it is possible to conclude with a maximum speed-up factor on 33 for the $v$-cycle algorithm.

For the full multigrid algorithm, the speed-up factor vary even more depending on number of grid cells. The reason for this is that the number of iterations in a full multigrid algorithm is independent of number of grid cells in the domain, distinct from the other methods (especially Gauss Seidel). Hence, it is clearly the fastest method to solve the Poisson equation. For the accuracy in the full multigrid algorithm, the RMS of the error in the solution domain will stabilize on an acceptable level when number of grid cells in the domain increases, according to plot 6.21.


Figure 6.19: The speed-up factor with respect to Gauss Seidel method. Purple: GS, green: SOR, light blue: two-step MG, orange: v-cycle d=3 MG, yellow: vcycle d=4 MG and dark blue: full MG.


Figure 6.20: Total number of iterations. Purple: GS, green: SOR, light blue: twostep MG, orange: v-cycle d=3 MG, yellow: v-cycle d=4 MG and dark blue: full MG.


Figure 6.21: RMS of the error in the domain for different number of grid cells. Purple: GS, green: SOR, light blue: v-cycle d=3 MG and orange: full MG.

### 6.2 Navier Stokes Solver

Several refinement tests are done to optimize the numerical result on the NavierStokes solver. The model in the refinement tests should be as similar to the actual test case as possible i.e. same geometry, fluid properties etc. Force coefficients for lift and drag are measured to compare the test results and to chose the the most proper refinement. The lift coefficient is measured as the maximum value over 10 periods at the end of the time-period. The drag coefficient is measured at the arithmetic average over 10 periods at the end of the timeperiod. Flow past a cylinder is a traditional fluid dynamic problem, and is therefore chosen as a test case. It is easy to find published experiments to compare result values with. The von Karmen vertex street in the wake of a cylinder has some characteristics which are useful to validate together with the forces and Strouhals number when vary the Reynolds number.

## Default case

The default test case is a channel flow with slip conditions at the walls, Dirichlet condition on the pressure at outflow and inflow velocity equals to $1.0 \mathrm{~m} / \mathrm{s}$, see figure 6.22 for more details. The domain $\Omega$ is [0:2]x[0:1]. The immersed boundary is stated by 50 points to create a proper circle and the diameter in the circle is equal to 0.1 and consists of approximately 12 cells. Reynolds number 20 and 100 are used to test the flow-field. The time-step $\Delta t$ is set to meet the stability criteria, i.e. $\Delta t_{R e=100}=0.001$ and $\Delta t_{R e=20}=0.0003$, and a time-series lasts to 30 $\sec ($ tmax $=30.0)$. All tests are done with the default test case when nothing else is specified. If any of the variables are specified later, the new value is the valid one.


Figure 6.22: The computational domain of the default case with BC's and domain size.

### 6.2.1 Time Refinement Test

A time refinement test is done for a time dependent problem to check the dependency between the time resolution and accuracy. Several tests are presented in table 6.1.

Table 6.1: Refinement of time.

| $\operatorname{Re}$ | $\Delta t$ | $C_{L}$ | $C_{D}$ |
| :---: | :---: | :---: | :---: |
| 20 | 0.001 | - | unstable |
|  | 0.0003 | - | 2.281875 |
|  | 0.0001 | - | 2.206216 |
|  | 0.00007 | - | 2.188227 |
|  | 0.00005 | - | 2.193227 |
| 100 | 0.001 | 0.249477 | 1.444527 |
|  | 0.0003 | 0.16241 | 1.378774 |
|  | 0.0001 | 0.141969 | 1.361831 |
|  | 0.00007 | 0.139043 | 1.359352 |
|  | 0.00005 | 0.137111 | 1.357709 |

The accuracy of the result is dependent of the time resolution in the solver. An explicit Euler scheme has a small stability area, hence considered as a less stable and more time-step restricted, i.e. need smaller time-steps, then other higher-order methods. All the tested $\Delta t$ for $\mathrm{Re}=100$ in table 6.1 are in the stable area for explicit Euler according to the stability analysis, but other factors may also influence the accuracy. Explicit Euler is a first-order accuracy method, thereby the result was expected and $\Delta t$ needs to be taken into consideration and may never converge. The optimal $\Delta t$ for the final test case should be chosen according to previous published experimental results and closes to the limit set by the stability criteria in the stable area.

### 6.2.2 Mesh Refinement Test

When using the FDM method, the accuracy of the solution is linked to the mesh size in the domain. When the mesh size decreases towards zero, the solution is moving toward the exact solution of the equation. Some limitations here are the time and limited computational resources. Therefore, it is important to find the optimal mesh size with an mesh refinement test where the goal is to minimize the error to a acceptable level depending on the analyzing goals.

In the mesh refinement tests, the mesh size is tested against the diameter of the cylinder, $\frac{D}{h}$, where $h=\Delta x=\Delta y$, i.e. an equidistant grid is kept. The test case setup is similar to the default case, but some changes are done for $\Delta t$. Only $\operatorname{Re}=$ 100 is tested for because of the high rate of changes in the velocity and pressure gradients trough the domain.

Table 6.2: Refinement of number of cells in cylinder diameter.

| Re | h | $\Delta t$ | $\frac{D}{h}$, cells | $C_{L}$ | $C_{D}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | $\frac{1}{64}$ | 0.006 | 6 | 0.119433 | 1.765178 |
|  | $\frac{1}{128}$ | 0.003 | 12 | 0.260477 | 1.498631 |
|  | $\frac{1}{256}$ | 0.0001 | 24 | 0.265365 | 1.497785 |

Table 6.3: Accuracy of the Poisson solver on domain [0:2]x[0:1].

| Number of cells (2nxn) | RMS of domain |
| :---: | :---: |
| $8192(\mathrm{n}=64)$ | $1.8068 \cdot 10^{-6}$ |
| $32768(\mathrm{n}=128)$ | $7.33725 \cdot 10^{-7}$ |
| $131072(\mathrm{n}=256)$ | $5.35976 \cdot 10^{-7}$ |

Another test is done to check the accuracy against an analytical solution, equation 6.2. To establish this test, the test problem from section 6.1 is used and the Poisson solver is tested. The difference between the numerical result and the analytical solution is calculated by a L2-norm (RMS) of the domain [0:2]x[0:1]. The results are presented in table 6.3.

Table 6.2 shows that the numerical results are dependent of the mesh resolution. The RMS of the solution differences in the domain are acceptable for all the tests. From table $6.2, \frac{D}{h}=12$ is has two decimals equals to $\frac{D}{h}=24$ for the force coefficients. Due to run-time of the time-series and the small difference in the solution coefficients, $\frac{D}{h}=12$ will be used in the final test case.

### 6.2.3 Domain Refinement Test

Different domain refinement tests are preformed to find the optimal refinement of the domain length $(\mathrm{L})$, domain width $(\mathrm{W})$ and the cylinder distance from the inflow (I). The results of the lift and drag coefficients for different L and W are presented in table 6.4 and table 6.5.

The force coefficients are not affected significantly by changing in the domain length. For $\mathrm{Re}=20$, this is as expected since no vortex shedding occur. For $R e=100$, this is more unexpected because of the large vortex velocity gradients that follows the von Karmen street downstream in the domain. The resolution of the vortex shedding is important, otherwise an unstable von Karmen street may distract the pressure distribution around the cylinder and effect oscillation of the drag force. $\mathrm{L}=20 \mathrm{D}$ is the longest possible construction of the domain and will be used for the final test case. It may turn out to not be long enough.

Table 6.4: Refinement of domin length.

| Re | L (length) | $C_{L}$ | $C_{D}$ |
| :---: | :---: | :---: | :---: |
|  | 12.5 D | - | 2.605942 |
|  | 15 D | - | 2.605528 |
| 20 | 17.5 D | - | 2.605466 |
|  | 20 D | - | 2.605461 |
| 100 | 12.5 D | 0.255942 | 1.444761 |
|  | 15 D | 0.25048 | 1.444593 |
|  | 17.5 D | 0.249475 | 1.444526 |
|  | 20 D | 0.248281 | 1.444507 |

In the domain refinement tests, the force coefficients are significantly affected by the change in the domain width. The coefficients are not converged properly, but $\mathrm{W}=17.5 \mathrm{D}$ will be used in the final test case and is the larges possible construction of the domain in the CFD-solver together with $\mathrm{L}=20 \mathrm{D}$.

Table 6.5: Refinement of domin width.

| $\operatorname{Re}$ | W (width) | $C_{L}$ | $C_{D}$ |
| :---: | :---: | :---: | :---: |
|  | 10 D | - | 2.605461 |
| 20 | 12.5 D | - | 2.515492 |
|  | 15 D | - | 2.461674 |
|  | 17.5 D | - | 2.426802 |
|  | 10 D | 0.248281 | 1.444507 |
| 100 | 12.5 D | 0.244023 | 1.407576 |
|  | 15 D | 0.240576 | 1.386462 |
|  | 17.5 D | 0.238610 | 1.373361 |

For the inflow refinement test, the length of the domain, $L$, is changed to 20D. This is done with respect to the length refinement test and are constant during domain inflow refinement test. The x-position in the cylinder center will vary depending on I and the length behind the cylinder will change between 13D-16D. If the cylinder is placed to close the inflow, the numerical solutions will be affected by the constant inflow velocity. The converged inflow coefficients are found for $I=6 D$, and will be used in the final test case.

Table 6.6: Refinement of domin inflow.

| Re | I (inflow) | $C_{L}$ | $C_{D}$ |
| :---: | :---: | :---: | :---: |
|  | 4 D | - | 2.443131 |
| 20 | 5 D | - | 2.426646 |
|  | 6 D | - | 2.425538 |
|  | 7 D | - | 2.425098 |
|  | 4 D | 0.310410 | 1.490689 |
|  | 5 D | 0.240358 | 1.386235 |
| 100 | 6 D | 0.238520 | 1.377452 |
|  | 7 D | 0.238758 | 1.376718 |

The domain refinement test are strongly dependent of the Reynolds number
because of the von Karmen vortex street. For higher Reynolds numbers, the test should be reverse.

### 6.2.4 Multigrid together with IBM

A final test case is made to test and analyses the results provided by a solver which used a multigrid method together with an IBM. To summarize the final test setup:
$L=20 \mathrm{D}$
$\mathbf{W}=17.5 \mathrm{D}$
$\mathbf{I}=6 \mathrm{D}$
$\Delta \mathbf{t}_{\mathbf{R e}=\mathbf{1 0 0}}=0.001$
$\frac{\mathrm{D}}{\mathrm{h}}=12$
$\mathbf{h}=\frac{1}{128}$
$\Delta \mathbf{t}_{\text {Re }=20}=0.0003$
The Poisson equation is solved with a full multigrid algorithm.
Strouhals number is a dimensionless frequency of the vortices which are shed from the body, given in equation 6.4. $f_{v}=\frac{1}{T_{v}}$ is the vortex shedding frequency, $T_{\nu}$ is a dimensionless time period, $D$ is the diameter of the body and $U_{\infty}$ is the inflow velocity.

$$
\begin{equation*}
S t=\frac{D f_{v}}{U_{\infty}} \tag{6.4}
\end{equation*}
$$

Table 6.7: Result from the final test case at $\mathrm{Re}=20$.

| Result source | $C_{D}$ |
| :---: | :---: |
| Present | 2.123974 |
| Taira and Colonius (2007) | 2.07 |
| Park et al. (1998) | 2.01 |
| Xu and Wang (2006) | 2.23 |

Table 6.8: Result from the final test case at $\operatorname{Re}=100$.

| Result source | $C_{L}$ | $C_{D}$ | Strouhals number |
| :---: | :---: | :---: | :---: |
| Present | 0.171374 | 1.281555 | 0.182 |
| Lai and Peskin (2000) scheme 1 | 0.3290 | 1.4630 | 0.144 |
| Lai and Peskin (2000) scheme 2 | 0.3299 | 1.4473 | 0.165 |
| Park et al. (1998) | 0.3321 | 1.33 | - |
| Xu and Wang (2006) | 0.34 | 1.423 | 0.171 |

Table 6.7 present the drag-coefficient at $\mathrm{Re}=20$. The coefficient for the present CFD-solver is lying in between the results from previous studies. Visualizations associated with the test are as expected and presented in figure 6.23 and 6.24.

For the test with $\mathrm{Re}=100$, several parameters are checked and presented in table 6.8. The Strouhals number is larger then from the other studies, but in an acceptable range. For the lift- and drag- coefficients, the previous studies presents much higher coefficients. As seen for the refinement tests, the coefficient values are more similar to those from previous studies. From the default case, only the domain size has been changed and the domain width had large impact on the coefficients. More thorough analyses should therefor be done on the domain before any conclusions are made. The visualizations of the pressure, velocities and streamlines, see figures 6.25 and 6.26 , are behaving as expected during the time-series.

The visualization defects of the velocities done in the post-processing stage should be taken into consideration when analyzing figures 6.24 and 6.26. This is described in subsection 5.8.


Figure 6.23: Pressure contours at $\mathrm{Re}=20$.


Figure 6.24: Pressure contours and velocity arrows at $\mathrm{Re}=20$.


Figure 6.25: Pressure contours at $\mathrm{Re}=100$.


Figure 6.26: Streamlines and velocity arrows at $\operatorname{Re}=100$.


Figure 6.27: Drag (green) and lift (purple) coefficients at $\mathrm{Re}=100$.

The displacement found in the Poisson solver for the Gauss Seidel algorithm generate a small contribution to the lift coefficient at Reynolds number 20. It may provide some contribution to the other coefficients too, but it is easier to notice in the lift coefficient calculations since it should have been zero. The produced error only differ $0.57 \%$ and will be neglected in all parts of the problem analysis.

### 6.2.5 Efficiency analysis

To analyses which part of the Navier Stokes solver who vast most of the running time, a time break-down of one time-step is presented for the final test case. Table 6.9 present the different parts in a Navier Stokes solver where the Gauss Seidel method is used in the Poisson solver and table 6.10 present the different parts in a Navier Stokes solver where a full multigrid algorithm is used in the Poisson solver. For both cases, it can be seen that the Poisson solver is the most decisive part, but there is an extreme difference by changing to full multigrid in the deflection on the print-out procedure. To illuminate, the print-out procedure will not run every time-step, only for visualization of the numerical result.

Table 6.9: Time break-down when using Gauss Seidel.

| Solution process | \% of the computational time |
| :---: | :---: |
| Poisson solver | $99.9 \%$ |
| IBM solver | $0.0 \%$ |
| Print-out procedure | $0.08 \%$ |
| Other | $0.02 \%$ |

Table 6.10: Time break-down when using full multigrid.

| Solution process | \% of the computational time |
| :---: | :---: |
| Poisson solver | $75.6 \%$ |
| IBM solver | $0.3 \%$ |
| Print-out procedure | $21.8 \%$ |
| Other | $2.3 \%$ |

## Chapter 7

## Conclusion and

## Recommendations for Further

## Work

### 7.1 Conclusions

To increase the calculation efficiency in a CFD-solver, investigation of the Poisson solver was mentioned. The vast majority of the run-time is spent at this process, and by solving it on a final test case with the iterative scheme Gauss Seidel minimum $99.9 \%$ of the computational time was spent here. A full multigrid method was developed and decreased the run-time of the Poisson solver with a factor of 110 (on a domain with 65536 grid-cells) compared to Gauss Seidel on a simple test case. The speed-up factor are related to the mesh resolution, but increases when the number of grid-cells increases. Consequently, the runtime spent on solving the Poisson equation in the CFD-solver on a final test case was reduced to minimum $75.6 \%$ with the full multigrid algorithm.

The CFD-solver with a full multigrid method was validated with an FSI problem solved by IBM. Force coefficients acting on a cylinder in a flow with Reynolds number 20 and 100 where used as reference values in several refinement tests. The accuracy of the resolution in the domain is significantly dependent on the size of $\Delta t$ in the numerical simulation. Explicit Euler has a small stability area which force $\Delta t$ to be quite small (depending on the problem) to provide reliable numerical results.

Areas of large velocity or pressure gradients need to have fine enough mesh resolution, e.g. areas close to the buff cylinder and in the von Karmen vortex street. Together with a large domain compared to the cylinder diameter, width should be at least 17.5 times the diameter and the length should be at least 20 times the diameter, the resolution is kept for $\mathrm{Re}=20$. The domain have a huge impact on the calculated force coefficients, so more thorough analysis should therefore be done on the domain to validate the numerical solution for $\mathrm{Re}=$ 100. In the next section some recommendations for further work and changes are provided to optimize the solver.

### 7.2 Recommendations for Further Work

In this section some recommendations for future work and changes are provided to optimize the solver.

### 7.2.1 Short-Term

One of the most important criteria for a CFD-solver is to provide accurate results in a certain time limit. To achieve that criteria for the present CFD-solver, the development of the domain and how to place the geometry in the flow should be reversed. A larger domain in both ( x - and y -) directions are preferred. To get a more versatile code, the IBM module should be validated for moving geometries and expand into a full fluid structure interaction solver.

Different experimentations consisting of changing the transformation schemes in multigrid to increase the efficiency could be done. The restriction procedure could for example be changed to full-weighted restriction, explained under chapter 3.

A part of the code which have potential for efficiency and accuracy increase of the numerical simulations without to much effort, is the temporal-discretization scheme. Explicit Euler is restricted to so small $\Delta t$ for this problem, hence a higher order Runge-Kutta scheme, see subsection 2.3.2, would use much less computational time.

### 7.2.2 Long-Term

If the CFD-solver shall work for turbulent or transitional flow, the resolution requires $3 D$ simulations. To capture all scales of motions $\Delta x_{i}$ and $\Delta t$ needs to be so small, hence a super computer and parallelization of the code is required. A CFD-solver with multigrid methods are highly parallelizable because each pro-
cesses can simultaneously be performed at all grid points. For more details of parallel multigrid processing see Brandt (1981).

To reduce the unnecessary computational effort preformed in the numerical simulation, adaptive grid refinement (subsection 2.2.2) should be included in the CFD-solver.

## Appendix A

## Acronyms and Symbols

Acronyms<br>CFD Computational Fluid Dynamics<br>IBM Immersed Boundary Method<br>SOR Successive Over Relaxation<br>GS Gauss Seidel<br>FSI Fluid Structure Interaction<br>MG Multigrid<br>GMG Geometric Multigrid<br>AMG Algebraic Multigrid<br>FMG Full Multigrid<br>FSI Fluid Structure Interactions<br>BC Boundary Condition

1D One-Dimension

2D Two-Dimensions

PM Projection Method
ODE Ordinary Differential Equation

PDE Partial Differential Equation

CFL Courant-Friedrichs-Lewy
FDM Finite Difference Method

FVM Finite Volume Method

FEM Finite Element Method

FTCS Forward-Time Central-Space

MAC Marker and cell
flops Floating Point Operations

RMS Root-mean square

CPU Central Processing Unit

## Symbols

$d$ Depth of an multigrid
$n$ Number of grid points
$\lambda$ Eigenvalue
$\Omega$ Computational domain
$\partial \Omega$ Boundary of domain
$\Omega_{b}$ Domain occupied by geometry
$\partial \Gamma_{b}$ Boundary of geometry
$\mathbf{f}_{\mathbf{b}}$ Forcing function
$h$ Grid cell-size, equidistant
$\Delta x_{i}$ Grid cell-size in x-direction (i=1) and y -direction ( $\mathrm{i}=2$ )
$t$ Time
$\Delta t$ Time-step
$x_{i}$ Cartesian coordinates, $(x, y)$
$u$ Velocity in x-direction
$v$ Velocity in y-direction
p Pressure
$\Delta p$ Change in pressure
$u^{*}$ Predicted velocity in x-direction
$v^{*}$ Predicted velocity in y -direction
$i$ Position in x-direction in a Cartesian grid
$j$ Position in y-direction in a Cartesian grid
$\rho$ Density
$v$ Kinematic viscosity

Re Reynolds number

St Strouhals number
$\mathscr{O}$
$\mathscr{R}$
n Normal vector
$\omega$ Damping coefficient
$\omega_{\text {opt }}$ Optimal damping coefficient
$C$ Courant number
$C_{\max }$ Criteria for CFL-condition
$I_{h}^{2 h}$ Restriction operator/matrix
$I_{2 h}^{h}$ Prolongation operator/matrix
$k$ Iteration counter
$\boldsymbol{e}$ Error
r Residual
f Right-hand side of a linear system

A Coefficient matrix in a linear system
$s$ Solve with iteration
$e$ Solve exact or with iteration
$r$ Restrict the system
p Prolongate the system
$\gamma$ Number of cycles in multigrid
$\nu_{1}$ Number of pre-iterations
$v_{2}$ Number of coarse-iterations
$\nu_{3}$ Number of post-iterations
$\beta$ convergence factor
$U_{i, j}$ Fluid velocity in a cell next to an immersed boundary
$C_{L}$ Lift coefficient
$C_{D}$ Drag coefficient
$F_{D}$ Drag force
$F_{L}$ Lift force
$U_{\infty}$ Inflow velocity
$f_{\nu}$ vortex shedding frequency
$T_{\nu}$ vortex shedding period

I Inflow length in domain

L Domain length

W Domain width

## Appendix B

## Source code

Listing B.1: head.h, all functions.

```
#ifndef Header_Header
#define Header_Header
int main();
void FDMsolver(double **, double **, double **);
void linearSolver(double t, double **, double **, double **, double **deltaP);
void multigrid(double t, double **, double **, double **, double **deltaP);
void GaussSeidel(int imax, int nn, double **f, double **phi, int *iter, double *res,
    double *error);
void SOR(int nn, double **f, double **phi, int *iter, double *res, double *error);
void correctVelo(int nn, double **, double **, double **deltaP, double **uFlag,
    double **vFlag);
void presCorr(int nn, double **p, double **deltaP);
void velBCfield(int nn, double **, double **);
void pBCfield(int nn, double **);
double residual(int nn, double **f, double **phi, int i, int j);
void weightedResidual(int nn, double **RHS, double **phi, double **R);
void injectedResidual(int nn, double **RHS, double **phi, double **R);
void injected(int nC, double **R);
void weighted(int nC, double **R);
void interpolation(int nC, double **E);
void addValue(int nn, double **E, double **phi);
20 void presCorr(int nn, double **p, double **deltaP);
```

```
void solveCoarse(double **phi, double **f);
void startResidual(int nF, double **RHS, double **phi, double **R);
void stream(double **, double **, double **);
void results (double **, double **, double **, double **, double **, double **,
    double **, double **, double **);
void IC(int, double **, double **, double **);
void validatePoisson();
void stability(void);
double avg(int nn, double ** matrix);
void CFL(double, double);
double maxNorm(int nn, double ** matrix);
double RMS(int nn, double **x);
double sum(int nn, double **matrix);
void toZero(int dim, double **matrix);
void toZeroM(int dd, double *** matrix);
void arrayMatrix(int nn, double ***array, double **matrix, int dd);
void matrixArray(int nn, double **matrix, double ***array, int dd);
void copy(double *** from, double *** to, int dd);
void ccopy(double **from, double **to);
double interp(void);
double linearInterp(double nn, double x0, double xl, double y0, double yl);
int powerOf(int k);
int log_2(int n);
//____ From the included file nrutil.c-__-_-_-_-_-_-_-_-_-_-_-_-_-_
void free_dmatrix(double **m, long nrl, long nrh, long ncl, long nch);
double **dmatrix(long nrl, long nrh, long ncl, long nch);
double ***f3tensorD(long nrl, long nrh, long ncl, long nch, long ndl, long ndh);
void free_f3tensorD(double ***t, long nrl, long nrh, long ncl, long nch,
    long ndl, long ndh);
void nrutil();
#endif
```


## Listing B.2: input.h, file to change input variables.

```
#ifndef SHAREFILE_INCLUDED
#define SHAREFILE_INCLUDED
#ifdef MAIN_FILE
/*------ Input variables
    const int n = 128; //Numer of internal cells
    const double epsi = 0.000001; // Error
    const int Re=100; //Reynholds number }->>\mathrm{ (RealRe/2*radius)
    const double rho = 1.0; // Density
    const double nu = 0.05; // Kinematic viscosity
    const double tmax = 30.0; //End time
    const double dt = 0.00001; //Time stepsize
    const int itmax = 500; //Max inerations
    const int itPre = 2; //Max inerations - PRE-smoothing MG
    const int itCoarse = 35; //Max iterations - COARSE-smoothing MG
    const int itPost = 8; //Max inerations - POST-smoothing MG
/*-__ Set wall type and velocity ___-___*/
    const int wall = 3; //1:Lid driven top,2:Couette flow,3:Channel-velocity,
        //4:No-slip channel flow,5:Preiodic-free-slip,6: Poiseuille flow
    const double velX = 1.0; //Stream velocity - x direction [m/s]
    const double velY = 0.0; //Stream velocity - y direction [m/s ]
    const double dimX = 1.0; // Scaling factor in x-dim
    const double dimY = 1.0; //Scaling factor in y-dim
    const int method = 2; //1: Gauss Seidel, 2:SOR, 3:two-grid iteration 4:V-cycle
        multigrid, 5:Full-multigrid
    const int d=0; //Depth of multigird }->>n=512, 256, 128, 64, 32, 16, 8, 4, 2. 
        d have to be at least 2.
    const int ncycle = 0; //Number of repeated V-cycles in multigrid
/*---_ IBM
```

$\qquad$

```
    const int runIBM = 1; //0:not run, 1:run
    const int calcForce = 1; // 0:not calculate forses, 1: calculate forces
    const int bType = 3; //1:random points as a simple polygon,
        //2:two lines-equal number of points (nPoint/2), 3:circle
    const int nPoint = 50; //Number of points to form the geometry
```

```
    const int bMotion = 0; //0: No body motion, 1: Body motion on
    const int mDir = 1; //0 = x-dir, l = y-dir of motion
    const double bFreq = 6.28; //MMotion frequency of the body, approx 2*pi
    const double bAmp = 0.001; //Motion amplitude of the body
    const double nMotion = 10; //Number of motion cycles.
    //Max and min positions of the geometry in domain
    const double xmin = 0.45;
    const double xmax = 0.55;
    const double ymin = 0.45;
    const double ymax = 0.55;
    const int maxIntersec = 500;
    //Simple polygon or two lines, {x-coord},{y-coord}
    const double pointPos[2][4] = {{0.0, 1.0, 1.0, 0.0},{0.90625, 0.90625, 0.09375,
        0.09375}};
    / / Cylinder
    const double CG[2] = {0.5,0.5};//Mass center of cylinder
    const double radius = 0.05; //Radius of cylinder
/*-_ Intervall for writing out to screen and vtf-file -__-_*/
    const int writeOut = 500; //Write out intervall for vtf-file
    const int printOut = 1; //Print out to terminal
```



```
    const int validate = 0; //0:no validation 1:Poisson validation
#else
    extern int n, Re, itmax, wall, nr, bType, nPoint, maxIntersec, method, runIBM, d,
        ncycle, itPre, itPost, itCoarse;
    extern int bMotion, mDir, calcForce, fromYin, toYin, fromYout, toYout, writeOut,
        printOut, validate;
    extern double epsi, tmax, dt, velX, velY, xmin, xmax, ymin, ymax, radius, rho,
        bFreq, bAmp, nMotion, nu, dimX, dimY;
    extern double elementl[5], element2[2], pointPos[2][50], CG[2];
#endif
#endif
```


## Listing B.3: main.c, main file of the solver.

```
#include "head.h"
#include <math.h>
#include <stdio.h>
#include <stdlib.h>
#include "nrutil.h"
#define MAIN_FILE
#include "input.h"
void printFile(double, double **, double **, double **, double [4][nPoint]);
void IBM(double t, double **, double **, double body[4][nPoint], double **uFlag,
    double **vFlag);
void setBody(double t, double body[4][nPoint]);
```



```
int main()
{
```



```
    int saveOut, newIC, step, time;
    int i, j, iter = 0, countW = 1, countP = 1, id;
    double omega, beta, div = 0.0, integer, divMax, diff;
    double **u, **v, **p, body[4][nPoint], fraction;
    double **uFlag, **vFlag, **deltaP;
    p = dmatrix (0, (int) (dimX*n) +2, 0, (int)(dimY*n) +2);
    u = dmatrix (0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);
    v = dmatrix (0, (int) (dimX*n) +2, 0, (int)(dimY*n)+2);
    deltaP = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    uFlag = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
    vFlag = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
```



```
    stability();
    if (validate == 1){printf("VALIDATION \n");validatePoisson();}
    else
    {
    /*-- Set initial conditions for primitive-variables --*/
    IC(newIC, u, v, p);
    toZero(n, deltaP);
    toZero(n, uFlag);
```

```
toZero(n, vFlag);
velBCfield(n, u, v);
/*-_______-_ Time iteration, main loop
                                    */
for (double t = 0; t <= tmax; t = t+dt)
    {
        step = (int)(t/dt) + 1;
        fraction = modf(step/printOut, &integer);
        /*Set body and calculate body motions if start motion is given*/
        setBody(t, body);
        /*-_-_-FSM predictor (Use FTCS-scheme with staggered grid) ---*/
        FDMsolver(u, v, p);
        velBCfield(n, u, v);
```



```
    if (runIBM == 1)
    {
        if (fraction == 0.0 && step == (printOut*integer)){printf("RUN IBM\n");}
        IBM(t, u, v, body, uFlag, vFlag);
        }
        /*-_______________________________
        iter = 0;
        if (method == 1 || method == 2)
        {
        if (fraction == 0.0 && step == (printOut*integer)){printf("LINEAR SOLVER \n"
    );}
            linearSolver(t, u, v, p, deltaP);
        }else if (method == 3 || method == 4 || method == 5)
        {
            if (fraction == 0.0 && step == (printOut*integer)){printf("MULTIGRID \n");}
            multigrid(t, u, v, p, deltaP);
        } else
            {
                printf("Error in choice of method,\n");
                printf("method = 1, method = 2 OR method = 3.\n");
                exit (1);
            }
        if (fraction == 0.0 && step == (printOut*integer)){printf("t = %f \n\n\n", t)
    ;}
```



```
    correctVelo(n, u, v, deltaP, uFlag, vFlag);
    velBCfield(n, u, v);
```



```
    printFile(t, u, v, p, body);
    }
}
free_dmatrix (p, 0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
free_dmatrix (u, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
free_dmatrix(v, 0, (int)(dimX*n) +2, 0, (int) (dimY*n) +2);
free_dmatrix(deltaP, 0, (int) (dimX*n) +2, 0, (int)(dimY*n)+2);
free_dmatrix(uFlag, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
free_dmatrix(vFlag, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
return 0;
87 }
```


## Listing B.4: solver.c, FDM-scheme.

```
#include "head.h"
#include <math.h>
#include <stdio.h>
#include <stdlib.h>
#include "input.h"
void FDMsolver(double **u, double **v, double **p)
{
    int i, j;
    double h = 1./n;
    double fux, fuy, fvx, fvy, visu, visv, pdu, pdv;
    for (i = 1; i <= (int)(dimX*n); i++)
        {
        for (j = 1; j <= (int)(dimY*n); j++)
{
            //Advective terms
    fux = (powf(u[i][j] + u[i+1][j],2) - powf(u[i-1][j] + u[i][j],2))* (0.25/h);
    fuy = (((v[i][j] + v[i+l][j]) * (u[i][j] + u[i][j+1])) - ((v[i][j-1] + v[i+1][j
        -1]) * (u[i][j-1] + u[i][j]))) * (0.25/h);
    fvx = (((u[i][j] + u[i][j+1]) * (v[i][j] + v[i+l][j])) - ((u[i-1][j] + u[i-1][j
        +1])* (v[i-1][j] + v[i][j]))) * (0.25/h);
    fvy = (powf(v[i][j] + v[i][j+1],2) - powf(v[i][j-1] + v[i][j],2)) * (0.25/h);
        //viscous terms = nu*laplacian/
    visu = (u[i+1][j] + u[i-1][j] + u[i][j+l] + u[i][j-1] - 4.0*u[i][j]) / (Re*powf(
        h,2));
    visv = (v[i+l][j] + v[i-1][j] + v[i][j+l] + v[i][j-1] - 4.0*v[i][j]) / (Re*powf(h
        ,2));
        //Pressure gradient/
        pdu = (p[i][j] - p[i+1][j])/h;
        pdv = (p[i][j] - p[i][j+1])/h;
    //PM-predrictor (u and v tilde), pdu - fux - fuy + visu = RHS /
    u[i][j] = u[i][j] + dt*(pdu - fux - fuy + visu);
    v[i][j] = v[i][j] + dt*(pdv - fvx - fvy + visv);
```

```
44 if (u[i][j] != u[i][j])
    {
    printf("NaN or inf achieved, program aborted... \n");
    exit(EXIT_FAILURE); // Exit program
    }
}
}
1 }
```

Listing B.5: IBM.c, all functions.

```
#include <math.h>
#include <stdio.h>
#include <stdlib.h>
#include "head.h"
#include "input.h"
/*Functions used in this file*/
void setBodyIBM(double xa, double xb, double ya, double yb, double body[4][nPoint],
    double bodyPos[2][nPoint], double bodyVel[2][nPoint]);
void gridShifting(double gridShift[2][n], int xDim, int yDim, int);
void intersectionP(int *nIntersec, int, int xDim, int yDim, int intersecInfo[3][
    maxIntersec], double intersecValue[3][maxIntersec], double bpdyPos[2][nPoint]);
void velocity(int nIntersec, double xa, double ya, double bodyPos[2][nPoint], double
    bodyVel[2][nPoint], int intersecInfo[3][maxIntersec], double intersecValue[3][
    maxIntersec], double **u, double **v,
double **uFlag, double **vFlag, double *Cl, double *Cd);
void IBM(double t, double **u, double **v, double body[4][nPoint], double **uFlag,
    double **vFlag)
{
    int nIntersec = 0;
    double h = 1./n, Cl=0, Cd=0;
    /*Domain around body, starting from zero, see report*/
    double xa = (bType == 2) ? 0.0:floor (xmin/h)*h, xb = (bType == 2) ? n*h:ceil (xmax/
        h)*h, ya = (bType == 2) ? 0.0:floor (ymin/h)*h, yb = (bType == 2) ? n*h:ceil (ymax
        /h) *h;
    int xDim, yDim; //Dimensions of the sorunding domain
    /*Define martix*/
    double bodyPos[2][nPoint], bodyVel[2][nPoint];
    double intersecValue[3][maxIntersec];
    int intersecInfo[3][maxIntersec];
    FILE *fileForce;
    xDim = (int) ((xb - xa) /h); yDim = (int) ((yb - ya)/h);
    setBodyIBM(xa, xb, ya, yb, body, bodyPos, bodyVel);
    //Finds intersectionInfo and Value for each intersection
    intersectionP(&nIntersec, 1, xDim, yDim, intersecInfo, intersecValue, bodyPos);
```

```
//Calculation the interpolated velocities
velocity(nIntersec, xa, ya, bodyPos, bodyVel, intersecInfo, intersecValue, u , v,
    uFlag, vFlag, &Cl, &Cd);
    //Print Forces to file
    if (calcForce == 1)
    {
        fileForce = fopen("Force_calculations.txt", "a");
        fprintf(fileForce, "%f %f %f \n", t, Cl, Cd);
        fclose(fileForce);
    }
}
|*================================================================*/
```



```
/ *==================================================================*/
void setBody(double t, double body[4][nPoint])
{
    /*Internal variables*/
    double h = 1./n, dTheta, theta, integer;
    int step = (int)(t/dt) + l;
    double fraction = modf(step/printOut, &integer);
    /*Set body values*/
    if (bType == 1 || bType == 2)
    {
        for (int point = 0; point < nPoint; point ++)
        {
            body[0][point] = pointPos[0][point]; //x-pos
            body[1][point] = pointPos[1][point]; //y-pos
            body[2][point] = 0.0; //u-vel
            body[3][point] = 0.0; //v-vel
        }
    }else if (bType == 3) // Cylinder
    {
        dTheta = 2*M_PI/nPoint;
        for (int point = 0; point < nPoint; point ++)
        {
            theta = point*dTheta;
            body[0][point] = CG[0] + radius*\operatorname{cos(theta);}
```

```
        body[1][point] = CG[1] + radius*sin(theta);
        body[2][point] = 0.0;
        body[3][point] = 0.0;
    }
    }else
    {
        printf("\n");
        printf("Fatal error when finding body values\n");
        printf("Not a valid body type.\n");
        exit (1);
    }
    //Apply body motions
    if (bMotion == 1 && bType == 3 && bFreq*t <= nMotion*2*M_PI)
    {
        if (fraction == 0.0 && step == (printOut*integer)){printf("IN MOTION\n");}
        for (int point = 0; point < nPoint; point ++)
        {
            body[mDir][point] += bAmp*(sin(bFreq*t));
            body[mDir+2][point] = bAmp*bFreq*\operatorname{cos(bFreq*t);}
        }
    }
    return;
}
/*
*================================================================*/
void setBodyIBM(double xa, double xb, double ya, double yb, double body[4][nPoint],
        double bodyPos[2][nPoint], double bodyVel[2][nPoint])
{
    /*Internal variables*/
    double h = 1./n;
    /*Error if the sorunding domain is less than two cells from the boundary of the
        computional domain*/
    if ((xa < 2*h || xb > (n*h - 2*h) || ya < 2*h || yb > (n*h - 2*h)) && bType != 2)
    {
        printf("\n");
        printf("Fatal error when using IBM\n");
```

```
    printf("The body is to close the boundary for the computional domain.\n");
        printf("Need at least two cells = %f distance\n", 2*h);
        exit (1);
    }
    for (int point = 0; point < nPoint; point ++)
        {
        bodyPos[0][point] = body[0][point] - xa;
        bodyPos[1][point] = body[1][point] - ya;
        bodyVel[0][point] = body[2][point]; // 0.0;
        bodyVel[1][point] = body[3][point]; //0.0;
        }
    return;
}
```



```
void gridShifting(double gridShift[2][n], int xDim, int yDim, int state)
{
    double h = 1./n;
    /*set values*/
    for (int vLine = 0; vLine < xDim; vLine++)
    {
        gridShift[0][vLine] = (vLine + 0.5*state ) *h;
    }
    for (int uLine = 0; uLine < yDim; uLine++)
    {
        gridShift[1][uLine] = (uLine + 0.5*state ) *h;
    }
    return;
}
l*====================================================================================*/
/*Find intersections positions (x,y) between body boundary and computional grid */
void intersectionP(int *nIntersec, int state, int xDim, int yDim, int intersecInfo
    [3][maxIntersec], double intersecValue[3][maxIntersec], double bodyPos[2][nPoint
    ])
```

```
/*Goal: find intersection points in x and y position,
    find the distance from the cloasest outer velocity in intersection direction
    */
    int count = 0, pointPlusEn, dummyl = 0, dummy2 = 0, dummy3 = 0;
    double h = 1./n, diff = h/10.0, pdy, pdx, ppdx, ppdy;
    double gridShift[2][n];
    //Set values for the soroundin grid at u- and v- lines
    gridShifting(gridShift, xDim, yDim, state);
    //Iterating trough points to find intersection points
    for (int point = 0; point < nPoint; point ++)
    {
    pointPlusEn = (point == nPoint -1) ? 0:point+1;
    pdx = bodyPos[0][pointPlusEn] - bodyPos[0][point];
    pdy = bodyPos[1][pointPlusEn] - bodyPos[1][point];
    //Finding intersection points close to velocity-lines in v-direction.
    for (int vLine = 0; vLine < xDim; vLine ++)
    {
        // If pointPlusEn has larger x-position compared to point
        if(bodyPos[0][pointPlusEn] > bodyPos[0][point]){int dd = point; dummy3 = 1;
        point = pointPlusEn; pointPlusEn = dd;}
            if ( (gridShift[0][vLine] >= bodyPos[0][pointPlusEn]) && (bodyPos[0][point] >=
        gridShift[0][vLine]))
        {
            intersecInfo[0][count] = 2; //intersection wall
            if (dummyl == 1 ) { dummyl = 0; pointPlusEn = 0; point = nPoint - 1;}
            else if (dummy3 == 1 ){int dd = point; dummy = 0; point = pointPlusEn;
        pointPlusEn = dd;}
            intersecInfo[1][count] = point;
            intersecInfo[2][count] = pointPlusEn;
            intersecValue[0][count] = (-pdx > 0) ? 1:-1;
            intersecValue[l][count] = gridShift[0][vLine]; //x-pos
            intersecValue[2][count] = bodyPos[1][point] - ((bodyPos[0][point]-gridShift
        [0][vLine])/pdx)*pdy; //y-pos
            count += 1;
        }
```

```
// Return dummy 3
    if( dummy == 1 ){int dd = point; dummy 3 = 0; point = pointPlusEn; pointPlusEn =
        dd;}
    }
    for (int uLine = 0; uLine < yDim; uLine ++)
    {
        // If pointPlusEn has larger y-position compared to point
        if(bodyPos[1][pointPlusEn] > bodyPos[1][point]){int dd = point; dummy2 = 1;
        point = pointPlusEn; pointPlusEn = dd;}
        if ( (gridShift[l][uLine] >= bodyPos[1][pointPlusEn]) && (bodyPos[1][point] >=
        gridShift[1][uLine]))
        {
        intersecInfo[0][count] = 1; //intersection wall
        if (dummyl == 1 ){dummyl = 0; pointPlusEn = 0; point = nPoint-1;}
        else if (dummy2 == 1 ){int dd = point; dummy2 = 0; point = pointPlusEn;
        pointPlusEn = dd;}
        intersecInfo[1][count] = point;
        intersecInfo[2][count] = pointPlusEn;
        intersecValue[0][count] = (pdy > 0) ? 1:-1;
        intersecValue[1][count] = bodyPos[0][pointPlusEn] - ((bodyPos[1][pointPlusEn
        ]-gridShift[1][uLine])/pdy)*pdx; //x-pos
        intersecValue[2][count] = gridShift[1][uLine]; //y-pos
        count += 1;
        }
        //Return dummy 2
        if (dummy2 == l ){int dd = point; dummy2 = 0; point = pointPlusEn; pointPlusEn
        = dd;}
        }
        //Return dummy 1
        if (dummyl == 1 ) {point = nPoint - 1; dummyl = 0;}
    /*Error if there is to many intersection points compared to the allocated matrix*/
    if (count >= maxIntersec)
    {
        printf("\n");
        printf("Fatal error when using IBM\n");
        printf("There is to many intersection points compared to the allocated matrix.\n
        ") ;
```

```
    printf("maxIntersec needs to be larger than %i\n", maxIntersec);
    exit (1);
    }
}
    *nIntersec = count; //Total number of intersections
    return;
```



```
l*====================================================================*/
//Finding IBM velocities with linear interpolation
void velocity(int nIntersec, double xa, double ya, double bodyPos[2][nPoint], double
        bodyVel[2][nPoint], int intersecInfo[3][maxIntersec], double intersecValue[3][
        maxIntersec], double **u, double **v, double **uFlag, double **vFlag, double *Cl
    , double *Cd)
{
    int line, node;
    double intersecVel, nodeVel, h = 1./n, Fl = 0.0, Fd = 0.0;
    double **uInterP, **vInterP; //Interpolated velocities
    double **fx, **fy; //Forcing terms. Force from body on fluid cells due to
        acceleration
    uInterP = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n) +2);
    vInterP = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    fx= dmatrix (0, (int) (dimX*n) -2, 0, (int) (dimY*n) -2);
    fy= dmatrix (0, (int) (dimX*n) -2, 0, (int) (dimY*n) -2);
    toZero(n, uInterP);
    toZero(n, vInterP);
    toZero(n, uFlag);
    toZero(n, vFlag);
    toZero(n-4, fx);
    toZero(n-4, fy);
    for (int i = 0; i < nIntersec ; i++)
    {
        if (intersecInfo[0][i] == 1)
    {
```

\}

```
//Find current velocity at intersection points from the cegment between the nodes/
intersecVel \(=\) linearInterp (intersecValue [2][i], bodyPos[1][intersecInfo[1][i ]], bodyPos[1][intersecInfo[2][i]], bodyVel[0][intersecInfo[1][i]], bodyVel[0][ intersecInfo[2][i]]);
//The number on \(u\)-velocity line in \(y\)-dir (where 1 is the \(u\)-velo corresponding to node 1)
line \(=(\) int \()((\) intersecValue \([2][i] / h)+0.5+\) floor \((y m i n / h))\);
//The nearest fluid node in \(x\)-dir. Starting from 1 , node 0 is the node outside the surounding domain.
node \(=(\) int \()(\) rint \(((\) intersecValue [1][i]/h) + intersecValue[0][i]*0.51) + floor \((\) xmin/h)) ;
//Impose the IBM conditions on the fluid/computional grid/
nodeVel \(=\) linearInterp (node \(*\) h , intersecValue[l][i] + xa, (node+intersecValue [0][i])*h, intersecVel, u[(int)(node+intersecValue [0][i])][line]);
//Forcing terms/
\(\mathrm{fx}[\) node] [line] \(=\mathrm{fx}[\) node][line] \(-((\) nodeVel \(-\mathrm{u}[\) node][line ] \() / \mathrm{dt}) *\) rho \(* \mathrm{~h} * \mathrm{~h}\);
//Store interpolated velocity/
u [node][line] \(=\) nodeVel;
//Flag the corrected velocity, PM-solver should not calculate it one more time uFlag[node][line] \(=1.0 ;\)
\}else if (intersecInfo[0][i] == 2)
\{
//Find current velocity at intersection points from the cegment between the nodes/
intersecVel \(=\) linearInterp(intersecValue[1][i], bodyPos[0][intersecInfo[1][i
]], bodyPos[0][intersecInfo[2][i]], bodyVel[1][intersecInfo[1][i]], bodyVel[1][ intersecInfo[2][i]]);
//The number on \(v\)-velocity line in \(x\)-dir (where \(l\) is the \(v\)-velo corresponding to node 1)
line \(=(\) int \()((\) intersecValue \([1][i] / h)+0.5+\) floor \((x m i n / h)) ;\)
//The nearest fluid node in \(y\)-dir
node \(=(\) int \()(\) rint \(((\) intersecValue \([2][i] / h)+\) intersecValue [0][i]*0.51) + floor \((\) ymin/h)) ;
//Impose the IBM conditions on the fluid/computional grid/
nodeVel \(=\) linearInterp (node \(*\) h , intersecValue [2][i] + ya, (node+intersecValue [0][i]) *h, intersecVel, v[line][(int)(node+intersecValue[0][i])]);
//Forcing terms/
```

```
        fy[line][node] = fy[line][node] - ((nodeVel-v[line][node]) / dt)*rho*h*h;
        //Store interpolated velocity/
        v[line][node] = nodeVel;
        //Flag the corrected velocity, PM-solver should not calculate it one more time
        vFlag[line][node] = 1.0;
    }
    }
    //Calculate forces
    if (calcForce == 1)
    {
        for (int i = 0; i <= (int) (dimX*n) -2; i++)
            {
            for (int j = 0; j <= (int) (dimY*n) -2; j++)
            {
                    Fl += fy[i][j];
                Fd += fx[i][j];
            }
            }
        * Cl = 2.0*Fl/(2*radius); // Cl = 2*Fl/(rho*V^2*A)
        *Cd}=2.0*\textrm{Fd}/(2*\mathrm{ radius });//\textrm{Cd}=2*\textrm{Fd}/(\operatorname{rhod}*\mp@subsup{\textrm{V}}{}{\wedge}2*\textrm{A}
    }
    free_dmatrix(uInterP, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    free_dmatrix(vInterP, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    free_dmatrix(fx, 0, (int) (dimX*n) -2, 0, (int) (dimY*n)-2);
    free_dmatrix (fy, 0, (int) (dimX*n) -2, 0, (int) (dimY*n) -2);
    return;
}
/*
```



```
/*===================================================================*/
double linearInterp(double nn, double x0, double x1, double y0, double yl)
{
    double linearInterp;
    /* nn = interp point
        x0 = boundary point, known function valuelvalue required as left operand of
        assignment
    xl = boundary point, known function value
    y0 = function value at x0
```

```
\stackrel{~}{~}
    yl = function value at xl
    */
    return linearInterp = y0 +((yl-y0)*fabs(nn-x0))/fabs(xl-x0);
304 }
```


## Listing B.6: linearSolver.c, Gauss Seidel method and SOR method is found here.

```
#include <math.h>
#include <stdio.h>
#include "head.h"
#include "input.h"
void linearSolver(double t, double **u, double **v, double **p, double ** deltaP)
{
    int print, iter = 0;
    double **RHS, div, h = 1./n, res = 0.0, error = 0.0, integer;
    int step = (int)(t/dt) + l;
    double fraction = modf(step/printOut, &integer);
    RHS = dmatrix (0, (int)(dimX*n)+2, 0, (int) (dimY*n)+2);
    toZero(n, RHS) ;
    //Forming the right hand side of the poisson equation rho/dt*div(u_tilde):
    for (int j = 1; j <= (int)(dimY*n); j++)
        {
        for (int i = 1; i <= (int)(dimX*n); i++)
    {
    div = (u[i][j] - u[i-1][j] + v[i][j] - v[i][j-1])/h; //Here, h = dx = dy
                RHS[i][j] = div/dt;
            }
    }
```



```
    if (method == 1)
    {
        GaussSeidel(itmax, n, RHS, deltaP, &iter, &res, &error);
        if (fraction == 0.0 && step == (printOut*integer))
    {
        printf("GAUSS SEIDEL \n");
        printf("Iterations: %i \n", iter);
        printf("Residual: %f. \n\n", res);
    }
    }else if (method == 2)
    {
        SOR(n, RHS, deltaP, &iter, &res, &error);
        if (fraction == 0.0 && step == (printOut*integer))
        {
```

```
    printf("SOR \n");
        printf("Iterations: %i \n", iter);
        printf("Residual: %f. \n\n", res);
    }
    }
    if (fraction == 0.0 && step == (printOut*integer))
        {
        printf("\nTotal nr of iterations: %i \n", iter);
        printf("End residual: %g \n", res);
    }
```



```
    presCorr(n, p, deltaP);
    free_dmatrix (RHS, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    return;
2 }
```




```
// Correct velocities without overwriting interpolated velocities from IBM
void correctVelo(int nn, double **u, double **v, double **deltaP, double **uFlag,
        double **vFlag)
{
    double h = 1./nn;
    if (runIBM == 1) //IBM
        {
        for (int j = 1; j <= (int)(dimY*nn); j ++)
{
    for (int i = 1; i <= (int)(dimX*nn); i++)
        {
                if (uFlag[i][j] == 1 && vFlag[i][j] == 1)
                {
                    continue; //Continue the for-loop
                }else if (uFlag[i][j] == 1)
                {
            v[i][j] = v[i][j] - (1/rho)*(dt/h)*(deltaP[i][j+l] - deltaP[i][j]);
                }else if (vFlag[i][j] == 1)
            {
```

```
                u[i][j] = u[i][j] - (l/rho)*(dt/h)*(deltaP[i+l][j] - deltaP[i][j]);
                    } else
                {
                u[i][j] = u[i][j] - (l/rho)*(dt/h)*(deltaP[i+l][j] - deltaP[i][j]);
                v[i][j] = v[i][j] - (l/rho)*(dt/h)*(deltaP[i][j+l] - deltaP[i][j]);
                }
            CFL(u[i][j], v[i][j]); //CFL-condition
    }
}
    } else
    {
        for (int j = 1; j <= (int)(dimY*nn); j ++)
{
    for (int i = 1; i <= (int)(dimX*nn); i ++)
        {
        u[i][j] = u[i][j] - (l/rho)*(dt/h)*(deltaP[i+1][j] - deltaP[i][j]);
        v[i][j] = v[i][j] - (l/rho)*(dt/h)*(deltaP[i][j+1] - deltaP[i][j]);
        CFL(u[i][j], v[i][j]); //CFL-condition
    }
}
    }
    velBCfield(nn, u, v);
    return;
}
```



```
/*-
void presCorr(int nn, double **p, double ** deltaP)
{
    double avgPress, h = 1./nn;
    for (int j = 1; j <= (int)(dimY*nn); j++)
        {
            for (int i = l; i <= (int)(dimX*nn); i++)
{
    p[i][j] = p[i][j] + deltaP[i][j];
}
    }
```

```
    if (wall == 5 || wall == 6)
```

    if (wall == 5 || wall == 6)
    {
    {
        avgPress = avg(nn, p);
        avgPress = avg(nn, p);
        for (int j = 1; j <= (int) (dimY*nn); j++)
        for (int j = 1; j <= (int) (dimY*nn); j++)
            {
            {
            for (int i = 1; i <= (int) (dimX*nn); i++)
            for (int i = 1; i <= (int) (dimX*nn); i++)
        {
        {
                p[i][j] = p[i][j] - avgPress;
                p[i][j] = p[i][j] - avgPress;
                }
                }
            }
            }
    }
    }
    pBCfield(nn, p);
    pBCfield(nn, p);
    return;
    return;
    }

```


```

void GaussSeidel(int imax, int nn, double **f, double **phi, int *iter, double *res,

```
void GaussSeidel(int imax, int nn, double **f, double **phi, int *iter, double *res,
    double *error)
    double *error)
{
    double h = 1./nn, **phiDiff, **phiPrev, **phiErr;
    double h = 1./nn, **phiDiff, **phiPrev, **phiErr;
    double residual = 0.0, testl, integer;
    double residual = 0.0, testl, integer;
    int it;
    int it;
    phiDiff = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    phiDiff = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    phiErr = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
    phiErr = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
    phiPrev = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    phiPrev = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    *iter = 0;
    *iter = 0;
    for (it = 1; it <= imax; it++)
    for (it = 1; it <= imax; it++)
        {
        {
        toZero(nn, phiDiff); toZero(nn, phiPrev); toZero(nn, phiErr);
        toZero(nn, phiDiff); toZero(nn, phiPrev); toZero(nn, phiErr);
        for (int j = 1; j <= (int) (dimY*nn); j++)
        for (int j = 1; j <= (int) (dimY*nn); j++)
            {
            {
            for (int i = 1; i <= (int) (dimX*nn); i++)
            for (int i = 1; i <= (int) (dimX*nn); i++)
                    {
                    {
                phiPrev[i][j] = phi[i][j];
                phiPrev[i][j] = phi[i][j];
                phi[i][j] = 0.25*(phi[i+1][j] + phi[i-1][j] + phi[i][j+1] + phi[i][j
                phi[i][j] = 0.25*(phi[i+1][j] + phi[i-1][j] + phi[i][j+1] + phi[i][j
    -l] - h*h*f[i][j]);
```

    -l] - h*h*f[i][j]);
    ```
```

            phiErr[i][j] = f[i][j] - phi[i][j];
                phiDiff[i][j] = phi[i][j] - phiPrev[i][j];
    }
    }
pBCfield(nn, phi);
//Find residual between RHS and LHS
testl = maxNorm(nn, phiDiff);
if (testl <= 0.0){residual = 0.0;}
else {residual = maxNorm(nn, phiDiff);}
if (residual <= epsi){break;}
if (it >= itmax){break;}
}
*error = maxNorm(nn, phiErr);
*res = residual;
*iter = it - l;
free_dmatrix (phiErr, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
free_dmatrix(phiDiff, 0, (int) (dimX*n) +2, 0, (int)(dimY*n)+2);
free_dmatrix(phiPrev, 0, (int) (dimX*n) +2, 0, (int)(dimY*n)+2);
return;
}
/*
void SOR(int nn, double **f, double **phi, int *iter, double *res, double *error)
{
double h = 1./nn, **phiErr, ** phiPrev;
double residual = 0.0, omega, testl;
int it;
phiErr = dmatrix (0, (int) (dimX*n) +2, 0, (int)(dimY*n)+2);
phiPrev = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
omega = interp(); //Using linear interpolation, omega_opt
*iter = 0;
for (it = 1; it <= itmax; it++)
{
toZero(nn, phiErr) ; toZero(nn, phiPrev);

```
```

            for (int j = l; j <= (int)(dimY*nn); j++)
    ```
            for (int j = l; j <= (int)(dimY*nn); j++)
            {
            {
                for (int i = 1; i <= (int)(dimX*nn); i ++)
                for (int i = 1; i <= (int)(dimX*nn); i ++)
                    {
                    {
                phiPrev[i][j] = phi[i][j];
                phiPrev[i][j] = phi[i][j];
                phi[i][j] = (1-omega)*phiPrev[i][j] + omega*0.25*(phi[i+1][j] + phi[i
                phi[i][j] = (1-omega)*phiPrev[i][j] + omega*0.25*(phi[i+1][j] + phi[i
    -1][j] + phi[i][j+1] + phi[i][j-l] - h*h*f[i][j]);
    -1][j] + phi[i][j+1] + phi[i][j-l] - h*h*f[i][j]);
            phiErr[i][j] = phi[i][j] - phiPrev[i][j];
            phiErr[i][j] = phi[i][j] - phiPrev[i][j];
        }
        }
}
}
            pBCfield(nn, phi);
            pBCfield(nn, phi);
            //Find residual between RHS and LHS
            //Find residual between RHS and LHS
            testl = maxNorm(nn, phiErr);
            testl = maxNorm(nn, phiErr);
            if (testl <= 0.0){residual = 0.0;}
            if (testl <= 0.0){residual = 0.0;}
            else {residual = maxNorm(nn, phiErr);}
            else {residual = maxNorm(nn, phiErr);}
            if (residual <= epsi){break;}
            if (residual <= epsi){break;}
            if (it >= itmax){break;}
            if (it >= itmax){break;}
            }
            }
    *res = residual;
    *res = residual;
    *iter = it;
    *iter = it;
    free_dmatrix(phiErr, 0, (int)(dimX*n) +2, 0, (int)(dimY*n)+2);
    free_dmatrix(phiErr, 0, (int)(dimX*n) +2, 0, (int)(dimY*n)+2);
    free_dmatrix (phiPrev, 0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);
    free_dmatrix (phiPrev, 0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);
    return;
    return;
}
```




```
1*
```

1*
/*_______________________________________________________________________l
/*_______________________________________________________________________l
double interp(void)
double interp(void)
{
{
double nn[9] = {0, 5, 10, 20, 30, 40, 60, 100, 500};
double nn[9] = {0, 5, 10, 20, 30, 40, 60, 100, 500};
double oo[9] = {1.7, 1.78, 1.86, 1.92, 1.95, 1.96, 1.97, 1.98, 1.99};
double oo[9] = {1.7, 1.78, 1.86, 1.92, 1.95, 1.96, 1.97, 1.98, 1.99};
int i, size;
int i, size;
double interp, x0, xl, y0, yl;
double interp, x0, xl, y0, yl;
size = 9;
size = 9;
for (i = 1; i < size; i++)
for (i = 1; i < size; i++)
{
{
if (nn[i] > n)
if (nn[i] > n)
{

```
{
```

```
224 x0 = nn[i-1];
    x1 = nn[i];
    y0 = oo[i-1];
    yl = oo[i];
    break;
    }
        }
    return interp = y0 +((yl-y0)*(n-x0))/(x1-x0);
}
```

Listing B.7: multigrid.c, all multigird functions are found here.

```
#include <math.h>
#include <stdio.h>
#include <stdlib.h>
#include "head.h"
#include "input.h"
void twoStepM(int nn, double t, double **RHS, double ** deltaP, int *iter, double
    error[ncycle], double endRes[ncycle]);
void Vcycle(int nn, double t, double **f, double **MVAL, int *iter, double error[
        ncycle], double endRes[ncycle]);
void fullMultigrid(int nn, double t, double **f, double **value, int *it, double
        error[ncycle], double endRes[ncycle]);
void multigrid(double t, double **u, double **v, double **p, double ** deltaP)
{
    int nF = n, k, iter = 0, step = (int) (t/dt) + l;
    double h = 1./n, integer, div, residual[ncycle], error[ncycle];
    double fraction = modf(step/printOut, &integer), **RHS;
    RHS = dmatrix (0, (int) (dimX*n) +2, 0, (int)(dimY*n)+2);
    toZero(n, RHS) ;
```



```
    k = log_2(n);
    if (n != powerOf(k))
    {
        printf("\n");
        printf("Fatal error when using MULTIGRID\n");
        printf("N is not a power of 2.\n");
        exit (1);
    }
    |/__ Set the right hand side
```



```
    for (int j = 1; j <= (int)(dimY*nF); j++)
        {
        for (int i = 1; i <= (int)(dimX*nF); i ++)
{
    div = (u[i][j] - u[i-1][j] + v[i][j] - v[i][j-1])/h; //Here, h = dx = dy
        RHS[i][j] = (rho/dt)*div;
        }
```

```
    }
    //_____________________m
        -/
    if (method == 3) //Two-step multigrid
    {
        if (fraction == 0.0 && step == (printOut*integer)){printf("TWO-STEP MULTIGRID\
        n') ; }
        twoStepM(n, t, RHS, deltaP, &iter, residual, error);
    }else if (method == 4) //V-cycle multigrid
        {
            if (fraction == 0.0 && step == (printOut*integer)){printf("V-CYCLE MULTIGRID \
        n\n");}
            Vcycle(n, t, RHS, deltaP, &iter, residual, error);
    }else if (method == 5) //Full multigrid
        {
            if (fraction == 0.0 && step == (printOut*integer)){printf("FULL MULTIGRID \n")
        ;}
        fullMultigrid(n, t, RHS, deltaP, &iter, residual, error);
    }
    if (fraction == 0.0 && step == (printOut*integer))
        {
        printf("\nTotal nr of iterations: %i \n", iter);
    }
    //_________________________mect pressure
    presCorr(nF, p, deltaP);
    pBCfield (n, p);
    free_dmatrix(RHS, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
/* two-step multigrid(fine -> coarce -> fine) */
void twoStepM(int nn, double t, double **RHS, double **value, int *it, double error[
        ncycle], double endRes[ncycle])
    int nC = nn/2, nF = nn, k, nIter = 0, iter = 0, numb = (int)(t/dt), print = 0;
    double h = 1./nn, res = 0.0, err = 0.0, integer;
    int step = (int)(t/dt) + 1;
    double fraction = modf(step/printOut, &integer);
```

\}
\{

```
double **R, **E, div;
R = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
E = dmatrix (0, (int)(dimX*n)+2, 0, (int)(dimY*n)+2);
//____-_Relax v times on the finest grid-_-_-_
GaussSeidel(itPre, nF, RHS, value, &iter, &res, &err);
if (fraction == 0.0 && step == (printOut*integer))
{
    printf("Pre-smoothing - iterations: %i \n", iter);
    printf("Residual: %g. \n\n", res);
}
//Loop trough a fixed number of V-cycles.
for (int c = 0; c < ncycle; c++)
    {
        if (fraction == 0.0 && step == (printOut*integer)){printf("\nCYCLE NUMBER %i \
    n", c+1);}
        //-- Restrict the residual from fine grid to coarse grid --/
        toZero(n, R);
            weightedResidual(nC, RHS, value, R);
        injectedResidual(nC, RHS, value, R);
        //Use zero as initial guess for E on the coarse grid approximation of the
        error E.
        toZero(nF, E);
        GaussSeidel(itCoarse, nC, R, E, &iter, &res, &err);
        if (fraction == 0.0 && step == (printOut*integer))
        {
            printf("Smooth coarse grid - iterations: %i \n", iter);
            printf("Residual: %g. \n\n", res);
        }
        //Interpolate from coarse grid to fine grid
        interpolation(nC, E);
        pBCfield(nF, value);
        addValue(nF, E, value);
        //Post-smoothing, removing error
        GaussSeidel(itPost, nF, RHS, value, &iter, &res, &err);
        if (fraction == 0.0 && step == (printOut*integer))
        {
```

```
        printf("Post-smoothing - iterations: %i \n", iter);
        printf("Residual: %g. \n\n", res);
        }
        nIter +=iter;
        endRes[c] = res;
        error[c] = err;
        if (res <= epsi){break;}
    }
    *it = nIter;
    free_dmatrix (R, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    free_dmatrix (E, 0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
    return;
*============================================================**/
/*V-cycle multigrid */ 
void Vcycle(int nn, double t, double **f, double **MVAL, int *it, double error[
    ncycle], double endRes[ncycle])
{//MVAL = deltaP
    int nC = nn/2, nF = nn, k, nIter = 0, iter = 0, dCurr, count = 0, numb, print = 0;
    double h = 1./nn, integer, res = 0.0, err = 0.0;
    int step = (int)(t/dt) + 1, limit;
    double fraction = modf(step/printOut, &integer);
```



```
    double **value, ** newValue, **R, **E, div;
    double ***RHS, ***VAL, **MRHS;
    MRHS = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    value = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
    newValue = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    R = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    E = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    RHS = f3tensorD (0, d, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    VAL = f3tensorD (0, d, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    toZero(n, value);
    toZero(n, R);
    toZero (n, MRHS) ;
```

\}
$\qquad$

```
for (int dd = 0; dd < d; dd++)
```

for (int dd = 0; dd < d; dd++)
{
{
toZeroM(dd, RHS);
toZeroM(dd, RHS);
toZeroM(dd, VAL);
toZeroM(dd, VAL);
}
}
matrixArray(nF, f, RHS, 0);
matrixArray(nF, f, RHS, 0);
matrixArray (nF, MVAL, VAL, 0);
matrixArray (nF, MVAL, VAL, 0);
//_-_-_-Relax v times on the finest grid-----/
//_-_-_-Relax v times on the finest grid-----/
GaussSeidel(itPre, nF, f, MVAL, \&iter, \&res, \&err);
GaussSeidel(itPre, nF, f, MVAL, \&iter, \&res, \&err);
if (fraction == 0.0 \&\& step == (printOut*integer))
if (fraction == 0.0 \&\& step == (printOut*integer))
{
{
printf("Pre-smoothing 1 - iterations: %i \n", iter);
printf("Pre-smoothing 1 - iterations: %i \n", iter);
printf("Residual: %g. \n\n", res);
printf("Residual: %g. \n\n", res);
}
}
//Loop trough a fixed number of V-cycles.
//Loop trough a fixed number of V-cycles.
for (int c = 0; c < ncycle; c++)
for (int c = 0; c < ncycle; c++)
{
{
if (fraction == 0.0 \&\& step == (printOut*integer)){printf("\nCYCLE NUMBER %i \
if (fraction == 0.0 \&\& step == (printOut*integer)){printf("\nCYCLE NUMBER %i \
n", c+1);}
n", c+1);}
nC=nn/2, nF = nn;
nC=nn/2, nF = nn;
//-- Restrict the residual from fine grid to coarse grid --/
//-- Restrict the residual from fine grid to coarse grid --/
arrayMatrix (nF, RHS, MRHS, 0);
arrayMatrix (nF, RHS, MRHS, 0);
// weightedResidual (nC, MRHS, MVAL, R) ;
// weightedResidual (nC, MRHS, MVAL, R) ;
injectedResidual(nC, MRHS, MVAL, R);
injectedResidual(nC, MRHS, MVAL, R);
//Set R equals to RHS for the current depth and store it in RHS
//Set R equals to RHS for the current depth and store it in RHS
matrixArray(nC, R, RHS, 1);
matrixArray(nC, R, RHS, 1);
k = log_2(nn);
k = log_2(nn);
limit = (k > d) ? d:k;
limit = (k > d) ? d:k;
dCurr = 2;
dCurr = 2;
//-_ Go coarser
//-_ Go coarser
while (dCurr < limit)
while (dCurr < limit)
{
// Set number of grid points in coarse and fine grid
// Set number of grid points in coarse and fine grid
nF=nC; nC = nF/2;
nF=nC; nC = nF/2;
//Use zero as initial guess for E on the coarse grid approximation of the error E

```
    //Use zero as initial guess for E on the coarse grid approximation of the error E
```

```
    toZero(n, E);
    toZero (n, MRHS);
    arrayMatrix (nF, RHS, MRHS, dCurr-1);
    GaussSeidel(itPre, nF, MRHS, E, &iter, &res, &err);
    if (fraction == 0.0 && step == (printOut*integer))
        {
        printf("Pre-smoothing %i - iterations: %i \n", dCurr, iter);
        printf("Residual: %g. \n\n", res);
        }
    //Store correrction
    matrixArray(nF, E, VAL, dCurr-1);
    //Restrict the residual
    // weightedResidual(nC, MRHS, E, R);
    injectedResidual(nC, MRHS, E, R);
    //Set R equals to RHS for the current depth and store it in RHS
    matrixArray(nC, R, RHS, dCurr);
    dCurr += 1;
```



```
        dCurr -= 1;
        if (nC < 2){printf("\n\nFatal error in MULTIGRID. \nCoarsest grid has n less
    than 2!\n"); exit(1);}
        //OR solve directly with A^Lh
        toZero(n, E);
        toZero (n, MRHS);
        arrayMatrix (nC, RHS, MRHS, dCurr);
        if (nC == 2 )
        {
        solveCoarse(E, MRHS);
        if (fraction == 0.0 && step == (printOut*integer)){printf("SOLVED EXACTLY
        FOR n = 2. \n");}
            } else
```

\}
\{

```
GaussSeidel(itCoarse, nC, MRHS, E, &iter, &res, &err);
```

GaussSeidel(itCoarse, nC, MRHS, E, \&iter, \&res, \&err);
if (fraction == 0.0 \&\& step == (printOut*integer))
if (fraction == 0.0 \&\& step == (printOut*integer))
{
{
printf("Coarsest grid - iterations: %i \n", iter);
printf("Coarsest grid - iterations: %i \n", iter);
printf("Residual: %g. \n\n", res);
printf("Residual: %g. \n\n", res);
}
}
}
dCurr -= 1;

```
    dCurr -= 1;
```




```
        while (0 <= dCurr)
```

        while (0 <= dCurr)
    {
//Interpolate from coarse grid to fine grid
//Interpolate from coarse grid to fine grid
interpolation(nC, E); //Get interpolated E
interpolation(nC, E); //Get interpolated E
toZero (n, MVAL);
toZero (n, MVAL);
arrayMatrix(nF, VAL, MVAL, dCurr);
arrayMatrix(nF, VAL, MVAL, dCurr);
// Set pressure BC on MVAL
// Set pressure BC on MVAL
addValue(nF, E, MVAL); //Get value = value + E
addValue(nF, E, MVAL); //Get value = value + E
pBCfield(nF, MVAL);
pBCfield(nF, MVAL);
toZero (n, MRHS);
toZero (n, MRHS);
arrayMatrix(nF, RHS, MRHS, dCurr);
arrayMatrix(nF, RHS, MRHS, dCurr);
//Post-smoothing, removing error
//Post-smoothing, removing error
GaussSeidel(itPost, nF, MRHS, MVAL, \&iter, \&res, \&err);
GaussSeidel(itPost, nF, MRHS, MVAL, \&iter, \&res, \&err);
if (fraction == 0.0 \&\& step == (printOut*integer))
if (fraction == 0.0 \&\& step == (printOut*integer))
{
{
printf("Post-smoothing %i - iterations: %i \n", dCurr+1, iter);
printf("Post-smoothing %i - iterations: %i \n", dCurr+1, iter);
printf("Residual: %g. \n\n", res);
printf("Residual: %g. \n\n", res);
}
}
nIter +=iter;
nIter +=iter;
if (dCurr == 0) {matrixArray (nF, MVAL, VAL, 0) ;}
if (dCurr == 0) {matrixArray (nF, MVAL, VAL, 0) ;}
// Set number of grid points in coarse and fine grid
// Set number of grid points in coarse and fine grid
nC = nF; nF = nC*2;
nC = nF; nF = nC*2;
dCurr -= 1;
dCurr -= 1;
}

```
```

        endRes[c] = res;
        error[c] = err;
        if (res <= epsi){break;}
    }
    *it = nIter;
    free_dmatrix (MRHS, 0, (int) (dimX*n)+2, 0, (int) (dimY*n) +2);
    free_dmatrix(value, 0, (int)(dimX*n)+2, 0, (int) (dimY*n)+2);
    free_dmatrix(newValue, 0, (int) (dimX*n) +2, 0, (int)(dimY*n)+2);
    free_dmatrix (R, 0, (int)(dimX*n)+2, 0, (int)(dimY*n)+2);
    free_dmatrix (E, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    free_f3tensorD(RHS, 0, d, 0, (int) (dimX*n)+2, 0, (int)(dimY*n) +2);
    free_f3tensorD (VAL, 0, d, 0, (int) (dimX*n)+2, 0, (int) (dimY*n) +2);
    return;
    /* Full multigrid */
/*=========================================================*/
void fullMultigrid(int nn, double t, double **f, double **value, int *it, double
error[ncycle], double endRes[ncycle])
{ //value = deltaP
int nC = nn/2, nF = nn, nnC, nnF, k, nIter = 0, iter = 0, dCurr, count = 0, numb,
print = 0;
double h = 1./nn, res = 0.0, err = 0.0, integer;
int step = (int)(t/dt) + l, limit;
double fraction = modf(step/printOut, \&integer);
k = log_2(nn);
limit = (k > d) ? d:k;
dCurr = limit - l;

```

```

    double **R, **MRHS, **MVAL, div;
    double ***reRHS, ***RHS, ***VAL;
    MRHS = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    MVAL = dmatrix (0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);
    R = dmatrix (0, (int)(dimX*n)+2, 0, (int)(dimY*n)+2);
    reRHS = f3tensorD (0, d, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    ```
\}
```

RHS = f3tensorD (0, d, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
VAL = f3tensorD (0, d, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
toZero(n, R) ;
toZero (n, MRHS);
toZero (n, MVAL);
for (int dd = 0; dd < d; dd++)
{
toZeroM(dd, reRHS) ;
toZeroM(dd, RHS);
toZeroM(dd, VAL);
}
//Forming the right hand side of the poisson equation
matrixArray(nF, f, reRHS, dCurr);
//-- Fill temporary coarser RHS with restrictions from the calculated RHS --//

```

```

while (dCurr > 0)
{
injected(nC, f);
// weighted(nC, MRHS, value);
matrixArray(nC, f, reRHS, dCurr-1);
dCurr -= 1;
nF=nC; nC = nC/2;
}

```

```

if (nF < 2){printf("\n\n Fatal error in MULTIGRID. \n Coarsest grid has n less
than 2! \n"); exit(1);}
injected (nC, f);
toZero (n, MVAL) ;
//Solve on coarsest grid
if (nF == 2){printf("SOLVED EXACTLY FOR n = 2. \n"); solveCoarse(MVAL, f);}
else
{
GaussSeidel(itCoarse, nC, f, MVAL, \&iter, \&res, \&err);
if (fraction == 0.0 \&\& step == (printOut*integer))

```
```

    {
        printf("Coarsest grid (START) - iterations: %i \n", iter);
        printf("Residual: %g. \n\n", res);
        }
    }
    matrixArray(nF, MVAL, VAL, dCurr);
dCurr += 1;
nC= nF; nF = nF*2;

```

```

while (dCurr < limit)
{
toZero (n, MVAL) ;
arrayMatrix (nC, VAL, MVAL, dCurr-1);
interpolation(nC, MVAL); //Get interpolated MVAL back
matrixArray(nF, MVAL, VAL, dCurr);
copy(reRHS, RHS, dCurr);
for (int c = 1; c <= ncycle; c++) //Loop trough a fixed number of V-cycles.
{
if (fraction == 0.0 \&\& step == (printOut*integer)){printf("CYCLE NUMBER %i \
n", c);}
nnF=nF; nnC = nC;
for (int dCalc = dCurr; dCalc >= 1; dCalc--) //Loop downward in V.
{
toZero(n, MVAL);
arrayMatrix (nnF, VAL, MVAL, dCalc);
toZero (n, MRHS) ;
arrayMatrix (nnF, RHS, MRHS, dCalc);
GaussSeidel(itPre, nnF, MRHS, MVAL, \&iter, \&res, \&err);
if (fraction == 0.0 \&\& step == (printOut*integer))
{
printf("Pre-smoothing %i - iterations: %i \n", dCalc, iter);
printf("Residual: %g. \n\n", res);
}

```
toZero ( \(\mathrm{n}, \mathrm{R}\) ) ;
//weightedResidual (nnC, MRHS, MVAL, R);
injectedResidual (nnC, MRHS, MVAL, R); //Restricted residual, use as the next RHS
matrixArray (nnC, R, RHS, dCalc-1);
toZero (n, MVAL) ;
matrixArray(nnC, MVAL, VAL, dCalc-1); //Zero as initial guess for next smoothning
            \(\mathrm{nnF}=\mathrm{nnC} ; \mathrm{nnC}=\mathrm{nnC} / 2 ;\)
        \}
    //Solve on coarsest grid
    if \((\mathrm{nnF}==2)\{\) printf ("SOLVED EXACTLY FOR \(\mathrm{n}=2\). \(\mathrm{ln} ")\); solveCoarse (MRHS, MVAL
) ;\}
    else
        \{
            GaussSeidel(itCoarse, nnF, R, MVAL, \&iter, \&res, \&err);
            if (fraction \(==0.0 \& \&\) step \(==(\) printOut*integer))
            \{
                printf("Coarsest grid - iterations: \%i \(\ n "\), iter);
                printf("Residual: \%g. \(\ln \backslash n "\), res) ;
            \}
        \}
    matrixArray (nnF, MVAL, VAL, 0) ;
    \(\mathrm{nnC}=\mathrm{nnF} ; \mathrm{nnF}=\mathrm{nnF} * 2\);
    for (int dCalc \(=1\); dCalc <= dCurr; dCalc++) //Loop upward in V.
        \{
            toZero (n, MVAL) ;
            toZero(n, value);
            arrayMatrix (nnF, VAL, MVAL, dCalc-1);
            arrayMatrix (nnF, VAL, value, dCalc);
            //Interpolate from coarse grid to fine grid
            interpolation (nnC, MVAL);
            addValue(nnF, MVAL, value); //Get value = value + E
```

                    // Set pressure BC on value
                pBCfield(nnF, value);
                    toZero(n, MRHS);
                arrayMatrix(nnF, RHS, MRHS, dCalc);
                    //Post-smoothing, removing error
                    GaussSeidel(itPost, nnF, MRHS, value, &iter, &res, &err);
                if (fraction == 0.0 && step == (printOut*integer))
                    {
                        printf("Post-smoothing %i - iterations: %i \n", dCalc, iter);
                        printf("Residual: %g. \n\n", res);
                    }
                    nIter +=iter;
                    matrixArray(nnF, value, VAL, dCalc);
                    nnC = nnF; nnF = nnF*2;
                }
            endRes[c-1] = res;
        }
    dCurr += 1;
    nC = nF; nF = nF*2;
    }
    *it = nIter;
    free_dmatrix (MRHS, 0, (int) (dimX*n)+2, 0, (int)(dimY*n) +2);
    free_dmatrix (MVAL, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    free_dmatrix (R, 0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);
    free_f3tensorD(reRHS, 0, d, 0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);
    free_f3tensorD(RHS, 0, d, 0, (int)(dimX*n)+2, 0, (int)(dimY*n) +2);
    free_f3tensorD (VAL, 0, d, 0, (int) (dimX*n) +2, 0, (int) (dimY*n) +2);
    return;
    ```


```

// r = f - A*phi, phi:approximation of value.
double residual(int nn, double **f, double **phi, int i, int j)
{
double R, h = 1./nn;

```
\}

```

return R;
}

```


```

void weightedResidual(int nC, double **RHS, double ** phi, double **R)
{
int ii, jj, nn = nC*2;
double Rcurr, R1, R2, R3, R4, R5, R6, R7, R8;
toZero(n, R);
for (int j = 2; j < (int)(dimY*nC); j++)
{
for (int i = 2; i < (int) (dimX*nC); i++)
{
jj = j*2+1; ii = i *2+1;
Rcurr = residual(nn, RHS, phi, ii, jj);
R1 = residual(nn, RHS, phi, ii - 1, jj - l);
R2 = residual(nn, RHS, phi, ii, jj - l);
R3 = residual(nn, RHS, phi, ii +1, jj - ) ;
R4 = residual(nn, RHS, phi, ii -1, jj);
R5 = residual(nn, RHS, phi, ii +1, jj);
R6 = residual(nn, RHS, phi, ii - l, jj +1);
R7 = residual(nn, RHS, phi, ii, jj +1);
R8 = residual(nn, RHS, phi, ii +1, jj+1);
R[i][j] = 0.25*(Rcurr + 0.5*(R2 + R4 + R5 + R7) + 0.25*(R1 + R3 + R6 + R8)
);
}
}
//Set ghost cells
for (int j = 1; j <= (int) (dimY*nC); j++)
{
jj = j*2-1;
Rcurr = residual(nn, RHS, phi, l, jj) ;
R[l][j] = Rcurr;

```
            Rcurr = residual(nn, RHS, phi, (int)(dimX*nn), jj);
        R[(int)(dimX*nC)][j] = Rcurr;
    }
    for (int i = 1; i <= (int)(dimX*nC); i ++)
    {
        ii = i*2-1;
        Rcurr = residual(nn, RHS, phi, ii, 1);
        R[i][1] = Rcurr;
        Rcurr = residual(nn, RHS, phi, ii, (int)(dimY*nn));
        R[i][(int)(dimY*nC)] = Rcurr;
    }
}
void injectedResidual(int nC, double **RHS, double **phi, double **R)
{
    int ii, jj, nF = nC*2;
    double h = 1./nF;
    toZero(n, R);
    //Loop over cells and find restricted residual for the coarse grid-cells
    for (int j = l; j <= (int)(dimY*nC); j ++)
        {
        for (int i = l; i <= (int)(dimX*nC); i ++)
    {
            jj = j*2; ii = i *2;
            R[i][j] = residual(nF, RHS, phi, ii, jj);
            }
    }
}
```




```
void weighted(int nC, double **R)
{
    int iC, iF, jC, jF, nF = nC*2;
    double **Rout;
    Rout = dmatrix (0, (int) (dimX*n) +2, 0, (int)(dimY*n) +2);
    toZero(n, Rout);
```

```
//Loop over cells and find restricted values for the coarse grid-cells
    for (jC = 1, jF = 2 ; jC <= (int) (dimY*nC); jC++, jF+=2)
    {
            for (iC = 1, iF = 2 ; iC <= (int) (dimX*nC); iC++, iF+=2)
{
            Rout[iC][jC] = 0.25*(R[iF][jF] + 0.5*(R[iF][jF-1] + R[iF-1][jF] + R[iF+1][
        jF]
    + R[iF][jF+1]) + 0.25*(R[iF-1][jF-1] + R[iF+1][jF-1] + R[iF-1][jF+1] + R[iF+1][jF
        +1]);
            }
    }
    ccopy(Rout, R);
    free_dmatrix (Rout, 0, (int)(dimX*n) +2, 0, (int)(dimY*n)+2);
}
void injected(int nC, double **R)
{
    int iC,iF, jC, jF, nF = nC*2;
    double **Rout;
    Rout = dmatrix (0, (int)(dimX*n) +2, 0, (int)(dimY*n) +2);
    toZero(n, Rout);
    //Loop over cells and find restricted values for the coarse grid-cells
    for (jC = 1, jF = 2 ; jC <= (int) (dimY*nC) ; jC++, jF+=2)
        {
        for (iC = 1, iF = 2 ; iC <= (int)(dimX*nC); iC++, iF+=2)
    {
            Rout[iC][jC] = R[iF][jF];
            }
        }
    ccopy(Rout, R);
    free_dmatrix(Rout, 0, (int)(dimX*n)+2, 0, (int)(dimY*n)+2);
}
/* ___ Add Value -
```



```
void addValue(int nn, double **E, double **phi)
{
    //Add interpolated value to fine grid cell value
```

```
    for (int j = 1; j <= (int) (dimY*nn); j++)
```

    for (int j = 1; j <= (int) (dimY*nn); j++)
    {
    {
        for (int i = l; i <= (int) (dimX*nn); i++)
        for (int i = l; i <= (int) (dimX*nn); i++)
    {
{
phi[i][j] += E[i][j];
phi[i][j] += E[i][j];
}
}
}
}
return;
return;
}

```




```

void interpolation(int nC, double **E)

```
void interpolation(int nC, double **E)
{
    double **returnE;
    double **returnE;
    int iC, jC, iF, jF, nF = nC*2;
    int iC, jC, iF, jF, nF = nC*2;
    returnE = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
    returnE = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
    toZero(n, returnE);
    toZero(n, returnE);
    // Bilinear interpolation for internal nodes
    // Bilinear interpolation for internal nodes
    for (jC = 0, jF = 0; jC <= (int) (dimY*nC); jC++, jF+=2)
    for (jC = 0, jF = 0; jC <= (int) (dimY*nC); jC++, jF+=2)
        {
        {
        for (iC = 0, iF = 0; iC <= (int) (dimX*nC); iC++, iF+=2)
        for (iC = 0, iF = 0; iC <= (int) (dimX*nC); iC++, iF+=2)
{
            returnE[iF][jF] = 0.5625*E[iC][jC] + 0.1875*(E[iC+1][jC] + E[iC][jC+1]) +
            returnE[iF][jF] = 0.5625*E[iC][jC] + 0.1875*(E[iC+1][jC] + E[iC][jC+1]) +
        0.0625*E[iC}+1][jC+1]
        0.0625*E[iC}+1][jC+1]
            returnE[iF+1][jF] = 0.5625*E[iC+1][jC] + 0.1875*(E[iC+1][jC+1] + E[iC][jC
            returnE[iF+1][jF] = 0.5625*E[iC+1][jC] + 0.1875*(E[iC+1][jC+1] + E[iC][jC
        ]) + 0.0625*E[iC][jC+1];
        ]) + 0.0625*E[iC][jC+1];
            returnE[iF][jF+1] = 0.5625*E[iC][jC+1] + 0.1875*(E[iC+1][jC+1] + E[iC][jC
            returnE[iF][jF+1] = 0.5625*E[iC][jC+1] + 0.1875*(E[iC+1][jC+1] + E[iC][jC
        ]) + 0.0625*E[iC+1][jC ];
        ]) + 0.0625*E[iC+1][jC ];
            returnE[iF+1][jF+1] = 0.5625*E[iC+1][jC+1] + 0.1875*(E[iC+1][jC] + E[iC][
            returnE[iF+1][jF+1] = 0.5625*E[iC+1][jC+1] + 0.1875*(E[iC+1][jC] + E[iC][
        jC+1]) + 0.0625*E[iC][jC];
        jC+1]) + 0.0625*E[iC][jC];
            }
            }
        }
        }
    // Set mixed prolongation at boundary nodes
    // Set mixed prolongation at boundary nodes
    for (jC = 0, jF = 0; jC <= (int) (dimY*nC); jF+=2, jC++)
```

    for (jC = 0, jF = 0; jC <= (int) (dimY*nC); jF+=2, jC++)
    ```
```

    {
    returnE[0][jF+1] = 0.75*E[1][jC+1] + 0.25*E[1][jC];
    returnE[1][jF] = 0.75*E[1][jC] + 0.25*E[1][jC+1];
    returnE[1][jF+1] = 0.75*E[1][jC+1] + 0.25*E[1][jC];
    returnE[(int)(dimX*nF)][jF+1] = 0.75*E[(int)(dimX*nC)][jC+1] + 0.25*E[(int)(
    dimX*nC)][jC ];
        returnE[(int)(dimX*nF)][jF] = 0.75*E[(int) (dimX*nC)][jC] + 0.25*E[(int)(dimX*
        nC)][jC+1];
        returnE[(int) (dimX*nF)+1][jF+1]=0.75*E[(int)(dimX*nC)][jC+1] + 0.25*E[(int)(
        dimX*nC)][jC];
            returnE[(int) (dimX*nF)+1][jF] = 0.75*E[(int) (dimX*nC)][jC] + 0.25*E[(int)(
        dimX*nC)][jC+1];
    }
    for (jC = 0, jF = 0; jC <= (int) (dimX*nC); jF+=2, jC++)
    {
        returnE[jF][1] = 0.75*E[jC][1] + 0.25*E[jC+1][1];
        returnE[jF+1][1] = 0.75*E[jC+1][1] + 0.25*E[jC][1];
        returnE[jF][0] = 0.75*E[jC][1] + 0.25*E[jC+1][1];
        returnE[jF+1][0] = 0.75*E[jC+1][1] + 0.25*E[jC][1];
        returnE[jF+1][(int)(dimY*nF)]=0.75*E[jC+1][(int)(dimY*nC)] + 0.25*E[jC][(int
        )(dimY*nC)];
            returnE[jF][(int) (dimY*nF)] = 0.75*E[jC][(int)(dimY*nC)] + 0.25*E[jC+1][(int)
        (dimY*nC)];
            returnE[jF+1][(int)(dimY*nF)+1]=0.75*E[jC+1][(int)(dimY*nC)] + 0.25*E[jC][(
        int) (dimY*nC)];
            returnE[jF][(int)(dimY*nF)+1]=0.75*E[jC][(int)(dimY*nC)] + 0.25*E[jC+1][(
        int)(dimY*nC)];
    }
    //Set return matrix
    ccopy(returnE, E);
    free_dmatrix (returnE, 0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
    return;
    6 }
07 /

```

```

void solveCoarse(double **phi, double **f)
double h = 0.5, **returnPhi;
returnPhi = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
toZero(n, returnPhi);
returnPhi[1][1] = (phi[0][1] + phi[2][1] + phi[1][0] + phi[1][2] - h*h*f[1][1])
/4.0;
ccopy(returnPhi, phi);
free_dmatrix(returnPhi, 0, (int)(dimX*n)+2, 0, (int)(dimY*n)+2);
}

```

```

/*- Transform array to matrix ——_ _ _ _ _ _ _ _ _

```

```

void arrayMatrix(int nn, double *** array, double **matrix, int dd)
{
for (int j = 0; j <= (int)(dimY*nn)+1; j ++)
{
for (int i = 0; i <= (int)(dimX*nn)+1; i++)
{
matrix[i][j] = array[dd][i][j];
}
}
}

```


```

void matrixArray(int nn, double **matrix, double ***array, int dd)
{
for (int j = 0; j <= (int)(dimY*nn)+1; j++)
{
for (int i = 0; i <= (int) (dimX*nn)+1; i++)
{
array[dd][i][j] = matrix[i][j];
}
}

```
```

22 int powerOf(int k)
int value;
if ( k < 0 )
{
printf("Error: b^c = a, c i negative. n needs to be positive.");
exit(1);
}
else if ( k == 0 ) {value = 1;}
else if ( k == 1 ){value = 2;}
else
{
value = 1;
for (int i = 1; i <= k; i++ )
{
value = value * 2;
}
}
return value;
}

```

\section*{Listing B.8: BC.c,velocity and pressure BC's.}
```

\#include "head.h"
\#include <math.h>
\#include <stdio.h>
\#include <string.h>
\#include "input.h"
/*
|* BC FOR VELOCITY */

```

```

void velBCfield(int nn, double **u, double **v)
{
double h = 1./nn;
if (wall == 1) //BC's for lid driven cavety flow
{
for (int j = 0; j <= (int)(dimY*nn)+l; j ++)
{
v[0][j] = -v[l][j];
v[(int)(dimX*nn)+1][j] = -v[(int)(dimX*nn)][j];
u[0][j] = 0.0;
u[(int)(dimX*nn)][j] = 0.0;
}
for (int i = 0; i <= (int) (dimX*nn)+1; i ++)
{
u[i][(int)(dimY*nn)+1] = -u[i][(int)(dimY*nn)] + 2.0*velX;
u[i][0] = -u[i][1];
v[i][(int)(dimY*nn)] = 0.0;
v[i][0] = 0.0;
}
}else if (wall == 2) //Couette flow
{
for (int j = 0; j <= (int)(dimY*nn)+1; j ++)
{
u[0][j] = u[1][j];
v[0][j] = v[l][j];
u[(int)(dimX*nn)+l][j] = u[(int)(dimX*nn)][j];
v[(int)(dimX*nn)+l][j] = v[(int)(dimX*nn)][j];
}

```
```

        for (int i = 0; i <= (int) (dimX*nn)+1; i++)
    {
v[i][(int)(dimY*nn)] = 0.0;
v[i][0] = 0.0;
u[i][(int)(dimY*nn)+1] = -u[i][(int)(dimY*nn)] + 2.0*velX;
u[i][0] = -u[i][1];
}
}else if (wall == 3) //Channel flow with inflow velocity
{
for (int j = 0; j <= (int)(dimY*nn) +l; j ++)
{
u[0][j] = velX;
v[0][j] = v[1][j];
u[(int)(dimX*nn)+l][j] = u[(int)(dimX*nn)][j];
v[(int)(dimX*nn)+1][j] = v[(int)(dimX*nn)][j];
}
for (int i = 0; i <= (int) (dimX*nn)+1; i++)
{
v[i][0] = 0.0;
v[i][(int)(dimY*nn)] = 0.0;
u[i][(int)(dimY*nn)+l] = u[i][(int)(dimY*nn)];
u[i][0] = u[i][1];
}
}else if (wall == 4) //Channel flow with inflow velocity
{
for (int j = 0; j <= (int)(dimY*nn)+l; j++)
{
u[0][j] = velX;
v[0][j] = v[1][j];
u[(int)(dimX*nn)+1][j] = u[(int)(dimX*nn)][j];
v[(int)(dimX*nn)+l][j] = v[(int)(dimX*nn)][j];
}
for (int i = 0; i <= (int) (dimX*nn)+1; i ++)
{
v[i][0] = 0.0;
v[i][(int)(dimY*nn)] = 0.0;
u[i][(int)(dimY*nn)+1] = -u[i][(int)(dimY*nn)];
u[i][0] = -u[i][1];

```
```

}
}else if (wall == 5) //channel flow, peroidic bc and free-slip
{
for (int j = 0; j <= (int)(dimY*nn)+l; j++)
{
u[0][j] = u[(int)(dimX*nn)][j];
v[0][j] = v[(int)(dimX*nn)][j];
u[(int)(dimX*nn)+l][j] = u[l][j];
v[(int)(dimX*nn)+1][j] = v[l][j];
}
{
v[i][(int)(dimY*nn)] = 0.0;
v[i][0] = 0.0;
u[i][(int)(dimY*nn)+1] = u[i][(int)(dimY*nn)];
u[i][0] = u[i][1];
}
}else if (wall == 6) //Poiseuille flow (peroidic bc and no-slip)
{
for (int j = 0; j <= (int)(dimY*nn)+l; j++)
{
u[0][j] = u[(int)(dimX*nn)-1][j];
v[0][j] = v[(int)(dimX*nn)][j];
u[(int)(dimX*nn)][j] = u[1][j];
v[(int)(dimX*nn)+l][j] = v[l][j];
}
for (int i = 0; i <= (int) (dimX*nn)+1; i ++)
{
v[i][(int)(dimY*nn)] = 0.0;
v[i][0] = 0.0;
u[i][(int)(dimY*nn)+1] = -u[i][(int)(dimY*nn)];
u[i][0] = -u[i][1];
}
}
}
/*
BC FOR PRESSURE

```
```

1 1 4 ~ v o i d ~ p B C f i e l d ( i n t ~ n n , ~ d o u b l e ~ * * p )
115 {
int i, j;
double h = 1./nn;
if (wall == 2 || wall == 3 || wall == 4 || wall == 8) // channel flow
{
for (j = 0; j <= (int) (dimY*nn) +1; j++)
{
p[0][j] = p[1][j];
p[(int)(dimX*nn)+1][j] = 0.0;
}
for (i = 0; i <= (int) (dimX*nn)+1; i++)
{
p[i][(int)(dimY*nn)+1]= p[i][(int)(dimY*nn)];
p[i][0] = p[i][1];
}
}
else if (wall == 5 || wall == 6 || wall == 7) // periodic BC at outflow
{
for (j = 0; j <= (int) (dimY*nn) +1; j++)
{
p[0][j] = p[(int)(dimX*nn)][j];
p[(int)(dimX*nn)+l][j] = p[l][j];
}
for (i = 0; i <= (int) (dimX*nn)+1; i++)
{
p[i][(int)(dimY*nn)+1]= p[i][(int)(dimY*nn)];
p[i][0] = p[i][l];
}
}
}

```

\section*{Listing B.9: results.c, functions for post-processing.}
```

\#include <stdio.h>
\#include "head.h"
\#include "input.h"
\#include <stdlib.h>
\#include <math.h>
void vtfFile(double **, double **, double **, double **, double **, int, double, int
, int, double [4][nPoint]);
void setBodyIBM(double, double, double, double, double [4][nPoint], double [2][
nPoint], double [2][nPoint]);
void gridShifting(double [2][n], int, int, int);
void intersectionP(int *, int, int, int, int [3][maxIntersec], double [3][
maxIntersec], double [2][nPoint]);
void IBMvelocity(double **, double **, double [4][nPoint]);

```



```

//Results and write out at writeOut intervall
void printFile(double t, double **u, double **v, double **p, double body[4][nPoint])
{
double **u_new, **v_new, **p_new, **psi_new, **div_new, **psi, **u_test, **v_test;
int step = (int)(t/dt) + 1, id = (int) (tmax/(dt*writeOut)) + 1, limit;
double integer, fraction = modf(step/writeOut, \&integer);
u_new = dmatrix (0, (int) (dimX*n)+1, 0, (int) (dimY*n) +1);
v_new = dmatrix (0, (int) (dimX*n) +1, 0, (int) (dimY*n) +1);
p_new = dmatrix (0, (int) (dimX*n) +1, 0, (int) (dimY*n) +1);
psi_new = dmatrix (0, (int) (dimX*n)+1, 0, (int) (dimY*n) +1);
div_new = dmatrix (0, (int) (dimX*n) +1, 0, (int) (dimY*n) +1);
psi = dmatrix (0, (int) (dimX*n) +2, 0, (int) (dimY*n)+2);
u_test = dmatrix (0, (int) (dimX N n ) +1, 0, (int) (dimY*n) +1);
v_test = dmatrix (0, (int) (dimX*n) +1, 0, (int) (dimY*n)+1);
ccopy(u_new, u_test); ccopy(v_new, v_test);
toZero(n-1, u_new);
toZero(n-1, v_new);

```
```

toZero(n-1, p_new);
toZero(n-1, psi_new);
toZero(n-1, div_new);
if (fraction == 0.0 \&\& step == (writeOut*integer))
{
stream(psi, u, v);
results(u, v, p, psi, u_new, v_new, p_new, psi_new, div_new);
vtfFile (u_new, v_new, p_new, div_new, psi_new, integer, t, id, writeOut, body);
}
free_dmatrix(v_test, 0, (int) (dimX*n) +1, 0, (int) (dimY*n)+1);
free_dmatrix(u_test, 0, (int) (dimX*n) +1, 0, (int)(dimY*n)+1);
free_dmatrix (p_new, 0, (int) (dimX*n) +1, 0, (int) (dimY*n)+1);
free_dmatrix (u_new, 0, (int) (dimX*n)+1, 0, (int) (dimY*n)+1);
free_dmatrix(v_new, 0, (int) (dimX*n)+1, 0, (int) (dimY*n)+1);
free_dmatrix (psi_new, 0, (int) (dimX*n) +1, 0, (int) (dimY*n) +1);
free_dmatrix(div_new, 0, (int) (dimX*n) +1, 0, (int)(dimY*n)+1);
free_dmatrix (psi, 0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
}

```

```

/*--_- calculating results for u, v, p, psi and div --_--*/

```

```

//Regenerating velocity vectors and pressure,
//removing ghost cells and averaging
void results(double **u, double **v, double **p, double **psi, double **u_new,
double **v_new, double **p_new, double **psi_new, double **div_new)
{
int i, j;
double h = 1./(n+1.);
for (i = 0; i <= (int)(dimX*n); i++)//Averaging for GLview
{
for (j = 0; j <= (int)(dimY*n); j ++)
{
u_new[i][j] = (u[i][j]+u[i][j+1])/2;
v_new[i][j] = (v[i][j]+v[i+1][j])/2;
p_new[i][j] = (p[i][j]+p[i][j+1]+p[i+1][j+1]+p[i+1][j])/4;
psi_new[i][j] = -(psi[i][j] + psi[i+l][j])/2;

```
```

}
}
for (i = 0; i <= (int)(dimX*n); i++)//Dicergence, needs u_new and v_new
{
for (j = 0; j <= (int)(dimY*n); j ++)
{
div_new[i][j] = (u_new[i+l][j]-u_new[i][j])/h + (v_new[i][j+l]-v_new[i][j])
/h;
}
}
}

```

```

/*-___-_calculating streamfunction

```

```

void stream(double **psi, double **u, double **v)
{
int i, j;
double h = 1./n;
for (i = 1; i <= (int)(dimX*n); i++)
{
psi[i][0] = psi[i-1][0] - v[i][0]*h;
}
for (i = 0; i <= (int)(dimX*n)+1; i ++)
{
for (j = 1; j <= (int)(dimY*n); j++)
{
psi[i][j] = psi[i][j-1] + u[i][j]*h;
}
}
}

```

Listing B.10: vtfFile.c, a function to generate the vtf-file for GLview.
```

\#include <stdio.h>
\#include "input.h"
void vtfFile(double **u_new, double **v_new, double **p_new, double **div_new,
double **psi_new, int count, double t, int id, int writeOut, double body[4][
nPoint])
{
int i, j, time;
double h = 1./n;
FILE *file;
if (count == 1)
{
file = fopen("glview.vtf", "w");
fprintf(file, "*VTF-1.00 \n \n");
fprintf(file, "*NODES 1 \n");
for (i = 0; i <= (int)(dimX*n); i++)
{
for (j = 0; j <= (int)(dimY*n); j ++)
{
fprintf(file, "%f %f %i \n", i*h, j*h, 0);
}
}
if (runIBM == 1)
{
fprintf(file, "\n\n*NODES 2 \n");
for (int point = 0; point < nPoint; point++)
{
fprintf(file, "%f %f %i \n", body[0][point], body[1][point], 0);
}
}
fprintf(file, "\n*ELEMENTS 1 \n");
fprintf(file, "%%NODES \#l \n");
fprintf(file, "%%%UADS \n");
for (i = 1; i <= (int) (dimX*n); i++)
{
for(j = 1; j <= (int)(dimY*n) ; j ++)

```
```

    {
    fprintf(file, "%i %i %i %i \n", j+(i-1)*((int)(dimY*n)+1),
    j+l+(i-l)*((int)(dimY*n)+l), j+l+i*((int)(dimY*n)+l), j+i *((int)(dimY*n) +l));
    }
        if (runIBM == 1)
        {
            if (bType == 1 || bType == 3)
            {
        fprintf(file, "\n*ELEMENTS 2 \n");
        fprintf(file, "%%NODES #2 \n");
        fprintf(file, "%%BEAMS \n");
        for (int point = 1; point <= nPoint; point++)
    {
if (point == nPoint){fprintf(file, "%i %i \n", point, 1);}
else{fprintf(file, "%i %i \n", point, point + l);}
}
} else if (bType == 2)
{
fprintf(file, "\n*ELEMENTS 2 \n");
fprintf(file, "%%NODES \#2 \n");
fprintf(file, "%%BEAMS \n");
for (int point = 1; point <= nPoint/2-1; point++)
{
fprintf(file, "%i %i\n", point, point + 1);
}
fprintf(file, "\n*ELEMENTS 3 \n");
fprintf(file, "%%NODES \#2 \n");
fprintf(file, "%%BEAMS \n");
for (int point = nPoint/2 + 1; point <= nPoint-1; point++)
{
fprintf(file, "%i %i \n", point, point + 1);
}
}
}
fprintf(file, "\n*GLVIEWGEOMETRY 1 \n");
fprintf(file, "%%ELEMENTS \n");
if (runIBM == 1)

```
```

            {
            if (bType == 1 || bType == 3){fprintf(file, "%i %i \n",2,1);}
            else if (bType == 2){fprintf(file, "%i %i %i \n",3,2,1);}
            } else
    {
fprintf(file, "%i \n", 1);
}
} else
{
file = fopen("glview.vtf", "a");
}
//Pressure result for each timestep
fprintf(file,"\n\n*RESULTS %i \n", count);
fprintf(file,"%%%IMENSION 1 \n");
fprintf(file,"%%PER_NODE \#1 \n");
for (i = 0; i <= (int)(dimX*n); i++)
{
for (j = 0; j <= (int)(dimY*n); j ++)
{
fprintf(file,"%f \n", p_new[i][j]);
}
}
//Velocity result for each timestep
fprintf(file,"\n*RESULTS %i \n", id + count);
fprintf(file,"%%DIMENSION 3 \n");
fprintf(file,"%%PER_NODE \#1 \n");
for (i = 0; i <= (int) (dimX*n); i++)
{
for (j = 0; j <= (int) (dimY*n); j++)
{
fprintf(file,"%f %f %f \n", u_new[i][j], v_new[i][j], 0.0);
}
}
//Streamfunction for each time-step
fprintf(file,"\n*RESULTS %i \n", (2*id) + count);
fprintf(file,"%%DIMENSION 1 \n");
fprintf(file,"%%PER_NODE \#1 \n");
for (i = 0; i <= (int) (dimX*n); i++)

```
```

    {
        for (j = 0; j <= (int) (dimY*n); j++)
    {
fprintf(file,"%f \n", psi_new[i][j]);
}
}
//Divergence for each time-step
fprintf(file,"\n*RESULTS %i \n", (3*id) + count);
fprintf(file,"%%DIMENSION 1 \n");
fprintf(file,"%%PER_NODE \#1 \n");
for (i = 0; i <= (int) (dimX*n); i++)
{
for (j = 0; j <= (int) (dimY*n); j++)
{
fprintf(file,"%f \n", div_new[i][j]);
}
}
//If last time-step, link results to it
if (t > ((double)tmax-(dt*writeOut)))
{
// Pressure
fprintf(file,"\n*GLVIEWSCALAR l \n");
fprintf(file,"%%NAME \"PRESSURE\" \n");
for (time = 1; time <= count; time++)
{
fprintf(file,"%%STEP %i \n", time);
fprintf(file,"%%STEPNAME \"Time: %f \" \n", dt*time*writeOut);
fprintf(file,"%i \n", time);
}
//Velocity
fprintf(file,"\n*GLVIEWVECTOR l \n");
fprintf(file,"%%NAME \"VELOCITY\" \n");
for (time = 1; time <= count; time++)
{
fprintf(file,"%%STEP %i \n", time);
fprintf(file,"%%STEPNAME \"Time: %f \" \n", dt*time*writeOut);
fprintf(file,"%i \n", id + time);
}

```
```

        //Streamfunction
        fprintf(file,"\n*GLVIEWSCALAR 2 \n");
        fprintf(file,"%%NAME \"STREAMLINES\" \n");
        for (time = 1; time <= count; time++)
    {
fprintf(file,"%%STEP %i \n", time);
fprintf(file,"%%STEPNAME \"Time: %f \" \n", dt*time*writeOut);
fprintf(file,"%i \n", (2*id) + time);
}
//Dirvergence
fprintf(file,"\n*GLVIEWSCALAR 3 \n");
fprintf(file,"%%NAME \"DIVERGENCE\" \n");
for (time = 1; time <= count; time++)
{
fprintf(file,"%%STEP %i \n", time);
fprintf(file,"%%STEPNAME \"Time:%f \" \n", dt*time*writeOut);
fprintf(file,"%i \n", (3*id) + time);
}
fprintf(file," \n");
}
//Close file
fclose(file);
}

```

Listing B.11: validation.c, a function to validate the Poisson solver.
```

\#include <time.h>
\#include <math.h>
\#include <stdio.h>
\#include <string.h>
\#include "input.h"
\#include "head.h"
void twoStepM(int nn, double t, double **RHS, double ** deltaP, int *iter, double
error[ncycle], double endRes[ncycle]);
void Vcycle(int nn, double t, double **f, double **MVAL, int *iter, double error[
ncycle], double endRes[ncycle]);
void fullMultigrid(int nn, double t, double **f, double **value, int *it, double
error[ncycle], double endRes[ncycle]);
void validatePoisson()
{
double h = 1./n, residual, err, endRes[ncycle], error[ncycle], x;
double **RHS, **exact, **deltaP, **diff;
int iter = 0, k = 2, nn, mh = method; //k = wave number
clock_t start, end;
double cpuTimeUsed;
FILE *fileError, *fileIter, *fileDiff, *fileCPU, *fileSolutions, *fileRes, *
fileGSerror;
RHS = dmatrix (0, (int)(dimX*n) +2, 0, (int)(dimY*n)+2);
exact = dmatrix (0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
deltaP = dmatrix (0, (int)(dimX*n) +2, 0, (int)(dimY*n)+2);
diff = dmatrix (0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);
for (nn = n; nn <= n; nn = nn*2)
{
toZero(n, deltaP);
toZero(n, RHS) ;
toZero(n, exact);
printf("\n nn = %i \n", nn);
h = 1./nn, residual = 0.0, iter = 0;

```
```

    for (int j = l; j <= (int)(dimY*n); j++)
    {
for (int i = 1; i <= (int)(dimX*n); i++)
{
//Test problem, set right hand side
RHS[i][j] = cos(k*M_PI*i*h)*cos(k*M_PI*j*h);
// The exact solution/analytical solution
exact[i][j] = (-1.0/(2.0*powf(k*M_PI,2)))*RHS[i][j];
}
}
//Set boundary conditions
pBCfield(nn, deltaP);
pBCfield(nn, exact);
if (mh == 1) //Gauss Seidel
{
//Set clock, start
start = clock();
//Run equation slover
GaussSeidel(itmax, nn, RHS, deltaP, \&iter, \&residual, \&err);
//Stop clock
end = clock();
printf("Tot iterations: %i \n", iter);
printf("Residual: %g \n", residual);
printf("Error: %g \n\n\n", err);
}else if (mh == 2) //SOR
{
//Set clock, start
start = clock();
//Run equation slover
SOR(nn, RHS, deltaP, \&iter, \&residual, \&err);
//Stop clock
end = clock();
printf("Tot iterations: %i \n", iter);
printf("Residual: %g \n", residual);
printf("Error: %g \n\n\n", err);
}else if (mh == 3) //Two-step multigrid
{

```
```

    //Set clock, start
    start = clock();
    //Run equation slover
    twoStepM(nn, 0, RHS, deltaP, &iter, error, endRes);
    //Stop clock
    end = clock();
        printf("Tot iterations: %i \n\n\n", iter);
    } else if (mh == 4) //V-cycle multigrid
{
//Set clock, start
start = clock();
//Run equation slover
Vcycle(nn, 0, RHS, deltaP, \&iter, error, endRes);
//Stop clock
end = clock();
printf("Tot iterations: %i \n\n\n", iter);
}else if (mh == 5) //Full multigrid
{
//Set clock, start
start = clock();
//Run equation slover
fullMultigrid(nn, 0, RHS, deltaP, \&iter, error, endRes);
//Stop clock
end = clock();
printf("Tot iterations: %i \n\n\n", iter);
}
//CLOCKS_PER_SEC = the number of clock ticks per second.
//Calculate processor time
cpuTimeUsed = ((double) (end - start)) / CLOCKS_PER_SEC;
//Print to file number of iterations
fileIter = fopen("Validation/validation_iteration.txt", "a");
fprintf(fileIter, "%i %i \n", nn , iter);
fclose(fileIter);
//Print to file the processor time
fileCPU = fopen("Validation/validation_CPU.txt", "a");
fprintf(fileCPU, "%i %f \n", nn , cpuTimeUsed);
fclose(fileCPU);

```
```

亏
// fprintf(fileDiff, "%f %g \n", x , diff[i][(int)(nn/2)]);
fprintf(fileSolutions, "%f %g %g \n", x , deltaP[i][(int)(nn/2)], exact[i
][(int)(nn/2)]);
}
fprintf(fileDiff, "%i %g \n", nn , RMS(nn, diff));
fclose(fileDiff);
fclose(fileSolutions);
//Print to file numerical error
fileError = fopen("Validation/validation_SOLUerror.txt", "a");
fprintf(fileError, "%i %g \n", nn , avg(nn, diff));
fprintf(fileError, "%i %g \n", nn , RMS(nn, diff));
fprintf(fileError, "%i %g \n", nn , maxNorm(nn, diff));
fclose(fileError);
if (mh == 3 || mh == 4)
{
//Print residual and error of each V-cycle
fileRes = fopen("Validation/validation_residual.txt", "w");
fileGSerror = fopen("Validation/validation_GSerror.txt", "w");
for (int c = 0; c < ncycle; c++)
{
fprintf(fileRes, "%i %g \n", c+1 , endRes[c]);
fprintf(fileGSerror, "%i %g \n", c+l , error[c]);
}
fclose(fileRes);
fclose(fileGSerror);
} else{
fileRes = fopen("Validation/validation_residual.txt", "a");

```
```

}
}
free_dmatrix(RHS, 0, (int)(dimX*n)+2, 0, (int)(dimY*n)+2);
free_dmatrix(deltaP, 0, (int)(dimX*n) +2, 0, (int)(dimY*n)+2);
free_dmatrix(exact, 0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
free_dmatrix(diff, 0, (int)(dimX*n)+2, 0, (int)(dimY*n)+2);
return;
}

```

Listing B.12: criteria.c, functions for CFL-condition, RMS, max-norm etc.
```

\#include <stdlib.h>
\#include <math.h>
\#include <stdio.h>
\#include "head.h"
\#include "input.h"
/*

```


```

void IC(int newIC, double **u, double **v, double **p)
{
int i, j;
FILE *file;
printf("n = %i, dt = %f, Re = %i \n", n, dt, (int)(Re*2*radius));
if (newIC == 0)
{
for (i = 0; i <= (int)(dimX*n)+1; i ++)
{
for (j = 0; j <= (int) (dimY*n) +1; j++)
{
v[i][j] = 0.0;
u[i][j] = 0.0;
p[i][j] = 0.0;
}
}
}
else
{
file = fopen("Timestep.txt", "r");
for (i = 0; i <= (int) (dimX*n) +1; i++)
{
for (j = 0; j <= (int)(dimY*n) +l; j++)
{
fscanf(file,"%lf %lf %lf", \&u[i][j], \&v[i][j], \&p[i][j]);
}
}
fclose(file);

```
```

    }
    }
/*-

```


```

void stability(void)
{
double h = 1./n;
//Stability requirements, CFL if velocity is equals to 1.
if (dt > h || dt > (((double)Re*powf(h,2))/4) || dt > (2/(double)Re))
{
printf("Warning! dt should be less then %f, %f or %f, but are %f \n", h, (()
double)Re*pow(h,2))/4) , (2/(double)Re), dt);
exit(EXIT_FAILURE); // Exit program
}
}

```



```

double maxNorm(int nn, double **matrix)
{
double max = 0.0;
for (int i = 1; i <= (int)(dimX*n); i++)
{
for (int j = l; j <= (int)(dimY*nn); j ++)
{
if (fabs(matrix[i][j]) > max) {max = fabs(matrix[i][j]);}
}
}
return max;
}

```

```

I

```

```

double RMS(int nn, double **x)
{
double RMS, **pow2;
pow2 = dmatrix (0, (int) (dimX*n)+2, 0, (int)(dimY*n)+2);

```
```

for (int i = 1; i <= (int) (dimX*nn); i++)
{
for (int j = 1; j <= (int)(dimY*nn); j++)
{
pow2[i][j]=x[i][j]*x[i][j];
}
}
RMS = sqrt(sum(nn, pow2)) /((int) (dimX*nn) *(int) (dimY*nn));
free_dmatrix (pow2, 0, (int) (dimX*n)+2, 0, (int) (dimY*n)+2);
return RMS;
}
/

```


```

double avg(int nn, double **matrix)
{
double avg = 0.0;
for (int i = 1; i <= (int) (dimX*nn); i++)
{
for (int j = 1; j <= (int) (dimY*nn); j++)
{
avg = avg + matrix[i][j];
}
}
avg = avg/((int)(dimX*nn)*(int)(dimY*nn));
return avg;
}
/*

```

```

double sum(int nn, double **matrix)
{
double sum = 0.0;
for (int i = 1; i <= (int) (dimX*nn); i++)
{
for (int j = 1; j <= (int) (dimY*nn); j++)
{
sum = sum + matrix[i][j];

```

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